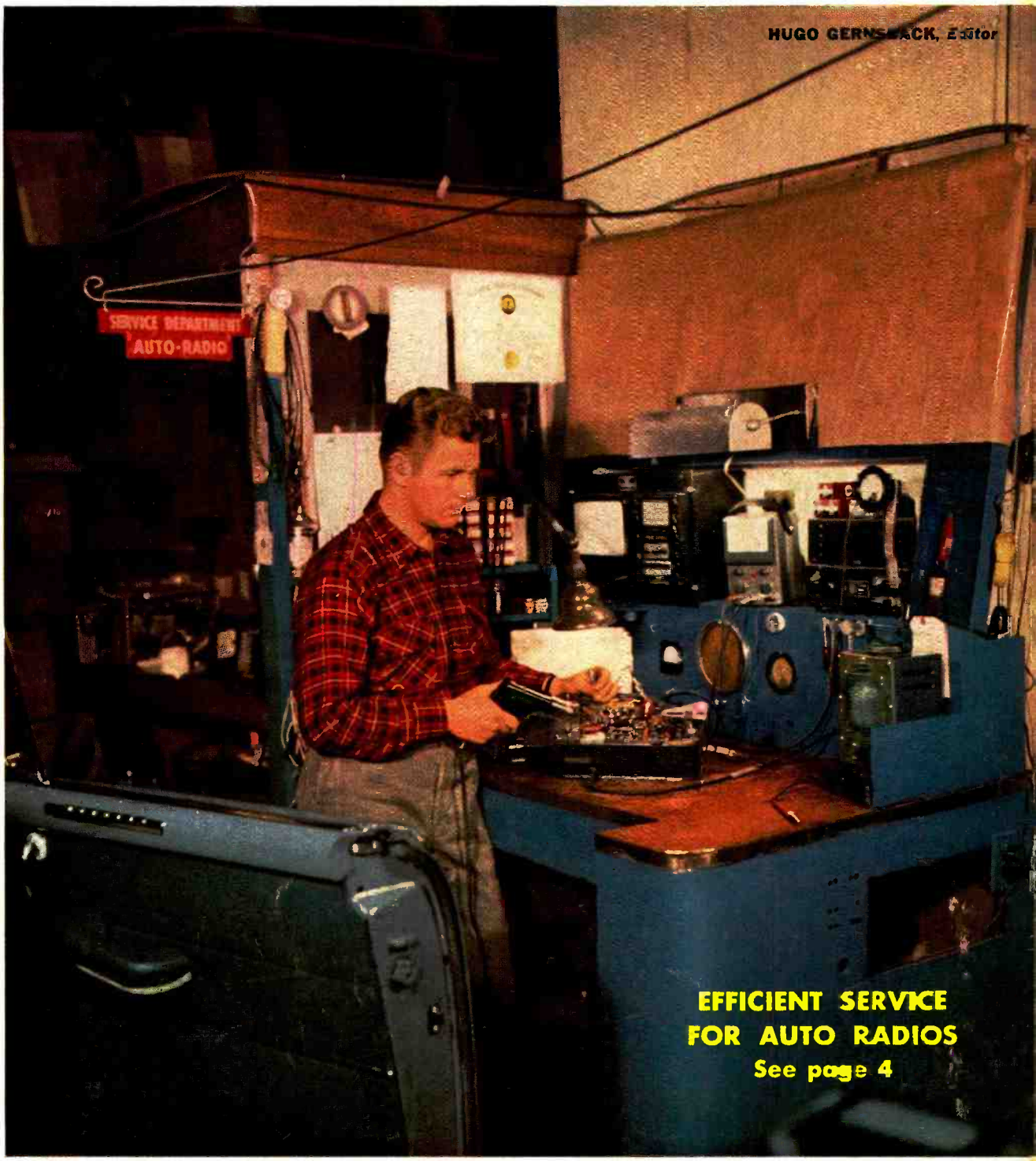
MAY 1952

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HUGO GERNSBACK, Editor



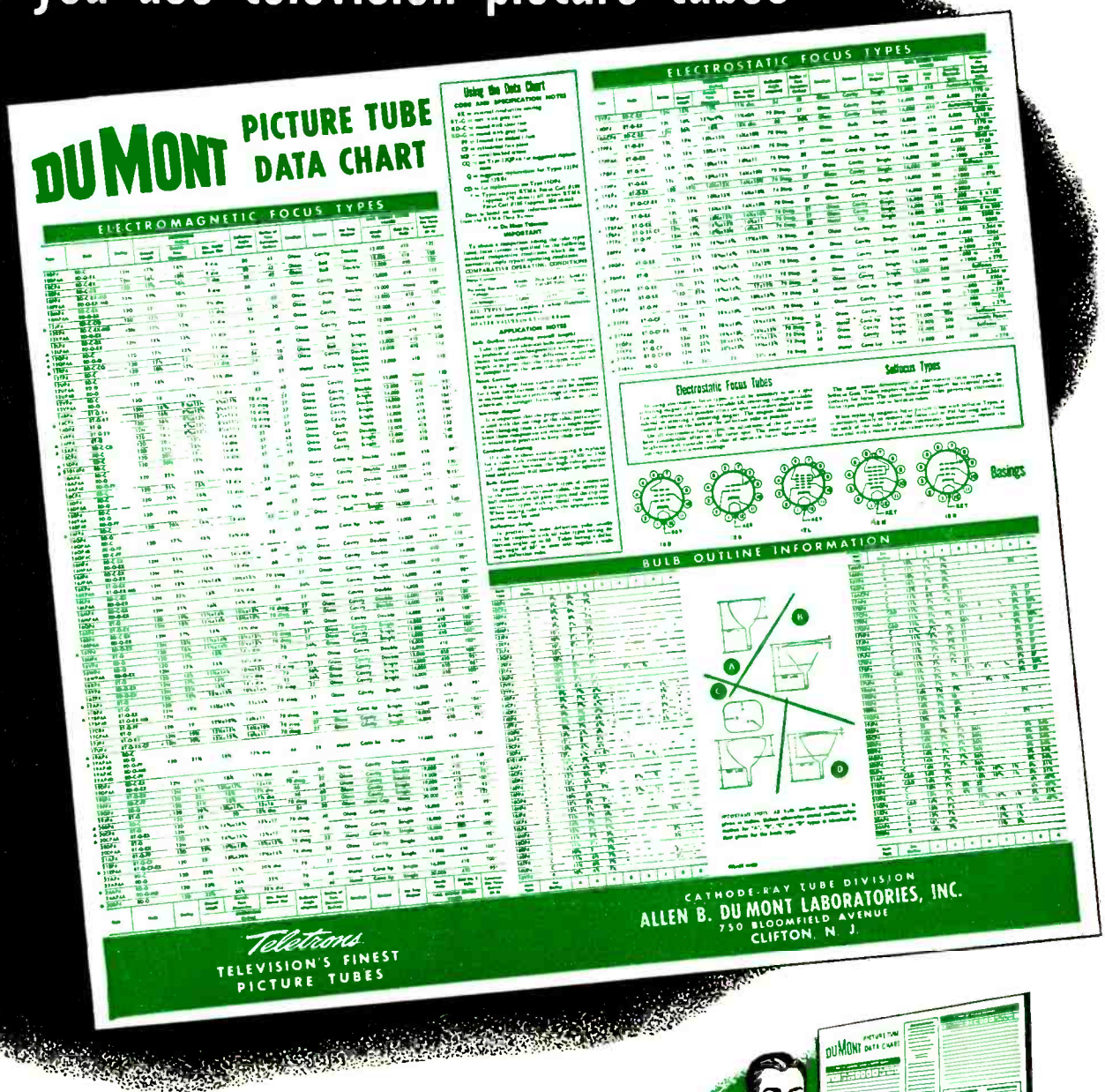
EFFICIENT SERVICE FOR AUTO RADIOS
See page 4

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In this issue: **TV Pattern for the Future • Practical TVI Filters • Converting the 9T-270**

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if you use television picture tubes



Whether it's for TV receiver design, research, or servicing be sure to have one of these charts handy. At a glance you can see all the electrical and physical characteristics for any modern RTMA-registered TV picture tubes. This is the latest edition of the Du Mont tube chart incorporating the very latest tube types. Ask your local Teletron Distributor, or write . . .



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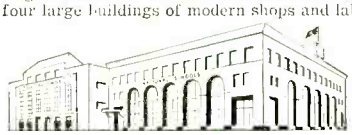
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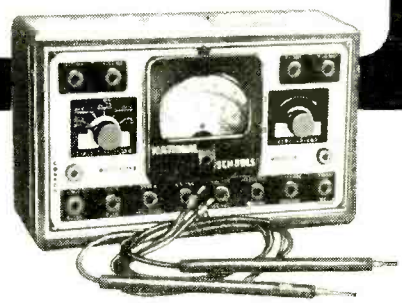
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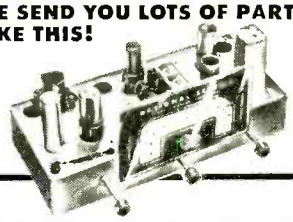
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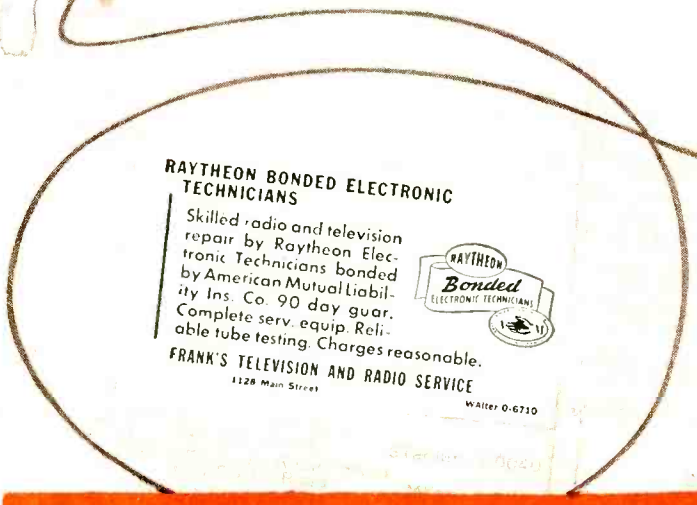
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HOW YOU CAN BE SUCCESSFUL IN RADIO-TV-ELECTRONICS

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Every success in Electronics has a story behind it. Sometimes you hear it's "luck." Other times, "contacts."

What do the successful men themselves say? *They give credit to training.* In addition, many men on the way up thank the day they sent for a booklet titled "Your Future in the New World of Electronics."

This is the eye-opening survey of the fast-growing world of Electronics. Many eager, ambitious men started their technical careers with a study of this booklet.

Expansion is phenomenal in this dynamic industry. There are over 100,000,000 radios in use! Experts predicted that by 1954 there would be 13,000,000 TV sets. That mark was passed a year ago. Today there are 16,184,000. 109 television stations are now in operation, and the lifting of the freeze will send 1500 to 2500 new stations scrambling for trained personnel—so urgently needed in every phase of electronics. That isn't the whole picture. Consider the tremendous defense orders for electronic installations—consider the fire and police departments, the railroads, the cabs, the aircraft—all using radio. Consider radar. Consider the maritime world with its navigational aids, fathometers, ship-to-shore and ship-to-ship communications. Think of electronic heating, fax and ultra-fax, of electronic medicine, and all the other applications of electronic know-how. Countless positions must be filled—in development, research, design, production, testing, inspection, manufacture, broadcasting, telecasting and servicing. Who can get those positions? You—if you prepare today—if you are alert and have the ambition to advance your knowledge. You—if you take 2 minutes to send for a free copy of "Your Future in the New World of Electronics." This helpful booklet shows you how CREI Home Study leads to greater earnings through the inviting opportunities described above.

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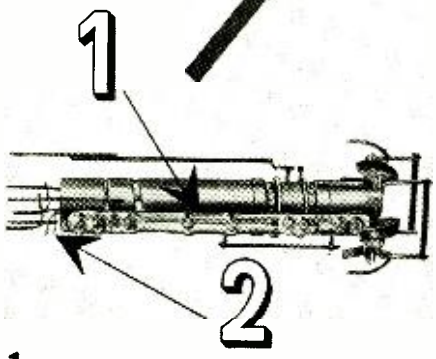
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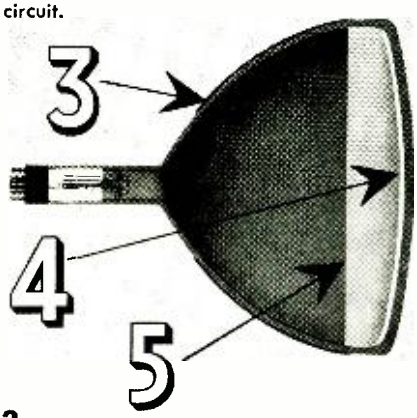
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Six quality features of all Tung-Sol Picture Tubes mean better TV receiver operation



1. Glass bead type assembly is stronger, both mechanically and electrically—gives greater protection against leakages and arcing.

2. Double cathode tab provides double protection against failure in the cathode circuit.

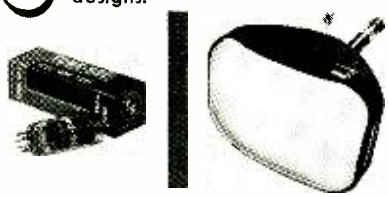


3. Low resistance of outside conductive coating minimizes radiation of horizontal oscillator sweep frequency.

4. Fortified screen composition resists burning (X pattern).

5. Rigid control of internal conductive coating materially improves service reliability.

6 Tung-Sol Picture Tubes can be used with single or double field ion trap designs.



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Tung-Sol makes All-Glass Sealed Beam Lamps, Miniature Lamps, Signal Flashers, Picture Tubes, Radio, TV and Special Purpose Electron Tubes.

EXPANSION OF TV NETWORK facilities is being speeded by American Telephone and Telegraph Co. Extension of existing networks to Miami, New Orleans, Houston, Dallas, Fort Worth, and Oklahoma City is now scheduled for completion in time for this year's major political conventions. In addition, the company is seeking more microwave channels for its Chicago-Omaha-San Francisco link.

A MILLION-WATT STATION, the most powerful in the world, is being constructed for the U.S. Navy near Seattle, Washington. Built for world-wide communication with the fleet, the station's 7,200 foot antennas are supported by towers two miles apart.

ARC WELDING OPERATIONS capable of causing radio or TV interference, will be governed temporarily by rules similar to those now covering induction heating equipment, according to the FCC. Final regulations for arc welding equipment will be adopted in about two years.

A RADIO WARNING SERVICE for Alaska and the North Pacific area has been opened by the National Bureau of Standards. Supplementing present long-range forecasts of transmitting conditions, the new service will report transient magnetic disturbances in the arctic auroral zones from several observation points.

SCATTER SOUNDING, a new technique for investigating h.f. propagation characteristics, has been announced by two outstanding radio amateurs, O. G. Villard Jr., and A. M. Peterson, in a release circulated by the American Radio Relay League. Using radar-type pulse transmissions, distances and directions of ground echoes are plotted to determine maximum skip distances. Results indicate the possibility of predicting the most effective frequency for transmission to a given point at any time.

SOUTHWESTERN I.R.E. conference and engineering exhibit will be held Friday and Saturday, May 16-17, in Houston, Texas. Scheduled speakers include Dr. Donald B. Sinclair, I.R.E. president; Commander R. A. M. Craven of Washington; Col. Edwin White of the FCC; and others.

Sectionalized technical sessions will increase time available for coverage of the 48 manufacturers' exhibits planned.

A full program of entertainment for visiting wives has been planned by the wives of Houston I.R.E. members.

This is the fourth southwestern I.R.E. conference.

MORE LIGHT ON V.H.F. propagation over long distances may be provided by a new theory announced by the National Bureau of Standards. Reflection in the upper atmosphere of frequencies above 100 mc may be predictable from a modified analysis of the change in refractive index with height. The new theory, developed by Dr. J. Feinstein of the NBS staff, indicates the possibility of dependable v.h.f. long-distance communication, and may complicate present plans for the allocation of TV channels by anticipating possible interference. (See "TV Pattern for the Future" elsewhere in this issue.)

THE FLYING TYPEWRITER, an



ultra-high-speed electro-mechanical printer which prints a line at a time, was announced recently by the Potter Instrument Company, Inc., of Great Neck, N. Y. Capable of handling 24,000 alphanumeric characters per minute, the Flying Typewriter can serve as an adjunct to a digital computer, or transcribe data directly from radio, wire line, or magnetic tape sources. Printing is on 8-inch wide paper tape, with two carbon copies available. Speeds as high as 900 lines per minute have been achieved.

TEXAN ROBERT T. BARTLEY was sworn in March 9 as a member of the Federal Communications Commission. Bartley, whose practical broadcast experience dates from 1939, was appointed by President Truman to fill the vacancy created by the resignation of FCC Chairman Wayne Coy.

THREE TV CHANNELS for non-commercial educational programs will be assigned to New York State by the FCC, according to Dr. Lewis A. Wilson, New York's State Education Commissioner. Official announcement of the allocations was expected March 25. In anticipation of the allocations, a bill was passed by the state legislature creating a fifteen-member commission to study and develop a program for most effective use of the channels.

The commission's findings, due in February, 1953, will include estimates of station construction and operating costs, and the relative desirability of station control and management by the State, or by private educational institutions.

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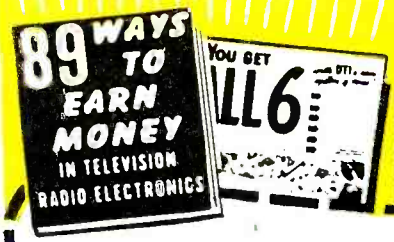


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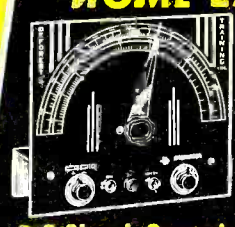
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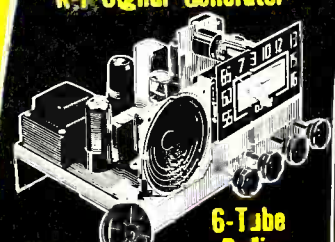
If you're subject to military service, the information we have for you should prove very helpful. Mail coupon today.

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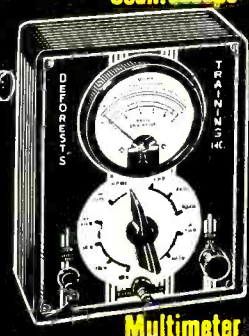
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Without obligation, I would like your Opportunity News Bulletin showing "89 Ways to Earn Money in Television-Radio-Electronics"; also, the folder showing how I may prepare to get started in this thrilling field.

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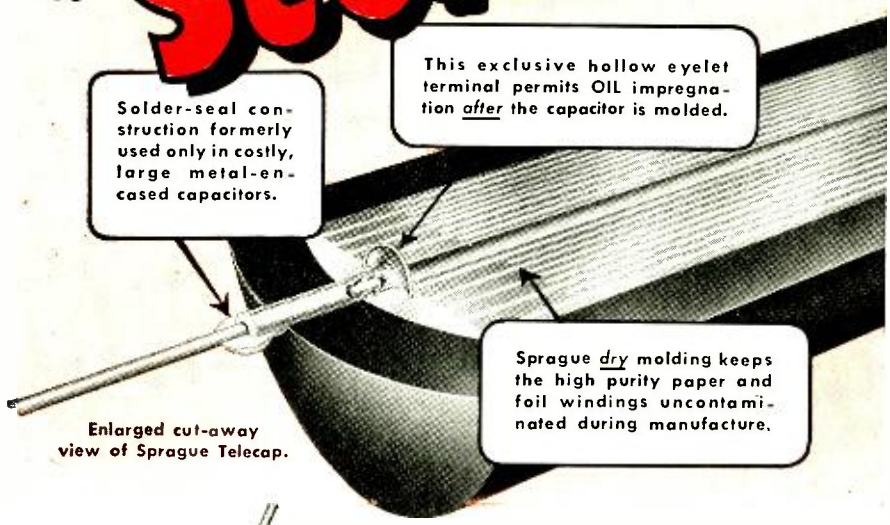
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Actual, on-the-job performance *proves* the superiority of Sprague "Black Beauties" beyond question. To find the secret that explains just why they're so much better, however, you've got to see inside of a Telecap itself.

The big feature is that every Sprague Telecap is molded into its sturdy Bakelite phenolic shell while its windings are still *dry*. Any chance of contamination by moisture or dust during manufacture is avoided. *After* molding, the capacitor is vacuum-impregnated with mineral oil through a tiny eyelet. The lead is then inserted, the terminal is solder-sealed—and you have a capacitor that has maximum resistance to heat and moisture . . . extra high insulation resistance and superior capacitance stability. *In short, a capacitor that brings you premium quality at no extra cost!*

. . . And that's the secret behind the fact that Sprague Telecaps are more widely used by leading television set makers . . . and why they're first choice of service technicians who value their reputations for good work!

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FELIX EHRENHAFT, noted physicist and early investigator of electronic phenomena, died March 4 in Vienna at the age of 73. A United States citizen since 1944, Professor Ehrenhaft fled Nazi persecution in 1939, and returned to Vienna three years ago as Guest Professor at the University's physics institute.

While in the United States, Professor Ehrenhaft attracted a great deal of attention with his statements of the existence of magnetic current and unipolar magnets. This material appeared first in RADIO-CRAFT in March, 1944, and later as papers at various sessions of the American Physical Society. Up to the time of his death he was engaged in studies of the behavior of small particles under the influence of light or other forces, when subjected to the influence of a magnetic field.

NEW CITIZENS BAND RULES became effective March 24. In addition to minor changes in procedure and in the technical requirements for existing Class A and Class B stations, a new class has been created exclusively for radio control of model planes, boats and cars. This new service, called Class C, has been assigned a spot frequency of 27.255 mc, with a power limitation of 5 watts and a maximum bandwidth of 10 kc.

TWENTY-FOUR RADIO BILLS were considered by the New York Legislature in its last session. The largest number were intended to prohibit landlords from charging for, or prohibiting tenants' TV roof antennas. Some of the bills would have required that the tenant pay the cost of any additional insurance that would be incurred because of the antenna's presence, and others wove in various safeguards and provisions around the general idea.

One bill would have deprived educational corporations of their tax exemption if they refused to permit their sports events to be telecast; others would have made the broadcasting of a person's name or picture without the person's consent an "invasion of privacy," and would permit New York City to levy a tax of 5%—collectable from the sponsors—on all radio and TV programs originating in that city. Only one—the Williamson bill banning the telecasting of any trial or proceeding in New York's state courts—was expected to pass, as the session drew to a close in the middle of March.

ULTRASONIC WAVE THERAPY has been successfully applied in Germany to patients suffering from lumbago, rheumatism and arthritis, according to a recent report. Direct applications of 1-mc vibrations through a small transmitter head have relieved pain and promoted healing of the affected areas. The method has also been applied with apparent success to the treatment of open sores and nervous diseases. Ultrasonic equipment is used by 30% of the major German clinics.

—end—

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"Thanks to your course I obtained my 2nd phone license, and am now employed by Civil Service at Great Lakes Naval Training Station as an Equipment Specialist."
Kenneth R. Leiser, Fair Oaks, Mtd. Del., McHenry, Ill.

GETS STATE POLICE JOB

"I have obtained my 1st class ticket (thanks to your school) and since receiving same I have held good jobs at all times. I am now Chief Radio Operator with the Kentucky State Police." Edwin Healy, 264 E. 3rd St., London, Ky.

GETS BROADCAST JOB

"I wish to thank your Job-Finding Service for the help in securing for me the position of transmitter operator here at WCAE, in Pittsburgh."
Walter Koschik, 1442 Ridge Ave., N. Braddock, Pa.

GETS AIRLINES JOB

"Due to your Job-Finding Service, I have been getting many offers from all over the country, and I have taken a job with Capital Airlines in Chicago, as a Radio Mechanic."
Harry Clare, 4537 S. Drexel Blvd., Chicago, Ill.

TELLS HOW—

EMPLOYERS MAKE JOB OFFERS LIKE THESE TO OUR GRADUATES EVERY MONTH!

Letter from Chief Engineer, Broadcast Station, North Carolina. "Need men with radiotelephone 1st class licenses. no experience necessary. Will learn more than at average station for we are equipped with Diesel Electric power, transmitting and studio equipment".

Telegram from Chief Engineer, Broadcast Station, Wyoming, "Please send latest list available first class operators. Have November 10th opening for two combo men".

Letter from Chief Engineer, Broadcast Station, Texas, "Please send list of latest licensed graduates".

These are just a few of the examples of the job offers that come to our office periodically. Some licensed radioman filled each of these jobs; it might have been you!

Ours is the only home study course which supplies FCC-type examinations with all lessons and final tests.

ACT NOW!

Get All 3 FREE

HERE'S PROOF FCC LICENSES ARE OFTEN SECURED IN A FEW HOURS OF STUDY WITH OUR COACHING AT HOME IN SPARE TIME:

Name and Address	License	Lessons
Lee Worthy, 2210½ Wilshire St., Bakersfield, Cal.	**2nd Phone**	**16**
Clifford E. Vogt, Box 1016, Dania, Fla.	**1st Phone**	**20**
Francis X. Foerch, 38 Beucler Pl., Bergenfield, N. J.	**1st Phone**	**38**
S/Sgt. Ben H. Davis, 317 North Roosevelt, Lebanon, Ill.	**1st Phone**	**28**
Albert Schoell, 110 West 11th St., Escondido, Cal.	**2nd Phone**	**23**

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Your FCC ticket is Recognized in All Radio Fields as Proof of Your Technical Ability.

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(Address to Desk No. to avoid delay.)

I want to know how I can get my FCC Ticket in a minimum of time. Send me your FREE booklet, 'How to Pass FCC License Examinations" (does not cover exams for Amateur License), as well as a sample FCC-type exam and the amazing new booklet," Money-Making FCC License information."

☐ Tell me how I can get your Free Television Course.

Name .....

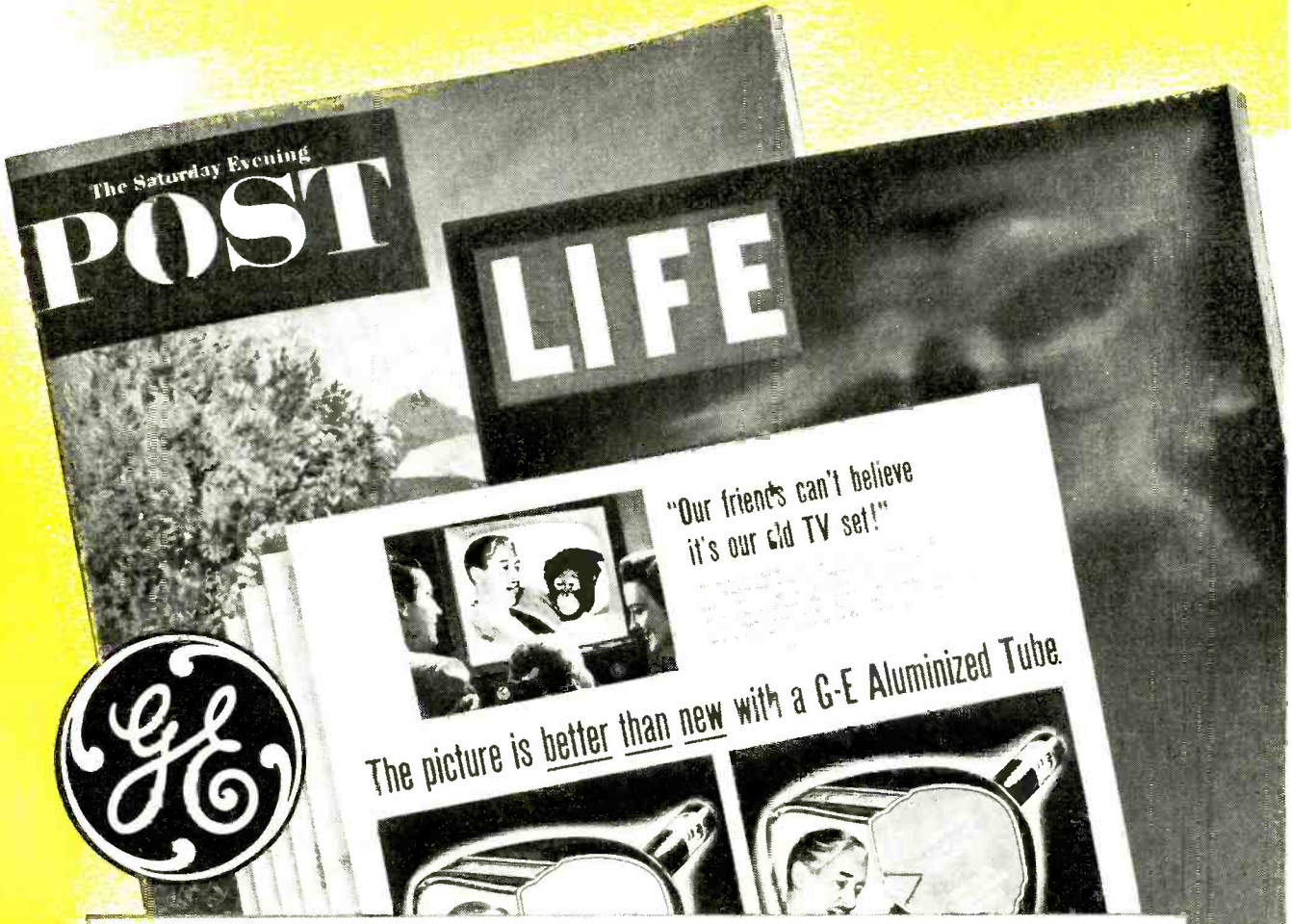
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● 35,000,000 people read G-E full-page tube ads. 35,000,000 TV owners and enthusiasts see *proof* month after month that General Electric tubes are superior!

● Every message emphatically directs these owners to you—the serviceman with the General Electric tube sign. The ads tell why patronizing *your* shop means brighter, sharper, more lifelike television pictures in the home.

● Take advantage of the big local market that G-E tube advertising creates for you! Make real money by selling G-E tubes to a *pre*sold television public!



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BUSINESS "LIFE" AND "POST" ADS!

We install Aluminized TV Picture Tubes "up to 100% brighter"

AS ADVERTISED IN LIFE AND SATURDAY EVENING POST

THIS SIGN PUTS G-E NATIONAL ADS TO WORK FOR YOU!



EVERY MINUTE of every hour, people who have read G-E tube advertising pass your shop. They want to know where to go for service. Use these colorful gummed streamers to tell them *you* install G-E tubes!

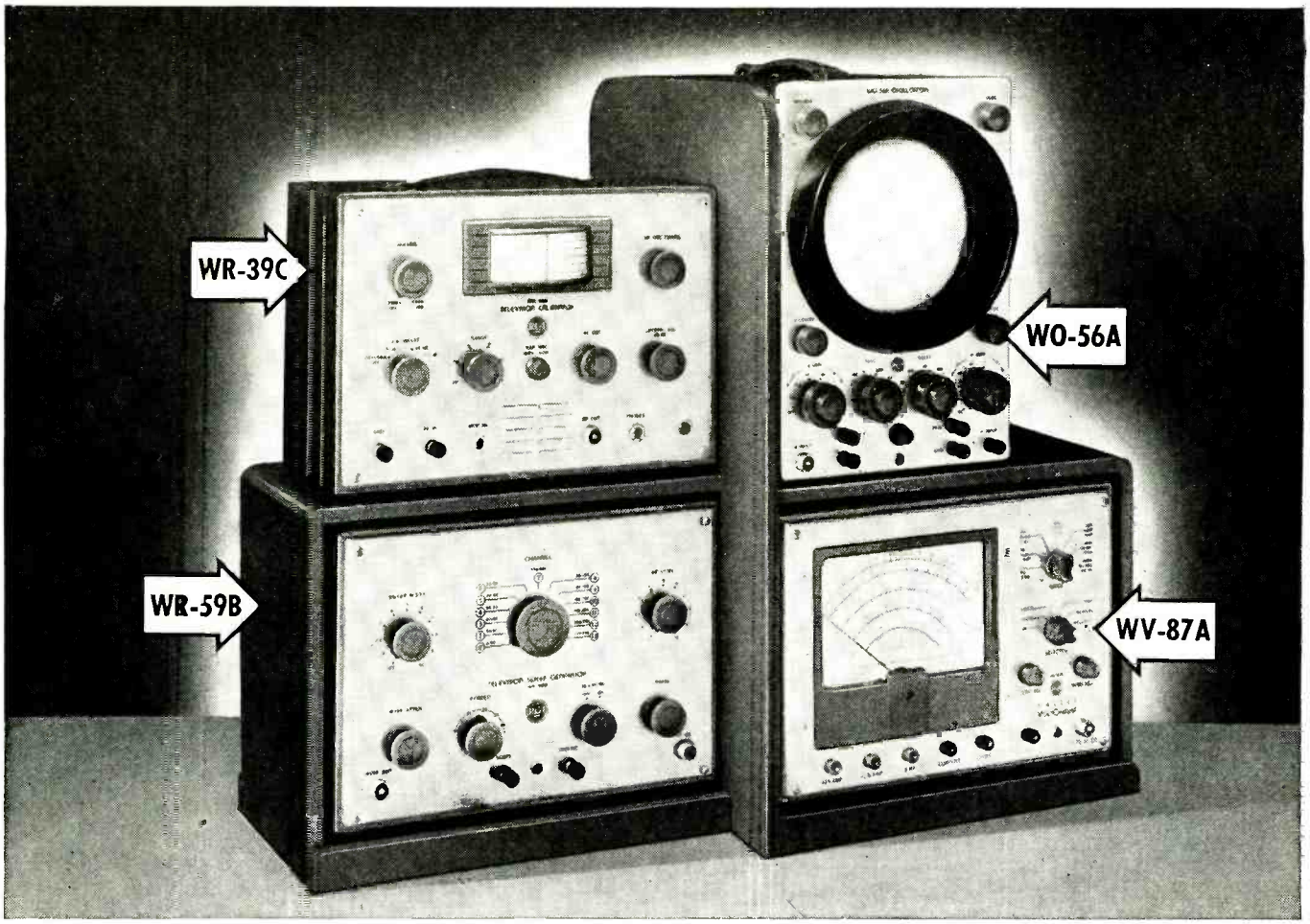
21" WIDE, the streamer is just the right size for your door or window. Blow-ups of LIFE-POST ads, supplied from time to time, can be mounted beneath. For counter giveaway, or for display where space is limited, actual-size ad reprints are available to you regularly.

YOUR G-E TUBE DISTRIBUTOR will be glad to supply you with streamers and reprints. See, phone, or write him today! Get *all* the tube and service business "Up to 100% brighter!" will bring to your door! *Tube Department, General Electric Company, Schenectady 5, New York.*

GENERAL ELECTRIC

161-1A2

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NOW... the RCA *UNIFIED* test position

Provides the best in television-servicing facilities

THE new RCA 4-position deluxe rack will add beauty and convenience to your test set-up. You'll like the way this service-engineered rack increases your operating efficiency . . . you'll be surprised to see how precious bench space is conserved. Furthermore, you'll be amazed how easy it is to get one of these handsome 4-position racks from your RCA Test Equipment Distributor. The rack accommodates four test instruments as illustrated.

WR-39C **Television Calibrator.** Variable-frequency oscillator provides fundamental output over entire range, with crystal-controlled check points at 2.5-Mc and 0.25-Mc intervals. Provides 4.5-Mc crystal-oscillator signal for intercarrier alignment and for dual markers at TV carrier frequencies. The WR-39C is a heterodyne frequency meter, a crystal standard (with 3 crystals supplied), a bar-pattern generator, and a TV re-broadcast transmitter.

WR-59B **Television Sweep Generator.** Covers all TV channels on preset fixed positions. Continuous tuning range from 300 Kc to 50 Mc covers video and intermediate frequencies. High-precision vibrating capacitor provides up to 12-Mc maximum sweep width, flat within ± 1 db, with good linearity. Has dual-piston attenuator for varying output voltage from 0.1 volt to 5 microvolts. Includes blanking for zero-reference line on 'scope.

WO-56A **Television Oscilloscope.** Uses 7" CR tube and direct-coupled, 3-stage, push-pull, vertical and horizontal amplifiers. Dual controls for "coarse" and "fine" adjustments. Frequency-compensated and voltage-calibrated attenuators on both amplifiers. Response flat within -2 db from dc to 500 Kc, within -6 db at 1 Mc. Vertical deflection sensitivity, 10.6 rms millivolts per inch. Magnetic shield on CR tube reduces effects of external fields.

WV-87A **Master VoltOhmyst*:** Has big 8½" easy-to-read meter. Measures dc voltages accurately in high-impedance circuits, even with ac present. It also reads rms values of sine waves and the *peak-to-peak* values of complex waves or recurrent pulses, even in the presence of dc. Measures resistance from 0.1 ohm to 1000 megohms, current from 10 microamperes to 15 amperes. Features ± 1% tolerance multiplier and shunt resistors, a meter movement having an accuracy within ± 2% and a tracking error of only ± 1%, high input resistance, zero-center scale adjustment for discriminator alignment, dc polarity-reversing switch, and sturdy metal case for good rf shielding.

For complete details, see your RCA Test Equipment Distributor, or write Commercial Engineering, Section EX49, Harrison, New Jersey, for descriptive folders on the individual instruments. *Reg. U.S. Pat. Off.

RCA **RADIO CORPORATION of AMERICA**

TEST EQUIPMENT **HARRISON, N.J.**

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Adds every UHF Channel . . . to any TV receiver . . .



Mallory UHF Converter

THAT'S RIGHT! The Mallory UHF converter adds *all* UHF channels to *any* TV set . . . in *any* UHF broadcast area. And installation involves only the connection of power lines and antenna leads; no internal adjustments of the receiver are necessary.

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- *No sacrifice of VHF channels*
- *Built-in UHF antenna*
- *High quality picture definition*
- *Fast, easy installation*

The Mallory UHF converter is small, attractive—precision-built to high Mallory standards. For complete information on this versatile converter, contact your Mallory distributor today.



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Television Tube Location Guide. Vol. 1. Over 200 pages of TV receiver tube position diagrams on hundreds of models. *Order* **TGL-1**.....*Only* **$1.50**

Making Money in TV Servicing. Tested proved methods of operating a profitable TV service business. Covers all important phases. Authoritative, valuable guide to success. Over 130 pages. *Order* **MM-1**.....*Only* **$1.25**

Servicing TV in the Customer's Home. Shows how to diagnose trouble using capacitor probe and VTVM. Short-cut methods help save time, earn more on outside service calls. *Order* **TC-1**.....*Only* **$1.50**

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Communications Receiver Manual. Complete analysis of 50 popular communications models. 246 pages, 8½ x 11". *Order* **CR-1**.....*Only* **$3.00**

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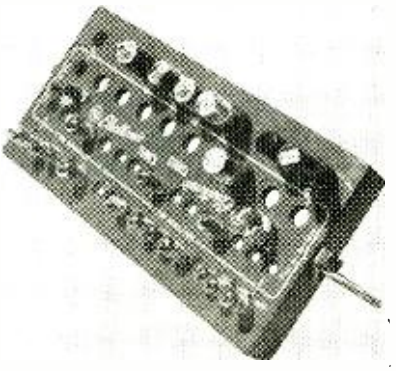
Dial Cord Guide. Vol. 1. Covers sets produced 1938 through 1946. *Order* **DC-1**.....*Only* **$1.00**

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HOWARD W. SAMS & CO., INC.

Merchandising and Promotion

General Electric's Tube Department, Schenectady, N. Y., announced a new tube rack which is available to radio



and TV service technicians through G-E tube distributors. Known as the "Tube-saver," it can hold as many as 52 tubes of all standard base types.

Sylvania Electric Products' advertising director Terry P. Cunningham, announced that the company will continue and expand its national promotion on behalf of TV-radio service technicians to the public. National consumer magazines, television programs, and local dealer displays will be used in the campaign.

Recoton Corp., New York City, released an illustrated cross index containing a breakdown of the phonograph needles used by various cartridge manufacturers. It lists competitive manufacturers' needles as well as those made by Recoton.

American Electrical Heater Co., Detroit, manufacturer of "American Beauty" soldering irons, announced stepped-up promotional plans, extending into 1953, which will include coverage of the electronic, aviation, radio-TV, and telephony fields. The Allman Co., Inc., Detroit, was named as the company's new advertising agency.

RCA Tube Department released a revised edition of its "Triple Pindex" socket manual, a compilation of socket-connection diagrams for more than 660 receiving tubes and kinescopes. It is available from RCA tube distributors and from the Commercial Engineering Division, RCA Tube Department, Harrison, N. J., for 75c.

Electronic Instrument Co., Inc., Brooklyn, N. Y., manufacturer of "Eico" test instruments and kits, released a new direct-mail booklet as a part of its "follow-through" promotion to back up its national advertising.

Radio's Master BAROMETER of the PARTS INDUSTRY

During March, 64 of the leading 375 manufacturers of Radio-Television-Electronic parts and equipment made changes in their lines. Actually there was an increase in "change activity" as compared to February.

In price revisions by the number of manufacturers and products affected, the following summary illustrates the comparative trend for February and March.

	No. of Manufacturers	
	Feb.	March
Increased prices	17	12
Decreased prices	16	28

	No. of Products	
	Feb.	March
Increased prices	451	482
Decreased prices	166	492

As evident from the above chart, price decreases showed the greatest change. For comparison, these figures are broken down into the following categories:

Product Group	Increased Prices		Decreased Prices		New Products		Discontinued Products	
	No. of Mfrs.	No. of Products	No. of Mfrs.	No. of Products	No. of Mfrs.	No. of Products	No. of Mfrs.	No. of Products
Antennas & Acces.	2	2↓	6	92↑	7	113↑	2	33↑
Capacitors	None	None↓	None	None	3	265↑	None	None
Controls & Resistors	1	40↑	None	None↓	3	22↓	3	5↑
Sound & Audio	2	6↓	5	139↑	12	65↓	7	59↑
Test Equipment	2	4↑	1	3↑	3	11↑	3	7↑
Transformers	None	None↓	1	70↑	3	119↑	2	142↑
Tubes	4	303↑	8	154↑	3	10↓	1	2↓
Wire, Cable, etc. Connectors	None	None↓	3	38↑	3	9↑	1	6↑

↑ Increase over February
↓ Decrease

Comment: Tube prices continue to increase. However, there are fewer manufacturers involved than in February.

↑ Increase over February
↓ Decrease

Comment: The manufacturers of antennas and audio products continue to be the most active.

This data is prepared by the staff of United Catalog Publishers, Inc., 110 Lafayette Street, N. Y. C., publishers of RADIO'S MASTER.

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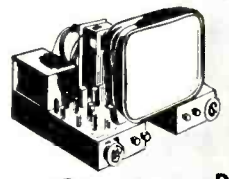


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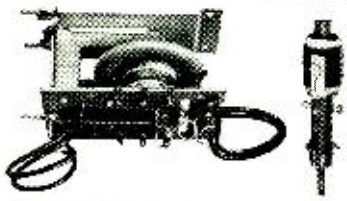
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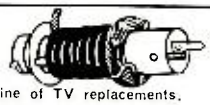
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Only complete line of TV replacements.



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MERIT'S 1952 Catalog No. 5211 with new MERIT IF-RF Coils.
Other MERIT service aids:
TV Repl Guide No. 404, 3500 models & chassis.
Cross Ref Data, IF-RF Coils, Form No. 14.
See your Jobber or write: Merit Coil and Transformer Corp., 4425 Clark Street, Chicago 40.



These three MERIT extras help you:
Exclusive: Tapemarked with specs and hook-up data.
Full technical data packed with every item.
Listed in Howard Sams Photofacts.

*Merit is meeting the TV improvement, replacement and conversion demand with a line as complete as our advance information warrants!

The RTMA released a new membership service brochure describing the association's activities and services. Prepared under the direction of the RTMA Promotion Committee, headed by J. J. Kahn, president of Standard Transformer Corp., it was designed to fully acquaint all RTMA members with the association's services, and to interest nonmembers in joining the RTMA.

Rinehart Books, Inc., New York City, issued two new illustrated circulars describing the first two volumes of the new Ghirardi's *Modern Radio and Television Servicing Library.*

Brach Manufacturing Co., Newark, N. J., is furnishing its distributors and dealers with display cards, posters, and mailing pieces to promote the sale of its new auto antenna line. The line features a new patented "Cowl Well" antenna which can be installed from the top by one man.



New Plants and Expansions

LaPointe-Plascomold Corp., Windsor Locks, Conn., manufacturer of "Vee-DX" antennas, boosters, and accessories, announced two major steps in its long-range expansion program. The first was the acquisition of the Press Wireless Mfg. Co., Hicksville, N. Y., and the second, the purchase of the Springville Mill in Rockville, Conn. The Rockville plant will house the Press Wireless Mfg. Co., which will also maintain a plant in West Newton, Mass.

Standard Coil Products Co., Inc., Chicago, purchased from the Espey Mfg. Co., New York, its Sherold Crystal Division, Kansas City, Kan. Sherold Crystal will become a wholly owned subsidiary of Standard Coil for the manufacture of quartz crystals for civilian and defense use.

Cleveland Graphite Bronze Co. has completed arrangements to buy the Brush Development Co., long established Cleveland research and manufacturing concern.

Motorola, Inc. established its National Defense Division headquarters in its Clybourn Ave. plant in Chicago. The entire plant, plus another plant of 50,000 square feet, will be devoted solely to military production, which is expected to account for 25% of the company's total volume during 1952. Motorola also established a Radio Message Service in Phoenix, Ariz., to permit field testing of its new two-way mobile radio equipment.

Business Briefs

. . . RCA completed arrangements to borrow $50,000,000 from investment institutions on long-term notes. Proceeds will be used for working capital and for general corporate purposes, including expanded defense production.

. . . **The 1952 NEDA Convention and Manufacturers' Conference** to be held in Atlantic City, N. J., September 20 to 24, will feature a series of business meetings and an educational program. Completely equipped conference booths will be available to each manufacturer. Cost of the booth will be included in the $300 participation fee.

. . . RTMA "task force" committee appointed by Dr. W. R. G. Baker, chairman of RTMA's Television Committee, reported that expansion of TV broadcasting to cities not now covered would not be delayed by defense production restrictions. Construction permits for 140 new TV stations should be issued by the FCC by the end of 1952, and 190 more by the end of 1953. Half of these were estimated to be for u.h.f. transmitters, and the balance for v.h.f. The "task force" further predicted that 22 new v.h.f. stations would go on the air in 1952, 21 of them in cities not now covered by TV.

. . . **Radio Receptor Co., Inc.**, Brooklyn, N. Y., was named Licensee No. 1 to manufacture germanium transistors and diodes in an agreement with Western Electric Co. which holds the patents.

THE 1952 ELECTRONIC PARTS SHOW

The 1952 Electronics Parts Show will be held in the Conrad Hilton Hotel, Chicago, from May 19th—22nd. 204 companies will exhibit in 164 booths in Exhibition Hall and in 136 display rooms. The educational program will include a nine-hour course in applied salesmanship plus seminars on topics vital to the distributing industry.

List of Exhibitors

COMPANY	EXHIBITION HALL BOOTH NUMBER ASSIGNED	DISPLAY ROOM NUMBER ASSIGNED
Aerovox Corporation	680	
Alliance Manufacturing Co.	322	
Allied Electric Products	201	
Alpha Wire Corporation	412	
Alprodco, Inc.	13	
Altec Lansing Corporation.	592	607
American Microphone Co.	302	
American Phenolic Corp.	207	560A-563A
American Radio Hardware Co.	415	
American Tel. & Radio	308	
Amperite Company	214	
Anchor Radio Corporation.	123	
Approved Electrical Instruments	113	
Argos Products Co.		500
Astatic Corporation	416	542A-544A
Atlas Sound Corporation	213	
Audak Company		547

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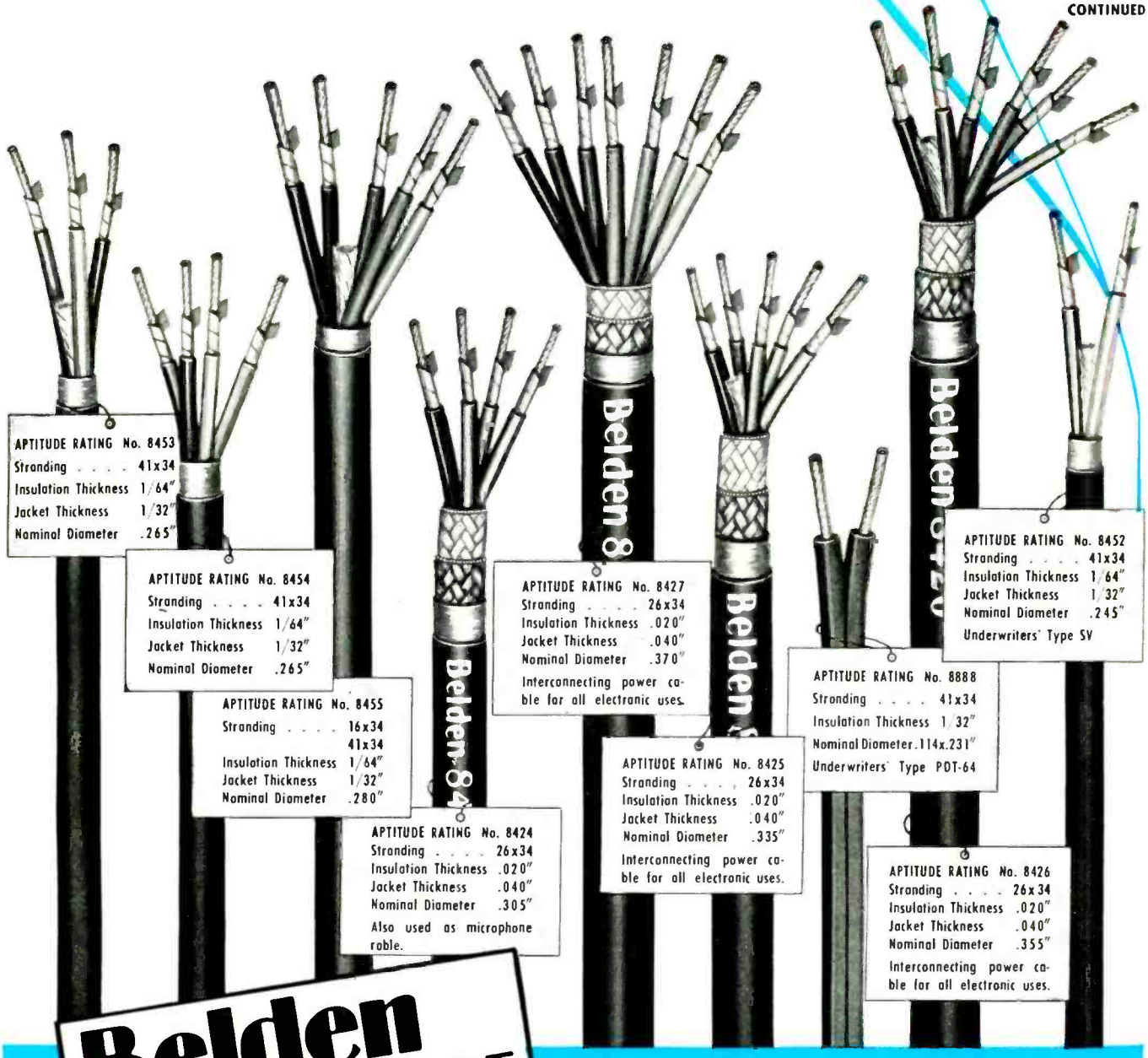
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Interconnecting power cable for all electronic uses.

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Stranding 26x34
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Jacket Thickness .040"
Nominal Diameter .335"
Interconnecting power cable for all electronic uses.

APTITUDE RATING No. 8888
Stranding 41x34
Insulation Thickness 1/32"
Nominal Diameter .114x.231"
Underwriters' Type POT-64

APTITUDE RATING No. 8426
Stranding 26x34
Insulation Thickness .020"
Jacket Thickness .040"
Nominal Diameter .355"
Interconnecting power cable for all electronic uses.

APTITUDE RATING No. 8452
Stranding 41x34
Insulation Thickness 1/64"
Jacket Thickness 1/32"
Nominal Diameter .245"
Underwriters' Type SV

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The Scanafar, new Astatic TV Booster development, incorporates improvements that match the forward strides made in newer model TV Receiver front-ends. It stands alone as a working companion with the new receivers, for added picture brilliance and clarity . . . and offers a still higher measure of reception improvement for older style sets. The Scanafar presents a new minimum noise figure with maximum gain. Band width (over seven megacycles on all channels) and picture definition are excellent. A balanced, cascaded circuit is employed, with a neutralized 6J6 tube driving a 6BQ7 (the highly touted "quiet tube"). **Both tubes are used over the entire TV frequency range.** It all adds up to booster performance that is unparalleled today. Test this new unit yourself . . . at your first opportunity. Be prepared for a new experience in booster aid to TV reception.

SEE ASTATIC'S NEW BOOSTER . . . OTHER NEW ASTATIC DEVELOPMENTS AT THE 1952 ELECTRONIC PARTS SHOW, May 19 to 22, Conrad Hilton Hotel, Chicago. ASTATIC BOOTH NO. 416—DISPLAY ROOMS 542-A and 544-A.

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Barker & Williamson, Inc.	225	
Belden Manufacturing Co.	405	
Bell Sound Systems	319	546A-548A
David Bogen Co.		539 & 553
Blonder-Tongue Labs.	6	
British Industries	301	
Brush Development Co.	678	
Bud Radio, Inc.		637
Burgess Battery Co.	313	
Bussmann Manufacturing Co.	105	
Camburn, Inc.		553A
Centralab Division	685	
Channel Master Corp.		549
Chicago Transformer Div.	684	522 & 520
Clarostat Manufacturing Co.	410	
Clear Beam TV Antennas	26	
Cleveland Electronics	312	658A-659A
Columbia Wire & Supply	587	
Condenser Products Corp.		620
Consolidated Wire & Assoc.	208	
Copperweld Steel Co.	117	
Cornish Wire Co.	683	
Crest Transformer Corp.	108	
Drake Electric Works	222	
Du Kane Corporation		556A-557A
Allen B. Dumont Laboratories	580	613-614
Duotone Company, Inc.	118	
Eicor, Inc.	8	700-01
Eldico of New York, Inc.		658-659
Electronic Devices, Inc.	203	
Electronic Instrument	202	
Electronic Measurements	112	
Electro Products Laboratories	414	
Electro-Voice, Inc.	128	550A-551A
Electrovox Company	129	
Erie Resistor Corp.	318	536A
Espey Manufacturing Corp.	673	
Freed Transformer Co.	303	
Fretco Television Co.	126	656
The Gabriel Company	674	612A-613A
Gee-Lar Manufacturing Co.	109	
General Cement Mfg. Co.	419	504A
General Electric Co.	676	537A
General Industries Company	417	521A
General Transformer Co.		629
Grayhill	588	
Guardian Electric Mfg. Co.	212	
Grayburne Corp.		637A
The Halldorson Company	586	
The Hallicrafters Company	574	512A-513A
Hammarlund Mfg. Co.	407	
Hickok Electrical Instr. Co.		528A-530A
Hi-Lo TV Antenna Corp.	3	
Hytron Radio & Electronics	305	
IE Manufacturing Co.	10	632
Illinois Condenser	687	
Illinois Transformer Co.		603A-609A
Indiana Steel Products Co.	408	502
Industrial Devel. Eng. Assocs.	116	
Insuline Corp. of America	206	523
International Resistance Co.	307	
Jackson Electrical Instrument	421	
James Vibrapowr Co.	127	
J-B-T Instruments	576	501A
Jensen Industries, Inc.	577	602
Jensen Manufacturing Co.	404	504-505
Jersey Specialty Company	115	
J. F. D. Manufacturing Co.	578	516
E. F. Johnson Company	133	
Kester Solder Company	122	
LaPointe Plascomold	688	653A
Lenz Electric Mfg. Co.	314	
Littelfuse, Inc.	317	539A
Lowell Manufacturing Co.	120	
P. R. Mallory & Company	573	
Markel Electric Products	24	644
Merit Transformer Corp.	689	
James Millen Mfg. Co.	217	
M. A. Miller Mfg. Co.	585	
Model Engineering & Mfg. Co.	102	
Mosley Electronics	119	
Don McGohan, Inc.	1	616-617
National Carbon Co., Inc.	125	621-622
National Company	575	
National Union Radio Co.	103	

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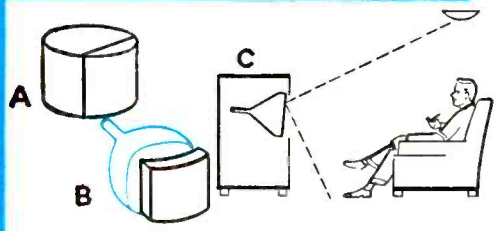


New CBS-Hytron cylindricals
17LP4 and 21FP4A low-voltage electrostatics
17QP4 and 21EP4A electromagnetics

Facts

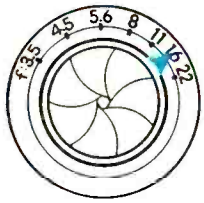
YOU'LL WANT TO KNOW ABOUT NEW

CBS-HYTRON *Cylindricals*



WHY CBS-HYTRON CYLINDRICAL?

To eliminate reflected glare? How? Simple as ABC: A. Imagine a cylinder; slice it vertically. B. You now have the shape of the face plate of a cylindrical tube: curved horizontally; straight, vertically. C. Light falling on this surface at an angle from above is reflected at the same angle...downward. Tilting the tube directs glare downward even more, away from the viewer's eyes.



WHY CBS-HYTRON SHIELDED LENS?

With this shielded lens in the electron gun, greater depth of field and better definition are achieved. Just as when you stop down the diaphragm of a large, fast camera lens (f/3.5) to a small aperture (f/16). Distortion caused by interaction of external electrostatic fields used to focus and accelerate the electron beam is avoided. Focusing is easier, less critical. Slight changes in voltages and currents do not cause drift.



WHY CBS-HYTRON BLUE-WHITE SCREEN?

Ever notice how a shirt laundered with bluing appears whiter? With the CBS-Hytron blue-white screen, whites appear whiter; blacks, blacker. Picture definition is crisper. In fringe areas, the expanded gray scale of the blue-white screen gives noticeably clearer pictures. No wonder CBS-Hytron's original blue-white screen is fast becoming the standard preferred by consumers for best definition.

CBS HYTRON RADIO TUBES

MANUFACTURERS OF RECEIVING TUBES SINCE 1921
HYTRON
RADIO AND ELECTRONICS CO.
A DIVISION OF COLUMBIA BROADCASTING SYSTEM, INC.

MAIN OFFICE: SALEM, MASSACHUSETTS

These are just a few reasons why it's smart to demand CBS-Hytron...original studio-matched rectangulars. Try the new CBS-Hytron cylindricals yourself. Discover for yourself why 9 out of 10 leading set manufacturers pick CBS-Hytron.

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You can't go wrong with a TURNER TV BOOSTER!



THE TURNER BOOSTER
List Price . . . $57.50

For television viewing you want the finest possible picture—whatever your receiving conditions. You don't want to compromise for anything less than a bright, clear picture, no matter where you are in the fringe area. And with the Turner Television Booster you don't need to compromise! The Turner Booster gives you the superior picture that's a delight to watch—the crisp, natural sound you've always wanted.

If it's a better picture you're after . . . if it's the finest possible performance you want from your TV set . . . don't settle for less than a Turner Booster!

YOU CAN'T GO WRONG WITH A TURNER TV BOOSTER!

THE TURNER COMPANY

933 17TH STREET N. E. — **CEDAR RAPIDS, IOWA**

IN CANADA: Canadian Marconi Co., Ltd. — **Toronto, Ont., & Branches**

EXPORT: Ad. Auriema, Inc. — **89 Broad St.** — **New York 4, New York**

For GREATER TV ENJOYMENT . . .



Cat. No. F-20
List $3.75



Cat. No. F-10
List $3.75

Install a MOSLEY 3-WAY ANTENNA SWITCH

Here's convenience! MOSLEY TV Antenna Switches give instant, easy selection of any one of three antennas. Special rotary type switch, making silver-to-silver contact, assures low loss, constant impedance.

Cat. No. F-10 is Flush Mounted Switch and Lead-in Socket combination for neat, concealed-in-wall installation in standard electrical box. Cat. No. F-20 is enclosed in attractive plastic case for mounting on wall or back of set. If mounting on back of set, attach special extension lever provided and install in position for easy accessibility.

At leading Radio Parts Jobbers everywhere

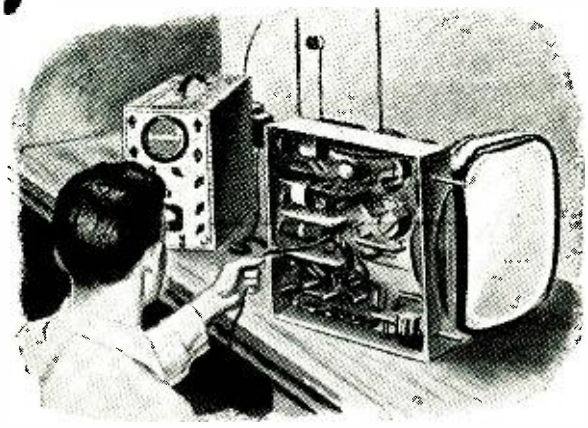
MOSLEY ELECTRONICS 2125 Lackland Road Overland, Missouri

National Video Corporation		533 & 536
Newcomb Audio Products	223	521
Oak Ridge Products	11	
Ohmite Manufacturing Co.	210	
Oxford Electric Corporation	309	557
Par-Metal Products Corp.	215	
Peerless Products Industries	9	
Penn Boiler & Burner Mfg. Co.	121	657
Penn Television Products	124	
Pentron Corporation	107	529
Permoflux Corp.	418	614A-615A
Permo, Inc.	104	
Philmore Manufacturing Co.		533A-534A
Phoenix Electronics	101	635A
Pickering & Company		657A
Potter & Brumfield	591	612
Precise Development Corp.	130	
Precision Apparatus Co.	403	501
Premax Products Division	135	
Presto Recording Co.		515A
Pyramid Electric Co.	671	
Quam-Nichols Co.	411	601
Racon Electric Co.	111	
Radelco Manufacturing Co.	23	
Radiart Corporation	209	610-611
Radio Apparatus Co.	205	
Radio City Products	409	
Radio Corporation of America	21	524A-526A
Radio Craftsmen, Inc.		505A-507A
Radio-Electronics Magazine		656A
Radio Merchandise Sales	691	
Radio Receptor Co., Inc.	5	
Radion Corporation		616A-617A
Ram Electronics, Inc.	110	
Rauland-Borg Corp.	204	618-619
Rauland Corporation	216	532A
Raytheon Mfg. Co.	422	
Recoton Corporation	590	
Reeves Soundcraft	27	
Rek-O-Kut Company		561
John F. Rider Publisher, Inc.	583	
Howard W. Sams & Co.	211	
Sangamo Electric Co.	316	
Walter L. Schott Co.	218	
Shure Brothers, Inc.	581	519A-520A
Simpson Electric Co.	219	509
Mark Simpson Mfg. Co.	679	512-513
Herman H. Smith, Inc.	582	
Snyder Mfg. Company	310	
Sola Electric Co.	413	
Spirling Products		556
Sprague Products	686	
Square Root Manufacturing Co.	14	633A-634A
Standard Transformer Corp.	401	605A-607A
Stromberg-Carlson		618A-619A
Switchcraft, Inc.	672	
Sylvania Electric Products	681	
Talk-A-Phone Company	221	610A-611A
Tape Master, Inc.		639-640
Tech-Master Products		560
Technical Appliance Corp.	22	
Telrex, Inc.	7	
Thomas Electronics		655A
Thordarson-Meissner Division	572	
Triad Transformer Mfg. Co.	402	600-602A
Tricraft Products Co.	677	
Trimm, Inc.	589	
Trio Manufacturing Co.	4	631A-638A
Triplett Electrical Instr. Co.	675	
Tung-Sol Electric Co.	106	517A
Turner Co.	220	
TV Products Co.	131	
Ungar Electric Tools	315	
United Catalog Publishers	12	
United Transformer Co.	406	604-605
Universal Co.		660-661
University Loudspeakers	304	509A
Utah Radio Products	25	
Vaco Products Co.	311	
Van Cleff Brothers	2	
V-M Corporation	306	507
Waldom Electronics	579	
Ward Leonard Electric	420	
Webster-Chicago Corp.	571	534
Weller Electric Corp.	584	
Wilcox-Gay Corp.	682	
Xcelite, Inc.	320	

—end—

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Here's your Opportunity



to prepare for a good job or a business of your own in TV SERVICING

There are today more good jobs open in TV Servicing than there are trained and experienced men to fill them. Yes, thousands of opportunities exist now for good-pay jobs offering employment security for years and years to come. Thousands of TV Servicing jobs are going begging. Do you want one of them?

Experts agree, that because of the critical shortage of trained and experienced TV Servicemen, and the tremendous future growth of the industry, no vocational field today offers more opportunities than TV Servicing.

The Big New Industry with a Great Future

Television is just in the beginning stages of its big industrial boom. Look at these amazing facts:

- Lifting the freeze on new TV stations will open many new TV areas and will improve the coverage of existing areas. The result will be an enormous demand for TV receivers.
- Within a few years over 1000 TV stations will be telecasting compared with 108 TV stations now on the air.
- Nearly one-half of all families living within the present TV areas do not yet own TV receivers.
- The new trans-continental video network plus better and more interesting programs plus larger viewing screens and color TV will increase the installation of new receivers, will induce present owners of 12-inch and smaller size viewing screens to buy newer model receivers.
- The power increases of many existing stations and improved reception range of current receivers will result in receivers being installed and serviced in the fringe areas of present stations.
- Under the FCC proposal, over 70 per cent of all communities will be served by UHF channels exclusively. This means TV servicemen must know UHF receivers before the new UHF stations in their area are opened.
- No one yet knows how great the industrial TV market will be.

RCA Institutes Home Study Course prepares you for a Career in TV Servicing

The addition of the RCA Institutes TV Service Training to your present radio-electronics experience will qualify you to step out and grasp the golden opportunities that now exist in television—America's fastest growing industry.

Learn at home—in your spare time—while you study the practical *how-to-do-it* techniques with *how-it-works* information. Easy-to-read and easy-to-understand lessons under the supervision of RCA engineers and experienced instructors quickly train you to qualify for the many good jobs now waiting for trained TV servicemen. Don't pass up this lifetime opportunity for financial security and a bright future in TV. Learn TV Servicing from RCA—pioneers and leaders in radio, television and electronic developments.

RCA Institutes conducts a resident school in New York City offering day and evening courses in Radio and TV Servicing, Radio Code and Radio Operating, Radio Broadcasting, Advanced Technology. *Write for free catalog on resident courses.*

Send for FREE BOOKLET

Mail the coupon—today. Get complete information on the RCA INSTITUTES Home Study Course in Television Servicing. Booklet gives you a general outline of the course by units. See how this practical home study course trains you quickly, easily. Mail coupon in envelope or paste on postal card.



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350 West Fourth Street, New York 14, N. Y.

Without obligation on my part, please send me copy of booklet "RCA INSTITUTES Home Study Course in TELEVISION SERVICING." (No salesman will call.)

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City_____ Zone_____ State_____

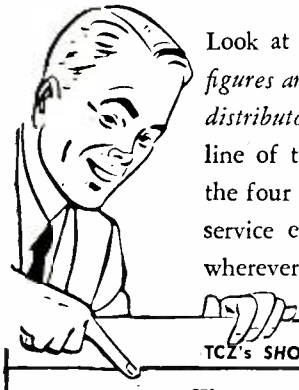
RCA INSTITUTES, INC.

A SERVICE OF RADIO CORPORATION of AMERICA

350 WEST FOURTH STREET, NEW YORK 14, N.Y.

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LOOK AT THE BOX



Look at the figures in the charts below. *These figures are taken from current catalogs listing stock distributor items.* Compare Centralab's complete line of temperature compensating capacitors with the four other leading makes. You'll see why more service engineers are standardizing on Centralab wherever capacitors of this type are required.

Remember too — Centralab was the first manufacturer to offer temperature compensating ceramic capacitors to the market.

For r.f. and resonant circuits — where frequency drift is critical — Centralab Temperature Compensating Capacitors are the last word in accurate stabilizing — *safest and best for guaranteed servicing.*

TCZ's SHOW NO CAPACITANCE CHANGE OVER WIDE RANGE OF TEMPERATURE (-20°C to +85°C)

CRL				COMPETITOR A**			COMPETITOR B**			COMPETITOR C**			COMPETITOR D**		
600VDCW	1200VDCT			(tubular) 500 VDCW			Disc. 500 VDCW — 1000 VDCT			(tubular)			(tubular) 500 WVDC		
										Voltage 500 VDCW					
CRL Part No.	Cap. mmf.	Tolerance	Net Price	Cap. mmf.	Tolerance	Net Price	Cap. mmf.	Tolerance	Net Price	Cap. mmf.	Tolerance	Net Price	Cap. mmf.	Tolerance	Net Price
TCZ- .5	0.5	± .25 mmf	.45	*			†			†			†		
TCZ- .68	0.68	± .25 mmf	.45	*			†			.75	± .1 mmf	.45	†		
TCZ- 1.0	1.0	± .25 mmf	.45	*			†			†			†		
TCZ- 1.5	1.5	± .25 mmf	.45	1.0	± 1 mmf	.30	†			1.5	± .5 mmf	.30	1.5	‡	.30
TCZ- 2.2	2.2	± .25 mmf	.45	*			†			†			†		
TCZ- 3.3	3.3	± .25 mmf	.45	3.0 3.3	± 1 mmf	.30	†			3.0 3.3	± 1 mmf ± .5 mmf	.30 .30	3.0 3.3	‡ ‡	.30 .30
TCZ- 4.7	4.7	± .5 mmf	.36	4.7	± 1 mmf	.30	†			4.7 5.0	± .5 mmf ± 1 mmf	.30 .30	4.7 5.0	‡ ‡	.30 .30
TCZ- 6.8	6.8	± .5 mmf	.36	5.0 6.8	± 1 mmf	.30	†			6.8	± .68 mmf	.30	6.8	‡	.30
TCZ- 10	10	± .5 mmf	.36	8.2 10	± 1 mmf	.30	10	‡	.30	10	± 1 mmf	.30	8.2 10	‡ ‡	.30 .30
TCZ- 12	12	± .5 mmf	.36	*			†			†			†		
TCZ- 15	15	± .5 mmf	.36	*			15	‡	.30	†			†		
TCZ- 18	18	± .5 mmf	.36	*			†			†			†		
TCZ- 20	20	± .5 mmf	.36	20	± 10%	.30	†			20	± 10%	.30	20	‡	.30
TCZ- 22.0	22	± 2½%	.30	*			22	‡	.30	†			†		
TCZ- 24	24	± 2½%	.30	25	± 10%	.30	25	‡	.30	25	± 10%	.30	25	‡	.30
TCZ- 27	27	± 2½%	.30	*			†			†			†		
TCZ- 30	30	± 2½%	.30	*			†			†			†		
TCZ- 33	33	± 2½%	.30	33	± 10%	.30	33	‡	.30	33	± 10%	.30	33	‡	.30
TCZ- 36	36	± 2½%	.30	*			†			†			†		
TCZ- 39	39	± 2½%	.30	*			†			†			†		
TCZ- 43	43	± 2½%	.30	*			†			†			†		
TCZ- 47	47	± 2½%	.30	*			47	‡	.33	†			†		
TCZ- 51	51	± 2½%	.30	50	± 10%	.33	†			50	± 10%	.33	50	‡	.33
TCZ- 56	56	± 2½%	.30	*			†			†			†		
TCZ- 62	62	± 2½%	.30	*			†			†			†		
TCZ- 68	68	± 2½%	.30	*			68	‡	.33	†			†		
TCZ- 75	75	± 2½%	.30	75	± 10%	.33	†			75	± 10%	.33	75	‡	.33
TCZ- 82	82	± 2½%	.30	*			†			†			†		
TCZ- 91	91	± 2½%	.30	*			†			†			†		
TCZ-100	100	± 2½%	.30	100	± 10%	.33	100	‡	.33	100	± 10%	.33	100	‡	.33
TCZ-110	110	± 5%	.30	*			†			†			†		
TCZ-120	120	± 5%	.30	*			†			†			†		
TCZ-130	130	± 5%	.30	*			†			†			†		
TCZ-150	150	± 5%	.30	150	± 10%	.36	150	‡	.36	150	± 15 mmf	.36	150	‡	.36
TCZ-160	160	± 5%	.30	*			†			†			†		
TCZ-180	180	± 5%	.30	175	± 10%	.36	†			175	± 17.5 mmf	.36	175	‡	.36
TCZ-200	200	± 5%	.30	*			†			†			†		
TCZ-220	220	± 5%	.30	*			†			†			†		
TCZ-240	240	± 5%	.30	*			†			†			†		
TCZ-270	270	± 5%	.30	*			†			†			†		
TCZ-300	300	± 5%	.30	*			†			†			†		

**Name on request. *Not cataloged item — available on special order. †Not cataloged ‡Tolerance not listed in literature

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SCORE! . . . Of the five leading makes of temperature compensating capacitors — Centralab gives you more values to choose from — closer tolerances you can rely on — at prices that are right!

TCN's VARY CAPACITANCE ACCORDING TO TEMPERATURE															
CRL				COMPETITOR A** (tubular)			COMPETITOR B** (disc)			COMPETITOR C** (tubular)			COMPETITOR D**		
CRL Cat. No.	Cap. mmf.	Tolerance	Net Price	Cap. mmf.	Tolerance	Net Price	Cap. mmf.	Tolerance	Net Price	Cap. mmf.	Tolerance	Net Price	Cap. mmf.	Tolerance	Net Price
TCN- 3	3	± .5 mmf	.36	*			†			†			†		
TCN- 5	5	± .5 mmf	.36	5	± 10% or ± 1 mmf	.30	†			5	± 10% or ± 1 mmf	.30	5	‡	.30
TCN- 10	10	± .5 mmf	.36	10	± 10% or ± 1 mmf	.30	10	‡	.30	10	± 10% or ± 1 mmf	.30	10	‡	.30
TCN- 12	12	± .5 mmf	.36	*			†			†			†		
TCN- 15	15	± .5 mmf	.36	*			15	‡	.30	†			†		
TCN- 18	18	± .5 mmf	.36	*			†			†			†		
TCN- 20	20	± .5 mmf	.36	*			†			†			†		
TCN- 22	22	± 2½%	.30	*			22	‡	.30	†			†		
TCN- 24	24	± 2½%	.30	*			25	‡	.30	†			†		
TCN- 27	27	± 2½%	.30	*			†			†			†		
TCN- 30	30	± 2½%	.30	*			†			†			†		
TCN- 33	33	± 2½%	.30	*			33	‡	.30	†			†		
TCN- 36	36	± 2½%	.30	*			†			†			†		
TCN- 39	39	± 2½%	.30	*			†			†			†		
TCN- 43	43	± 2½%	.30	*			†			†			†		
TCN- 47	47	± 2½%	.30	47	± 10%	.30	47	‡	.30	47	± 10%	.30	47	‡	.30
TCN- 51	51	± 2½%	.30	*			†			†			†		
TCN- 56	56	± 2½%	.30	*			†			†			†		
TCN- 62	62	± 2½%	.30	*			†			†			†		
TCN- 68	68	± 2½%	.30	*			68	‡	.30	†			†		
TCN- 75	75	± 2½%	.30	75	± 10%	.30	†			75	± 10%	.30	75	‡	.30
TCN- 82	82	± 2½%	.30	*			†			†			†		
TCN- 91	91	± 2½%	.30	*			†			†			†		
TCN-100	100	± 2½%	.30	100	± 10%	.30	100	‡	.30	100	± 10%	.30	100	‡	.30
TCN-110	110	± 5%	.30	†			†			†			†		
TCN-120	120	± 5%	.30	†			†			†			†		
TCN-130	130	± 5%	.30	†			†			†			†		
TCN-150	150	± 5%	.30	†			150	‡	.30						
TCN-160	160	± 5%	.30	†			†								
TCN-180	180	± 5%	.30	†			†								
TCN-200	200	± 5%	.30	†			200	‡	.30						
TCN-220	220	± 5%	.30	†			220	‡	.30						
TCN-240	240	± 5%	.30	†			†								
TCN-270	270	± 5%	.30	†			†								
TCN-300	300	± 5%	.30	†			†								
TCN-330	330	± 5%	.30	†			330	‡	.30						
TCN-360	360	± 5%	.30	†			†								
TCN-390	390	± 5%	.30	†			†								
TCN-430	430	± 5%	.30	†			†								
TCN-470	470	± 5%	.30	†			†								
TCN-510	510	± 5%	.30	†			†								
TCN-560	560	± 5%	.30	†			†								
TCN-620	620	± 5%	.30	†			†								
TCN-680	680	± 5%	.30	†			†								
TCN-750	750	± 5%	.30	†			†			†			†		

**Name on request.

Centralab Temperature Compensating Capacitors are available in five body sizes, *with most values in the smaller dimensions*. For more information, see your Centralab Distributor.

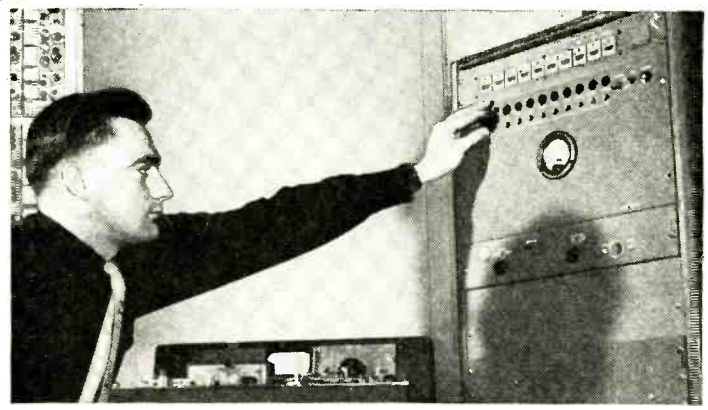
Centralab (CRL) ®

A Division of Globe-Union Inc.

922 East Keefe Avenue • Milwaukee 1, Wis.

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Thunder Hunters





Thunder hunting equipment on location near Madison, Florida. Loop antenna on truck picks up static. The engineer in top picture is watching the indication of a circuit which registers how often the static exceeds a given level.

Many new telephone circuits have two jobs to do—carrying your voice and transmitting signals to operate dial exchanges in distant towns. And an old-fashioned thunderstorm can interfere with both!

"Rolling static" comes from many storms over a wide area and can interfere with clear telephone talk. A nearby lightning flash makes "crack static" which, unchecked, plays hob with dial system signals.

So Bell Laboratories scientists go "Thunder Hunting" in the storm centers of the United States — "capturing" storms by tape recorders. Back in the Laboratories, they recreate the storms, pitting them against their new circuits. This method is more efficient and economical than completing a system and taking it to a storm country for a tryout. It demonstrates again how Bell Telephone Laboratories help keep costs down, while they make your telephone system better each year.

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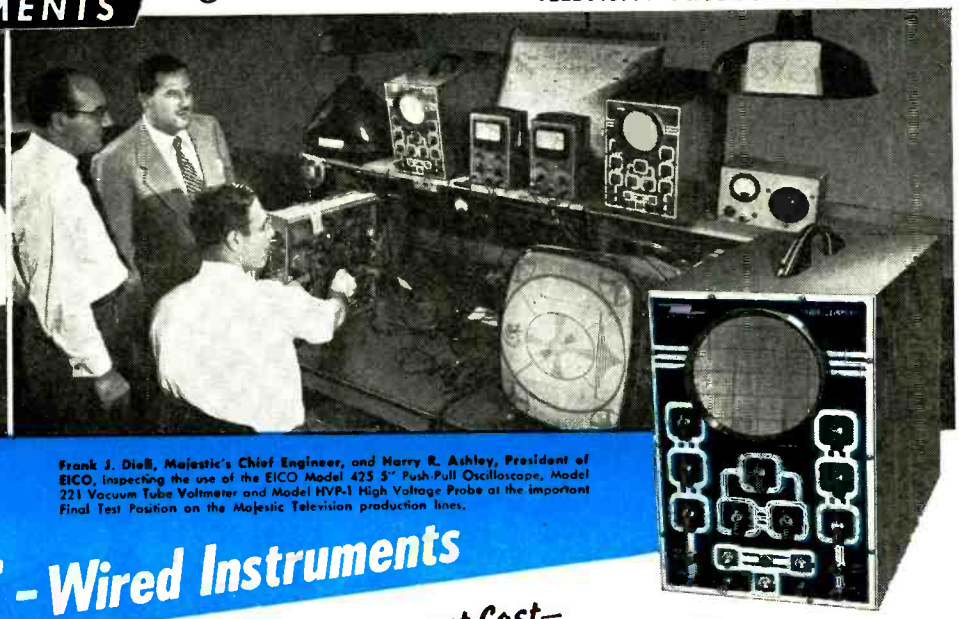
EICO TEST INSTRUMENTS

Guards Majestic

HIGH STANDARDS OF TELEVISION PRODUCTION QUALITY



In the Majestic design laboratories, Frank J. Dieli and assistant, Paul Smith, discuss with Harry R. Ashley, some important prototype-circuit measurements just taken with the 425 Oscilloscope, #221 VTVM and #HVP-1 HV Probe.



Frank J. Dieli, Majestic's Chief Engineer, and Harry R. Ashley, President of EICO, inspecting the use of the EICO Model 425 5" Push-Pull Oscilloscope, Model 221 Vacuum Tube Voltmeter and Model HVP-1 High Voltage Probe at the important Final Test Position on the Majestic Television production lines.

KITS - Wired Instruments

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BECAUSE —like Emerson, Tele-King, Tele-Tone, CBS-Columbia, and many another famous TV manufacturer coast to coast, Majestic knows that

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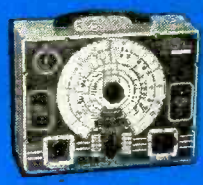
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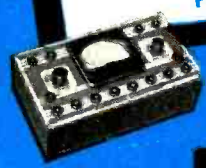


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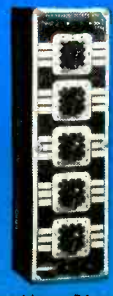
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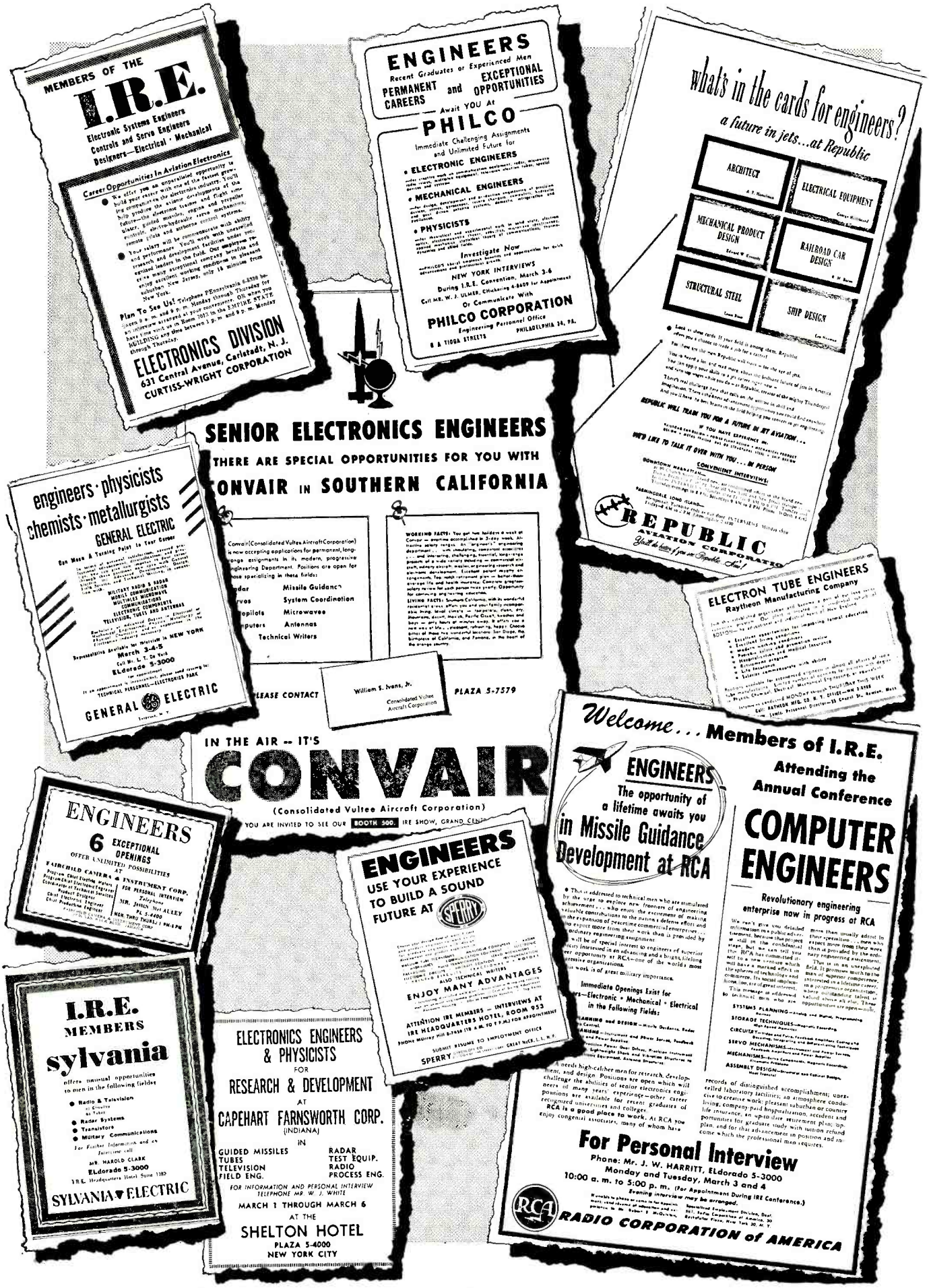
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To make it possible to run the feature on this page Electronic Instrument Company, Inc. (Eico) kindly consented to relinquish this space. The Eico advertisement will be found on the preceding page.

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"GO ELECTRONIC, YOUNG MAN!"

. . . The world's greatest bonanza—radio electronics . . .

By HUGO GERNSBACK

NEARLY 100 years ago, one of the greatest editors of all time, Horace Greeley, in a letter to W. H. Verity, wrote these words of advice: "Go West, young man!" These four words became a household word in this country and soon accelerated the migration—which was in the making—of young men seeking their fortunes in the West. The advice was excellent because Horace Greeley knew what he was talking about. The West, indeed, proved to be a land of unprecedented opportunities, enriching hundreds upon thousands of young men who took the advice.

Today, with technological evolution expanding at an unprecedented rate, we no longer need to migrate from one part of the country to another. There are fabulous, undreamt-of opportunities all around us, making it possible for the young man to stay right at home and progress to a most lucrative future, if he but enter the century's greatest endeavor—radio-electronics. Recently, in our November, 1951, issue, we predicted that "sales of the entire radio-electronic industry by 1960 should reach no less than $10,000,000,000." As the months pass, it appears that this figure may even be exceeded. The reason is that the radio-electronic industry today ranks next to steel and aircraft in importance, and may soon exceed both.

The new giant industry has grown at such a breathtaking rate that new records in all directions are set up almost every week. So fast has been its growth that today it is so short of radio and electronic engineers that the various manufacturers are outbidding each other to fill vacancies—most of which cannot be filled for years to come simply because there are not enough trained men to fill the positions. This trend is certain to continue for many years.

To show to what extent the industry is going in its search for available men, we cite a most astonishing event which occurred last March. During the first week of that month, the Institute of Radio Engineers held their annual meeting in New York. In a single issue of *The New York Times*, there appeared over a dozen advertisements using large space in an endeavor to secure radio-electronic engineers. Some of these advertisements cost close to a thousand dollars apiece. A few of them are reproduced on the facing page as a permanent record of what lengths manufacturers are going to, to secure the talent they so badly need. Indeed, the situation will probably get much worse for some years to come before it will improve.

What then is the answer? While it is possible to graduate a small quantity of men from the existing ranks in the industry, only exceptional men can make the grade without the necessary education that these positions demand. Even radio and TV technicians from the servicing industry are being pulled out and made into "engineers," helping to cripple the servicing trade in the process. This, then is not the answer for a long term pull.

What we need is to educate parents, grade and high schools, that lucrative positions are now going begging for want of electronic engineers. But an electronic engineer is not made overnight. *It is a long evolutionary and educational process.* It starts with a boy of six or less, making him conscious of radio-electronics, and instilling in him the germ of the future engineer by supplying simple radio-technical literature to the young boy, gradually stepping it up over the years. Parents and educators can help the country's economy and incidentally assure the young man of a worthwhile future in the process.

Grade schools and high schools can do a tremendous service by educating young boys in the intricacies of radio-electronics. This is not as difficult as it sounds, because there is always a large percentage of young boys who are mechanically inclined and radio-minded. By supplying them with tools and a few simple radio appliances a young boy can, in easy stages, be made into a technician.

It is much more difficult to instill the radio-electronics spark into a boy once he has reached puberty. The sooner he begins the quicker he will become proficient in the greatest endeavor the world has ever seen. Moreover, as has been found out by past experience, boys who start young in this endeavor are not likely to land in poolrooms and become public charges later.

There is, perhaps, nothing quite so intriguing to the young mind as radio-electronics today. If the boy is started young and kept interested, he will not have to be pushed on by others. He will push himself ahead and be the better for it in the future.

Nor is it expensive to start a young boy off on this technical path. It does not cost more to supply him with radio-electronic gadgets than with other toys. In the end, it will pay big dividends.

If you who read this know of a young boy who needs coaching, this is the time to get him started. If 100,000 of our readers who read this will pass these two pages on to parents of young boys, the shortage of radio-electronic engineers fifteen years hence will no longer be a matter of concern—and you will be doing the boy—and your country—a tremendous favor.

—end—

REPRINTS OF THIS TWO-PAGE EDITORIAL CAN BE HAD AT COST FROM THE PUBLISHERS IN SINGLE LOTS OR QUANTITY.

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TV PATTERN FOR THE FUTURE

By RAYMOND F. GUY*

Planning a nation-wide television system — An outstanding authority discusses the tremendous technical problems involved, and the methods developed by industry and the FCC for the solution of the difficulties

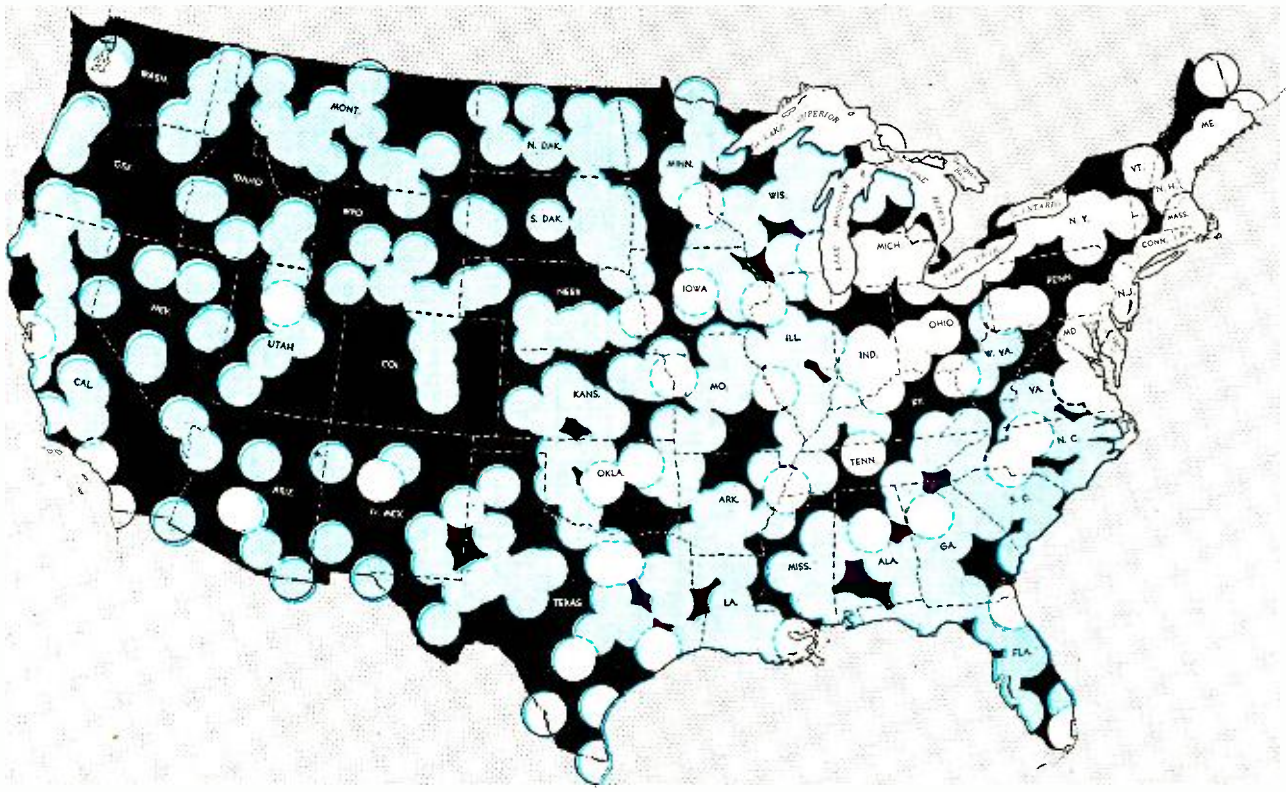
BASED upon long experience it would seem that the planning and adjustment phases of a radio service never reach a point where they may be considered complete or permanent. Developments follow in endless succession to provide service to more people, or better service, or to crowd more message intelligence into a segment of the frequency spectrum, or to combine such improvements. A classic example is the compatible color television system, which more effectively utilizes the 6-mc channel to transmit full color programs fully equal in quality and detail to present black-and-white pictures.

A clear thinker aptly remarked that he was interested not in the past or the present, but only in the future, because he expected to spend the rest of his life there. But all our experience, knowledge and ability to rationalize and plan came from the past. We are not always able to plan wisely. Employment of radio services cannot be postponed until engineers know all there is to know about the behavior of radio waves and the systems which utilize them. Often the pressure of events leaves inadequate time for accumulation of a broad base of experience and knowledge, and we must adjust as required and as the opportunity affords.

The television freeze was imposed because of such a desire to adjust: to minimize TV interference before its growth reached the point of no return. That is our present position. From the

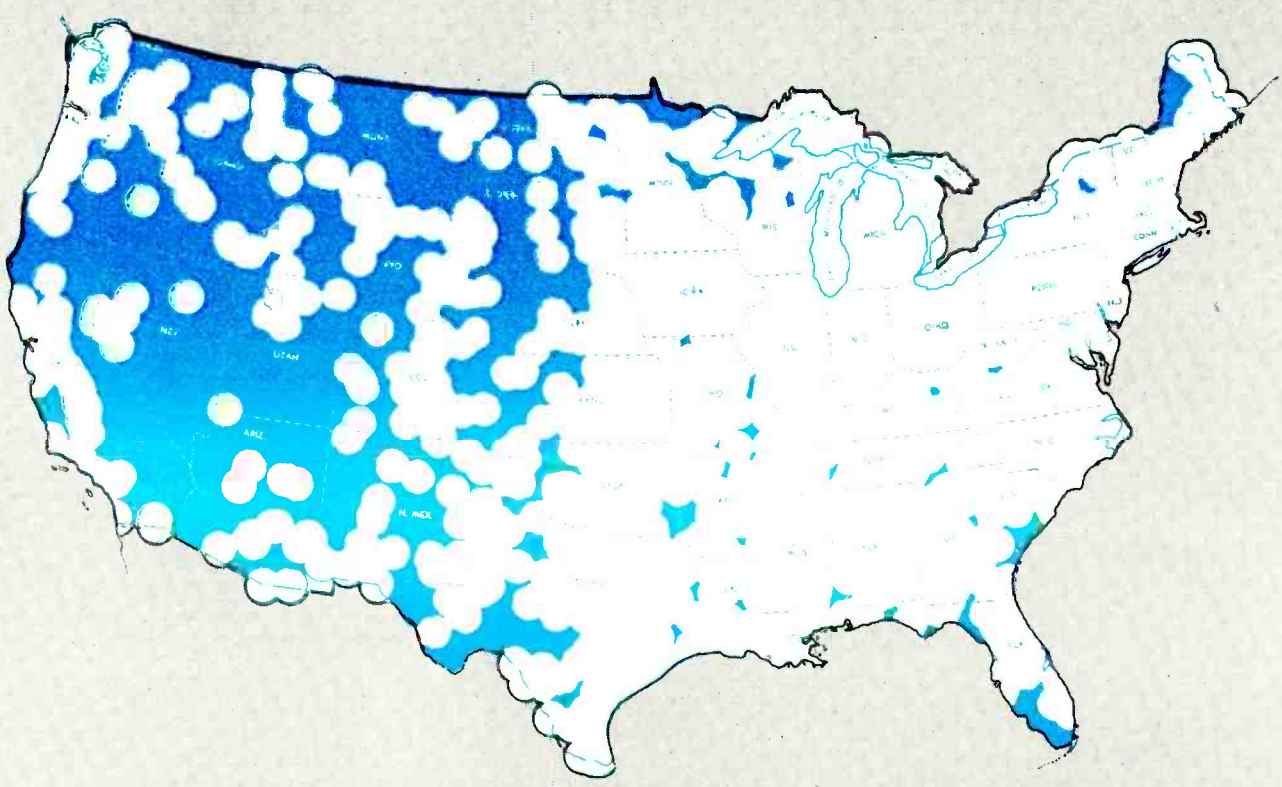
* Manager, Radio and Allocations Engineering, National Broadcasting Company.

Service Areas of Operating and Proposed VHF Television Stations

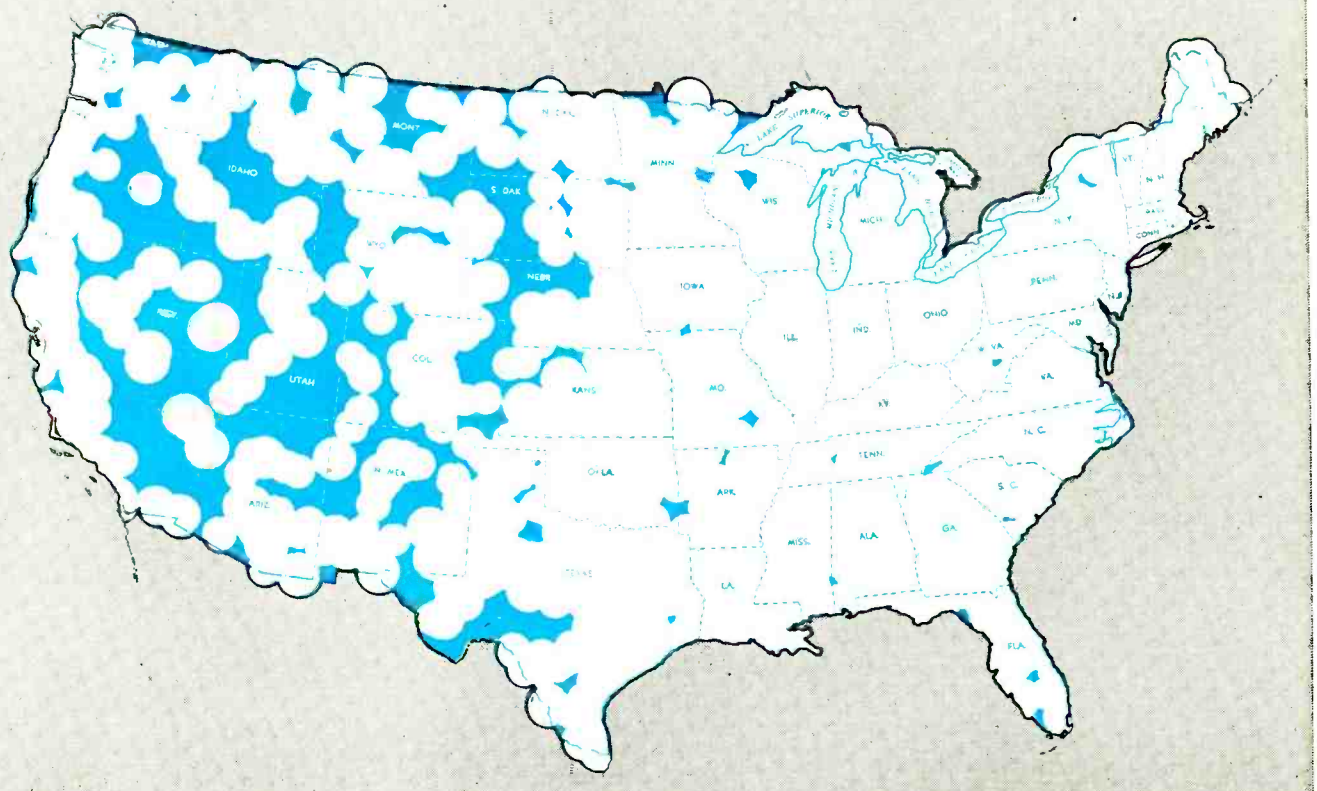


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Service Areas of Proposed UHF Television Stations



Service Areas of All Operating and Proposed VHF and UHF Television Stations



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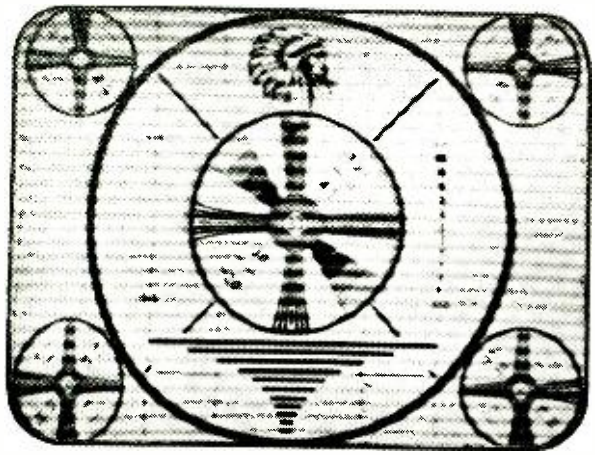


Fig. 1—"Venetian-blind" effect caused by minute frequency differences between carriers of co-channel television stations.

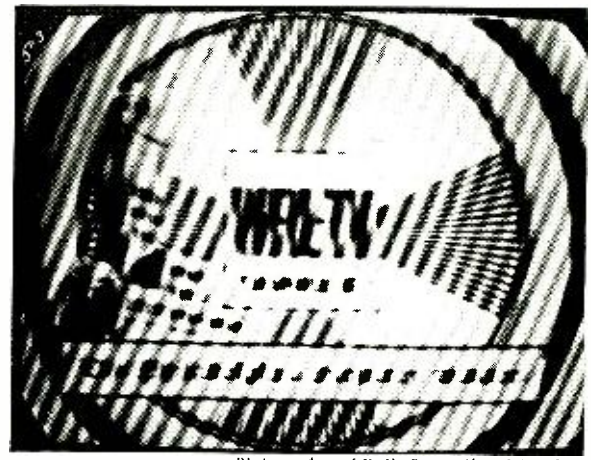


Photo courtesy of Radio Corporation of America

Fig. 2—Typical interference pattern due to pickup of radiation from the local oscillator of another television receiver.

events of the past a pattern is taking shape for the future. It merits display against the background of the past.

Brief history of allocations

In 1928 the author participated in the establishment of station W2XBS in New York, which was probably the the world's first television station to go into permanent operation. The Federal Radio Commission then considered visual broadcasting a matter of speculation. In 1929 four 100-kc experimental channels were established between 2 and 3 mc. But RCA and NBC were even then planning the move to 40 mc and to the Empire State Building which was accomplished by 1931.

In 1936 the commission allocated 19 channels to television in the area now used, and by 1939 commercial licenses were being sought. They were denied as premature.

In April 1941 one of the television channels was diverted to FM broadcasting and new rules were adopted for commercial operation. A few weeks later the NBC Empire State station became the world's first commercial television station, and was followed by a half-dozen more before the war stopped construction.

At a postwar hearing television allocations were cut down from 18 to 12 v.h.f. channels and the uncharted u.h.f. spectrum (now 470–890 mc) was earmarked for future expansion.

As a general rule the commission specified a geographical separation of 150 miles between v.h.f. television stations operating on the same channel, but in making assignments these minimum separations could not always be observed. The 150-mile separation was based on inadequate knowledge and consideration of tropospheric propagation, with the result that severe interference became a major problem as new stations were built. Its magnitude was such that the commission felt compelled to call a halt, and imposed the freeze which is now over three years old.

Many issues face the commission with respect to the formulation of new television rules, standards, and allocations. The rules and standards have as their primary purpose the establishment of a satisfactory foundation upon which to build an allocation structure, and the routines and ground rules by which it may be administered. Our neighboring countries to the north and south either have or are contemplating television service. Our plans must dovetail with theirs if we are to avoid the difficulties experienced in the past in standard broadcasting. In its early years, this service found itself faced with intolerable interference from stations in bordering countries. Through the co-operative efforts of the North American countries an international allocations plan was adopted in the 1930's. To meet the provisions of this agreement scores of stations in the United States alone had to make changes in their operating frequencies, facilities, or both, with much inconvenience, and in some cases, at great expense.

With the experience of the past in mind, the new television-allocations plan will include an agreement with our neighboring countries by which all may have television service through joint use of v.h.f. and u.h.f. channels without conflict.

In order to provide greater freedom from interference among domestic stations, and guard against conflicts with stations in bordering countries, an adjustment has become necessary, consisting of changes in the authorizations of the 31 stations listed to the right.

Offset carrier operation

As a result of observations of television co-channel interference caused to and by its own stations and others, NBC undertook research programs in 1948 and 1949 in co-operation with RCA to develop methods of eliminating or minimizing such interference. The efforts were successful and the technique is now in common use. The interference is caused mainly by tropospheric propagation over distances up to about 300 miles. Differences of up to a few thousand cycles in the carrier frequencies of the desired and undesired stations produced beat notes in receivers. These beat frequencies create horizontal bars on the kinescope similar to venetian blinds, and these lines move in the vertical plane when the carrier frequency of either station changes (See Fig. 1).

Since identical carrier frequencies would produce no beat notes, an automatic synchronizing method was developed in the RCA Laboratories. A receiving station was necessary at a point between the desired and undesired stations with a separate highly-directional antenna directed at each station. These antennas fed individual sharply tuned amplifiers and circuits which extracted the frequency and sense of the beat note. This was transmitted via leased wire lines to *one* of the stations, where the beat note produced a control voltage which caused the oscillator to hunt for and lock at zero beat automatically. WNBT (New York) and WNBW (Washington) were controlled from a receiving station near Philadelphia and WNBK (Cleveland) and WWJ-TV (Detroit) were controlled from a receiving

Station	*City*	*Present Channel*	*Proposed Channel*
WOI-TV	Ames, Iowa	4	5
WSB-TV	Atlanta	8	11
WBRC-TV	Birmingham	4	6
WTTV	Bloomington, Ind.	10	4
WBKB	Chicago	4	2
WLWT	Cincinnati	4	5
WKRC-TV	Cincinnati	11	12
WCPO-TV	Cincinnati	7	9
WXEL	Cleveland	9	8
WNBK	Cleveland	4	3
WLWC	Columbus	3	4
WLWD	Dayton	5	2
WHIO-TV	Dayton	13	7
WOC-TV	Davenport	5	6
WLAV-TV	Grand Rapids	7	8
WSAZ-TV	Huntington, W.Va.	5	8
WJAC-TV	Johnstown, Pa.	13	6
WGAL-TV	Lancaster	4	8
WAVE-TV	Louisville	5	3
WHAS-TV	Louisville	9	11
WMCT	Memphis	4	5
WTMJ-TV	Milwaukee	3	4
WNHC-TV	New Haven	6	8
WTAR-TV	Norfolk	4	10
WKY-TV	Oklahoma City	4	7
WDTV	Pittsburgh	3	2
WJAR-TV	Providence	11	10
WHAM-TV	Rochester	6	5
WRGB	Schenectady	4	6
WSYR-TV	Syracuse	5	3
WDEL-TV	Wilmington, Del.	7	12

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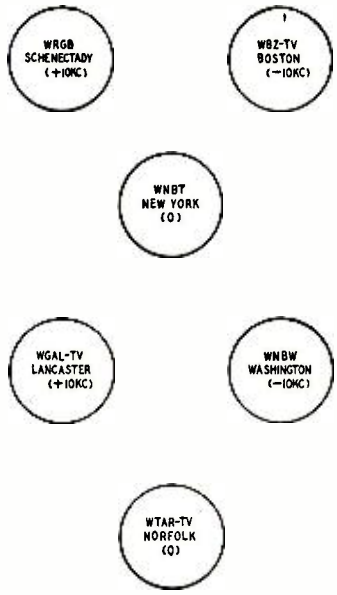


Fig. 3 (left)—Co-channel carrier offset plan proposed by the author and currently in use in northeastern United States.

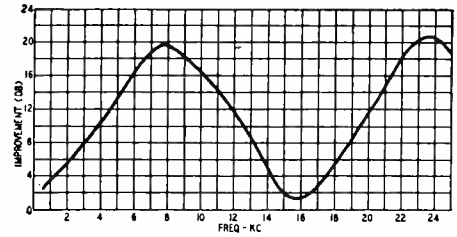


Fig. 4 (above)—Reduction in co-channel interference obtained by offsetting carrier frequencies by controlled amounts.

station near Cleveland. The results were successful and it was planned to synchronize other stations with WNBT. But simultaneously other methods were being investigated, including offsetting the carrier frequency of one of the stations by various controlled amounts.

This method offered the great advantages of simplicity and low cost because it required only a change in the transmitter oscillator of one station, and eliminated the receiving station, wire line, and complex control circuits. It was so successful in laboratory tests that FCC approval was immediately granted for field trials. The laboratory results were duplicated in tests at NBC stations WNBT, WNBW, and WNBK and the carrier-offset system was adopted in 1949, making obsolete the synchronizing method.

The offset frequency schedule proposed by the author, adopted and still used, is shown on Fig. 3.

Fig. 4 shows the approximate relationship of frequency offset and interference reduction. The new FCC proposals contemplate 10-kc offset operation as a standard practice to take advantage of the 17-db reduction in interference provided. In combination with the proposed co-channel geographic separation, the new standards will reduce interference and facilitate increasing transmitter powers to the proposed 100-kw to 200-kw figures, or higher.

Oscillator radiation

The new television allocation plan contemplates other improvements. Service technicians have observed the degradation on some channels from receiver oscillator radiation and are familiar with the causes and effects. (See Fig. 2.) The new plan is based upon the new sound i.f. of 41.25 mc, but also attempts to minimize interference from existing receivers utilizing 21.25 mc without reducing the number of v.h.f. assignments. The u.h.f. allocation plan separates by at least 60 miles those stations 7 channels (42 mc) apart, and thus protects one receiver from the oscillator radiations of others to the same degree that it would be protected from a co-channel station.

Intermodulation

Very high field intensities from undesired stations may produce intermodulation in receiver circuits, particularly when the channels are not widely spaced in frequency. (The effect of this type of interference is to produce a picture from the unwanted station which apparently swings back and forth behind the picture to which the receiver is tuned.) To minimize or eliminate such effects the u.h.f. allocation plan proposes that stations less than 20 miles from each other shall be at least 6 channels apart.

Image interference

Image problems have not arisen in v.h.f. television reception because the images fall outside the channels. But the large numbers of contiguous channels possible in u.h.f. could lead to very destructive image interference.

To guard against such effects u.h.f. channels separated by twice the picture i.f. (91.5 mc, or 15 channels) are proposed to be separated 75 miles or more. Correspondingly, channels separated by twice the sound i.f. (82.5 mc, or 14 channels) are proposed to be separated by 60 miles or more. These separations also are intended to give each television receiver the same degree of protection as from co-channel stations.

I.F. beat

If two local television stations operate on channels separated in frequency by an amount corresponding to the receiver i.f., the two signals may be received directly in the receiver i.f. circuits. This may occur for separations of 7 or 8 channels when the sound i.f. is 41.25 mc and the picture i.f. 45.75 mc. Since stations separated by 7 channels are proposed to be geographically separated at least 60 miles because of oscillator radiation interference, we must consider only what to do about 8-channel separations. The FCC proposes at least 20 miles minimum geographical separation between all such stations.

National coverage

The commission has striven to provide an allocation framework which will as nearly as possible assure television service to all people of the United States and which will also fairly distribute television stations among the states and communities. The implications of this plan are illustrated in the series of maps on pages 30 and 31. In preparing these figures it was assumed that each station would provide its normal coverage to an average distance.

The map on page 30 shows service to be provided by existing and proposed v.h.f. stations. The white discs surround existing stations; the blue discs are centered on proposed ones. The maps on page 31 show service areas of proposed u.h.f. stations, and of all operating and proposed stations. In these maps, white represents service areas and blue, those outside the range of reliable service.

Many have expressed the view that the freeze was unnecessary. This author feels that television of the future will benefit greatly from it. At the time it was imposed no such techniques as carrier synchronism or offset-carrier operation had been demonstrated for television. The full impact of the technical inadequacies in the old standards and rules had not been felt because of the relatively limited number of stations then in operation. But in the Northeastern States the operation of co-channel stations having inadequate protection against interference was causing much concern. In addition, new stations were scheduled to go into operation in such large numbers that the practical difficulties inherent in correcting the shortcomings of the technical standards would have compounded rapidly and perhaps made solution impossible.

Television will become increasingly important in our national life from now on. The commission carries grave responsibility because the pattern established in the present will shape the national service of the future.

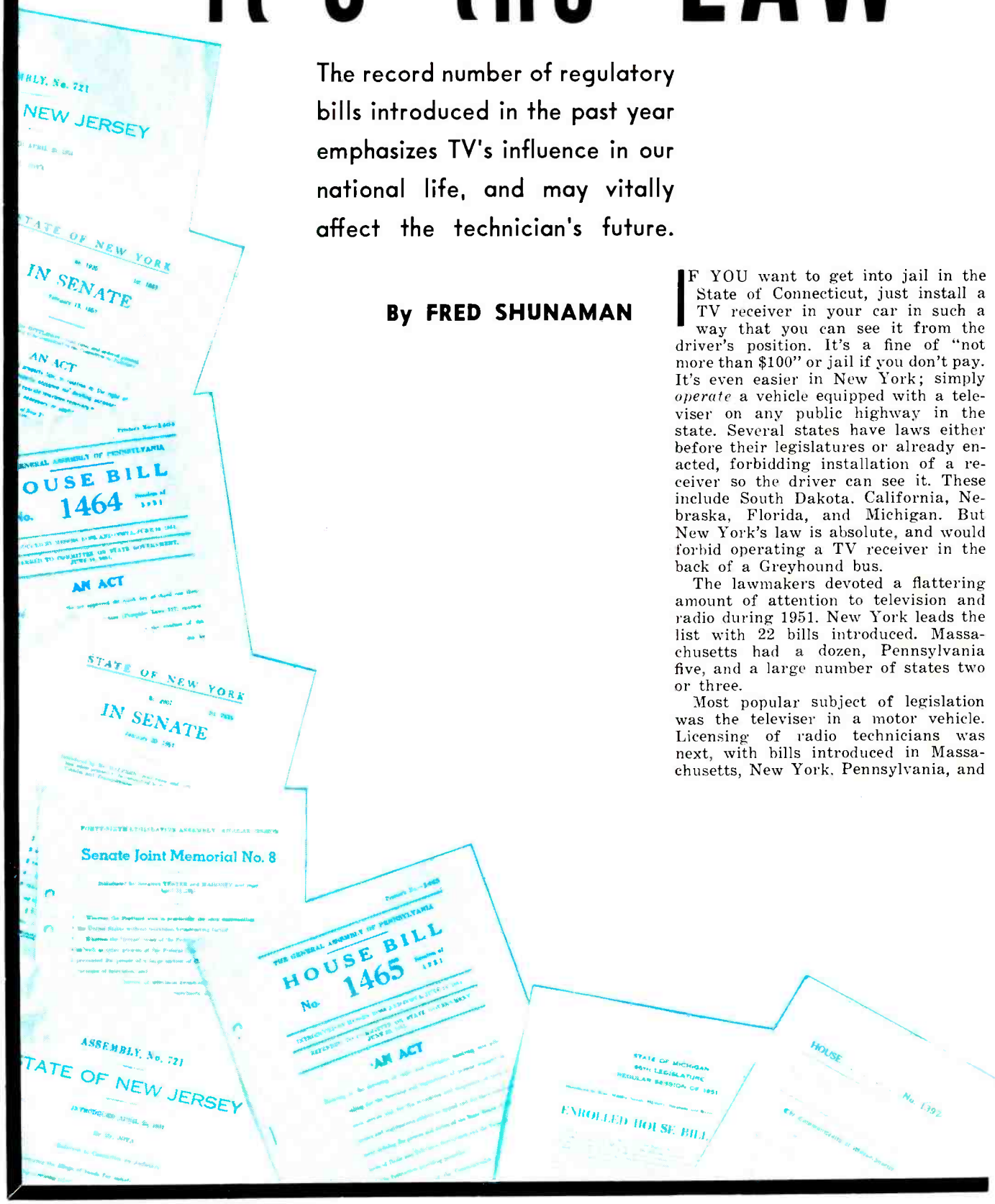
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it's the LAW

The record number of regulatory bills introduced in the past year emphasizes TV's influence in our national life, and may vitally affect the technician's future.

By FRED SHUNAMAN



IF YOU want to get into jail in the State of Connecticut, just install a TV receiver in your car in such a way that you can see it from the driver's position. It's a fine of "not more than $100" or jail if you don't pay. It's even easier in New York; simply *operate* a vehicle equipped with a televiser on any public highway in the state. Several states have laws either before their legislatures or already enacted, forbidding installation of a receiver so the driver can see it. These include South Dakota. California, Nebraska, Florida, and Michigan. But New York's law is absolute, and would forbid operating a TV receiver in the back of a Greyhound bus.

The lawmakers devoted a flattering amount of attention to television and radio during 1951. New York leads the list with 22 bills introduced. Massachusetts had a dozen, Pennsylvania five, and a large number of states two or three.

Most popular subject of legislation was the televiser in a motor vehicle. Licensing of radio technicians was next, with bills introduced in Massachusetts, New York, Pennsylvania, and

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Wisconsin (as well as at least four cities, Los Angeles, Miami, Milwaukee, and New York). Another important subject is protection of moneys paid for TV contracts, either by bonding, escrow, contractor licenses, or a combination. Several states introduced bills requiring colleges receiving state aid to permit their athletic events, or other affairs to be televised, so that the taxpayer who is financing the affair can see it. Other bills relate to the appearance of minors on TV shows, or cover other public-interest angles of the art.

Licensing bills have attracted more attention than any others. Most of them have one feature in common: They propose setting up one or more grades of TV service technicians, and boards of examiners to determine those qualifications. They also provide for license fees. In the Massachusetts, Pennsylvania, and Wisconsin bills (and that proposed for the City of New York) the administrative board would have at least one representative from among the radio technicians. The Pennsylvania bill provides that *three* of the board shall have experience in electrical servicing, including TV, and that the other two have experience in training TV and radio service personnel.

Licensing is still a live issue in Pennsylvania and in the cities of Los Angeles and New York. It is dormant at other points, or has been completely abandoned, as in Milwaukee. A campaign of education and control by dealers and service technicians in that city cut TV service complaints down to a point the local Better Business Bureau considered surprising, and little more was heard of the licensing proposal.

Adherents of licensing believe that an examination and license would give the technician a semiprofessional standing, would assure the customer that the service technician he called would be a real technician and not a high-school boy masquerading as such, and would help the employed technician by making it impossible for service companies to hire cheap, untrained men to do their work. This, they say, would increase the demand for trained technicians, and thereby raise their living standards.

Opponents of licensing have been equally quick to point out that customers will not be protected from dishonesty, which according to Better Business Bureaus and other authorities, is a more serious cause of complaint than incompetence. They also point out that action can be taken against improper service tactics without first licensing the technician or organization, and point to Los Angeles, where TV repairmen are doing time in the local jail.

Another large number of bills—practically all of which have fallen by the wayside—seek to protect the buyer of a TV service contract. By license, bonding, or escrow arrangements, or a combination of the three, they try to assure that the TV set owner will not be left holding the bag after having bought and paid for his contract. A typical bill is one from Rhode Island, which was before the 1951 session, and has been introduced at this year's sitting. It provides for licenses for all sellers of service contracts, plus a bond of $2,000 for each licensee. New Jersey had a bill which provided for bonding all persons or firms receiving money under contract for TV servicing. Several similar bills were introduced in the New York Legislature, some calling for bonding, others for deposit of all moneys received as payment for TV contracts in a trust fund, and for making monthly withdrawals.

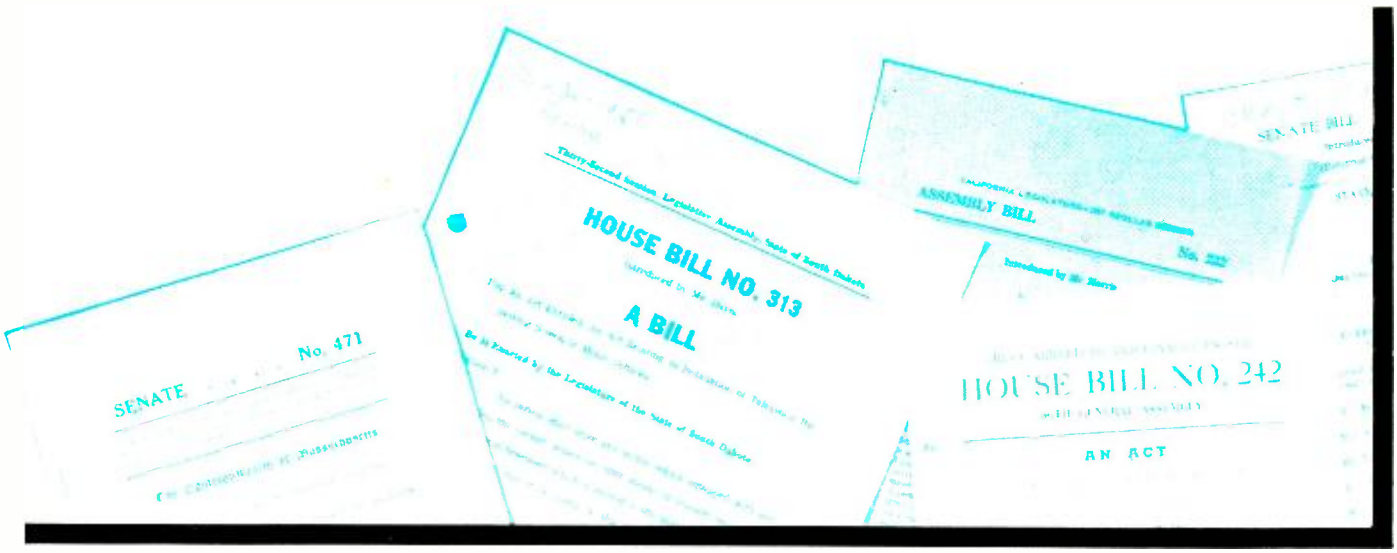
Education by television was the subject of five of Massachusetts' twelve bills, though the subject was not touched by any other state. Two of the five bills petition the Federal Government to set aside allocations for educational broadcasting. The others would establish a State Television Authority to direct the State Department of Education to establish a program of television education, over the state's own TV station if need be.

Several states were interested in seeing that state institutions supported by taxes refrain from entering into contracts which might prevent the taxpayer from seeing football games or other events. These ranged from resolutions urging colleges to have their games televised to strongly worded bills directing that no state-owned stadium be used for such events, or that state aid be cut off immediately if televising were restricted. Unlike most TV bills, the majority of these acts were passed by the legislatures in which they were introduced.

A few bills had technical or safety aims. New York added to its law forbidding radio antennas or other wires within 10 feet of a roof, the words "and no radio, television antennae, or other wires shall be attached to any fire escape or to any soil or vent line extending above the roof." Massachusetts had a bill which would have authorized their department of public safety to investigate the necessity of uniform rules and regulations in regard to television sets and antennas, and would have prevented any city or town in the Commonwealth from setting up rules taxing or licensing TV sets or antennas until such study should have been made. New Hampshire enacted a law authorizing the erection of television structures, poles, and underground conduits or cables along or across public highways on the same footing as other utilities.

But perhaps the bill that shows more than any other the position TV has gained in our life is a proposed amendment to a law relating to exemption from execution and attachment. Introduced in the California Assembly, it provides that among the goods exempt from seizure for debt shall be included, together with "household, table, and kitchen furniture . . . beds, bedding," and other bare necessities, "also one radio, one television set and equipment . . ." The TV receiver, in the mind of one California legislator at least, has taken its place with the family bed and table as one of the necessities of which a judgment debtor may not be deprived.

—end—



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CONVERTING THE RCA 9T-270

A successful conversion of a popular receiver, with a minimum of mechanical and electrical modifications.

By GERALD SHIRLEY

IN THE field of TV conversions more 10-inch sets are converted than any other size, and the great majority of these are probably converted to 14-inch rectangulars. The chief reason for this is that the original cabinet can be used.

A potential field for conversions also exists among 16-inch round-tube sets, since in most cases a 20-inch rectangular will fit into the original cabinet (with some alterations of course). The rear end of the new tube may protrude several inches at the back of the cabinet. This may or may not be a deterrent, depending on where the set is placed in the room or whether the owner objects to having it a little further from the wall. Where a set is placed diagonally in a corner of the room the protruding rear end of the tube is no problem at all.

When a 16GP4 or any other *wide-angle* tube is replaced with a 20-inch rectangular, a perfectly satisfactory picture should be obtained on the new tube without making any electronic changes in the set (assuming, of course, that the set is in first-class operating condition). There may be a temptation to try a few tricks for increasing the high voltage, (such as reconnecting the ground side of the h.v. filter condenser to the hot terminal of the horizontal output transformer, etc). It should be borne in mind that a limitation is imposed on increasing the h.v. by the need for ample picture width and for some reserve sweep power to compensate for tube aging, etc.

The conversion described in this article was done on an RCA 9T-270, a high-definition table model using the long 16AP4. The high-voltage supply uses a doubler circuit which puts out about 12,000 volts. Since this is sufficient for a 20CP4 we decided to try to sweep the new tube with the original deflection circuit, substituting only a new yoke to avoid neck shadow.

The first step (standard operating procedure in any conversion) was to put the receiver into first-class condition. It should be possible to oversweep the 16AP4 with both width-selector and horizontal drive controls at reduced settings. Refer to service manual for diagram. A 20-inch tube was then substituted temporarily with no change except for a recessed-cavity type h.v. connector. The original yoke gave some shadow, as had been expected, but surprisingly less than one normally encounters when swinging a 70-degree tube with a 50-degree yoke. It is possible that with painstaking adjustments of the yoke, focus coil and ion trap the original yoke can be used. However, the length of a 50-degree yoke places the focus coil too far back for greatest effectiveness, and too close to the ion trap.

Electrical Changes

Cosine-wound 70-degree yokes are now available from several manufacturers. The inductance of the horizontal windings should be approximately 8 mh. to match the deflection winding of the RCA flyback transformer. We used a Philco yoke (stock No. 32-9644) which required some physical modifications to fit the RCA yoke cradle.

Substituting the Philco yoke for the original RCA yoke, we obtained an excellent, unshadowed picture on the 20CP4. With the width-selector and horizontal drive controls set for maximum picture width, the raster overlapped the tube face and the actual pictures (which are always smaller than the raster) just filled the screen. As stated earlier, a certain amount of reserve sweep should be provided on any conversion job; otherwise, as tubes age and the picture shrinks, it will be necessary to replace such tubes as the horizontal output, its driver, and the power rectifier much more often.

The method we used to achieve the extra sweep consists of a form of feedback from the horizontal output transformer. The hot secondary tap of the horizontal output transformer (terminal 4) is coupled through a very small capacitor to the grid of the 6BG6-G. Since large amplitude pulses are present in this feedback loop, the capacitor must have a very high voltage rating. We used the inherent capacitance between the two conductors of a length of 300-ohm line, while the plastic insulation between them provides a healthy safety factor against breakdown.

A length of about 2½ feet added over an inch to the sweep width without lowering the 12,000 volt anode supply. This caused slight nonlinearity at the extreme edges. Fig. 1 is a photograph taken after the conversion was completed, showing that the *over-all* linearity is very good.

Still more sweep was obtained by lengthening the 300-ohm line to 4 feet, at the expense of noticeable nonlinearity at the edges. Further increases in the feedback capacitance caused a drop in high voltage, poor regulation, and picture blooming.

The 2½ feet of 300-ohm line was rolled up tightly, and taped, and mounted on a porcelain standoff insulator under the chassis near the 6BG6 tube socket. (See Fig. 2) We now had a picture that more than filled the tube with the width selector at its mid-position, and the horizontal drive control 1½ turns from maximum. The over-all focus was excellent, and the picture brightness was very good.

Mechanical Changes

The front of the cabinet was taken off, and the white inner plastic mask was unscrewed from it. The 16AP4

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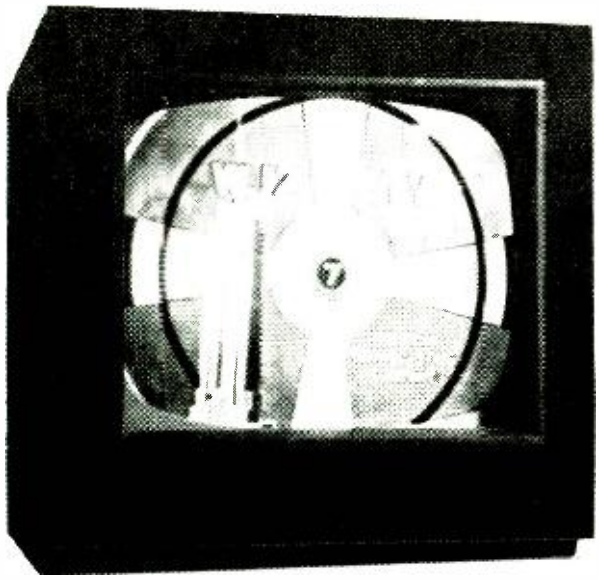


Fig. 1—Picture quality—the test of a successful conversion.

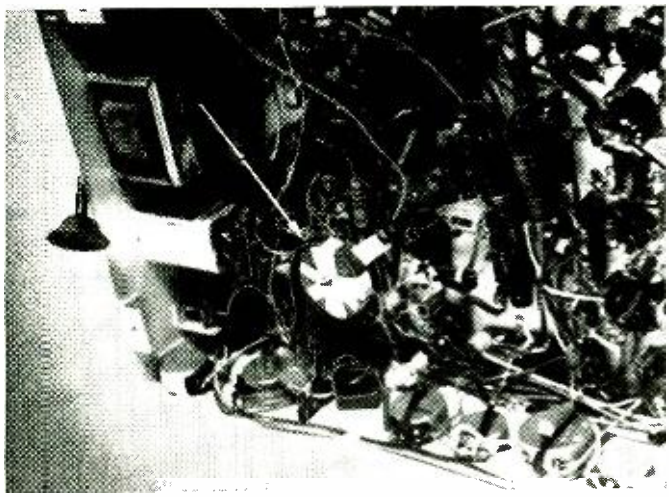


Fig. 2—Location and mounting of the 300-ohm line feedback capacitor.

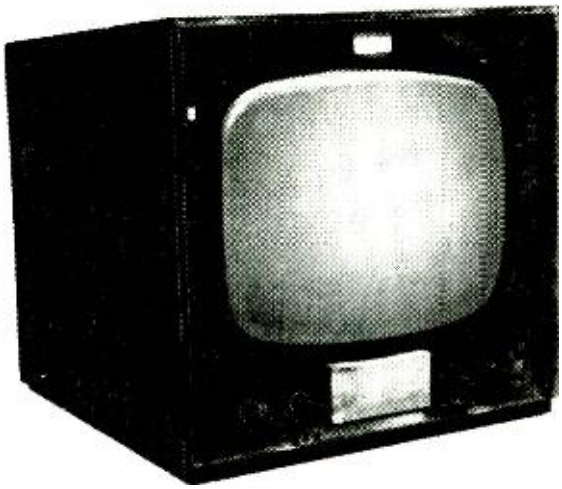


Fig. 3—The front removed from the receiver, showing CRT supports.

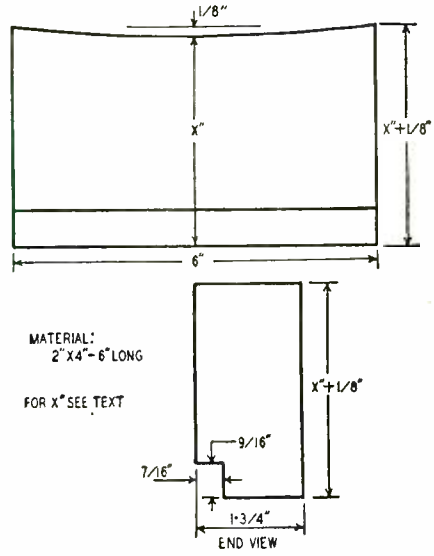


Fig. 4—Details of the lower supporting block for the 20-inch glass picture tube.

was removed and the four plastic tube positioners were unfastened from the inner wooden panel. The cabinet was then placed on the floor, face up, and the 20CP4 was placed in the round opening of the inner wooden panel. (Because of its rectangular shape the 20CP4 will not fall through this opening). The tube was oriented and aligned with the cabinet as accurately as possible. Then with the aid of a small square and an ice-pick, the outline of the tube at its widest points was pricked into the wooden panel below. At the same time, a measurement was taken of the distance from the bottom center of the tube to the cabinet floor. This measurement is used in designing the wooden support block, shown in Fig. 3.

The tube was then removed from the cabinet, and a fresh outline was made on the inner wooden panel ¼ inch *higher* than the first. The new outline was then cut out by drilling a series of closely-spaced ⅛-inch holes along the outline and cutting through them with a keyhole saw. An outline drawing of the supporting block is shown in Fig. 4. The block is concave on top to fit the shape of the tube and provide even support for it. The top of the block should be covered with a layer of sponge rubber, ¼ inch to 5/16 inch thick. The height of the block at its midpoint (dimension "x" as shown in Fig. 4) is calculated as follows: add ¼ inch to the measurement taken earlier of the distance from the bottom-center of the tube to the cabinet floor, and subtract the thickness of the rubber layer when it is compressed by the weight of the tube. The block is channelled at the bottom as shown in Fig. 4 to clear the front strip on the cabinet floor, and is fastened flush against the strip by two 1½-inch woodscrews which run up through the cabinet floor.

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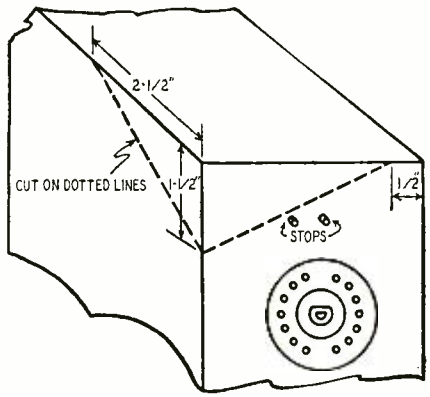


Fig. 5—Sketch of the tuner enclosure, showing material that must be removed.

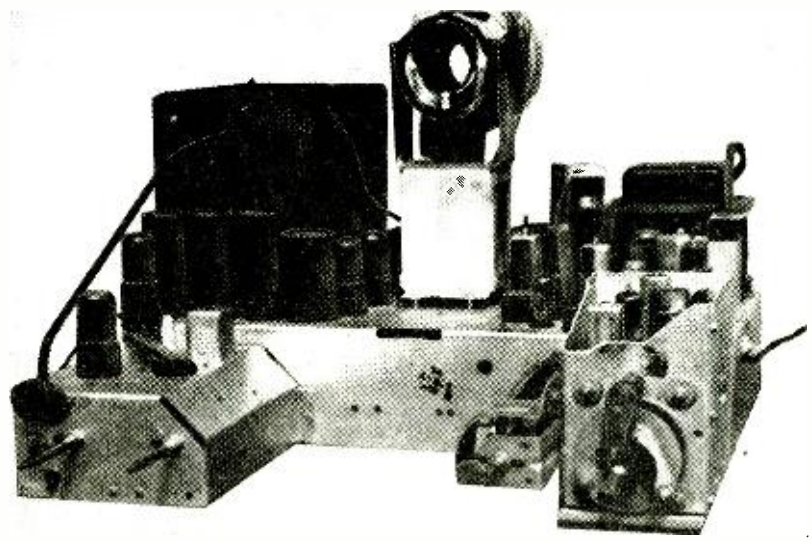


Fig. 6—All necessary mechanical changes are shown in this view.

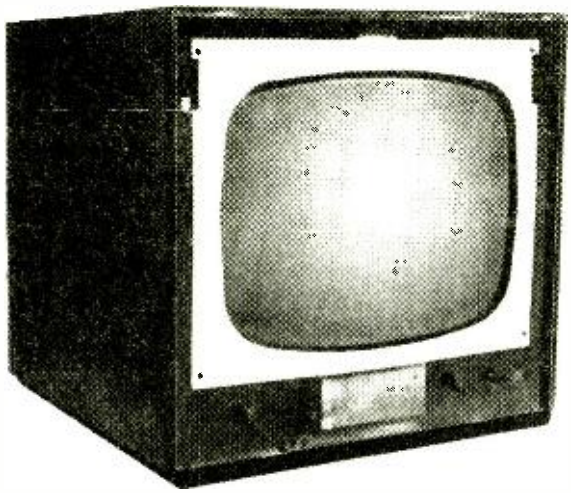


Fig. 7—Installation of the removable picture-tube mask.

Three mechanical changes must be made to the chassis. The upper left-hand corner of the tuner shield must be cut away, one tube moved to a new location, and the yoke mounting bracket must be moved forward and raised. Each of these changes we will discuss in turn.

Fig. 5 shows the portions of the tuner that must be cut down. Be careful to clear the two punched-out mechanical stops for the tuning control. (Before cutting remove the tubes and cover all openings in the tuner so as to keep out metal filings. Fig. 6 shows the front end after it was cut down. We had to saw it three times before we had enough metal off, so it does not look as neat as if we had known in advance how much to remove.) It is necessary, of course, to use care, and to see that the blade at no time strikes the transformer mounted near the front of the tuner.

The 6SN7 on the *left* "front-porch" assembly of the chassis had to be moved since its top prevented the picture tube from going all the way in. Rather than go through the headaches of making a hole in the chassis for a new socket, we simply mounted a new socket on two standoffs a short distance away, as shown in Fig. 6. Before mounting it, we soldered on eight wires of equal length whose other ends were soldered into a male octal plug made from the base of a burned-out tube. The whole operation did not take over half an hour, and the performance of the set was in no way affected by moving the tube.

Next, the bracket assembly which holds the yoke and focus coil was moved forward 3/4 inch by drilling four new mounting holes. Four tubular metal spacers 1/4 inch high were used to raise the bracket assembly in its new location. The details are shown in Fig. 6.

The chassis was put back in the cabinet and bolted in place. The picture tube was inserted, and then the front of the cabinet was put in place temporarily so that the proper location of the picture tube—fore and aft—could be determined. The face of the tube should not quite touch the safety glass insert. With the picture tube properly positioned, the yoke cradle was adjusted to bring the yoke as far forward as possible on the neck of the tube. (Because of the winding configuration of the 70-degree yoke, it may be necessary to remove the original rubber bumpers from the yoke cradle to get the necessary room.)

To bring the focus coil closer to the yoke, it is necessary to shorten the three springs and bolts which hold the focus-coil bracket to the cradle. The springs were cut down to about 1/2 inch in length, and the bolts to about 1 inch. A new *single-magnet* ion trap was then installed.

To hold the tube more securely in position, we wedged another block of wood—also rubber lined—between the top of the tube and the ceiling of the cabinet. This can be seen in Fig. 3.

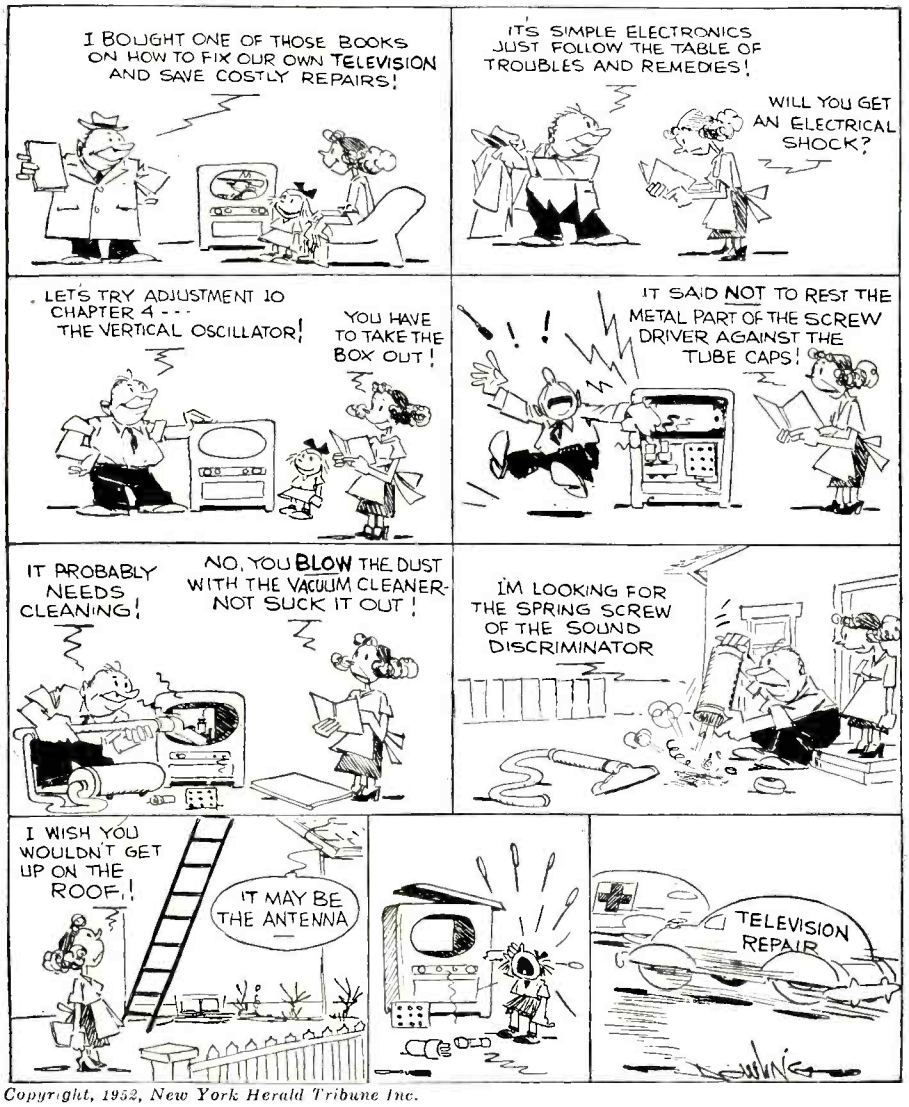
For a mask we used a large cream-colored mat of the type available from most camera supply houses. An outline of the useful screen area was made on the mat and then carefully cut out with a single-edge razor blade. This mask was fastened to the inner wooden panel with four screws and washers, as it must be removable. It is shown in Fig. 7. There may be a commercially available open-face mask which can be adapted easily to this conversion. If a solid plexiglass mask is used, it may be necessary to remove the pane of safety-glass which is in the front frame.

RCA made a number of different models using this same chassis. It should be possible to convert any of these other models following the procedure outlined in this article. The same holds true for the 16-inch models in the preceding 8T series.

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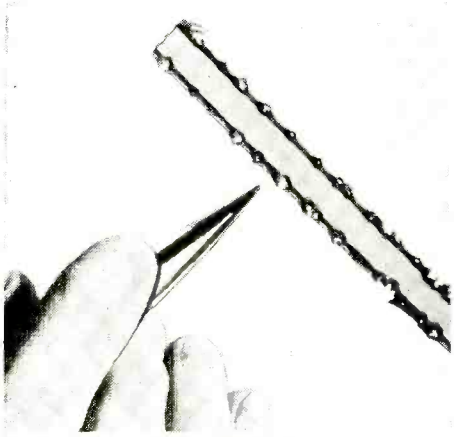
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HOW TO FIX YOUR OWN TELEVISION SET



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When Lightning Strikes the Lead-In



Courtesy American Phenolic Corp.

Lightning struck this section of Twin-Lead, and this is what happened. The polyethylene body of the line is relatively untouched, but the copper conductors are completely vaporized, and the insulation covering them is melted.

This is just a mild illustration of what lightning can do. Proper grounding of TV antennas and masts will do much to prevent this and worse damage to antennas, masts, receivers and homes or shops.

TV DX FOR MAY

EVERYONE looks forward to May, and no one more than TV dx enthusiasts and the hams who operate on the v.h.f. bands, for while "spring is busting out all over," so is sporadic-E dx. After dragging through eight months when dx has been infrequent at best, owners of TV sets almost anywhere in North America should be able to bring in strong signals intermittently during late April, and more frequently in May. Generally warmer weather will also have a beneficial effect on local coverage, and fringe-area signals will begin their climb toward the summertime peak.

The most common low-band dx reception will take place over distances between 600 and 1,200 miles, tending toward the higher figure at first, then coming in closer in the latter part of the month. Most dx will be caught in the early evening, though viewers who have an opportunity to make daytime checks will find the morning hours worth watching closely. The low spot of the day will most probably be in the late afternoon, and most evening openings will fade out before 11 pm local time. Channels 2, 3, and 4 will be affected most often.

Exact date and time prediction is still largely in the crystal-gazing category, but the observer himself can make his own predictions for May by recording results in April. If pronounced dx develops in April, look for recurrences 27 to 28 days later. The May recurrence should be longer and more widespread than its April predecessor. Current indications are that a break may occur—at least in Southern states—between April 28 and May 2. There should be a good period around the middle of the month, and probably the best dx so far in 1952 during the last week of May.

As weather gets steadily warmer, tropospheric propagation will improve. Areas that have had snowy reception from distances of 100 miles or more in the winter months will note considerable rise in average signal level on all channels, and there will be the first signs of "ducting" on the high channels, making possible occasional reception over distances up to 500 miles or more on channels 7 to 13. Considerable co-channel interference can be expected in areas where there have been frequency reassignments within 150 miles or less. The cure, of course, is an antenna system of higher directivity to knock down the signal from the unwanted direction.

In locations where there is dense foliage, signal levels may be lower when the leaves make their appearance. Raising the antenna to clear nearby trees may be desirable, but in many instances the improved propagation of the spring season will counterbalance foliage losses.

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TV SERVICE CLINIC

Conducted By

MATTHEW MANDL*

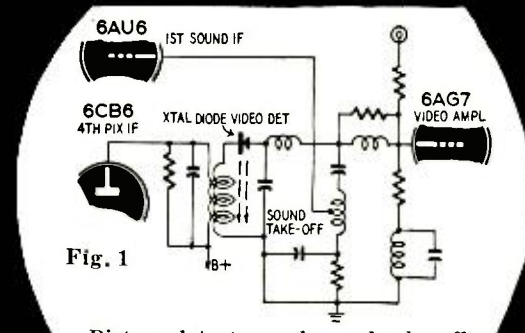


Fig. 1

Picture detector and sound take-off circuits in RCA KCS-66A series.

OFTEN readers of the Television Clinic forward information to us regarding unusual servicing problems. On other occasions they report discovering some little trick which overcame a particularly tough problem. On occasion we will pass these along so that the service technician can make notes of them and try corrective measures such as these when similar conditions are encountered.

A. D. Marikle of New York reports an unusual symptom in the RCA KCS-66A series receivers. He has encountered conditions where the receiver has a normal raster, fair or even good sound, but no picture. Normally this would indicate trouble *after* sound take-off. In three instances, however, he has found this trouble to be a defective 1N60 crystal diode video detector as shown in Fig. 1. This would not ordinarily be suspected, as the sound take-off is *beyond* the detector circuit. Evidently the rectifying action of these crystals can decline considerably but still permit heterodyning of sound and picture signals to secure the necessary 4.5-mc frequency for the sound i.f. stages.

M. Savka of Newark, N. J. found a method for minimizing afterglow effects in the Hallicrafters 600 receiver. In this model, as with many others, the afterglow is centered on the screen after the set is shut off, and remains there while slowly dimming out. Our reader found that a very slight rotation of the ion trap a few degrees in one direction or another altered the afterglow condition. The slight adjustment was sufficient to cause the afterglow to sweep upward and disappear as soon as the set was shut off. There is usually sufficient latitude with regard to a few degrees rotation of the ion trap where brightness is not diminished. This depends on gun structure and circuit design and will not work with all receivers.

J. K. Cross of Greenwich, Connecticut, has found a way to eliminate the foldover which often occurs on the Philco 48-1000 after conversion.

*Author: *Mandl's Television Servicing.*

In several instances he has encountered severe foldover after converting these models and tried all normal solutions without help. Eventually he found that these receivers have a very fast inherent flyback time. Ordinary horizontal output transformers having longer retrace cause a portion of the retrace to be unblanked. Our reader found that by using a voltage doubling type of horizontal output transformer, the Q difference permitted the flyback time to be more nearly that required by the receiver.

He used a RCA 218T1 transformer with matching yoke, driving a 20-inch tube. This eliminated the foldover though he found that the drive was rather sensitive. He corrected this by making the 820-μμf capacitor a variable padder. This is in the plate circuit of the horizontal oscillator. With these components he gets sufficient drive for a 6CD6 without instability or overheating. One of these converted sets has been in use for over a year without any trouble.

Pincushion effect

I am running into a severely distorted picture in a Trav-ler 64-R50 receiver. The sides of the picture are bent to resemble pincushion effect. I have checked the focus coil, changed the ion traps, and replaced all tubes.

I have also checked the components in the horizontal and vertical sweep systems without finding the trouble. C. W. B., Marshalltown, Iowa.

The pincushion effect which you are experiencing in the Trav-ler 64-R50 receiver could be caused by a defective deflection yoke. Often shorted turns in a yoke will produce this condition as shown in Fig. 2. Pincushion and barrel effect can also be caused by a mismatch between the horizontal output transformer and the yoke.

You should also check to see that there is no magnetic field too close to the picture tube. Make sure the speaker and the transformers are not creating magnetic fields which would cause picture distortion. (A small pincushion effect is a normal characteristic of most high-efficiency 70-degree deflection yokes, especially those with cosine-type windings. The picture size is

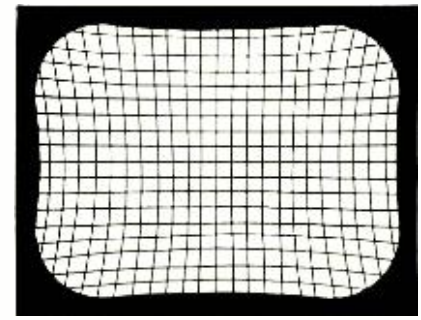


Fig. 2—Cross-hatch pattern showing the "pincushion" effect discussed in the text.

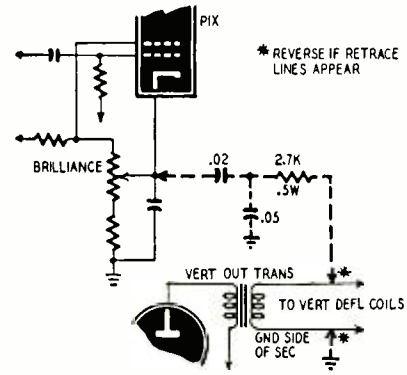


Fig. 3—Vertical retrace-eliminating circuit adaptable to many TV receivers.

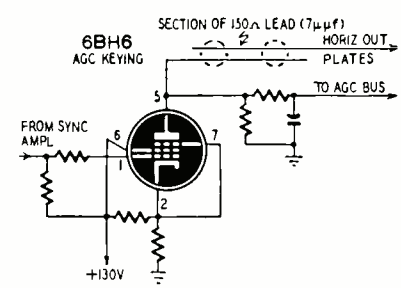


Fig. 4—Schematic of the keyed a.g.c. circuit used in Westinghouse model H609T10.

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usually adjusted so that the concave edges are outside the mask.)

You mention changing all tubes and presumably you have tried a new horizontal output tube as well as a new high-voltage rectifier tube. Decreased emission from these tubes can cause some blooming and also picture distortion.

Split-sound buzz

In an RCA 6T54 a hum or buzz is heard which is produced at most of the settings of the fine-tuning control. The adjustment is critical and the buzz can be minimized only at one narrow point. Also the point of best picture reception is not the best point for sound, and this is the case for all stations. H. S., Brooklyn, N. Y.

This seems to indicate improper tracking in the tuner. With the tuner frequency adjusted to favor one segment of the bandpass over the other, the hum or buzz becomes more pronounced. This is not an intercarrier receiver, and therefore the buzz you experienced would be of the tunable type caused by detuning from the correct relationship between picture and sound. You should check the tracking and also the alignment of the receiver with your sweep generator, marker, and scope, against those shown in the schematic for this receiver. Also try a new tube in the local oscillator stage of the tuner, for you may be getting tunable hum. This is caused by a heater-cathode short or leakage in the local oscillator tube.

Retrace elimination

I would like to eliminate the vertical retrace which occasionally appears. The receiver is a Tele-King model 410. D. S. W., Kent, Ohio.

Fig. 3 is a retrace eliminating circuit which can be added to the Tele-King 410. The portion of the schematic in broken lines represents the additions to be made to the present circuit.

Arcing at grounding springs

In a DeWald receiver, the original 10-inch tube has been replaced with a 12LP4 with no other changes. The receiver worked well for a year but suddenly started to arc around the corona ring and between the picture tube graphite coating and the two grounding springs at the yoke. I cleaned the corona ring and changed the 1B3-GT as well as the 6BG6-G without improvement. Inserting insulation between the corona ring and the high-voltage tube socket stopped the arcing there but it still arcs at the grounding springs. The arcing increases as the brightness control is advanced. M. W., Detroit, Mich.

The cause of these symptoms is often poor contact between the grounding springs and the graphite coating of the tube. Sometimes the grounding springs wear away portions of the graphite coating and do not make good contact. A high-voltage charge accumulates on the surface of the tube, and arcing will thus occur. You should check the graphite coating to see whether it is intact at the grounding springs. If it is worn, replace with graphite dope available at your local distributor. You could also rotate the tube slightly to present an unbroken graphite surface area to the contact springs.

Inasmuch as you have changed associated tubes such as the 1B3-GT and 6BG6-G, the only other condition which might cause this would be a defective picture tube.

Intermittent raster

On an RCA 721 receiver, operation is normal for the first few minutes; then the raster and picture disappear. The sound remains during this condition. Variation of the brightness control restores the picture but focus seems to be affected and if the control is advanced to a greater degree the picture disappears. E. S. S., Hammond, Ind.

The last video amplifier of this receiver is directly coupled to the picture-tube grid. This means that both the grid and the cathode are at a positive d.c. voltage but that the grid must be less positive than the cathode so that the proper negative bias will be established. If this relationship has been upset it could cause the condition you describe. You should check the grid and cathode voltages and related component parts to see that there is proper negative bias *between grid* and *cathode* of the picture tube. After warmup, troubles often develop in the tubes, capacitors, etc. The grid should have a *70-volt plus* potential on it, while the B+ feed to the brightness control should be 225 volts. Also check the brightness control for defects and check for an intermittent 100,000-ohm resistor from the brightness control to ground.

Also test the 1B3 and 6BG6 tubes. If voltages, tubes, and parts check normal, the trouble could be a defective picture tube.

Transmission line

I have heard that a 300-ohm transmission line can be taped down along the pipe mast of the antenna for a distance to offset automobile ignition and other interference. Does this procedure minimize noise pickup because of the mast acting as a shield? S. F. P., Boynton Beach, Fla.

Taping the transmission line to the pipe mast is not recommended because the shunt capacitance from the line to the mast would cut down the signal strength. The higher the channel frequency the more noticeable the loss would become because the *shunt* reactance would be reduced.

To reduce noise, give the line a twist every foot or so along its length. This cuts interference pickup from the line by about 30%. Coaxial cable can be used if the signal strength is sufficient to overcome the losses in the coaxial line.

Intermittent channel 2

On an RCA 9TC24T receiver the picture and sound blank out intermittently on channel 2. All other channels function normally. If I turn the selector switch slightly on channel 2 it occasionally restores normal picture and sound though some microphonics are present. I have cleaned the switch contact terminals with carbon tetrachloride but this only restored normal operation for a short time. Can you suggest other procedures? D. P., Red Bank, N. J.

The fact that the cleansing with carbon tetrachloride restored the set to normal operation for a while indicates that you have localized the source of trouble. Carbon tetrachloride will clean the contacts but provides no means of maintaining good electrical connection. Most technicians use one of the several chemical compounds available at wholesalers for this purpose. These contact cleaning fluids leave a slight deposit on the contacts which acts as a combination lubricant and electrical contact element.

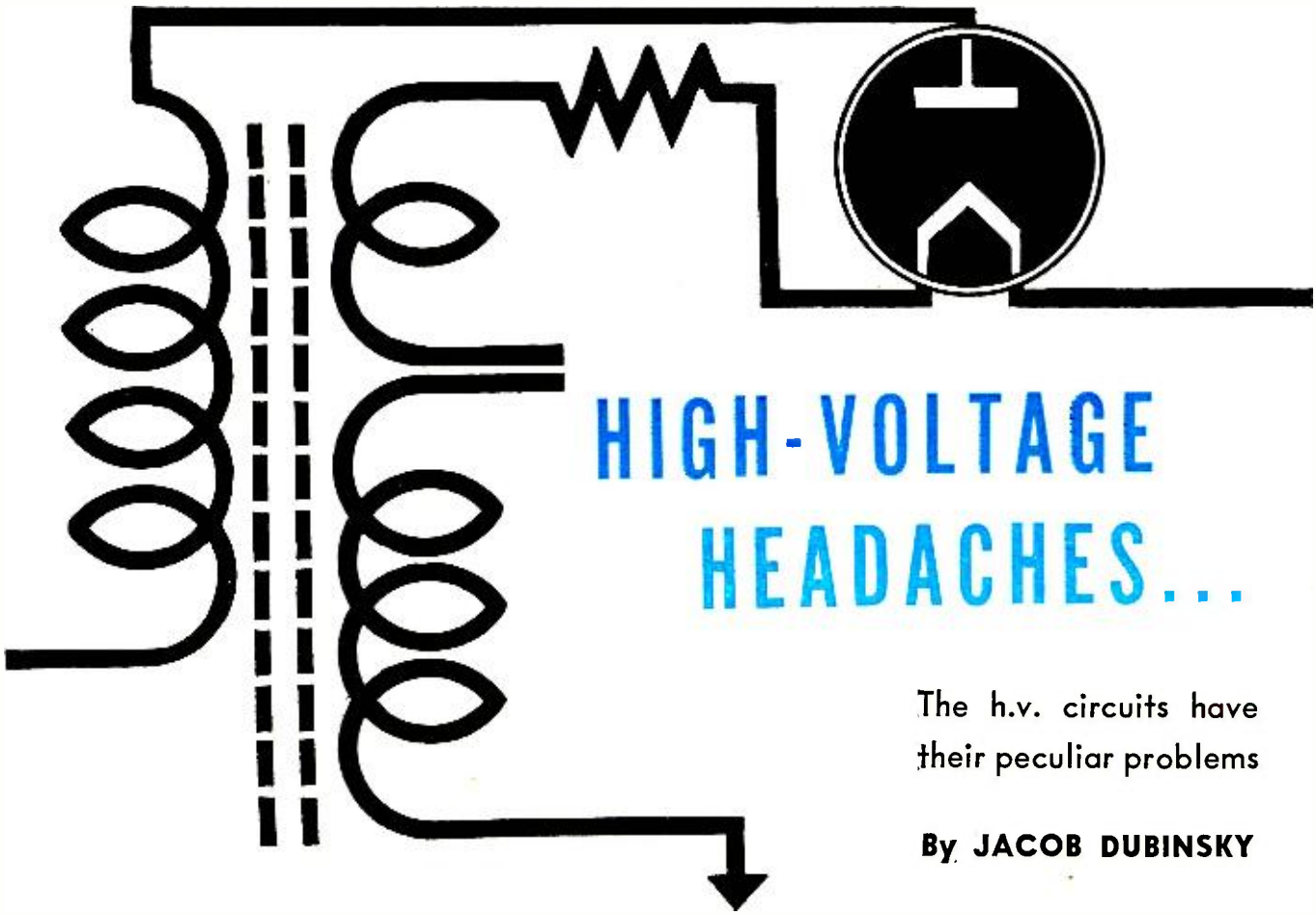
Defects in a.g.c.

In a Westinghouse model H-609T10 receiver there is intermittent picture and sound, though the raster remains during this time. After one-half hour of continuous operation the set functions normally, but only for a short time. I checked voltages and they all indicated proper values. When I place a meter from ground to the a.g.c. circuit, both picture and sound reappear but there is loss of vertical and horizontal sweep. Upon removal of the meter, picture and sound again disappear. Tubes check all right but if the keyed-a.g.c. 6BH6 tube is removed, picture and sound come in normally but with poor horizontal and vertical synchronization. What could cause this trouble? H. W. H., St. Louis, Mo.

The fact that both picture and sound reappear when you apply a meter to the a.g.c. circuit would indicate that the resistance of the test equipment is establishing sufficient continuity in the a.g.c. circuit and partially correcting for defects therein. The lack of sync stability under such a condition indicates insufficient bias and overload of the subsequent circuits. The same condition prevails when you remove the a.g.c. tube. You should try a new 6BH6 a.g.c. tube and also check for defective resistors and capacitors in this circuit. This model uses a section of transmission line for coupling the horizontal pulse to the plate of the a.g.c. tube. The transmission line (Fig. 4) is used as a capacitor. Measure the voltage along the a.g.c. bus. Test to see whether the a.g.c. voltage varies as you tune over the different channels. Check at the grids of the r.f. amplifier and picture i.f. tubes. It would appear that the defect is causing excessive bias and cutting off these tubes, thus obliterating both the picture and sound.

—end—

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HIGH-VOLTAGE HEADACHES...

The h.v. circuits have their peculiar problems

By JACOB DUBINSKY

HAVING read practically every article and book on the subject of television servicing in the field, I have been struck by the fact that few really gave any hints on how to service a set which shows no picture.

The vast majority of troubles of this kind (high-voltage or otherwise) will be found due to defective, weak, or gassy tubes. Obviously the best set made will not operate with bad tubes, and no competent technician will start ripping a set apart before he has assured himself that the tubes are O.K., either by using a tube checker or by replacement of the suspected tube

If tube replacement does not solve the problem, the logical procedure is to check for the presence of high voltage at the picture tube, and then work back through all preceding circuits. Typical troubles and their remedies follow:

Shorted high-voltage capacitors: This is rare but does happen, especially in the long plastic capacitors used in Philco, Stromberg-Carlson, and others. Replace, of course.

Defective or changed-value resistors: Usually output is through a 500,000-ohm to 1-megohm filter resistor. Replace with heavier unit or with lower resistance. The filament winding for the rectifier tube often has a 2- or 3-ohm resistor in series with the 1B3-GT. These often change value. These resistors are also responsible for picture blooming. A common cause of trouble in high-voltage doubler and tripler circuits is the charging resistor running from the filament of one 1B3 to the plate of the other. This resistor, generally 2 megohms, is shown in Fig. 1. An inexpensive and permanent repair is to replace it with three 680,000-ohm, 2-watt resistors in series. Be careful in soldering the resistors together and in making the circuit connections. Make round smooth joints and solder with short leads. Keep the resistors well away from other units and especially from the 6BG6. I have seen them arc over to the 6BG6 and actually burn a hole in the tube.

Here one can be fooled. While servicing a Crosley 12-inch receiver, I did get a heavy spark on the high-voltage lead and still the picture refused to come on. The trouble was a shorted 1X2-A which was feeding a.c. to the picture tube.

Ordinary troubles in the output stage would be:

Blown fuse. The ¼-amp fuse often burns out. Replace with same size fuse. Most service technicians use a clip-on holder and place the new fuse in the holder. I prefer soldering a single fuse holder to the terminals of the blown fuse and replacing the fuse. This makes a permanent job and does not take up the space of the other method.

Cathode resistor of the horizontal output tube often changes value or burns out. This unit should be at least 2 watts. I often use two 2-watt resistors in parallel to make a good heavy-duty 4-watt resistor.

Defective flyback or r.f. coil. An internal short sometimes can be seen by turning off the lights. A tiny pinpoint of white light will give it away.

Shorted or arcing lead. These can be cured by painting with high-voltage dope or by placing additional insulation between the leads.

And now we come to the damper circuit. In most sets, the damper tube actually supplies the primary of the flyback transformer with its plate voltage. Obviously, if the tube is weak or defective the high voltage will be out. An open or grounded linearity coil will also stop the high voltage. I have seen dozens of linearity, width, and ringing coils shorted to the slug. The result is a dead B-plus short with red-hot 5U4's or blown fuses.

Common sources of trouble are the two capacitors across the linearity coil.

If we have tested all these units and replaced them if necessary, we should now have our high voltage. But here again we may still find no picture.

I spent a good many hours on a Capehart 17-inch job in the customer's home, and although everything tested fine, there was no high voltage. Finally I

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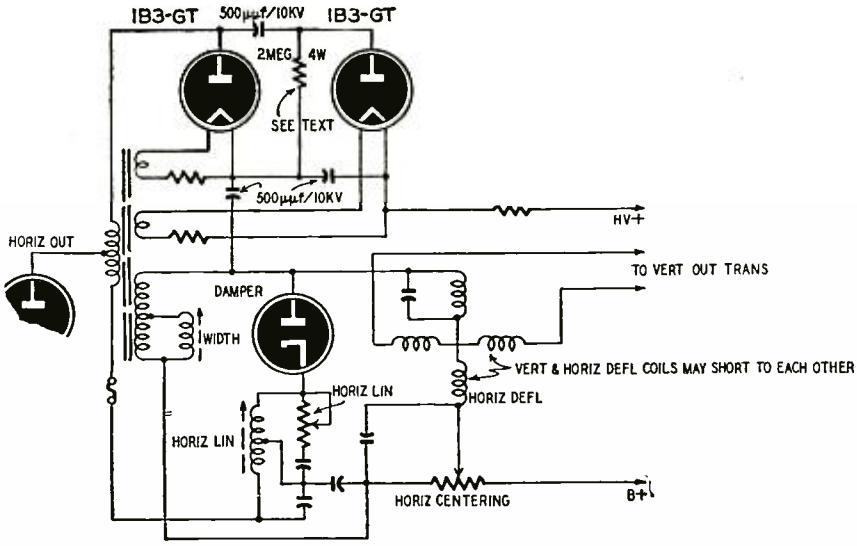
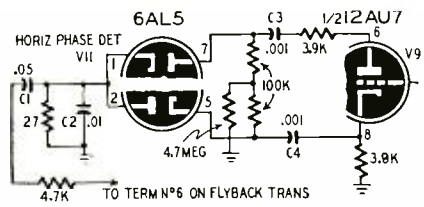
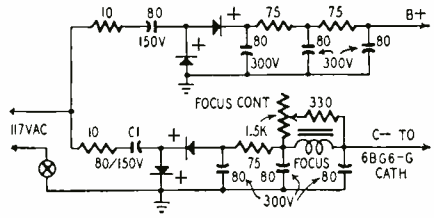


Fig. 1
The resistor marked "See Text" is responsible for many breakdowns.

Fig. 2, top—How "unrelated" circuits can cause trouble. Fig. 3, below—An intermittent with an uncommon cause.





removed the chassis to the shop, leaving the picture tube and deflection coils in the cabinet.

The set was tested and the high voltage was fine. The set was gone over with a fine-tooth comb. No intermittent units could be found. Returned the set and connected it up. Again no high voltage. The trouble was caused by a short in the deflection yoke between the horizontal and vertical coils.

Oscilloscope methods

Tracking down lack of high-voltage sweep in the earlier stages with an oscilloscope is a simple matter. If the sawtooth generator is operating improperly, or not at all, the trouble may be in the Synchrolok coil, the horizontal blocking-oscillator coil, the ringing coil, or any of the various methods used to get the initial sawtooth charge. Of course open or shorted capacitors or changed-value resistors anywhere in those circuits should not be too difficult to track down.

If the oscillator is working, the next step is to check the signal through the coupling capacitors, grid resistors, and input circuits right up to the output tube.

In a Muntz set, lack of horizontal oscillation was traced to a breakdown of the mica in the horizontal drive padding capacitor. The wise technician will always check those horizontal drive capacitors and circuits as well as horizontal drive variable resistors.

An instance where an apparently unrelated circuit can cause loss of high voltage was found in an Artone. This set is made by Tele King and there are thousands of them about. They are also called the A. & S. Lyrtone. The phase-detector circuit in this set is shown in Fig. 2.

Capacitors C2, C3, and C4 break down often. These immediately kill the high voltage. A breakdown of C1 will burn out the 27,000-ohm resistor, too. Another cause of intermittent high voltage is a 120-μμf capacitor across terminals 4 and 5 of the high-voltage (flyback) transformer.

Servicing high-voltage intermittents can be quite a headache. The real rogue in this picture is the 1B3 or the 1X2-A. The tubes become intermittent and if in doubt, replace same. Don't fool around—replace both high-voltage rectifiers and the horizontal output tube.

Another source of intermittent picture loss is a loose connection at the base of the picture tube. If the tube fails to light, check the socket connections and the tube base. Quite often you can effect permanent cures by resoldering the pins. Lay the set face down on the floor. Use a cushion or a couple of books to protect the cabinet or knobs. Now you can resolder the tube base pins and the solder will run down and make a very good contact.

One of the writer's unusual experiences was with a 12-inch Emerson model 571. The complaint was intermittent high voltage. On the first call, the 6BG6 and the 1B3 were replaced and the high voltage came on fine. All sorts of checks were made and the set worked fine. Two days later came the same complaint.

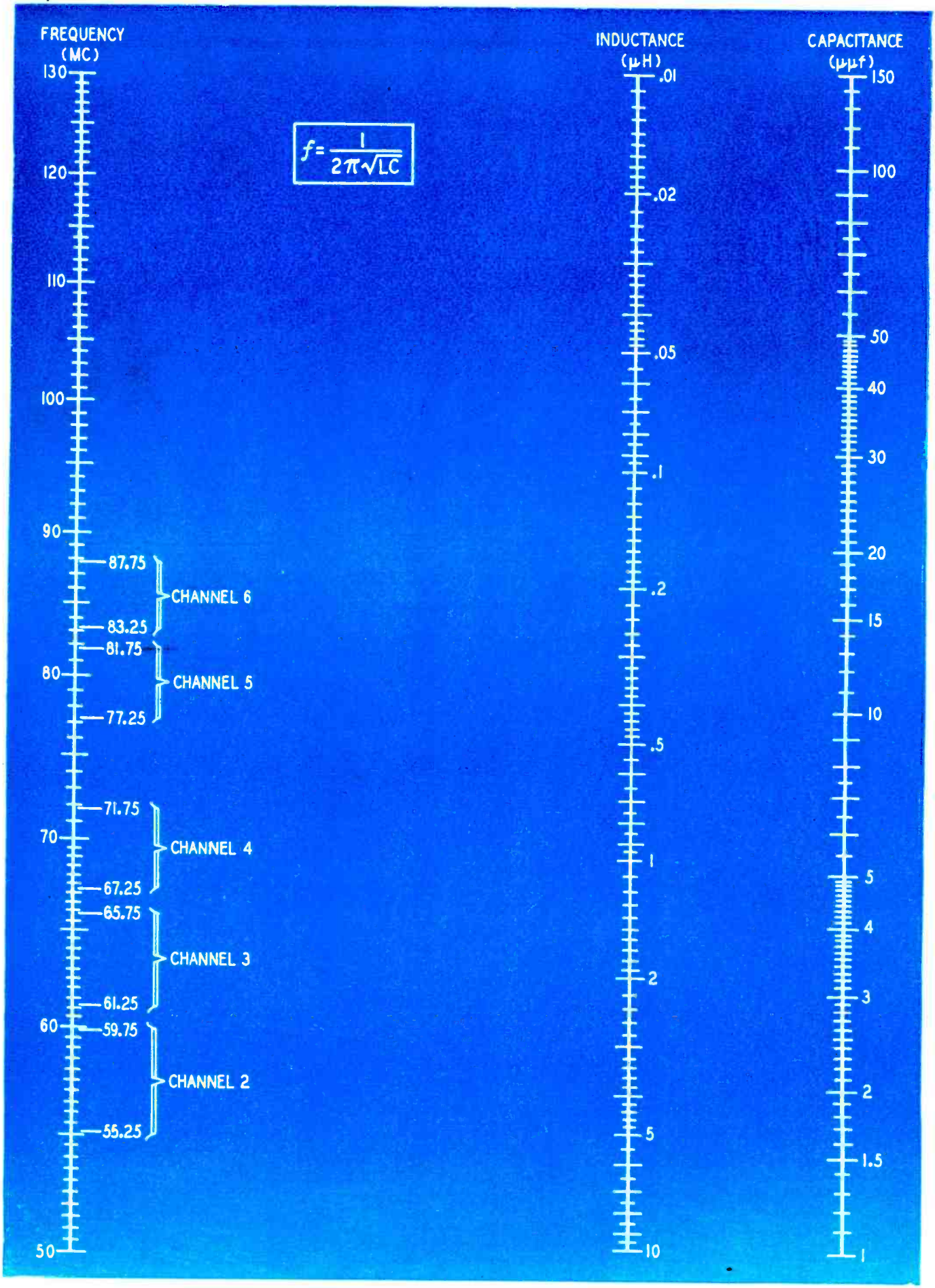
The set was removed from the cabinet and voltages were checked against the Emerson Service Manual. The 6BG6 tube voltages were incorrect.

The i.f. and audio circuits all showed proper voltages. The trouble was traced to an open 80-μf, 150-volt electrolytic capacitor (C1 in Fig. 3). This open capacitor cut off the power supply to the sweep circuits without affecting the video and audio circuits.

Narrow pictures that cannot be widened may be caused by shorted turns in the flyback transformer or in the deflection yoke. If in doubt try a good yoke or transformer. On a recent job on a 12-inch Sylvania set with r.f. high-voltage supply the picture could not be widened. I found both the deflection yoke and horizontal output transformer defective. Rather than go to the expense of replacing both these units, I changed the entire high-voltage system to a standard flyback type. The picture worked out fine.

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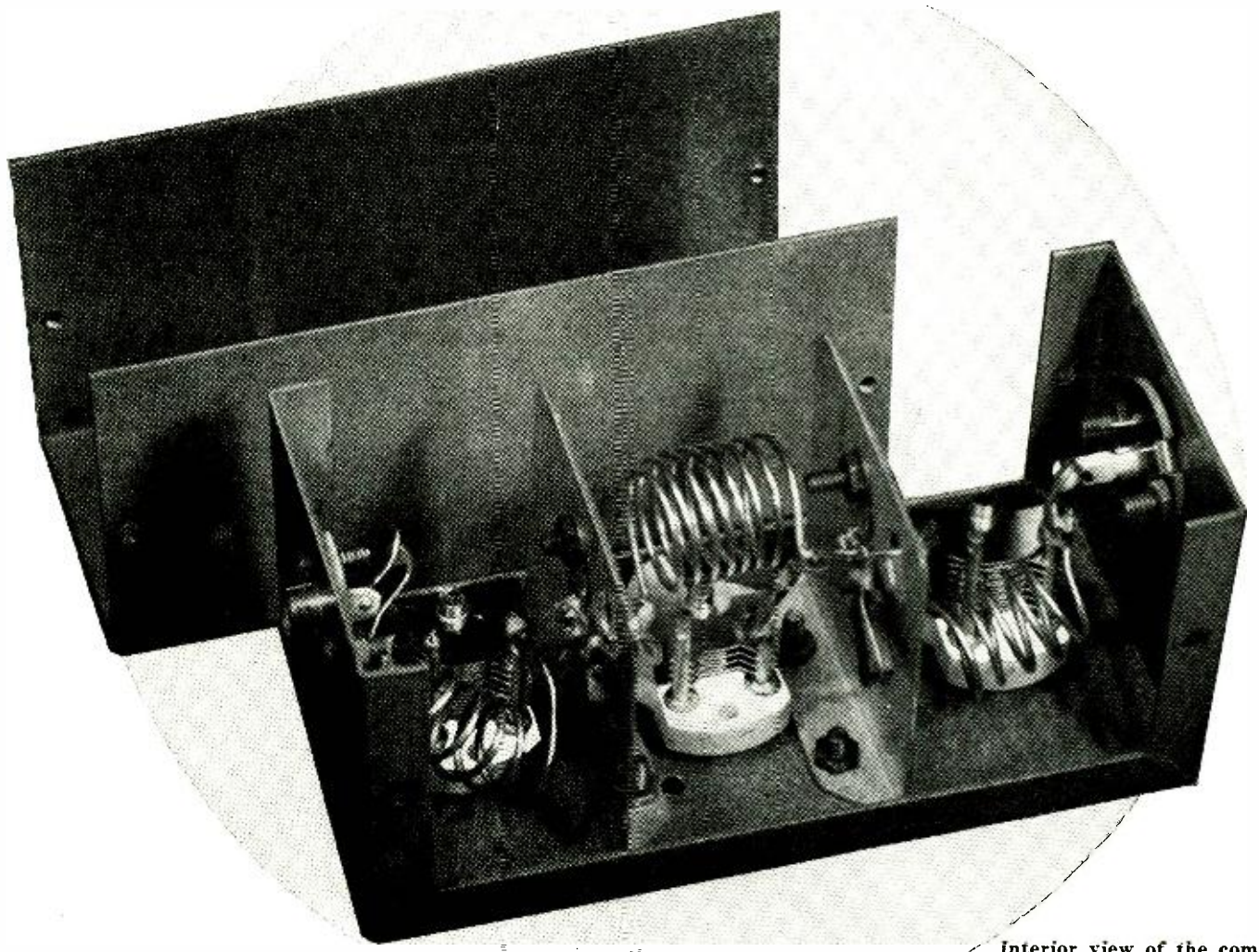


Nomograph for computing TVI filters

Courtesy Radio Corporation of America

RADIO-ELECTRONICS

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Interior view of the complete TVI harmonic filter.

PRACTICAL TVI FILTER

The XYL's TV set can help you design low-pass filters for your transmitter

By JIM OWENS, W2FTW*

NINE-TENTHS of all the TV interference attributed to amateur operation is the fault of the television receiver itself. Deficient rejection permits signals to ride through on the set's intermediate frequency. In all such cases the FCC will back up the amateur. If he is so operating that a well-engineered TV set within 100 feet of the transmitter produces a perfect picture on all channels, the owner of the set is advised to install filters to prevent signals on his intermediate frequency from getting through the front end. (See "TV I.F. Interference," RADIO-ELECTRONICS, February, 1952.)

In some cases the amateur is actually radiating harmonics which fall in the television band. In this event, the only remedy is to annihilate the harmonic. A low-pass filter in the feeder is indicated.

The construction of a TVI low-pass filter for your transmitter is simple. All you need to do is to follow the instructions and then line it up with a Q-meter or accurate grid-dip meter. If you don't have either of these expensive pieces of test equipment (each of which costs more than a manufactured TVI low-pass filter) maybe you can borrow one. If you can't borrow one, you are right back where you started, unless you can find some other way to do the job.

*Manager, Test Equipment Renewal Sales Section, Tube Department, Radio Corporation of America, Harrison, N. J.

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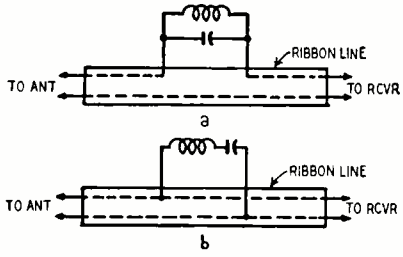


Fig. 1—Circuits for adjusting filter with TV receiver.

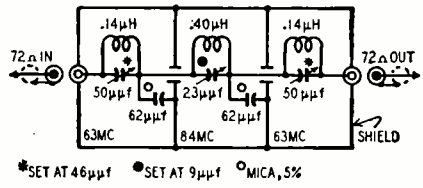


Fig. 2—Schematic diagram of the TVI filter unit.

Now we come to the substance of this article. There is another way—or let us say other equipment—that can be used for the alignment procedure. You simply make use of the XYL's television set.

Tuning to frequency

To start with an example, suppose your calculations call for a resonant circuit composed of an inductor and capacitor, both of nonstandard values (like 0.14 μh or 9 μμf). The capacitor presents no serious problem. You will probably use a variable air capacitor, and will be able to set it close enough to the specified value by estimating the percentage of plate mesh as a percentage of total capacitance. The inductor may present much greater difficulty. Winding a coil to a fairly close approximation of the specified value of inductance in microhenries is not easy. Even if you could get the coil to within say 20% of its proper value, the *combined* error of both capacitor and inductor could add up to a large figure so that the circuit would be completely ineffective as a TVI low-pass filter.

Fortunately, there is a very simple way to get this filter tuned to the *exact* frequency. If it happens to be a parallel network, all you have to do is insert it in one side of the transmission line to the TV receiver as in Fig. 1-a. If it's a series resonant circuit, you connect it directly across the TV set antenna transmission line. See Fig. 1-b.

The next step is to set the receiver to the r.f. channel in which the filter is supposed to be resonant. Then you adjust the capacitor to the point where the TV signal is attenuated and the picture rolls or tears. At this point, you will note that the capacitor seems to be meshed too much or too little to provide the specified value of capacitance, so you prune the coil or wind a larger one, then repeat the tuning process. Fine adjustment of the coil inductance can be made by spreading or squeezing the turns of wire.

Incidentally, you can adjust the circuit to resonate at either the picture-carrier frequency or the sound-carrier frequency. When you tune it to the picture carrier, you can pull the picture out completely; when you tune it to the sound carrier, you can drop the sound level below the noise level.

Using this same procedure, you build and adjust all of the resonant circuits called for in the filter design. Then you mount them on a metal chassis, with shielding plates between each section. If possible, you shield the entire filter so that no radiation can take place. Of course, the mounting and shielding steps have disturbed the tuning of the individual resonant circuits, and some readjustment will be required for best performance. The filter is a shunt-derived low-pass type designed by A. M. Seybold, W2RYI. It is designed for a 72-ohm line and provides peak attenuation of harmonics interfering with channels 3 and 6. Its circuit is shown in Fig. 2.

The unit is constructed in a 5 x 2¼ x 2¼-inch Bud Minibox with partition shields added. Refer to the photograph and note carefully the placement of all parts, particularly the two 62-μμf mica capacitors. Input and output connections are made through phono jacks and plugs.

Connect filter to set

The next and final step of the tuning procedure is to connect the *complete filter* in series with the transmission line to the TV set. If your filter was designed for use in series with a coaxial transmission line, and the TV set happens to be fed with balanced twin-lead, don't let it worry you. Cut the line and connect one of the wires to the ground side of the filter and the other one to the top or hot side of the filter, on both the input and output ends. Now you can tune the receiver to one channel after another and progressively touch up each section of the filter.

The only precaution to be observed in the tuning processes is to eliminate the effects of body capacitance and resistance. Don't touch the filter or filter sections! Mount them on a piece of dry wood a few inches long to hold in one hand, and use a nonmetallic screwdriver to adjust the variable air capacitors with the other hand.

Adjusting inductors

In some filter designs, inductances which are not part of tuned circuits are specified. These inductors can be built and adjusted to their precise values by adding one additional step to the procedure. By using the nomograph, you can determine the value of capacitance in parallel required to resonate the specified inductance at one of the TV channel frequencies. After the tuning procedure has been completed, the inductor can be disconnected from the test capacitor and then soldered permanently into the circuit. Of course, you have to take care to avoid changing the shape of the inductor during the transfer.

This system of adjusting tuned circuits can be used for other purposes. For example, suppose you want to get additional attenuation of a powerful harmonic that falls right in one of the television channels. You decide to accomplish the objective by "sucking out" the harmonic with a parallel-tuned trap placed near the final amplifier tank coil, or connected in series with the plate lead to the final amplifier tube in the transmitter. This trap can be adjusted as described, by placing it in series with one side of the transmission line to the TV receiver, and tuning it to the sound or picture carrier or to a mid-point between the two, as desired.

Design data on low- and high-pass filters can be found in most radio engineering texts but if you are looking for practical stuff, you will find lots of it in Mack Seybold's articles in the August, 1947, and December, 1949, issues of *QST* and in an article by another author in the November-December, 1949 issue of *G-E Ham Tips*.

The elimination of TVI at the transmitter is not confined solely to the use of low-pass filters. The rig must be free from high-intensity harmonics and subharmonics of the output frequency. Adequate shielding and traps must be used to insure against direct radiation through space and radiation from the power lines.

(In some instances, there may be severe sound interference on all channels without any interference showing up in the picture. This type of BCI—well known to amateurs—is caused by rectifying the fundamental in the grid circuit of the first a.f. stage. The cure is to bypass the grid of this stage to ground with a small mica capacitor.—*Editor*)

A large number of other articles on television interference elimination have appeared in various technical publications. One book, *Television Interference*, contains reprints of 21 such articles and a bibliography of about 85 other articles and items on the subject. (25¢, Remington Rand Inc., 315 Fourth Ave., New York 10, N. Y., attention Miss Ann Smith.)—*Editor*

—end—

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Small service benches make for big business

A BUSINESS BASED ON AUTO RADIO SERVICE

By ERIC LESLIE

OPERATED by a man-and-wife team, Lucien and Marie Merle, the Merle Radio Company of Plainfield, N. J., has followed a number of original lines ever since it started in 1934. The fruition of one of these is the subject of our cover this month. *No bench in Merle Radio has room for more than one man.* Although one of the service benches (used for television) is more than 20 feet long, it is still strictly a one-man working space. The bench shown on the cover is one of two used for auto radio servicing, and there are one each for home broadcast radios and for audio-record changer work.

Another original feature of the organization is that from its beginning it has been oriented primarily toward auto radio servicing. This was one of the factors leading toward the present bench system. In a period where auto radio service was almost universally performed in the mud behind the radio shop, Merle realized very early that "the place where the man works is important." Room was made for several cars *inside* the shop, and Merle had one of the first "drive-in" auto radio service shops in the country.

Once alerted to the value of excellent working surroundings, Merle began to see the disadvantages of the communal bench. Workers encroached on each other's territory. Technical—and other—discussions consumed valuable time. An inconsiderate technician could put the whole bench on edge. The shop still remembers when one man was laid off with a broken finger, due to "borrowing" one tool too many from a bench neighbor who was holding a wrench at the moment.

Nothing of that kind can happen now. With his own tools at hand, and with the "home feeling" of his private bench, each man can turn out more and better work. Specialization of instruments becomes possible, and while there is some necessary duplication, cost of extra instruments is more than offset by time saved, because no one has to wait for a piece of equipment.

When the company started business in 1934, practically all its business was installing and servicing radios for motor car dealers. In those days an installation was a two-man job and required from six to eight hours work. To assure a clean and workmanlike job, work was carefully divided between the installation men. One, the "greasy" partner, did all the under-the-hood work; the "clean" man stayed strictly inside the car. Such neatness and strict attention to good workmanship soon built prestige in a period which saw more than a little "brute-force" auto radio installation.

In those days, the auto radio could be sold to the dealer in whose car it was installed, and profits were made on sales as well as service. In 1935, Philco began making a radio for Ford, and Merle Radio was appointed a Philco factory installation and service station, with four men working on Philco-Ford jobs alone. Sales to car dealers were reduced increasingly through '36 and '37 as more auto manufacturers brought out their "own" radios, but rose again when Motorola brought out an auto radio for sale to radio dealers, independent auto sales or service organizations, or direct to motor car owners.

The war brought a drastic reduction in consumer auto (and other) radio production, together with a severe curtailment of auto travel. With Merle teaching radio for the Army at Rutgers University, Mrs. Merle ran the shop with a staff of two, and sometimes three elderly men. Merle Radio started to service home broadcast receivers for the first time. It was during this period that Mrs. Merle learned to service radios. This she no longer does, but she finds that her knowledge of components and their peculiarities and tolerances gained then is very useful to her as buyer for the shop.

The postwar auto radio boom necessitated keeping a staff of five to six men on installations alone. This happy period lasted until 1948, when the car manufacturers introduced their present system, which tends to keep car radio business—both sales and service—in the hands of the factory or its regular dealers. This, Merle believes, was a great mistake, since it tended to disorganize the force of highly skilled auto radio service technicians who had come up with the industry. Few of them found work with the car dealers and auto repair shops—most shifted to other phases of radio work, in which they often earned far less than in their own specialty.

Television was an early interest of the company, and even before the war Merle Radio had a number of installations in taverns and other public places. At present one man is occupied with television service exclusively. Installations are farmed out to an independent organization, another original, but by no means exclusive, idea of the organization.

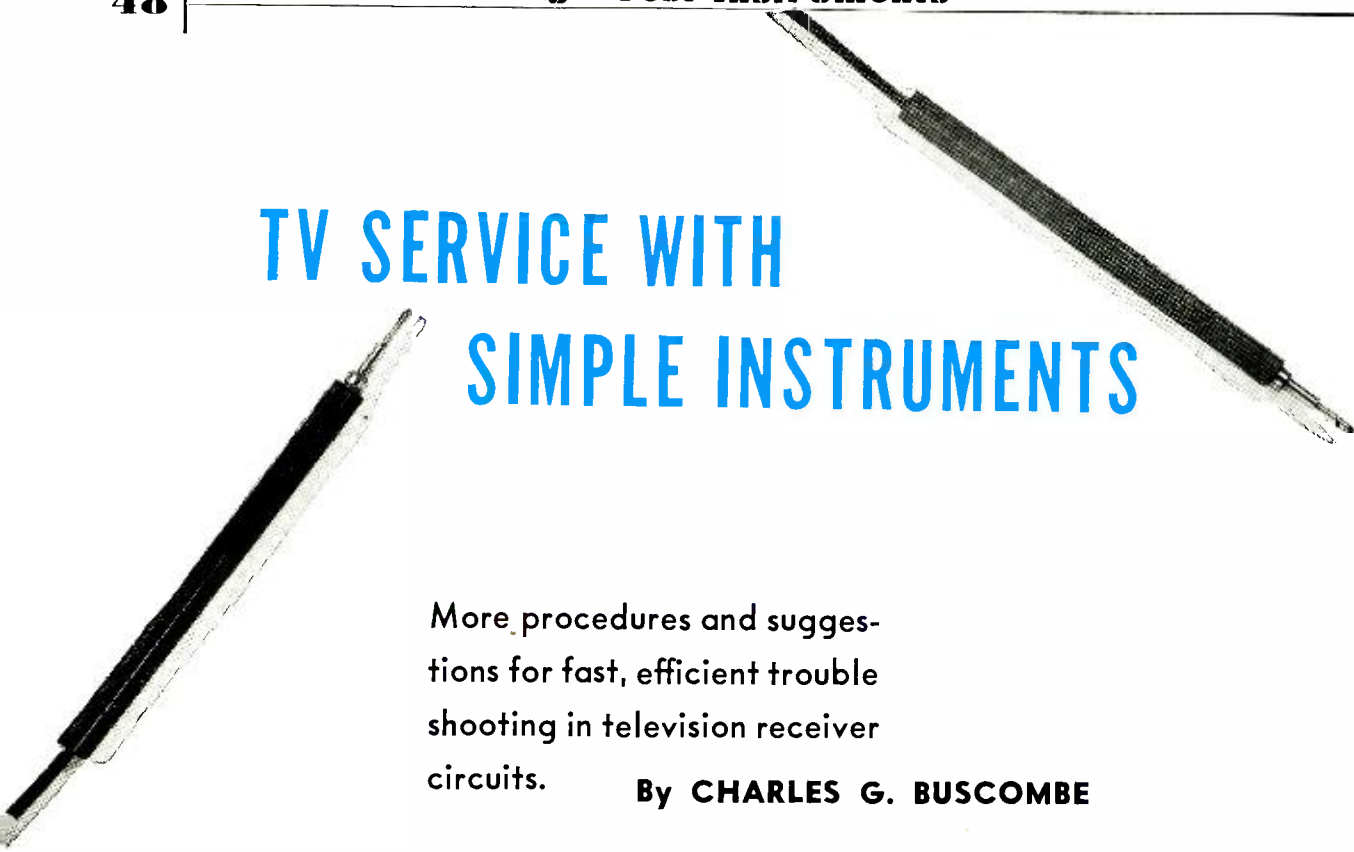
Success has followed the application of original technical systems and sound business methods. The company is now an authorized service branch and parts distributor for Philco, Motorola, Colonial, and Bendix. It is also the exclusive factory service agency for the Lincoln-Mercury works in nearby Metuchen, repairing all radios found defective in new cars or damaged in installation. The present staff consists of seven, plus the two owners.

The shop occupies a 35 x 90-foot space on Plainfield's Seventh Street, a main auto road, and less than a block from one of the city's main business streets. A little less than half the space is a salesroom devoted largely to television. The rear is the drive-in auto service shop. Television receivers, home radios, and audio equipment, all have their own separate benches in the basement.

Merle has just purchased the local FM station, WXNJ, and has an application for an AM station pending before the FCC. In thus uniting both ends of the chain of broadcast services the organization is certainly original—if not unique.

—end—

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TV SERVICE WITH SIMPLE INSTRUMENTS

More procedures and suggestions for fast, efficient trouble shooting in television receiver circuits.

By CHARLES G. BUSCOMBE

THE first installment of this story in last month's RADIO-ELECTRONICS described TV troubles that could be found with the TV Service Aid (RADIO-ELECTRONICS, March, 1952, page 28) or with other simple test equipment. Troubles in the high- and low-voltage supplies and picture-tube circuits were covered. This month we will try to find troubles in the other parts of the TV receiver, beginning with the sweep circuits and working back through the i.f.'s to the front end.

Vertical sweep section. If unable to lock (even momentarily) with hold control, oscillator trouble is indicated. Substitute tube; check socket voltages to localize defective component; look for leaky coupling capacitors and changed resistor values. Where there is complete or partial loss of vertical deflection, determine whether oscillator or amplifier is at fault. One method is to feed 6 volts from heater circuit through a .25-μf capacitor to amplifier grid. If height increases, amplifier is probably O.K. Presence of sawtooth at amplifier grid can also be determined by an a.c. voltage check or by coupling this point through a blocking capacitor to video or audio amplifier, using picture tube or speaker as an indicator.

If oscillator is at fault, check its components as mentioned above, not neglecting integrator network and coupling capacitor from sync circuits. Where manual control is possible for short intervals, and oscillator tube is O.K., it can be assumed that sync pulses have been lost or attenuated in preceding stages (sync amplifiers, separators, limiters, integrator or even in video stages). Where vertical amplifier is at fault and there is sufficient sawtooth drive on its grid, try tube substitution. Next check for sawtooth at amplifier plate, and if none, measure socket voltages and look especially for open cathode circuit, shorted cathode bypass, or open output transformer primary. If sawtooth is O.K. at plate, test for break in transformer secondary or vertical deflection yoke. Shorted yoke turns will produce a keystone raster. In electrostatic sets, most tests are essentially the same except for R-C coupling to the picture tube.

In general, where symptoms are loss of height with sync instability (rolling), the oscillator and integrator circuits may be suspected. Where problem involves height and linearity, the amplifier or its output coupling is probably responsible.

Horizontal sweep section. If unable to lock the horizontal oscillator with hold control or other frequency adjustments, try tube substitution followed by the same socket voltage measurements and component tests mentioned for vertical oscillator troubles. If picture can be locked in but will not hold, or evinces pulling, bending, horizontal shift, jitter or tearing, trouble may lie in a.f.c. circuit or sync stages.

Drive is normally adjusted for maximum raster width and brilliance without vertical overdrive bars on screen. If width is excessive, use width control. If linearity is impaired, correct with linearity control or slight readjustment of drive. If drive adjustment causes loss of sync, correct with hold control.

If r.f. type h.v. supply is used and there is no horizontal deflection, trouble is in horizontal sweep circuit. For same symptom with flyback supply, transformer output winding, damper circuit or horizontal yoke can be considered responsible.

In electrostatic sets, test horizontal output tube, output coupling capacitors, and load resistors.

Video amplifier and pix detector

Symptoms: Raster O.K., no picture; poor contrast; distorted pictures (smearing or phase reversals). Sound may or may not be impaired, depending on whether set is intercarrier or dual channel. Sync may or may not be unstable.

Start by substituting tubes, then if necessary apply signal tracing, using one or more of following methods:

(1) Inject audio to picture tube input (grid or cathode); attentuate signal and adjust brilliance and contrast controls until developed sound bars appear light gray. Feed signal to preceding points, noting increases or decreases in bar contrast. Continue as far as detector load resistor. Where there is no improvement in contrast between plate and grid of any tube, that stage can be considered at fault.

(2) Follow up by checking socket voltages, continuity of peaking coils, load resistor values, and low-frequency compensating components. Where raster brilliance is consistently too high or too low, and brightness control has negligible effect, look for defective coupling capacitor from video output to picture tube.

(3) With antenna connected and station tuned in, adjust tuner for maximum contrast. With signal tracer follow signal from detector load resistor through amplifier to picture-tube input, noting relative changes in level. Audible indication of this signal is of course the raspy tone commonly referred to as sync buzz.

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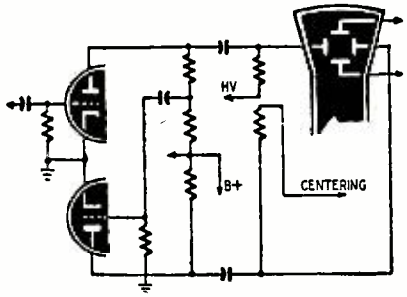
The signal injection method of tracing can make use of an a.f. generator, neon relaxation oscillators, or sawtooth voltage taken from the vertical sweep oscillator through a blocking capacitor.

Sync circuits

Symptoms: Partial or complete loss of sync as evidenced by rolling, jitter, pulling, or tearing.

Assuming oscillators are running at correct frequencies and are capable of being triggered, determine if pulses are reaching point of sync takeoff by observation of sync and blanking bars on picture tube. This is done by adjusting hold or centering controls. By manipulating brilliance and contrast controls, sync bar should normally appear very dark against the gray background of the blanking bar. If not, a previous stage is responsible for attenuation of sync voltage.

Try substitution of all sync-amplifier and separator tubes, including the a.f.c. control tube. Trace pulses from takeoff point up to inputs of vertical or horizontal oscillators. (Some attenuation normally results between input and output of clipper tubes.)



Electrostatic deflection output stage.

If pulses can be traced up to integrator, follow through integrator or a.f.c. (depending on whether vertical or horizontal sync is at fault). Substitution of the integrator is readily accomplished with one of the printed-circuit types. If necessary, check socket voltages of a.f.c. tube, followed by associated component testing. Particularly investigate feedback loop, then make various adjustments required.

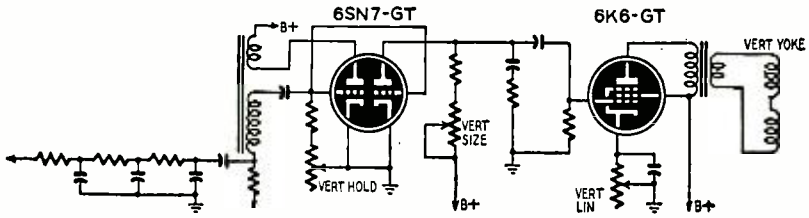
Where hum bar appears on raster or in sound, trouble is often due to cathode-heater leakage in a video or sync tube or poor filtering in the low-voltage supply. These are very common causes of sync instability.

(A set should never be considered to have good sync unless the picture locks in abruptly with the vertical hold control and shows no signs of vertical jitter or rolling when changing channels. Indications of horizontal stability are where hold control is not particularly critical and pix does not tear when channels are switched.

Picture i.f. amplifier

Possible symptoms (depending whether set is intercarrier or dual-channel): No pix, no sound; sound but no pix; poor pix contrast or resolution; pix smear with sync instability.

(The video amplifier can also be responsible for these symptoms, so it is up to the technician to decide which stage to investigate first.) In intercarrier models try tube substitution in all stages. In dual-channel receivers if sound is O.K. be concerned only with those tubes following sound takeoff. The picture i.f. is prone to few troubles other than tube failure or misalignment. Occasionally, however, a



Typical vertical sweep circuit used in electromagnetic television receivers.

shorted screen bypass capacitor or a defective decoupling resistor may be responsible. The troublesome stage can be localized by signal tracing with one of following methods: (1) With antenna attached and set tuned to an operating channel, use crystal probe to follow signal from mixer output through various stages, toward detector. Trouble will be found in stage following point where signal was last recorded. (2) Inject a suitable signal into check points in the i.f. amplifier, working back from detector toward front end. An AM or sweep generator may be used for this purpose, or, lacking these, use a noise signal from the vertical sweep amplifier or damper plate with a suitable isolating resistor and capacitor in series with the lead.

Sound i.f. det.—audio

Symptoms (raster and picture O.K.): Sound may be completely lost, weak, or distorted.

If audio amplifier or speaker is suspected, touch hot end of volume control for the usual hum or growl. If not heard, try tube or speaker substitution. Next use signal tracing, employing neon oscillator or noise signal taken from vertical oscillator or damper. Another method is to feed signal through a small capacitor from different points in AF amplifier to the hot end of video detector load resistor. Sound bars on picture tube will indicate where signal is present. If a.f. section is O.K., first make certain that front-end oscillator is not mistuned, then proceed to trouble-shoot sound i.f. strip. This can be done with either a generator or noise signal as mentioned above. Signal *crossover* method may be employed by using crystal tracer probe between i.f. test point, and either audio or video amplifier inputs.

Where minor sound misalignment is apparent, a tolerable job of sound i.f. alignment can be done by ear. The procedure is to adjust the fine tuner for the best possible sound, then detune *slightly* in the direction necessary to obtain the best picture. Leaving tuner set on the edge of sound signal, adjust all tuned circuits in sound strip for maximum volume from speaker (not forgetting the sound takeoff trap). Again adjust tuner in direction of best picture, peaking tuned circuits again for loudest sound. Repeat as often as necessary until optimum picture and sound are received at one setting of fine tuner. Next step is to adjust secondary of discriminator transformer for minimum audio distortion and sync buzz. This method cannot be used on intercarrier receivers for the obvious reason that sound is fixed at 4.5 mc and misalignment of this strip will only weaken or distort the sound.

The front end tuner

Symptoms: Raster O.K., no picture, no sound; picture but no sound, or weak distorted sound; poor contrast with excessive snow.

If no sound or picture, particularly on high channels, but considerable interference from FM and auto ignition the oscillator is probably inoperative or badly mistuned. Replace the tube, and adjust oscillator slug or trimmer to bring in sound and picture.

Weak picture and sound and high noise level, may be due to a weak oscillator or defective mixer or r.f. tube. Try substitution. If no improvement, investigate for possible antenna trouble, such as change of orientation, loose or open connections, or a broken transmission line.

These symptoms on only one or two channels may indicate misalignment of r.f.-mixer adjustments. To verify this, try peaking them for improved picture contrast on a troublesome channel. (Final alignment of this section must be done with proper equipment, otherwise picture quality may be impaired.) Picture-sound mistracking cannot always be blamed on the tuner. However, a similar condition may prevail which tuner adjustments will correct. This is where picture is received at one extreme of tuner range and sound is either missing or weak and distorted. The procedure here calls for setting fine tuner at midposition, and adjusting the over-all oscillator slug for best sound and picture on the highest channel. Try all other channels and if necessary adjust their individual oscillator slugs without touching fine tuner. A little extra effort spent on this operation will please the customer, as it saves him the annoyance of having to manipulate the tuner every time a new channel is selected.

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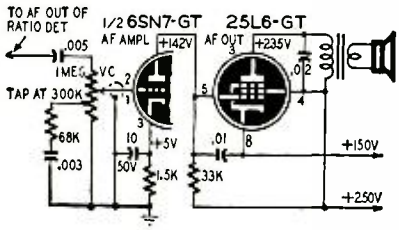


Fig. 1—Motorola direct-coupled audio.

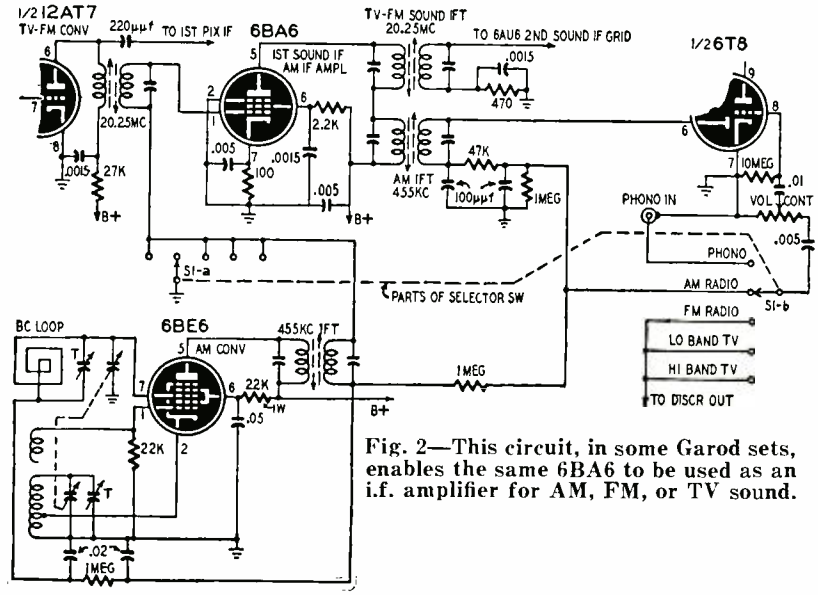


Fig. 2—This circuit, in some Garod sets, enables the same 6BA6 to be used as an i.f. amplifier for AM, FM, or TV sound.

short circuits

By ROBERT F. SCOTT

New features in sound and picture circuits of current TV receivers.

IN THE January, 1952, issue, we discussed some of the new and unusual circuits in this year's crop of TV sets. Last month, we covered some of the less familiar features and circuits of the current FM-AM combinations. This month, we have again concentrated on circuits in TV sets and will try to brief you on what to expect in the way of unusual circuitry in some of them.

Some of the old-timers in the service game remember the nights they spent sweating over some of the Loftin-White direct-coupled amplifiers, trying to get them to work as the designers said that they would. They probably recall the relief they felt as the last of those old-time troublemakers faded away into junk boxes, attics, and basements. Well, boys, I have news for you! The ghost of the direct-coupled audio amplifier has come back to haunt us. But, it looks like the ghost is pretty well tamed now and won't be a bit of trouble. In the January issue, we discussed the direct-coupled circuit in the Bendix long-range chassis. Fig. 1 shows a somewhat similar circuit in the Motorola TS-314 and similar chassis.

The plate and screen grid of the 25L6-GT and the plate of the a.f. amplifier (one-half of a 6SN7-GT) are supplied from a source of 250 volts. The cathode of the 25L6 is returned to plus-150 volts. Under normal conditions, the 6SN7 draws enough current through the 33,000-ohm plate load resistor to bring the plate voltage—and the voltage on the grid of the 25L6—down to 142. Under these conditions, the cathode of the 25L6 is 8 volts positive with respect to the grid, thus providing the required 8 volts of bias.

Garod AM tuner

Whenever AM reception is included in a TV receiver, we usually find at least three extra tubes. In the 10TZ20, 12TZ20, and a few other chassis, Garod has worked out a neat trick which gives AM reception with only one extra tube. See Fig. 2. Existing tubes are used for other AM circuit functions.

The secondary of the first 455-kc AM i.f. transformer is in series with the secondary of the TV-FM converter transformer, so the 6BA6 first sound i.f. amplifier (20.25 mc) also functions as the 455-kc AM i.f. amplifier. The primary of the 455-kc i.f. output transformer is in series with the plate circuit of this stage and develops the signal voltage when a 455-kc signal is fed into the grid. (Since parallel-resonant circuits have maximum impedance at resonance and negligible impedance at frequencies far removed from resonance, the tuned circuit not in use can be ignored.)

The secondary of the second 455-kc i.f. transformer feeds into one of the diodes of the 6T8 TV-FM discriminator and first a.f. amplifier. The output of the diode appears across the 47,000-ohm and 1-megohm resistors in series. The voltage at their junction is tapped off and fed through the volume control to the first a.f. amplifier and through a 1-megohm filter resistor to the a.v.c. line which controls the grids of the 6BE6 converter and the 6BA6 when operating at 455 kc.

When the selector switch is in the PHONO, FM or TV positions, S1-a grounds the control grid of the 6BA6 through the secondary of the TV-FM converter transformer. A separate section of the selector switch (not shown on the diagram) opens the B-plus line to the 6BE6 when receiving TV, FM, or operating the phonograph.

Westinghouse audio circuit

The average service technician takes audio circuits pretty much for granted.

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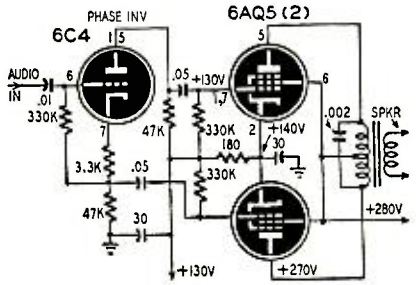


Fig. 3—Westinghouse "floating" audio.

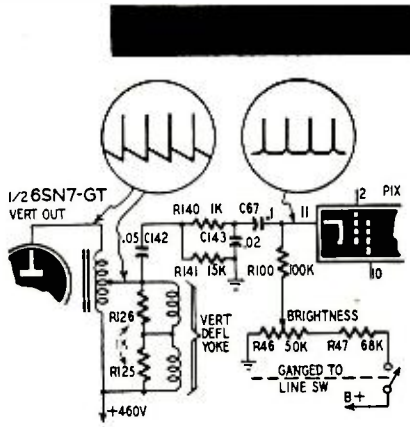


Fig. 4—Raytheon vertical retrace-blanking and h.v. spot-elimination circuits.

For example: In a push-pull cathode-biased stage, we expect the grids to be at ground potential with the cathodes only a few volts above ground (positive). We are so accustomed to the zero- or negative-potential control grid that we almost invariably start replacing coupling capacitors whenever we find a positive voltage there. A study of the audio circuits in some of the latest TV sets shows that the grids of some of the tubes are operated away up in the air, so you had better think first before using the old finger-on-the-grid technique of locating trouble in a dead audio circuit.

In Westinghouse models H-660C17 and H661C17, the push-pull 6AQ5 audio output tubes are used as parallel d.c. dropping resistors to reduce the B-plus voltage from 280 volts to 130 volts (Fig. 3). This lower voltage is for the i.f. and other stages of the receiver. The grid-cathode return point of the output stage is at a positive potential of 130 volts. The cathodes are biased for proper operation by the 10-volt drop developed across the 180-ohm cathode biasing resistor.

Raytheon beam blanking

Raytheon has incorporated into its latest sets two simple innovations which blank out vertical retrace lines and prevent the brilliant spot which normally occurs in the center of the screen shortly after the set is turned off. These two blanking circuits are shown in Fig. 4.

Up to about a year ago, set manufacturers depended on the blanking signals from the TV station to blank out the vertical retrace lines and prevent them from appearing as light diagonal lines on the TV screen. Under ideal conditions, the blanking pulses from the station do the job rather effectively. But, when the signal level is low or when washed-out, weak film is being televised, or when some types of camera effects are used, retrace lines often appear and spoil what would otherwise be an acceptable picture.

To eliminate this, Raytheon and a number of other manufacturers use the pulse or overshoot which occurs at the end of each vertical sawtooth to blank out the beam during the retrace period. The vertical deflection signal (Fig. 4) is tapped off the vertical deflection yoke and the sawtooth component is removed by a differentiator consisting of C142 and R141. The resulting pulse is cleaned up by passing it through an integrator—R140 and C143—and then fed to the cathode of the picture tube.

This pulse is positive and has sufficient amplitude to bias the picture tube to cutoff during the retrace interval thus preventing the retrace lines from appearing on the picture or the raster.

Bright spot

When a TV set is turned off, the cathode of the picture tube continues to emit electrons for a considerable time until it cools. Since the drain on the high-voltage supply is negligible, its filter capacitor holds a charge for a long period of time. It is this charge which draws the undeflected electron stream to the center of the screen and causes the brilliant circle of light.

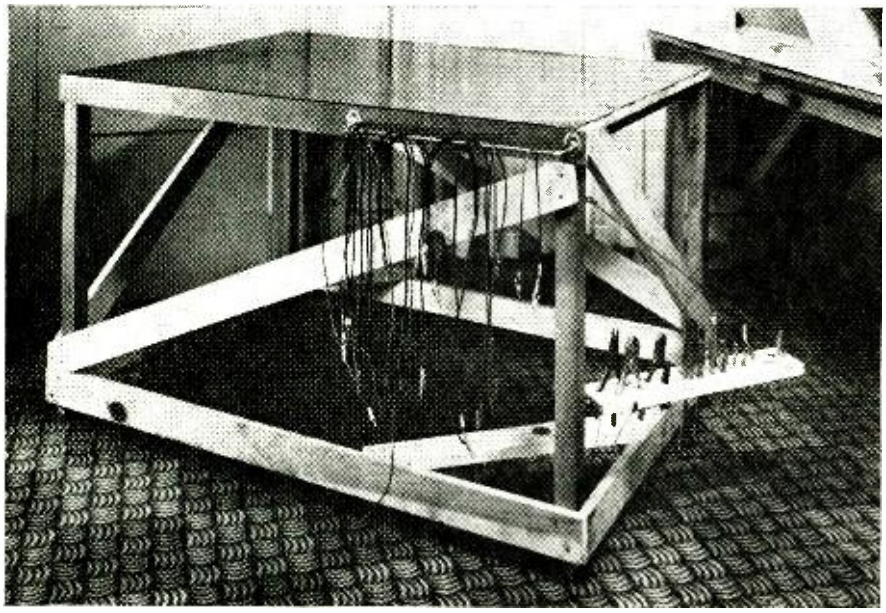
To eliminate this occurrence which sometimes burns the phosphor due to over-excitation, Raytheon has ganged a s.p.s.t. switch to the on-off switch on the volume control and connected it in series with the B-plus lead supplying fixed bias to the picture tube cathode.

When the set is operating, the switch is closed and the major portion of the operating bias is developed by the bleeder current flowing through R47 (Fig. 4) and the brightness control so the cathode current is comparatively low. When the switch is opened, the fixed bias is removed from the cathode. The anode current increases greatly and rapidly drains off the charge on the high-voltage filter capacitor. With this source of attraction removed, the electrons are not drawn to the screen.

This feature also provides a measure of protection for the service technician since it automatically discharges the high-voltage capacitor and the coating on the tube, eliminating a shock hazard.

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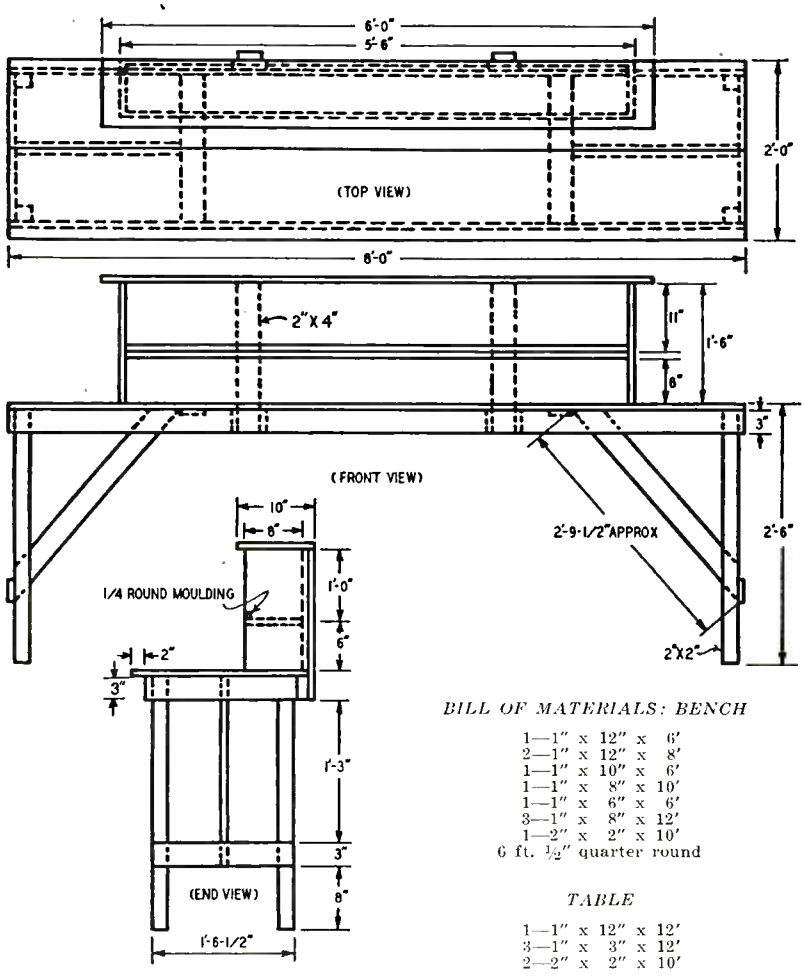


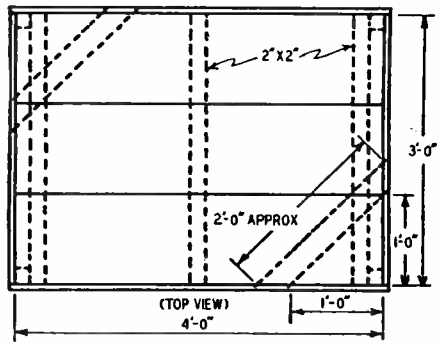
TV SERVICE TABLE

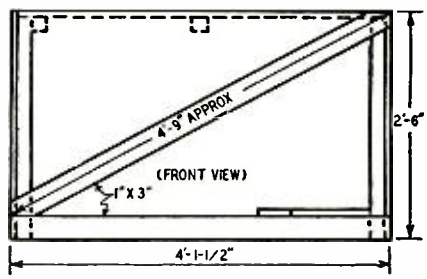
A rolling service table can add flexibility to any shop's workbench arrangements.

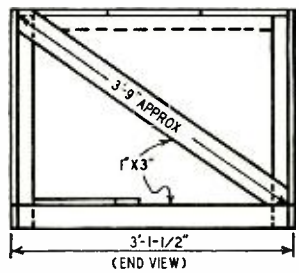
ROLLS UP TO BENCH











BILL OF MATERIALS: BENCH

1—1" x 12" x 6'
2—1" x 12" x 8'
1—1" x 10" x 6'
1—1" x 8" x 10'
1—1" x 6" x 6'
3—1" x 8" x 12'
1—2" x 2" x 10'
6 ft. ½" quarter round

TABLE

1—1" x 12" x 12'
3—1" x 3" x 12'
2—2" x 2" x 10'

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THIS service bench is only two feet deep instead of having the four foot depth found in many other benches. Four feet is an awkward reach when one is seated, and equipment markings are much harder to read at this distance. A two-foot bench will not accommodate a large chassis, but this problem has been solved by the use of the special service table described here.

This table is equipped with casters and can be easily moved to any part of the bench, or rotated when one wants to work on the opposite side of a chassis. Fastened to one of the legs of the table is an easily made swing-away type of tool rack which places tools within easy reach. Also mounted on the table is a towel rack which holds the many test leads used with the equipment.

The bench and table are covered with linoleum. A light pattern gives the bench a cheerful, modern appearance, and small parts are easily located. Small mats cut from excess linoleum are used under chassis to protect the bench and table tops. Waxing the linoleum will improve the appearance and help to protect the surface.

The bench itself is easily wired and is equipped with several surface-type outlets. The master switch is mounted on the bench lip. The advantage of a master switch should be noted. All instruments can be controlled from one point and once you get into the habit of turning this switch off when you leave the bench, you will no longer worry about forgetting to turn off some individual piece of equipment. For safety the wiring is fused for only 10 amperes.

Antenna and ground connections are brought to a barrier-type terminal strip mounted on the front lip of the bench. A television antenna connection is similarly made by means of a special jack.

A 6.3-v filament transformer is mounted under the bench surface which operates a small plug-in trouble light.

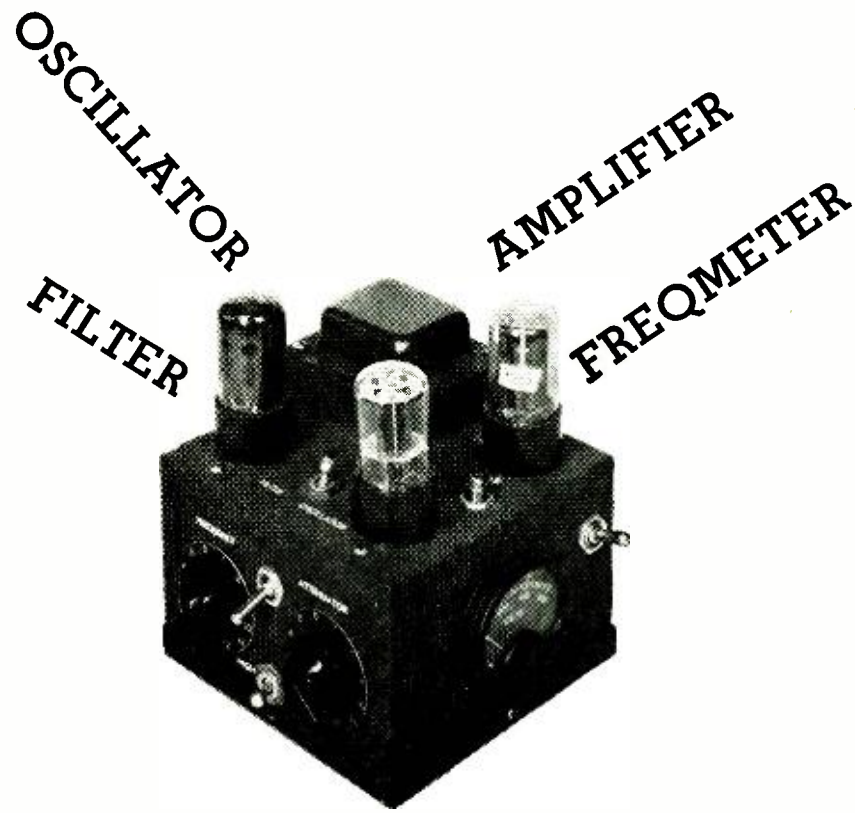
A most important factor in service bench design is the placement of test equipment. Items which are used together should be placed near each other. Decide which are your most-used pieces of equipment and place them at central points. By mounting the tube tester on a sloping rack, you will be able to test tubes easily whether you are standing or seated.

Panel mounting of test equipment was ruled out because this would make it difficult to change instrument arrangement when new units are added, and duplicate equipment would be needed for outside work.

Construction details of the bench and table are given in the accompanying drawings. Dimensions can be easily modified to suit individual space requirements.

Lumber may be any good grade desired. The table and bench shown were made of No. 1 Ponderosa Pine.

—end—



4 instruments in 1 package

More than just a gadget—a combination of highly useful functions for the technician.

By I. QUEEN

THIS multipurpose audio instrument, based on an article by Villard in *Electronics*, July, 1949, operates as an oscillator, rejection filter, or selective amplifier, depending on control settings. Readers may remember a number of versions of this circuit—particularly in the amateur press—shortly after the publication of Villard's original article. The novice whose memory does not extend to 1949, and the amateur and audio experimenter who may not have been interested at the time may find it worth their while to examine the equipment again. This one has been in use at W2OUX three years and has become more valuable each succeeding year. For greater usefulness we have added a novel direct-reading indicator to measure frequency. It operates in the range 175 to 6,000 cycles.

The schematic of this instrument is drawn in Fig. 1. The heart of the circuit is its two-stage phase shifter which includes V1 and V2. The shifter advances phase by 180° at the frequency to which it is tuned.

The phase-shifter principle is shown in Fig. 2. A center-tapped a.f. source is shunted by an R-C network. Resistance is adjustable to equal capacitive reactance at the desired frequency. The vector diagram shows that under this condition the phase of the output (B-D) is advanced 90° compared with the input (A-C). Furthermore, the output amplitude remains constant at half the input at any frequency. This is an important requirement.

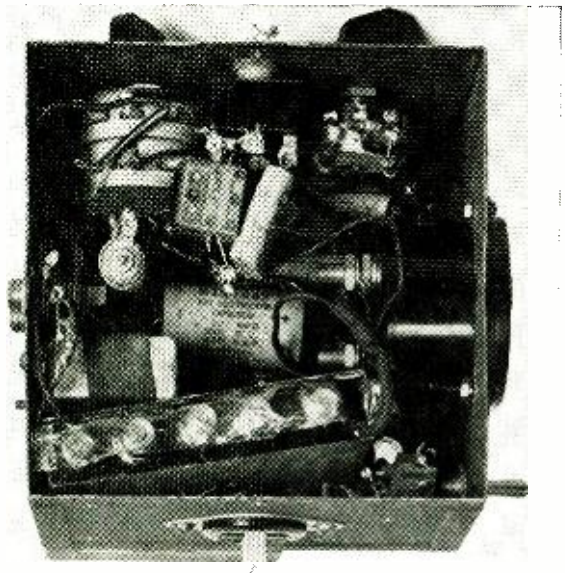
Referring back to Fig. 1, note that V1 and V2 have balanced plate and cathode loads. Each triode provides the "center-tapped" a.f. signal required. An identical R-C network is connected across the output of each tube. These triodes and their respective networks comprise the phase shifter. The resistance of each network can be varied to equal the X_c of the capacitor at the desired frequency.

The OSCILLATOR-FILTER switch, S3, combines signals in or out of phase as desired, converting the unit from an oscillator to a rejection circuit.

As an oscillator

Fig. 3-a shows the basic oscillator

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Inside the chassis of the multi-purpose instrument. This degree of compactness is convenient but layout is not critical.

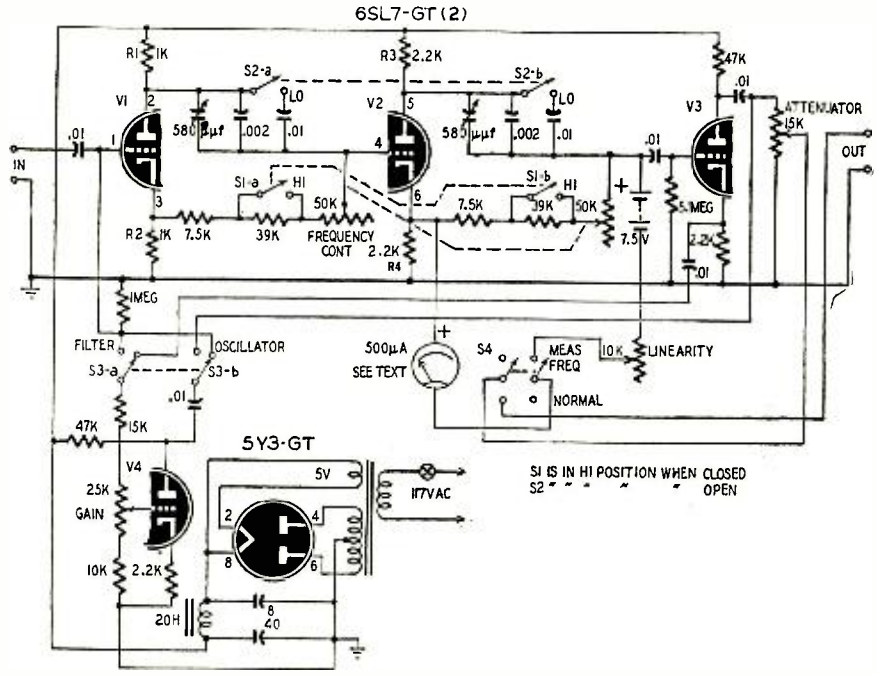


Fig. 1—Schematic of the unit. Certain critical values are discussed in the text.

circuit. The phase shifter feeds an amplifier (V4) which again reverses phase. Therefore the amplifier output is in phase with the shifter input and oscillations can be produced. An isolating stage follows the oscillator.

As an amplifier

Frequency is determined by the shifter adjustment. If the amplifier gain is reduced sufficiently, oscillations cease, but there is still positive feedback, and at the tuned frequency the circuit becomes a highly selective regenerative amplifier. The desired frequency is accentuated above all others.

As a filter

Fig. 3-b is the filter circuit. An input signal feeds the phase shifter and amplifier V4 simultaneously. V4 shifts phase by 180°. The signal through the shifter-V3 channel is not changed in phase. If these signals are equal they cancel at the output terminals. The null is deeper and sharper than that of a parallel-T network.

The frequency control is a dual 50,000-ohm potentiometer. When set to zero resistance the frequency is maximum. For still higher frequencies the d.p.s.t. switch S1-a and S1-b is closed. S2 is the band switch. The 580-μμf trimmers are adjusted as follows: Set S3 to the OSCILLATOR position; set S1 and S2 to HIGH. Tune the oscillator to a frequency of 4 kc. Now throw S2 to LOW, and adjust the two trimmer capacitors for an output of 1 kc, or exactly one-quarter the first frequency. (Keep the trimmers at about the same capacitance during adjustment.)

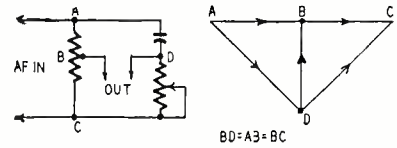


Fig. 2—Simple 90° phase-shift circuit.

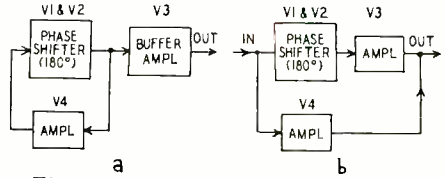


Fig. 3—Basic oscillator and filter schemes.

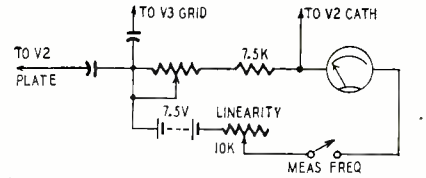


Fig. 4—Frequency meter circuit details.

Frequency ranges are approximately as follows:

With S2 closed

S1 open	175–325 c.p.s.
S1 closed	320–1,800 c.p.s.

With S2 open

S1 open	700–1,300 c.p.s.
S1 closed	1,280–7,200 c.p.s.

Frequency meter

A meter and battery circuit is used for measurement of frequency. It is in the V2 plate circuit. The principle of operation is shown in Fig. 4. In this circuit the meter indication is approximately inversely proportional to resistance. Since this is the same relationship which exists between frequency and resistance, the meter can be calibrated in cycles. We used a meter with a basic 500 microampere movement. It carries two scales (marked volts) the upper one 0–15 and the lower 0–600. We use the meter to indicate to 1,500 cycles on low range and to 6,000 cycles on the other. The linearity control is used to calibrate the readings near full scale.

Switch S4 is a momentary type. When depressed, frequency is measured and the output is disconnected. When released, the meter is out of the circuit and the oscillator-filter operates normally. Resistors R1, R2, R3, and R4 should be of the precision, wirewound type.

Output from the oscillator is ample for a.f. testing, bridge supply, low power modulation, and other applications. The filter can be used to eliminate interference, or measure frequency.

Materials For Oscillator-Filter

Resistors: 2—2,200, 2—8,200, 1—10,000, 1—15,000, 2—39,000, 2—47,000 ohms, 1—1 meg, ½ watt; 2—1,000, 2—2,200 ohm precision type.
Potentiometers: 1—10,000, 1—15,000, 1—25,000, 1—dual 50,000 ohms.
Capacitors: 2—.002, 7—.01, mica; 2—580 μμf mica trimmers; 1—40, 1—8 μf, 450 volts, electrolytic.
Switches: 1—d.p.d.t. momentary, 1—d.p.d.t., 2—d.p.s.t., 1—s.p.s.t.
Power transformer: 200—200 V @ 50 ma.
Miscellaneous: 1—7.5-v battery, 2 phone jacks, 1—0—500 microammeter, 1 metal box 5x5x3½, filter choke, line cord, wire, solder, hardware.

—end—

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More Notes on TV Troubles

By MICHAEL L. TORTARIELLO

General Electric 802 and 803

Sound and picture normal on channels 2-4-5. No sound, but pictures normal on channels 7, 9, 11, and 13.

Characteristics of 7F8 radio-frequency oscillator tube have changed with age. Replace with new one.

General Electric model 802 (AM-FM-TV combination)

Picture normal; sound on AM normal; no sound on FM or TV.

Resistor R783 (4,700-ohm, ½-watt) open. Replace with 4,700-ohm, 1-watt.

Westinghouse model H618T16

Sound normal; video signal and raster present, but no horizontal or vertical synchronization.

Replace 6C4 sync phase inverter tube.

Westinghouse model H605T12

Sound normal; no high voltage.

Resistor R409, 560 ohms, 5 watts, red hot, capacitor C506 (.047 μf, 400 volts) shorted. Resistor R502 (68 ohms, ½ watt), damaged. Replace capacitor with .035-μf 600-volt unit. Replace resistor R409 with 5-watt, 500-ohm. Replace resistor R502 with 100-ohm, 1-watt unit.

Westinghouse model H626T16

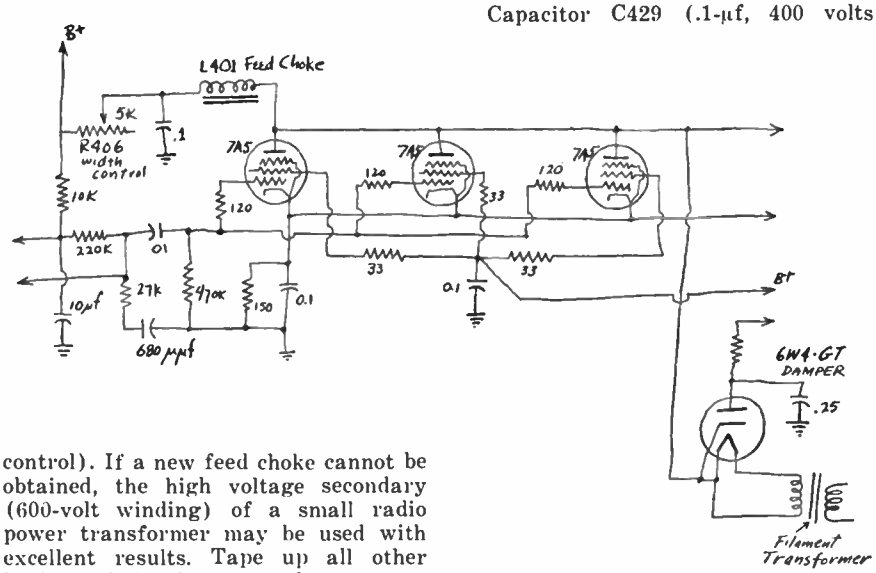
Sound normal; vertical and horizontal sweeps normal; high voltage normal; no video signal at cathode of 16RP4 C-R tube.

Capacitor C315 (.05-μf, 400 volts) shorted. The shorting of this capacitor also opened up contrast control R319 (1,500 ohms). Replace C315 with .05-μf, 600-volt unit. Replace R319 with V-9877 assembly, which includes contrast control, volume control, and a.c. on-off switch.

Westinghouse model H600T16

Sound normal; vertical sweep and high voltage present, but raster only 1 inch wide.

Winding of L401 feed choke (supplying B-plus to the three 7A5 horizontal output tubes) shorted to ground. This also burned out R406 (5,000-ohm width control). If a new feed choke cannot be obtained, the high voltage secondary (600-volt winding) of a small radio power transformer may be used with excellent results. Tape up all other leads and insulate transformer case from chassis. Replace R406.



Sound normal; video signal and raster present, but raster shows a bright white line 2 inches wide from top to bottom of picture tube.

Replace burned-out 6W4 damper tube.

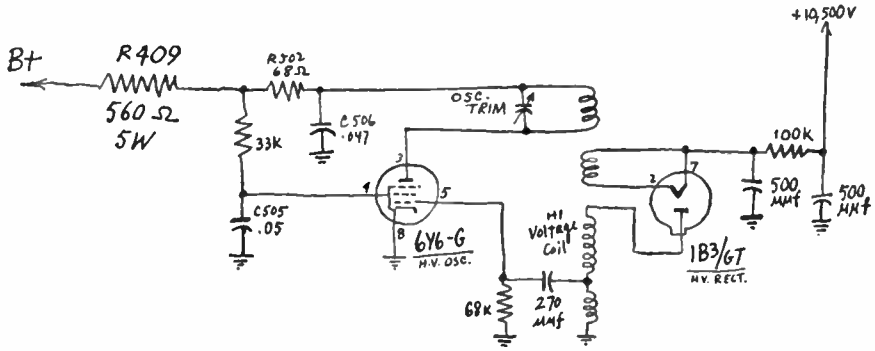
Sound normal; video signal present; raster keystoned wide at top, narrow at bottom, very much wrinkled.

Shorted 56-μμf, 1,500 volt capacitor across one half of horizontal deflection coil. Replace with 56-μμf ceramic.

Westinghouse model H627K16

Sound normal; no high voltage; plate of 6AU5 horizontal output tube red. Oscilloscope showed horizontal sawtooth at pin 6 of 12AU7 horizontal multivibrator.

Capacitor C427 (.01-μf) shorted. This capacitor is rated at 400 volts. Replace with 600-volt unit.



R.f.-type high-voltage circuit used in the Westinghouse model H605T12 receiver.

Westinghouse model H630T14

No picture; no high voltage; sound distorted.

Capacitor C429 (.1-μf, 400 volts) from pin 8 of horizontal output tube (6AU5) to ground, shorted. Replace this unit with a 0.1-μf, 600-volt type.

Westinghouse model H619T12

Sound distorted; no high voltage.

Capacitor (0.1 μf, 400 volts) from pin 5 of horizontal output tube (6AU5) and horizontal deflection coil, shorted. 1,500-ohm width control burned out. Replace 0.1-μf capacitor with 600-volt unit. Replace width control.

Crosley model 10-421 MU

No horizontal synchronization; rotation of horizontal hold control had no effect on picture. Very loud high-frequency whistle emanating from flyback transformer.

Replace 6SN7 horizontal a.f.c. and oscillator tube, with a *brand-new one*, as not all 6SN7 tubes will work in this application.

Crosley model 9-407-M-3

Weak sound; no high voltage.

Section A of resistor R-36 rated at 7,000 ohms, reads 2,000 ohms. This resistor is attached to chassis and is enclosed in a metal sleeve. Open end of resistor arcing to ground. Replace with 7,000-ohm 10-watt wire-wound unit.

Admiral model 25A16

Sound normal; no horizontal sweep or high voltage.

C53 capacitor (50 μμf) between pin 4 of 6SN7 (V16B) horizontal oscillator and ground open. Replace C53.

—end—

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Electronics and Music

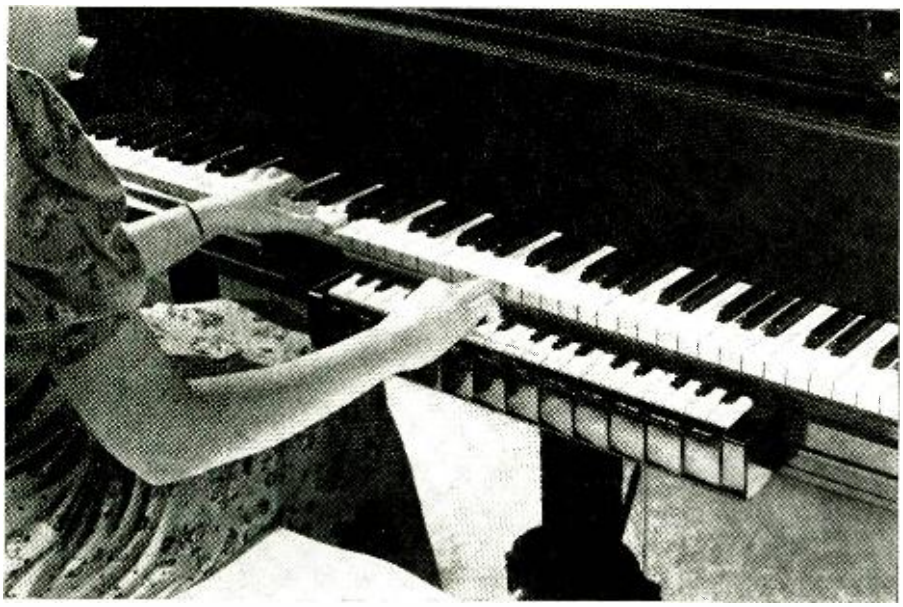


Fig. 1—Typical Hammond Solovox installation. The miniature keyboard fastened to the piano front contains playing keys and all controls.

Part XXIII—The construction and circuit details of the popular Solovox in its new, all-electronic version.

By RICHARD H. DORF

THE Hammond Solovox (Hammond Instrument Company, Chicago, Ill.) is and has been for a number of years the best-known monophonic electronic musical instrument made in this country. While it permits the playing of only a single note at a time, and has neither the types nor variety of tone colors to appeal to most serious musicians, it has found extensive use in popular-music ensembles and particularly in the home among amateurs. It is ordinarily used with the piano—the player's right hand playing the melody on the Solovox and the left hand playing an accompaniment on the piano—where its sustained tones contrast with the percussive effects of the piano to produce pleasing sounds with a minimum of study, effort, and expense.

Unlike the Hammond organ, the Solovox is completely electronic, with no moving parts other than the keys and controls. (To be accurate, the older models J and K had a vibrating-reed vibrato system, but the present model L is electronic in even this respect.) This article describes the model L, which does not differ from the earlier J and K models in principle.

A typical Solovox installation is shown in Fig. 1. The two principal units are the keyboard and a tone cabinet. The tone cabinet (not shown in the illustration) houses the speaker and all vacuum tubes. The keyboard, attached to the front of the piano, holds the switches which are actuated by the keys, and all control circuits.

Fig. 2 is a block diagram of the Solovox which shows the principal components and their relationships. A master oscillator is tuned through a 3-octave range by the keys, and its frequency may be varied cyclically to produce vibrato. The oscillator synchronizes a frequency divider which produces similar tones one octave lower down. This, in turn, synchronizes a second and third frequency divider.

One output is taken from the oscillator, which operates in the highest three-octave range of the instrument, and one from each of the frequency dividers. In accordance with their pitch ranges the outputs are labelled SOPRANO, CONTRALTO, TENOR, and BASS. Any one or a combination may be switched into a common output bus which goes to a series of five tone filters. Whatever tone qualities are switched on are passed to a preamplifier, thence to a push-pull control stage. In the control stage the output volume is controlled by a knee lever fastened under the keyboard, and the attack of each note is slowed down by using an extra set of keyboard contacts to remove cutoff bias on the stage at a controlled rate of speed. From here the signal passes to an output stage and loudspeaker.

Master oscillator

The master-oscillator circuit is diagrammed in Fig. 3. It is basically very simple and capable of wide-range operation. The output of V1-a is R-C

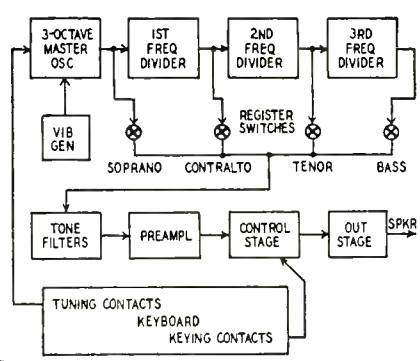


Fig. 2—Block diagram showing the operating circuits of the Hammond Solovox.

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coupled to the grid of V2-a. The plate of V2-a is R-C coupled back to the grid of V1-a. Since the circuit is reentrant and the feedback phase is positive, the combination oscillates. The frequency of oscillation is controlled by capacitance and resistance placed between the grid of V1-a and ground.

Two step-type controls are provided. C1 is the main tuning capacitor, and C2, C3, and C4 are added to give the exact value required for the fixed capacitance. The next bank of six .002-μf capacitors is so arranged that as the arm labeled ROUGH TUNING is moved upward, it contacts the capacitors one by one and at maximum position all six are across the main tuning capacitors. Six steps of 400 μμf each are available with a similar switching arrangement for the fine-tuning adjustment.

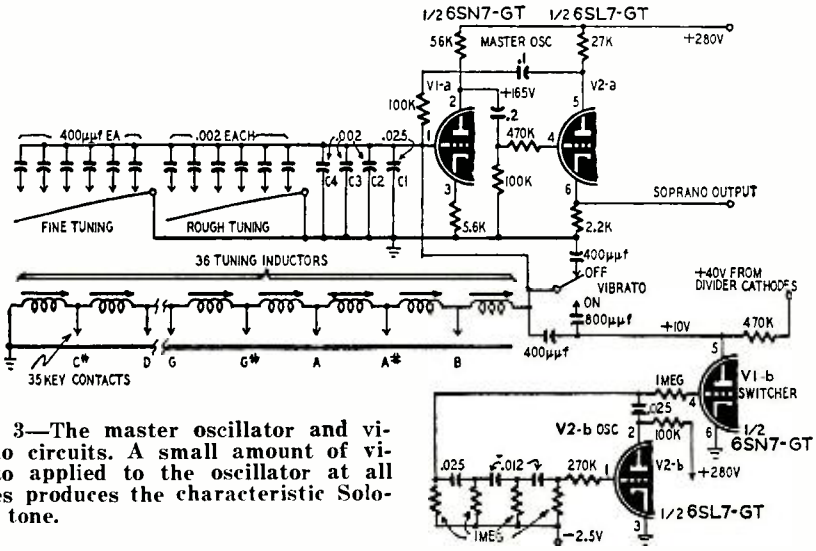


Fig. 3—The master oscillator and vibrato circuits. A small amount of vibrato applied to the oscillator at all times produces the characteristic Solovox tone.

The inductance part of the tuned circuit is used to vary the frequency to give the pitch required for each key over the three-octave range of the oscillator (523 to 3951 cycles). Thirty-six small inductors, each with a movable core for individual adjustment, are wired in series, with a switch contact connected between each adjacent pair. When a key is pressed, the corresponding contact is grounded, decreasing the net inductance between the grid of V1-a and ground. When the lowest C key is pressed, no contact operates—the full value of all the series inductors is in place and the lowest frequency sounds. (Actually this frequency is being generated all the time, even when no key is being pressed. The control tubes, however, block the amplifier until a key is pressed, as described later.) When the topmost key (B of the top octave) is pressed, all inductors but the one nearest the grid are shorted to ground and the remaining inductance is just large enough to tune the circuit to the topmost note. With this arrangement, no spurious notes are heard even when two or more keys are pressed at once by accident; only the uppermost of the notes played is heard.

The vibrato circuit includes the two remaining triodes of the 6SN7-GT and 6SL7-GT used in the oscillator. V2-b is the 6-cycle oscillator, a standard phase-shift unit, the output of which is fed to V1-b, a switching tube. The plate-supply potential for V1-b is only 40 volts, obtained from the drop across the frequency-divider cathodes (see Fig. 4). With the low plate potential of 10 volts and zero bias, the comparatively small signal from the vibrato oscillator is sufficient to cut off the switching tube when the signal is in the negative direction.

With the vibrato switch on, paralleled 400-μμf and 800-μμf capacitors (total value of .0012 μf) are connected from one side of the audio tuned circuit, through the switching tube, to ground. On the half-cycles of vibrato frequency during which the switching tube conducts, the capacitance is across the audio tuned circuit, changing its frequency to some degree. On the half-cycles during which V1-b is cut off, the audio frequency is unchanged. The frequency is thus switched at the vibrato-oscillator rate of 6 cycles per second, giving a vibrato effect.

With the vibrato swtch off, a permanent capacitor of 400 μμf is connected across the tuned circuit. The 400-μμf capacitor between V1-b plate and the audio tuned circuit is still in place and the switching tube is still doing its job. The vibrato effect is therefore still present to a very slight degree. This is desirable, for it is enough to destroy the "perfection" of the electronically generated tones, which would otherwise be so perfectly steady as to lack interest.

This is an interesting point in all electronic instruments—perfection is undesirable! A pipe organ, a wind instrument, a violin—all of them have inherent random irregularities of pitch and volume caused by small variations in the wind supply or slight unsteadiness in the player's control. One of the essential factors in art appreciation by the emotions is variation; monotony is inartistic and unpleasant. Thus the natural slight unsteadiness of acoustic instruments is welcome, and to attain a really ideal musical instrument, the electronic engineer should deliberately avoid the perfection which we normally look for in engineering. In one very practical sense this is a major difference between a set of code-practice oscillators tuned to musical pitches and a good electronic musical instrument. The code oscillators have constant pitch and no variation in tonal quality. The musical instrument must have at least a vibrato and a selection of tone colors.

Frequency dividers

Frequency dividers are very common in electronic musical instruments. In polyphonic instruments there is usually one set of them for each of the 12 notes of the scale and each divider need work at only one frequency. In the Solovox there is only a single set of three dividers, each of which must work over a three-octave range. To fulfill this requirement they are designed to be not particularly frequency-selective and they are of the non-oscillating multi-vibrator type. This means that in the absence of a synchronizing signal they do not oscillate but remain in one or the other of their two stable conditions.

The frequency-divider section of the Solovox appears in Fig. 4. The first tube V3-a is a rectifier which rectifies the output of the master oscillator. The grid is coupled to the oscillator plate through C1. The waveshape of the master oscillator output is roughly symmetrical and contains principally odd harmonics, sounding like a muted instrument, or a woodwind, or stopped pipe. The rectified output from V3-a is no longer symmetrical and contains even harmonics as well as odd ones.

V3-b is a pulse rectifier. Because of the capacitive coupling between V3-a and V3-b, the rectified output of V3-a appears as a.c. on the grid of V3-b. Due to the average plate currents of the tubes in the dividers the cathode of V3-b is 40 volts positive, giving the tube a high negative grid bias. Negative input to the grid therefore has no effect, but positive input increases the plate current and produces negative pulses at the plate.

V4-a and V4-b are the first frequency divider. In the resting condition one of the tubes is cut off and the other is conducting. When the driver V3-b puts out a negative pulse, it passes through C3 and C4 to the divider grids. The negative pulse has no effect on the tube which is cut off, for instance V4-a. However, it causes the tube which is drawing current, V4-b in this case, to put out a positive pulse at its plate. The positive pulse is transferred to the grid of V4-a through the R-C plate network, causing V4-a to conduct and put out a negative pulse of its own. This negative pulse is transferred to the grid of V4-b, adding to the negative input signal. In a very short time V4-b is cut off and V4-a is conducting, the reverse of the original state. At this point the circuit is again stable. However, the

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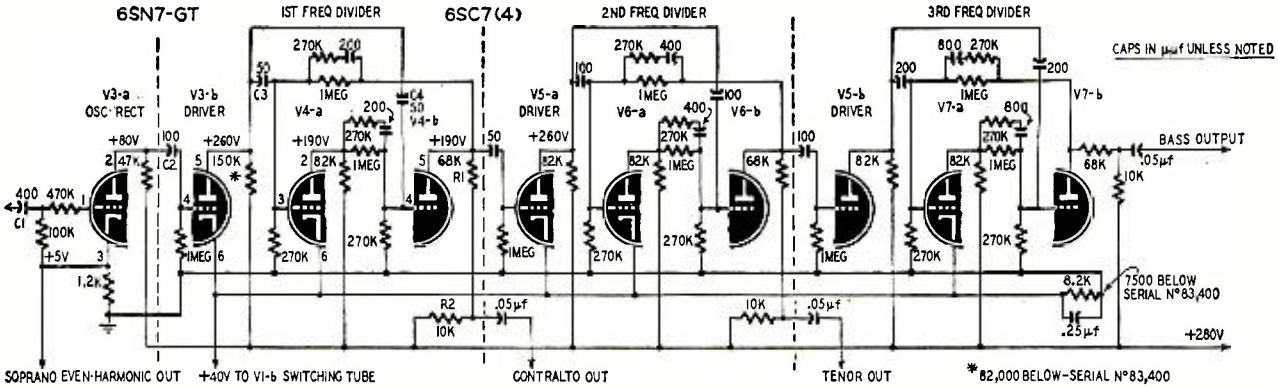


Fig. 4—Schematic of the Solovox frequency-divider chain. Each stage divides by two, reducing the frequency one octave.

next negative pulse to come from the plate of V3-b starts things all over again and in the same manner V4-a now cuts off and V4-b conducts.

In this way, it takes two input pulses from V3-b to make the V4 circuit execute a complete cycle of change, returning to its original condition. Since the frequency of pulses from V3-b is the oscillator frequency, the contralto output taken from the plate circuit of the divider at the junction of R1 and R2 is one-half the oscillator frequency and has a rectangular waveshape.

Each of the two following dividers works in the same way and includes a driver-rectifier triode (V5-a and V5-b) and two multivibrator triodes (V6-a and V6-b, V7-a and V7-b). In each case the input frequency is divided in half, so that there are four outputs from the generating section of the instrument—one from the oscillator and three from the dividers, each output being one octave below the input.

Tone color selection

Two circuits are shown in Fig. 5. The first is the register-control section of the Solovox and the second the tone controls.

The register controls do two jobs. The first and most obvious is the selection of which ranges shall be sounded. The entire instrument covers six octaves. When the soprano switch is closed the three highest octaves are fed to the output bus. When the contralto switch is closed, each note keyed sounds one octave lower, which adds one lower octave to the instrument, and so on down to the bass switch.

The outputs of the frequency dividers are symmetrical in waveform. This is a "muted" tone carrying only odd harmonics. To add even harmonics to the tones of the bass register, a certain amount of tenor output can be added, since the fundamental of the tenor is the second harmonic (one octave above) of the fundamental of the bass. The amplitude of the added tenor must be kept down so that it does not sound to the ear like an additional octave repetition. If, for example, the original bass tone has ⅓ as much third harmonic as fundamental, ⅑ as much fifth harmonic as fundamental, and so on, then adding a tenor fundamental about ½ as loud as the bass fundamental will give a second harmonic to the bass which will simply fill out the harmonic content of the bass in the correct proportion. The effect is to get rid of the muted tone quality.

With the mute switch of Fig. 5 in the off position the bass receives some additional tone for this purpose from tenor; tenor receives some from contralto; and contralto receives some from soprano. Since there is nothing higher than soprano the special oscillator rectifier of Fig. 4 supplies even-harmonic additions for the soprano tone. With the mute switch on, these additions are removed and the muted quality is sounded.

There are five tone-control switches in Fig. 5. All the filters are in series across the register-control output bus. The tone switches are normally closed; when a tone quality is selected the switch is opened. With all but the DEEP TONE switches closed, the tone develops across a highly capacitive load and the high-frequency harmonics are very much reduced. With the FULL TONE switch open, frequency response is almost flat, but with some attenuation of treble to round off the sharp edges of the waveform. FIRST VOICE and SECOND VOICE are roughly 400-cycle and 800-cycle resonant circuits which give brassy and reedy tones, while the BRIL-

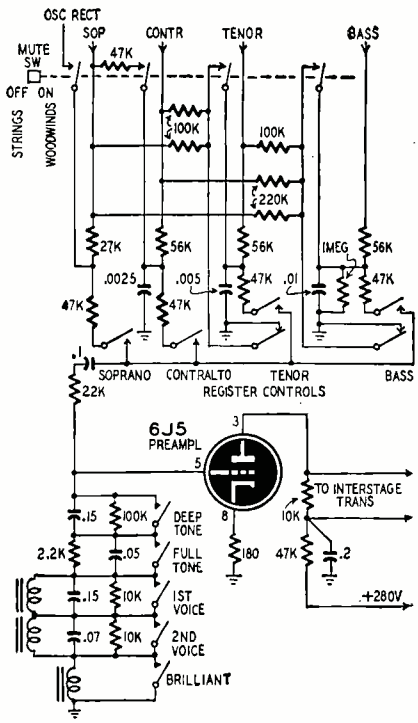


Fig. 5—Register-control and tone color-selection circuits. Instrument tones are produced by harmonic combinations.

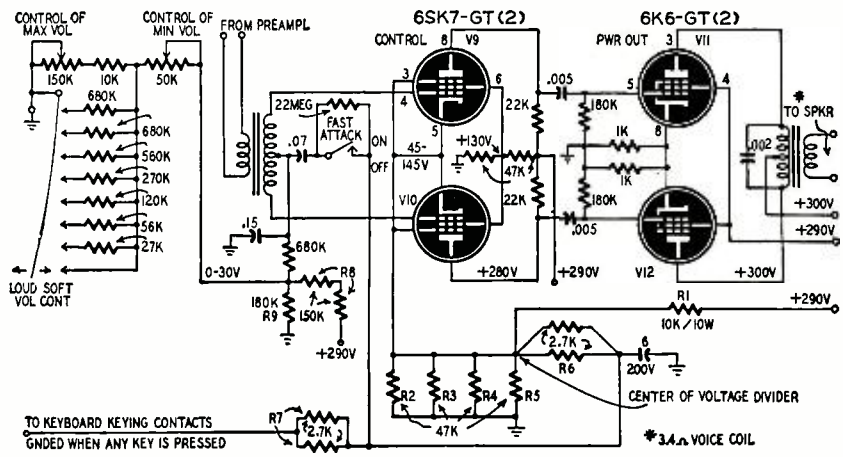


Fig. 6—Control stage slows attacks and varies output volume of the instrument.

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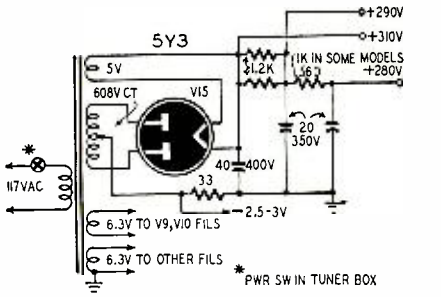


Fig. 7—Supply has four output levels.

LIANT filter is a high-pass filter with a very bright tone. The filters are in the grid circuit of the preamplifier 6J5 the plate of which couples to the control stage through a transformer.

Control and output stages

The control stage, diagrammed in Fig. 6, consists of a pair of push-pull, remote-cutoff 6SK7's. The two cathodes are connected to the center of a voltage divider consisting of R1 as one leg and R2, R3, R4, and R5 in parallel as the second leg. Normal voltage at the cathode tap is 145 because of the connection of plus 290 volts to the input of the voltage divider. The center of the voltage divider is also connected through R6 and R7 to a bus running the length of the keyboard. One of the contacts under each key is permanently grounded. When any key is pressed the bus is grounded, placing R6 and R7 across the lower (cathode) leg of the divider and reducing cathode voltage to about 45. The rate of drop of the voltage is controlled by the 6-μf capacitor, which causes a time delay.

A second voltage divider is placed across the 290-volt supply, with R8 as its upper leg and R9 as its fixed lower leg. The center of this divider goes to the center-tap of the input transformer and thence to the grids. Shunted across the lower leg of the divider is the network of resistors and the selector switch shown, which varies volume by varying the d.c. grid voltage. At maximum volume the grids are about 30 volts above ground. Since the cathode, when a key is down, is about 45 volts positive, the net grid bias is about 15 volts and the tubes operate normally. As the volume control is closed the lower leg of the grid divider is shunted more and more and the grids become less positive. They therefore become more and more negative with respect to cathode. When no key is pressed the cathodes are about 145 volts positive, enough to cut off the tubes no matter what the position of the volume control.

The fall of grid-cathode voltage when a key is pressed is normally slowed up additionally by the .07-μf capacitor between transformer center-tap and keying circuit. For faster attack the switch is opened and a 22-megohm resistor is in series with the capacitor.

The output stage is conventional, using a pair of 6K6 tubes. The power supply is shown in Fig. 7.

(To Be Continued)



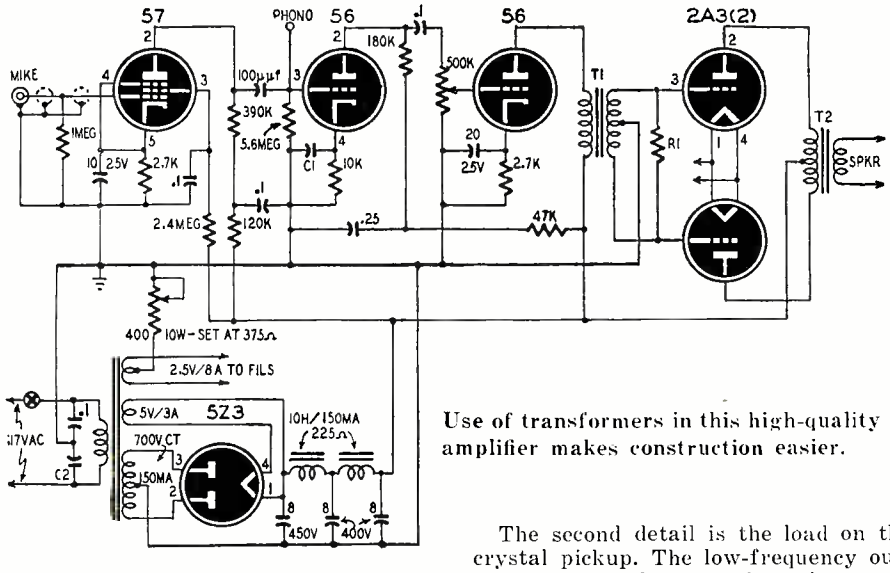
TRANSFORMER COUPLED PHONO AMPLIFIER

By CHARLES R. AMMERMAN

A GOOD-quality amplifier can be simply and easily built. This amplifier was designed to have a frequency response satisfactory for use with good phonograph records, adequate power output, and a certain degree of versatility. It was considered a foundation unit to which preamplifiers, compensators, and other equipment, could be added. Therefore a flat frequency characteristic was desired. Its primary use was to operate directly from a microgroove crystal pickup. An AM or FM tuner also may be used as a signal source. Occasionally some sort of PA system is handy, so a mike preamplifier was built in for convenience. The preamplifier frequency response is poor, since it is adapted to the crystal pickup, but for most PA and amateur work the frequency response is of little consequence.

The units delivers about 4½ watts without severe distortion, with 0.88 volt input, at full gain. The frequency response is 3 db down at about 20 and 10,000 cycles. (These frequencies depend almost wholly on the transformers used.) Since feedback was to be avoided in the interests of simplicity, push-pull class A 2A3's were used for low output impedance and low distortion.

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Use of transformers in this high-quality amplifier makes construction easier.

Since 2A3 tubes were used in the output, 2.5-volt tubes were also used in the other stages. There would be no objection to using the 6.3-volt equivalents all the way through, except that 6A3's seem harder to find. The equivalent 6B4-G's or 6A5-G's could also be used, of course. In the other stages two 6C5's or 6J5's (or one 6SN7) and one 6J7 could be substituted. (The first tube may be omitted if a microphone is not to be used.)

Circuit features

There are very few unusual features about this circuit. The performance depends almost entirely upon the transformers T1 and T2. For T2, any push-pull transformer matching the speaker to 4,500 ohms will do the job. *The better the transformer, the better the amplifier frequency response.* Similarly T1 can be almost any single-plate to push-pull grid transformer. This one came from an old but good radio. (Interstage transformers in old sets are often very poor.) Thordarson types T-20A23 and T-22S70 would probably be satisfactory for most applications.

Three details make a slightly better amplifier than might be expected with any given set of transformers. The first is the resistor R1 shunting the interstage transformer. This improves the frequency response at both the high and low ends, and also tends to reduce the Q at the transformer resonance peak. When a square-wave was fed into the amplifier and the output waveform was observed on an oscilloscope, transient oscillations on the square-wave due to transformer T1 ringing were very noticeable when the resistor was not used. The smaller it is made the less ringing is seen. The only disadvantage of small values is that the amplifier gain is reduced. A value of 100,000 ohms was chosen for this amplifier. The experimenter without test equipment should use the smallest resistance consistent with adequate gain (although not lower than about 25,000). High quality transformers will not require shunting resistors.

The second detail is the load on the crystal pickup. The low-frequency output of a crystal is very dependent upon the load resistance, so that the grid resistor of the 56 was made 5.6 megohms. Its coupling capacitor of 100 μμf has very high reactance at low frequencies, hence the low-frequency input impedance is nearly 5 megohms.

Just a general tip: Don't use a volume control in this circuit. The input capacitance of the tube is high, due to Miller effect, and a high-resistance volume control will make the high-frequency response fall off as the volume is decreased.

The third place where frequency response may be improved is in a compensating circuit in the cathode of the first triode. In general, to get good low-frequency response it is necessary to use very large bypass capacitors, and it is better to leave them off if you can stand the loss in gain. Here it was decided not to bypass the first triode's cathode. Then the idea of using this stage to improve high-frequency response came. A *small* capacitor, C1, is used, that starts to bypass at about the same frequency the transformers start to cut off. This will maintain good response to a somewhat higher frequency. Care must be taken that it is not made too large, or a peak will occur near the high-frequency end. In this particular amplifier an optimum value of 0.003 μf was found. Further compensation could be added, if desired, by treating the next cathode capacitor the same way, but of course there would be some loss in gain. An audio oscillator or standard frequency record is almost a necessity in determining the proper size capacitor to use. If you don't have either of these it might be safer to omit the cathode capacitor entirely.

Hum should not be excessive and may be treated in common ways. The preamplifier should be well shielded, including the grid lead. Do not make the mistake the author did and bring the 117-volt line and phonograph input connections to the same terminal strip. This caused unnecessary grief that was finally cleared up by installing capacitors across the line, and trying various values for C2 until the hum was balanced out. There was one value that worked well—larger or smaller values gave more hum. Start with 0.1, then try larger or smaller values until the proper one is found.

This amplifier will develop all the power needed to enjoy music in the home, and has very good quality. Remember that the speaker is *at least* as important as the amplifier in any installation. A speaker not less than eight inches in diameter, and preferably larger, should be used; best results may be obtained with some sort of woofer-tweeter combination. The speaker will not be at its best unless used in an adequate mounting. Simple mountings that give good results are a large flat baffle, three feet or more on a side, or a large open-back cabinet. Bass-reflex and horn-type enclosures may give somewhat better results.

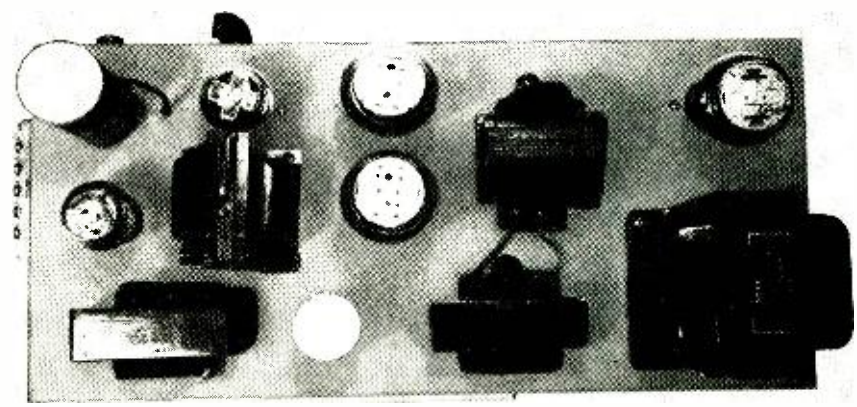
Materials for amplifier:

Resistors: 1—400 ohms, 10 watts, with slider; 2—2,700, 1—10,000, 1—47,000, 1—120,000, 1—180,000, 1—390,000 ohms, ½ watt; 1—1, 1—2.4, 1—5.6 megohms, ½ watt; 1—500,000 ohm potentiometer with audio taper. (See text for R1.)

Capacitors: (mica) 1—100 μμf, 500 volts; (paper) 1—0.1 μf, 600 volts; 3—0.1, 1—0.25 μf, 400 volts; (electrolytic) 1—10, 1—20 μf, 25 volts; 3—8 μf, 450 volts. (See text for C1 and C2.)

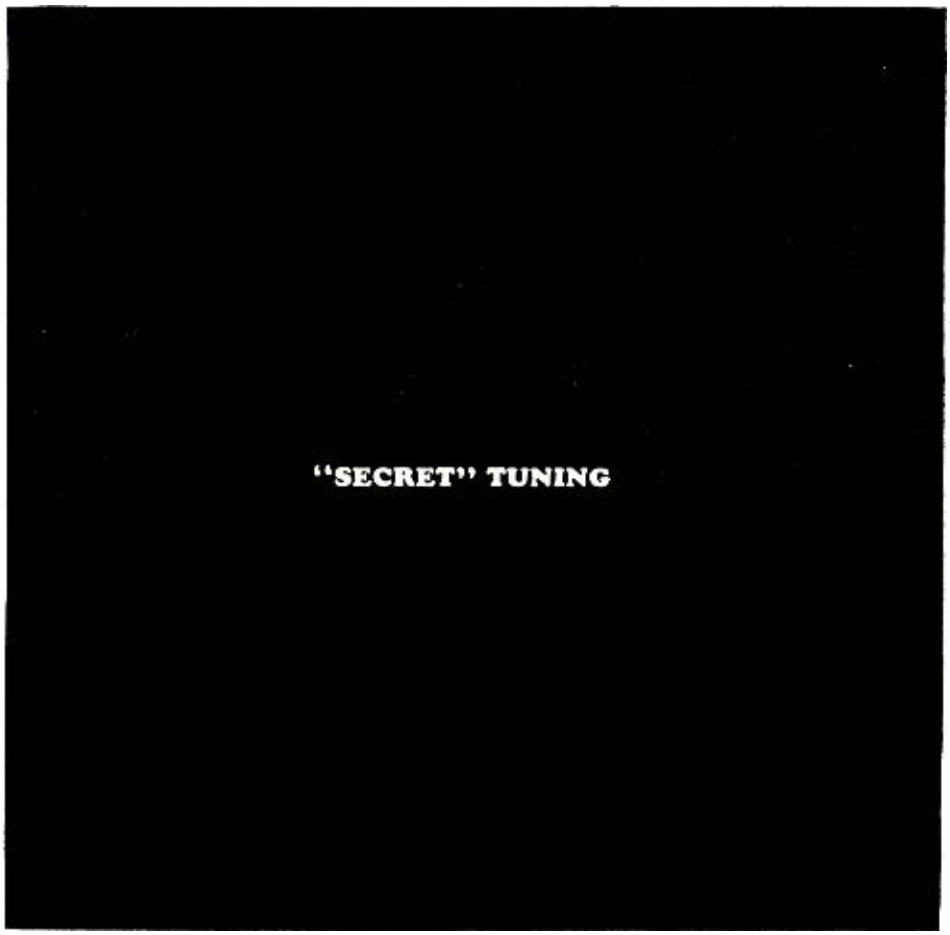
Miscellaneous: Tubes: 1—57, 2—56, 1—5Z3, 2—2A3. Sockets: 1—6 prongs, 2—5 prongs, 3—4 prongs. Transformers: 1—700 volts c.t., 150 ma; 5 volts, 3 amp; 2.5 volts c.t., 9 amp; 1—interstage audio, single plate to p-p grids; 1—10-watt output, primary 4,500 ohms plate-to-plate, secondary to match voice coil; 2—chokes, 10 henries, 150 ma, 225 ohms (approx.). Chassis, hookup wire, hardware.

—end—



Top view shows layout. The filter chokes are those nearest the power transformer.

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Frequently used—
but rarely explained—
the technique of
tuning L/C circuits by
resistance control.

By JOHN K. FRIEBORN

IN CERTAIN television receivers the horizontal oscillator frequency is controlled by a method which apparently has never been fully explained in data intended for service technicians. Although is it possible to service a receiver without completely understanding it, many technicians want to know, as I did, just what goes on in these receivers and what other applications the same principle may have. Most publishers of information for technicians seem to believe that their readers are unable or unwilling to learn anything more than their day-to-day work forces them to know. If the material published in RADIO-ELECTRONICS reflects the wants of its readers—and of course it has to—those readers know that things which do not seem to have any immediate application in their work today may still be worth reading about, either because they may be needed tomorrow, or simply because they are parts of the field of electronics, which many of us find so interesting that it is not only our business but our hobby.

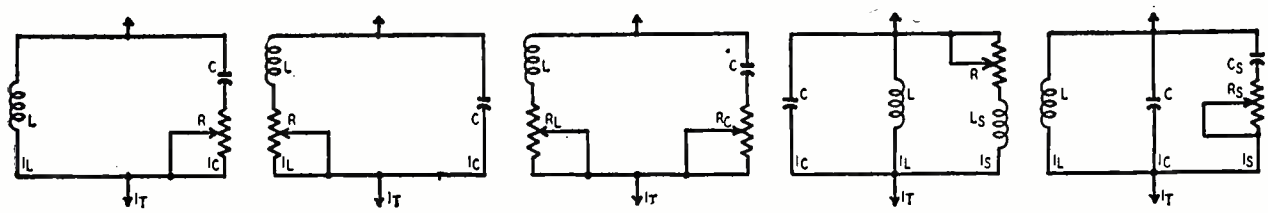
Ask any radioman how the resonant frequency of a parallel resonant circuit can be changed and he will probably answer something like this: "By changing the inductance or the capacitance, of course; how else?" There is enough truth in this to make it accurate for all practical purposes, but there is enough error in it to hide a principle which has been used in the design of certain television receivers, but not explained in the service data. Actually there is nothing very complicated about it. (Incidentally, if you have been looking ahead and the mathematical formulas worry you, skip them. You don't need them, except to quote to the fellow who quotes the formula that "everybody knows". These formulas, being longer, should put *him* in his place, so remember where you saw them.)

What is resonance?

One fact which confuses the situation is that there are different definitions for the resonant frequency of a parallel resonant circuit: the frequency at which the inductive and capacitive reactances are equal; that at which the current is minimum and the impedance is maximum; and that at which the current is in phase with the voltage and the impedance is equivalent to a pure resistance. The usual formula $F=\frac{1}{2\pi\sqrt{LC}}$ is correct for the first definition, but in actual circuits the important frequency is usually one of the latter two, the frequency of maximum impedance in a tuned amplifier, and the in-phase-current frequency in an oscillator. These frequencies are affected by the presence of resistance in series with either of the legs. The resistance of the coil produces such an effect, but usually a negligible one. Deliberate insertion of a substantial amount of resistance in either or both legs, makes it possible to tune the circuit within certain limits by varying the resistance. Although very little has been published on this type of resistance tuning, it was used in experimental AM receiver designs more than fifteen years ago, in military FM equipment during World War II, and in postwar television receivers.

The tuning effect of the added resistance can be accounted for by considering the resonant frequency of a parallel L-C circuit as that at which the currents through the inductive and capacitive branches are approximately equal in amplitude and opposite in phase, producing a minimum total current and maximum impedance. Inserting resistance in series with one leg will decrease the current through that leg and disturb the resonant condition. We can get back to resonance by increasing the reactance of the other leg to reduce its current. This can be done either by changing the value of the inductance or capacitance or by changing the frequency. For example, inserting resistance in series with the capacitance reduces the leading current in the circuit, requiring an increase in the inductive reactance to reduce the lagging current. By increasing the size

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Figs. 1 through 5 (left to right)—Inserting resistance in the branches shown changes the resonant frequency of each circuit.

of the inductance, the same resonant frequency could be restored; if the inductance is unchanged, the resonant frequency would increase. Adding resistance in series with the capacitance as in Fig. 1 reduces the current through the capacitive leg as if the capacitance itself had been decreased; decreasing the capacitance would increase the resonant frequency. Adding resistance in series with the inductance, as in Fig. 2, would of course have the opposite effect.

The mathematics

Anyone interested in exact quantitative results can find mathematical treatments in many standard books.

These books often (probably unintentionally) steer their readers away from the principle which is the subject of this article by remarking that—in the circuits usually used in radio—all three of the definitions of resonance are approximately equivalent. For example, *Mathematics for Electricians and Radiomen*, by Cooke (McGraw-Hill), pages 478-480, gives, for the frequency at which the current is minimum and the impedance is maximum,

$$f=\frac{1}{2\pi}\sqrt{\frac{1}{LC}-\frac{R^4C}{2L^3}}$$

and, for the frequency at which the current is in phase with the voltage and the circuit acts like a pure resistance,

$$f=\frac{1}{2\pi}\sqrt{\frac{1}{LC}-\frac{R^2}{L^2}}$$

In both of these, R is the resistance in series with the inductive leg. In either formula, increasing that resistance would decrease the resonant frequency.

Cledo Brunetti and Eric Weiss, in "Theory and Application of Resistance Tuning," *Proceedings of the I.R.E.*, June, 1941, pages 333-344, give a formula for the frequency at which a circuit with resistance in both legs (Fig. 3) acts like a pure resistance:

$$f=\frac{1}{2\pi\sqrt{LC}}\sqrt{\frac{1-\frac{C}{L}R_L^2}{1-\frac{C}{L}R_C^2}}$$

This also indicates that increasing R_L would decrease the resonant frequency and increasing R_C would increase the frequency.

As we might expect, there is a disadvantage in this method of changing resonant frequency: adding resistance to the circuit reduces the Q. The more the frequency is changed in this way, the lower the Q becomes.

Terman's *Radio Engineers' Handbook* (McGraw-Hill), pages 145-8, gives a very complete discussion of the effect of resistance on the maximum-impedance and in-phase-current frequencies, including curves which show how adding resistance in series with the inductance not only flattens the peak of the impedance-frequency curve, but changes the frequencies at which maximum impedance and zero phase angle occur.

Resistance tuning may be used for small frequency variations by having only part of the inductive or capacitive current pass through the added resistance, as in Figs. 4 and 5. The change in frequency is smaller and so is the reduction in Q.

A few examples

An early example of resistance tuning was in an experimental circuit for automatic tuning of AM receivers, described by Charles Travis in "Automatic Frequency Control", *Proceedings of the I.R.E.*, October, 1935, pages 1125-41. The circuit is shown in Fig. 6. Capacitor C1 and the plate resistance of the tube V2 form a series circuit in parallel with the tank L-C, so this circuit is of the same form as that in Fig. 5. Changing the plate resistance of the tube by changing the bias changes the amount of signal current through C1 and its effective capacitance, thus changing the frequency of the oscillator. Travis pointed out that this particular circuit is not very suitable for automatic tuning over the wide range of frequencies in the broadcast band (a ratio of about three to one), but similar circuits have been used in receivers with narrower ranges, such as military FM sets.

The chief application of resistance tuning to postwar television receivers has been for control of the horizontal oscillator frequency. Fig. 7 shows the horizontal oscillator circuit of *RCA* model 630TS. R168 is the manual horizontal frequency control. The series combination of R168, R196, and C172 is in parallel with the oscillator tank. Varying R168 varies the frequency of the oscillator.

Although R168 and R196 form the grid-leak resistance of this oscillator, the principle involved is not the same as that in a blocking oscillator. In the blocking oscillator, the time constant of the grid resistor and capacitor combination determines the length of time the tube remains cut off, that is, the time between cycles of the sine wave oscillations in the grid circuit. In this oscillator, however, there is no break between successive sine-wave cycles. In a blocking oscillator, increasing the resistance increases the length of time between oscillations in the grid circuit, and the length of the sawtooth cycle in the plate circuit. In fewer words, increasing the resistance *reduces* the frequency. But, as already pointed out, increasing resistance in series with capacitance across a parallel L-C circuit *increases* the resonant frequency.

In this circuit, varying R168 will also have other effects on the functioning of the circuit. There will be some variation in the input capacitance of the tube when its bias is changed, due to the Miller effect, but this is a minor matter at the television horizontal scanning frequency. More important is the fact that varying the grid resistor will vary the amplitude and waveform of the oscillations. In fact, extreme variation of the value of the grid resistor in either direction would cause the oscillator to stop. The practical

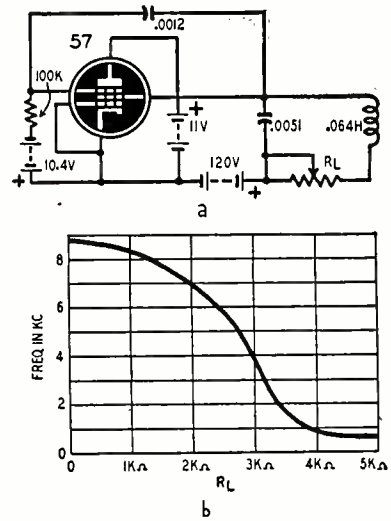
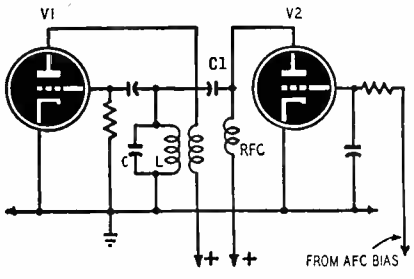
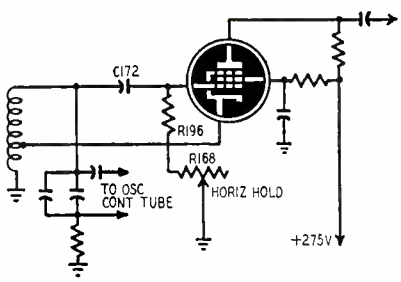
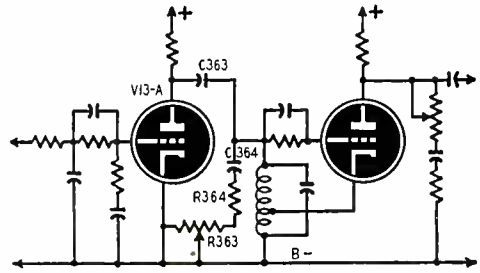


Fig. 9—Circuit for wide frequency range.

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Figs. 6, 7 and 8 (left to right)—Three applications of "secret tuning" to automatic frequency control. Details in text.

range of frequency variation is therefore smaller than it would be if the resistor and capacitor were used only across part of the tank. In this application, this is not a disadvantage, for several reasons: the desired frequency is always approximately the same; the oscillator circuit used is sufficiently stable not to require very large corrections; and the oscillator is used with a system of automatic frequency control for the correction of errors.

An a.f.c. application

The automatic frequency control of the horizontal oscillator in the 630 makes use of a reactance tube, which acts like an inductance in parallel with the tank, so that its effect is equivalent to inductive tuning. However, in some General Electric and Zenith receivers, the frequency of the horizontal oscillator is controlled both manually and automatically by resistance tuning. Fig. 8 shows the horizontal oscillator and control tube circuits of G-E model 16T3. R363, R364, and C364 are the manual frequency control circuit, and C363 and the plate resistance of V13-a are the automatic frequency control, similar to the Travis circuit in Fig. 5. Since this tube functions purely as a resistance, it is not a reactance tube in the usual meaning of the term, although it is sometimes referred to as such.

Unfortunately, giving it a name which immediately calls up a definite image in the mind of the service technician by no means helps in understanding the actual functioning of the circuits.

Larger variations

Most of the applications of resistance tuning to date seem to have been in circuits where only a small frequency variation is required. However, Brunetti and Weiss showed that a very large frequency variation could be obtained with some sacrifice of Q, and that, with certain circuits, the variation in frequency is approximately proportional to the change in resistance. Figs. 9, 10, and 11, adapted from their paper, give some idea of the possibilities. Fig. 9-a shows a transitron oscillator with a resistance-tuned tank, the resistance being in series with the inductive arm. Fig. 9-b shows the variation of frequency with resistance. Figure 10-a shows a tank for the same oscillator with the resistance in series with the capacitive arm, and Fig. 10-b the resulting frequency variation. Fig. 11-a shows a third tank circuit for the same oscillator, with a potentiometer arranged so that resistance taken from one arm is added to the other. The accompanying graphs in Fig. 11-b show the frequency variations obtained using potentiometers having total resistances of 5,000 ohms and 2,000 ohms, respectively. The first gives a roughly linear variation of frequency with resistance over a very wide range, while the second gives a frequency variation which is almost perfectly linear over a range of about 1.5 to 1.

Although resistance-tuned L-C circuits used to date seem to have been confined to oscillator tanks, the same principle could of course be applied to other resonant circuits.

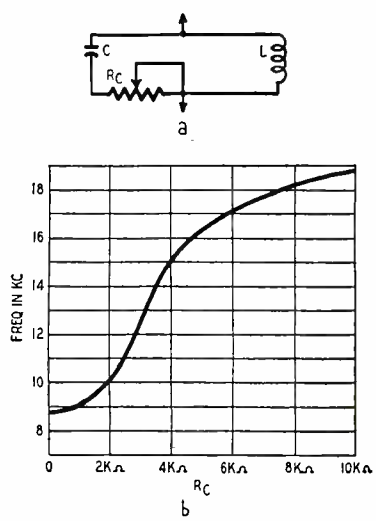
Another application

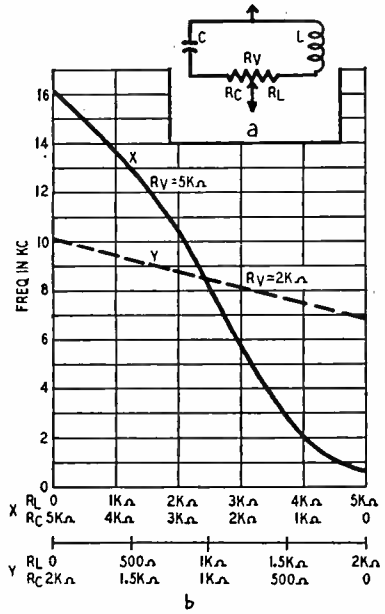
Another application of the principle which apparently has not been mentioned in previous publications, is its use with series resonant circuits. Just as the frequency of a *parallel* circuit can be changed by inserting resistance in *series* with one of the arms, so the frequency of a *series* resonant circuit can be changed by the insertion of resistance in *parallel* with one of the members. In Fig. 12, resistance in parallel with the capacitance reduces its impedance. For resonance, the impedance of the inductive member must be reduced, either by a decrease in inductance or by a reduction in frequency. The smaller the resistance, the greater the effect. The frequency at which the current is in phase with the voltage is

$$f=\frac{1}{2\pi}\sqrt{\frac{1}{LC}-\frac{1}{C^2R^2}}$$

If this article has revealed any secrets which engineers have been keeping to themselves, it is because I believe it can do no great harm for service technicians to know what goes on in the television receivers they work with.

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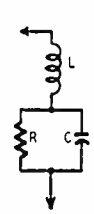


Fig. 10—A modification of Fig. 9 circuit.

Fig. 11—Another modification of Fig. 9.

Fig. 12—"Secret tuning" in series circuit.

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A group of easily constructed circuits, using the advantages of this inexpensive thyratron in various control applications.

THE VERSATILE 2050

By ED BUKSTEIN*

INDUSTRIAL electronics could never have reached its present state of development without the thyratron. This tube has proven invaluable in a great variety of control circuits. It has been used in such diverse applications as centering postage stamps within their perforated boundaries, scaling down the counting rate of radiation counters, measuring the muzzle velocity of guns, and controlling the rotational speed of radar antennas.

The thyratron is a hot-cathode, gas-filled tube containing a control grid. Unlike the *vacuum tube*, small changes in grid voltage do not produce *corresponding* changes of plate current in the thyratron. The thyratron, like a switch, is either cut off or completely conductive; either the bias is sufficiently negative to prevent the flow of plate current or it is not. Once conduction has started, the grid loses all control; only removal or reduction of the plate voltage will restore the thyratron to the cutoff condition.

The 2050 is a small thyratron available at most radio supply houses and on the war-surplus market. This tube is classified as a shield-grid thyratron or a gas tetrode. The purpose of the second grid is to reduce the value of control grid current and also to permit variations in the firing characteristics of the tube. In most applications, however, the shield-grid is connected to the cathode. The filament of the 2050 is rated at 6.3 volts at 0.6 amp. The peak cathode current is 500 ma and the average cathode current is 100 ma. Some manufacturers recommend that the cathode be preheated at least 10 seconds before anode voltage is applied.

Four control circuits employing the 2050 are described below. These are basic circuits, and variations of the same principles make these circuits usable in an almost endless variety of control applications.

The diagram of an automatic timing circuit is shown in Fig. 1. This timing circuit is often used when it is desired to apply power to certain apparatus, then have the power automatically disconnected after a given length of time. Resistance welders, enlargers, printers, r.f. heating equipment, and X-ray machines usually have this type of control. Accuracy and efficiency requirements preclude manual control by the operator.

When S1 (Fig. 1) is open and the upper side of the power line is negative, capacitor C charges. The path taken by this charging current is shown by the arrows. This charging current is actually the grid current of the 2050. The charge on capacitor C applies a negative potential to the grid of the 2050 and prevents the tube from conducting.

To start the timing interval, S1 is closed. S1-b now allows current to flow through the normally closed relay contacts, through the controlled device and back to the other side of the power line. Capacitor C begins to discharge through resistor R connected across it. As C discharges, the grid of the 2050 becomes less negative until the tube fires (ionizes). When the gas ionizes, the tube draws sufficient plate current to energize the relay. The normally closed relay contacts now open and disconnect the controlled device from the power lines.

Since the thyratron operates with a.c. plate voltage, the gas deionizes during every negative half-cycle. To prevent the relay from chattering at the line frequency, a capacitor is connected across its winding. This capacitor keeps the relay closed by discharging through it during each negative alternation. The 100-ohm resistor limits surge currents which might damage the thyratron.

Duration of the timing interval is determined by the values of R and C. A larger resistance will reduce the rate of discharge and therefore increase the timing interval. A larger

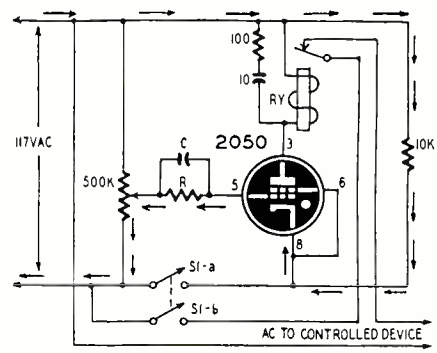


Fig. 1—An a.c.-operated circuit for thyratron control of small timing intervals.

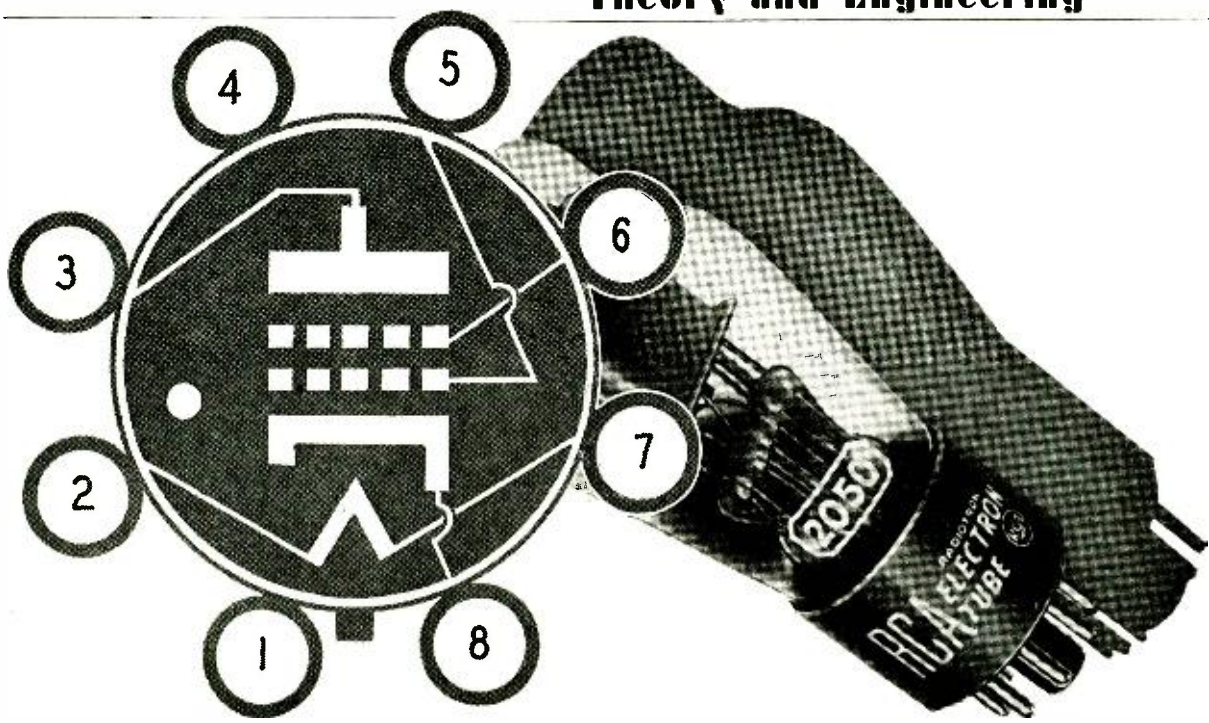
capacitor will also require more time to discharge. The values of R and C are therefore chosen on the basis of the time duration desired. The resistor may be made variable to control the time delay. Several time-ranges can be made available by the use of a selector switch and several different values of capacitance. The potentiometer shown in the grid circuit also provides some control of the timing interval. Moving the slider toward the S1 end will cause C to charge to a greater voltage. More time will then be required to discharge this capacitor.

Photoelectric control

The high sensitivity of the thyratron has been extensively utilized in its application to photoelectric control devices. These circuits have been used for opening garage doors when an automobile approaches, counting objects passing on a conveyor belt, turn-

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ing on lights at sundown, burglar and fire alarms, traffic surveys, race timers, etc.

Fig. 2 shows the circuit diagram of a photoelectric control which operates directly from the a.c. power line. The transformer is so connected that when the upper end of the primary is positive, the upper end of the 6-volt secondary is negative. Under these conditions, the thyratron cannot ionize (each time the plate goes positive, a negative bias is applied to the grid). If light is now allowed to strike the phototube, its cathode will emit electrons. This flow of photocurrent through R produces a voltage drop of opposite polarity to the bias. Since this IR drop makes the thyratron grid positive, ionization occurs and the resulting plate current energizes the relay.

The 1-megohm and 470,000-ohm resistors form a voltage divider to cut down the line voltage to a value suitable for the anode of the phototube (90 volts maximum for the 930).

Another photoelectric control is shown in Fig. 3. This circuit is of the type known as *self-latching;* i.e., once the relay has energized, it remains energized even though the amount of light on the phototube is restored to its original value. This is the type of circuit used for intruder alarms. When the intruder passes in front of the phototube he breaks the light beam. This energizes the relay and turns on an alarm bell. The bell then continues to ring even though the burglar moves away from the phototube.

In the circuit of Fig. 3 R1 and R2 form a voltage divider from B-plus to ground. The positive voltage at the junction of these two resistors is applied to the cathode of the thyratron. This cathode bias is sufficient to prevent ionization.

When the light to the phototube is obstructed, the internal impedance of this tube increases and a greater voltage drop appears across it. This voltage drop makes the thyratron grid positive enough to overcome the cathode bias. The 2050 then ionizes and energizes the relay. After a thyratron has ionized, variations of grid voltage do not change the plate current. This loss of grid control accounts for the self-latching feature of the circuit. To de-energize and release the relay, it is necessary to remove the plate voltage momentarily.

If the positions of the 10-megohm resistor and the phototube are reversed, the relay will be energized whenever light *strikes* the phototube.

The diagram of a thyratron contactor, sometimes known as a contact amplifier, is shown in Fig. 4. Initially, ionization of the thyratron is prevented by the application of negative voltage to the control grid. When the switch S is closed, the grid is connected to the cathode. Under this zero-bias condition, the thyratron fires, and its plate current energizes the relay. This circuit will be self-latching; once the thyratron is fired, opening the switch will not deionize it. If this self-latching feature is not desired, transformer windings may be used in place of the batteries shown in Fig. 4. These windings should be so arranged that when the thyratron plate is positive, its grid will be negative.

In practice, the thyratron contactor is used when the switch contacts are too delicate or too small to handle enough current to operate a relay directly. The relay contacts can be used to energize a circuit which will counteract the original increase which closed the switch contacts. In this manner, the quantity being metered can be regulated or held within specified limits.

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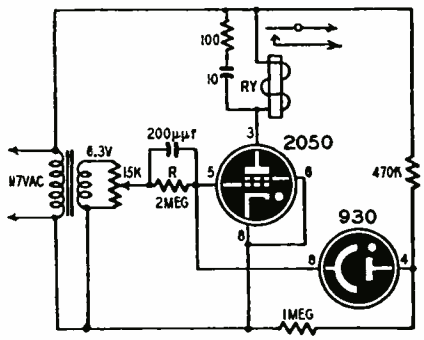


Fig. 2—A simple photoelectric control circuit using the 2050 thyratron tube.

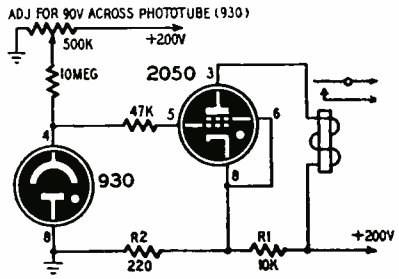


Fig. 3—The 2050 thyratron in a self-latching photoelectric alarm circuit.

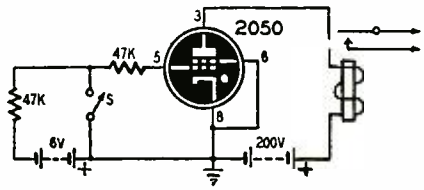
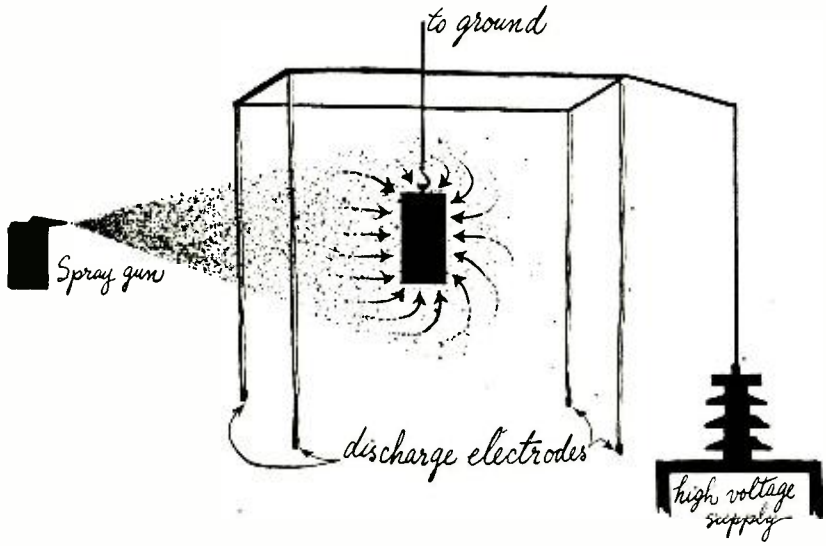


Fig. 4—A sensitive relay circuit, or "contact amplifier," using the 2050 thyratron.

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ELECTROSTATIC FINISHING



Conventionalized representation of electrostatic painting equipment.

Painting becomes easy with this technique in which the paint seeks out its object

By JERRY S. ADAMS

ELECTROSTATIC finishing offers the alert service technician a field with many potential applications. Recently introduced, it effects large savings in spray-finishing operations by polarizing the minute particles of paint so that they are attracted to grounded objects by electrostatic force.

The spray is polarized by directing it through a series of fine wires as shown above. The wires (known as discharge electrodes) are charged to a potential of approximately 100,000 volts by a step-up transformer and rectifier operating from the power line. Powerful electrostatic fields exist between these wires and nearby grounded objects.

The spray enters these fields at the high-potential end, the particles become positively charged, and are attracted at high velocity to the grounded object. Dispersion and waste of the finishing material is eliminated and the time required for the operation considerably reduced. Normal current in the high-voltage circuit due to ionization of the air surrounding the wires is approximately 10 ma.

The danger of fires or personnel accidents is relatively slight because there is no tendency to "spark" in an atmosphere laden with coating particles. However, fires can be started by failures in electrical equipment or unpredictable accidents, so two methods of protection are used.

A constant-voltage transformer in the power-line circuit reduces hazards due to possible line-voltage fluctuations; and a special protector unit guards against sparking in the high-voltage circuit. Current is supplied to all operational units through a five-pole magnetic contactor. The holding coil of the contactor is energized through a thyratron, operated from a small auxiliary power supply. When a dangerous increase occurs in the normal 10-ma current the thyratron fires, opening the holding circuit of the five-pole contactor and energizing a two-pole relay which actuates a warning bell and a signal light on the spray-booth control panel. If a failure should take place in some component of the spark guard, work would be halted the same as if a sparking condition existed; but, when repairs cannot be made in a reasonable time, a locking switch can be utilized to bypass the spark guard, permitting operations to continue on an emergency basis.

Articles which are being electrostatically finished are usually grounded via metallic fixtures or metallic conveyor units, on which they are mounted for movement through the spray booth. In some cases, difficulties have been experienced due to the tendencies of certain nonmetallic articles to resist the influence of a negative charge; and it has occasionally been found that such articles can possess an inherent degree of polarity which will actually repel the sprayed coating particles. As a rule these difficulties can be overcome if nonmetallic articles are reinforced with strong metallic conductors during the finishing process.

Coating materials are usually thinned with solvents to minimize the sizes of sprayed particles, thus facilitating polarization, and to maintain the "wetness" of the particles during the relatively long time interval that may elapse before they are attracted by a grounded surface. Spray guns are carefully regulated for low atomizing pressures (about 15 to 30 pounds per square inch), and are rigidly mounted.

Generally speaking, two or more spray guns are simultaneously operated in each electrostatic spray booth. Each is positioned at least 12 inches away from a discharge electrode, and aimed so that its output will be almost parallel to the direction of conveyor travel—directly coating articles which are two or three feet distant.

Electrostatically coated articles are usually conveyed past a bank of infra-red lamps for rapid drying action. In some cases they may receive a preliminary infra-red heat treatment to remove greases and other fluids which might prevent the adhesion of coating materials.

The normal operations of an electrostatic spray booth are started and stopped by means of a simple push-button switch on the control panel.

A variation of the electrostatic spraying technique is the process known as "electrostatic detearing," recently developed by Ransburg Electro-Coating Corp. It consists of dip-coating and draining an article in a conventional manner, then (by means of a grounded conveyor) passing the article over a high-voltage grid so that electrostatic influences will remove the unsightly "tear drops" which would not ordinarily drain from the lower edges of a dip-coated product.

Several manufacturers are currently reported to be in the process of developing "dry electroplating" techniques, in which pneumatic metallizing guns may be used to atomize molten alloys so that the latter can be sprayed on both metallic and nonmetallic articles via the ionizing wires of a discharge electrode. However, despite the fact that suitable spray guns are known to be available, no accomplishments in this category have yet been announced.

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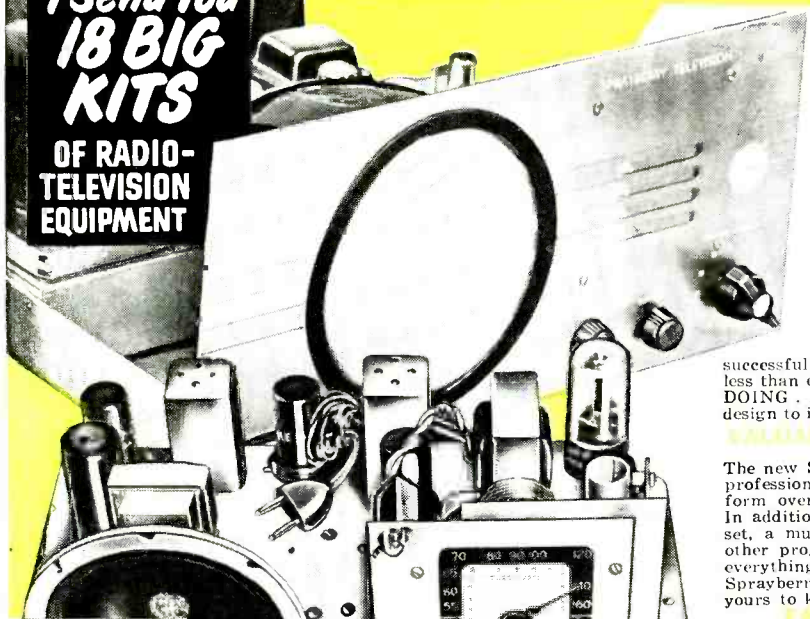
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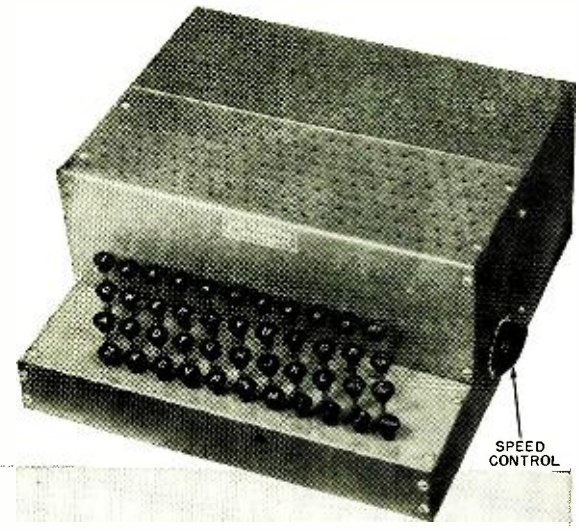
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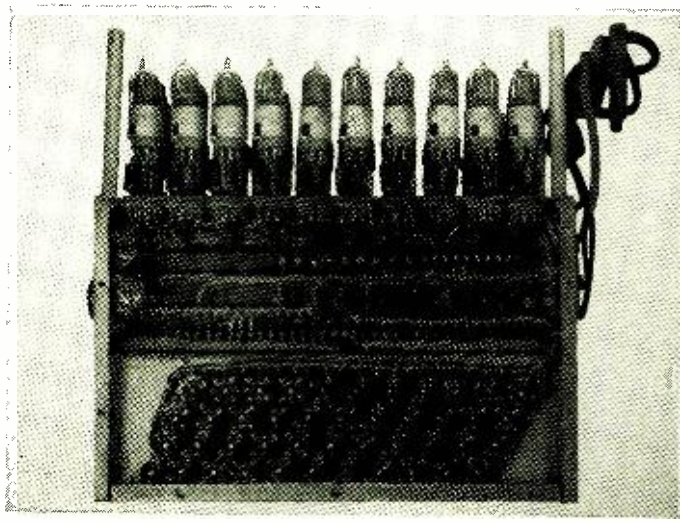
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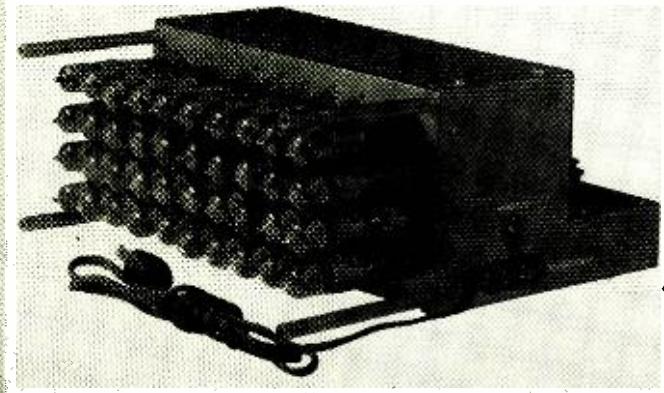
CODETYPER

How computer-type circuits automatically form Morse Code characters.

By NATHANIEL G. A. DORFMAN







These three views of the Codetyper show its external resemblance to a standard "mill," and some of its unique constructional features. Plug-in cell units for all tube circuits provide complete accessibility and allow instant replacement.

THE dream of every amateur radio operator (and many professionals) —a perfect "fist"—may become a reality with the development of the *Codetyper*. Automatically translating the characters of a standard typewriter keyboard directly into perfectly formed and spaced dots and dashes, it may also benefit commercial circuits. By eliminating personal idiosyncrasies from code transmission it may enable consistent, errorless reception under difficult receiving conditions.

The Codetyper incorporates many of the counter and gating circuits used in recent electronic computing devices. Although no larger than a portable typewriter, it contains 40 miniature tubes, power supply, and all wiring and control circuits. (See photographs)

The dots and dashes of the code are formed by a series of on-off switching oscillators called "unigenerators." Each unigenerator is a cathode-coupled multivibrator with one stable state. The schematic of a typical unigenerator stage is shown in Fig. 1-a, and operating waveforms are shown in Fig. 1-b. V1 and V2 in the discussion below may refer to two separate tubes, or—as in the unigenerators—the two halves of a 6J6 dual-triode.

In the stable condition V2 is made to draw heavy plate current by applying a positive voltage to its grid from the voltage divider R1-R2. The plate of V2 is thus effectively shorted to its cathode. V1 is completely cut off by the large bias voltage developed across the common cathode resistor R4 by the plate current of V2. Thus the plate of V1 is at full B-plus voltage. Capacitor C is charged to the difference in voltage between the plate of V1 and the grid of V2, with the polarities shown in Fig. 1-a.

The unigenerator remains in this condition until a large positive pulse from an external source applied to the grid of V1 overcomes the cutoff bias from the cathode resistor. The resulting flow of plate current in V1 produces several effects simultaneously, shown graphically in Fig. 1-b.

1. The internal resistance of V1 falls to a very low value, effectively shorting its plate and cathode.

2. Capacitor C discharges rapidly through R3, R2, R4 and the low internal resistance of V1.

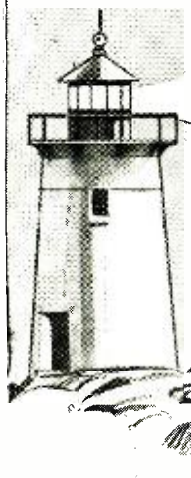
3. The heavy flow of electrons from the grid end of capacitor C to ground during this discharge is in the opposite direction to the flow of bleeder current through R2, and cancels the positive voltage on the grid of V2.

4. V2 is now cut off by the bias across cathode resistor R4 developed by the plate current of V1, and its plate is at full B-plus voltage.

Normal conditions in the unigenerator are now reversed. It will remain in this state until the grid end of capacitor C again charges to a positive voltage through R2. The instant this positive voltage overcomes the cutoff bias on V2, the unigenerator reverts to its original condition. The time of this recovery depends on the product of R3 and C, and on the positive voltage required. Since R3 and C are fixed, the

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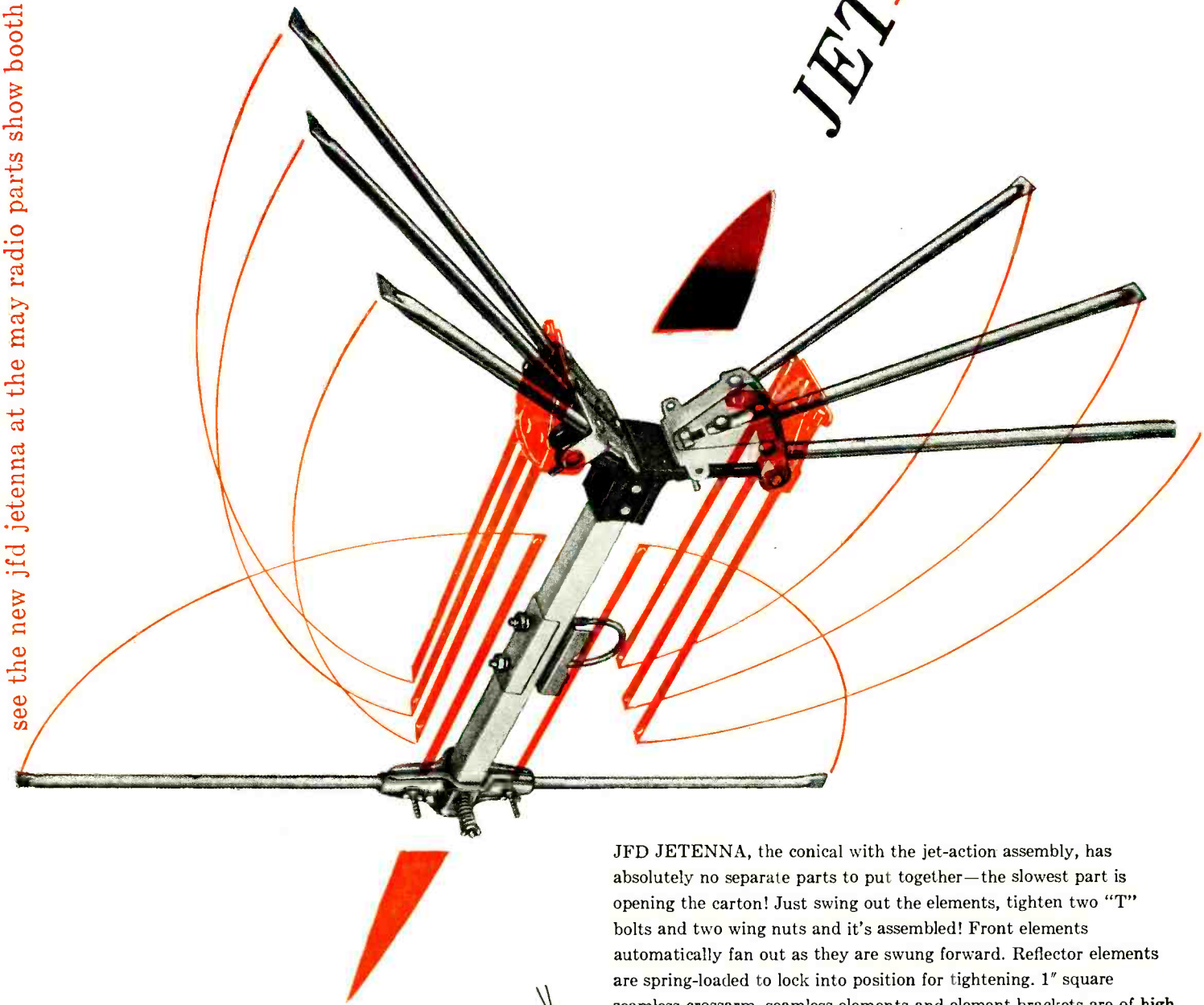
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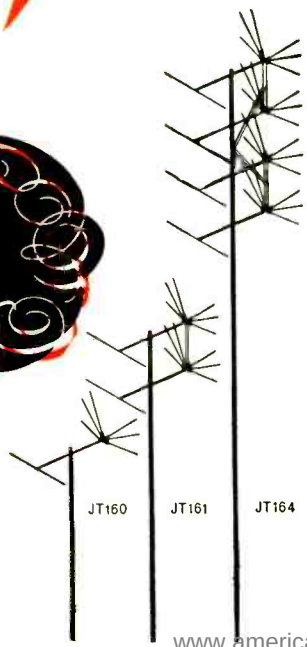


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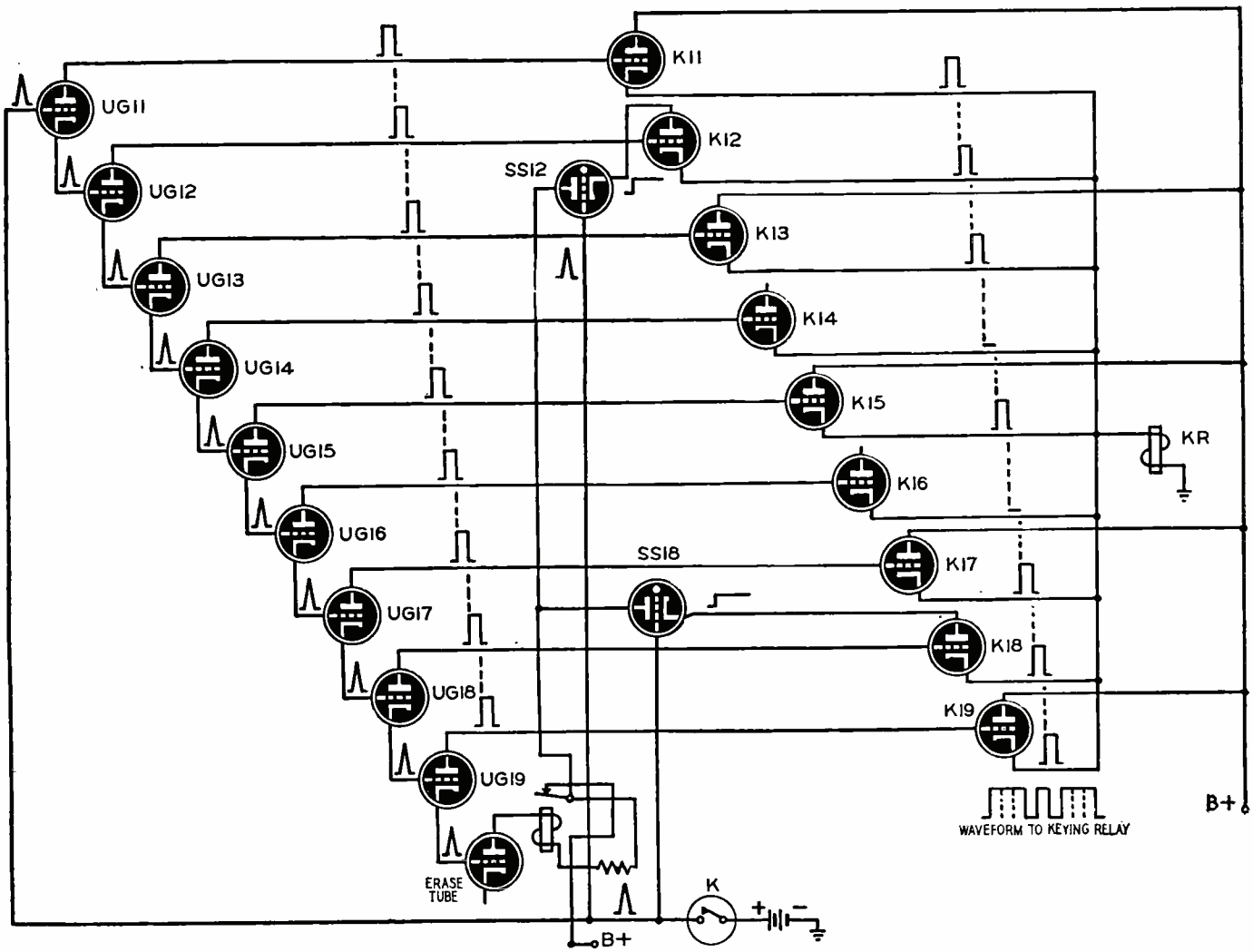
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Functional diagram of the Codetyper, showing the components and circuitry involved in automatically transmitting letter "K".

recovery time can be varied by an adjustable positive-bias control (R2).

The waveforms of Fig. 1-b show that a positive square wave appears at the plate of V2 each time a positive pulse is applied to the grid of V1. At the same time a negative square wave appears at the common cathode point, since V1 is adjusted to draw slightly less plate current than V2 when conducting.

Nineteen code components

The Codetyper utilizes a chain of 19 identical unigenerators to produce up to 19 successive square waves. Each succeeding stage is triggered from the cathode of the preceding stage through a differentiator circuit which converts the leading and trailing edges of the square waves to negative and positive pulses. The negative pulse has no effect, since the tube to which it is applied is already biased beyond cut-off. The positive pulse overcomes the bias, and triggers the unigenerator.

If the starting trigger pulse is applied to the input of the first unigenerator in the chain, square waves will appear *in succession* at the outputs of each of the 19 stages. Fewer than 19 successive square waves are obtained by applying the starting pulse to the input of the appropriate unigenerator stage. Individual compensating adjustments in each stage (not shown in Fig. 1-a) permit equalizing the widths and amplitudes of all 19 outputs. A common adjustable positive bias for all stages controls recovery time (keying speed).

The positive square wave from the output plate of each unigenerator is applied to the grid of its associated *keying tube*. The cathodes of all 19 keying tubes are connected in parallel, and return to B-minus through the coil of the keying relay. The odd-numbered tubes are connected to plus-B and are biased to cutoff, so that the keying relay is not energized without signal. The plate of each even-numbered keying tube is connected to B-plus through a "sequence-selector" thyratron which is normally nonconducting. Thus an odd-numbered keying tube requires only a positive square wave on its grid from its associated unigenerator to make it conduct fully and energize the keying relay. An even-numbered keying tube, however, requires not only the grid square wave but also a conductive sequence-selector to energize the keying relay.

In the International Morse Code the basic timing unit or interval is the duration of one *dot*. A *dash* has a length of three intervals, and the *space* between dots or dashes within a character is equal to one interval. The Codetyper has only two states. It can transmit a dot (marker) or a blank interval (space). If none of the sequence-selectors are activated, a voltage applied to the first unigenerator will cause each alternate keyer tube to act in turn, sending a series of dots separated by spaces. The sequence-selectors cause a space to become a dot, and therefore permit sending three dots with no interval between them. This is a dash. Thus the three elements of the code—dot, dash, and space—become two, and can be handled by an on-off device.

Odd and even intervals

Since dots and dashes represent *odd* numbers of intervals (1 and 3) spaces within a character will always occur on even-numbered intervals. For example, the letter "L" contains a total of 9 intervals:

1	2	3	4	5	6	7	8	9
DOT		DASH				DOT		DOT

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The numeral "5" also contains 9 intervals:

1	2	3	4	5	6	7	8	9
DOT		DOT		DOT		DOT		DOT

The longest single character (the numeral "zero") contains 19 intervals:

1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19
DASH		DASH		DASH						DASH						DASH		

A special "error" signal, consisting of 10 dots and 9 spaces, also contains 19 intervals:

1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19
DOT	DOT	DOT	DOT	DOT	DOT	DOT	DOT	DOT	DOT	DOT	DOT	DOT	DOT	DOT	DOT	DOT	DOT	DOT

Thus in transmitting characters consisting only of dots, (E, I, H, S, 5, and the error signal) the even-numbered intervals are not keyed. In transmitting characters containing dashes, only the even-numbered intervals falling in the middle of a dash are keyed. Fig. 2 shows how this principle is utilized in the operation of the Codetyper in transmitting the letter "K".

1	2	3	4	5	6	7	8	9
DASH				DOT		DASH		

Since the letter "K" contains 9 intervals, only the last 9 unigenerators in the chain of 19 are required. The starting trigger pulse must be applied to the input of unigenerator 11. Thus only keying tubes 11 through 19 will receive positive pulses on their grids, as shown below.

Unigenerators / Keying tubes	11	12	13	14	15	16	17	18	19
	DASH				DOT		DASH		

Since no keying is necessary for the spaces 14 and 16, only even-numbered keying tubes 12 and 18 are required to conduct through their associated sequence-selector thyratrons. All the units involved are shown below:

Unigenerators	11	12	13	14	15	16	17	18	19
Keying tubes	11	12	13	14	15	16	17	18	19
Sequence selectors Conducting		12						18	
	DASH			DOT			DASH		

Striking the letter "K" on the keyboard closes a switch which applies a positive voltage to the control grids of sequence-selector thyratrons 12 and 18, and to the input grid of unigenerator 11. This part of the equipment, known as the "phantom switch network," is a form of coder (function table, matrix). The principle of these devices is described in the series "How an Electronic Brain Works" (Berkeley and Jensen) Part XII, RADIO-ELECTRONICS, September, 1951. Briefly, a coder is a device with which a single-pole, single-throw switch can actuate a number of circuits, and other similar switches can actuate some of the same circuits together with others, making it possible to have a large number of combinations with a practical number of switches. Thus any one of the combinations described above may be thrown into action by pressing a single key switch on the typewriter-like keyboard.

With the exception that neon lamps are used instead of the rectifiers, the phantom switch network is much like that shown in the article in the September, 1951, RADIO-ELECTRONICS.

Releasing the key removes the voltage placed on the grids, but the following sequence of events has already taken place:

Conduction has started through sequence-selectors 12 and 18, connecting the plates of keying tubes 12 and 18 to B-plus. (Removal of the positive voltage from the thyratron control grids cannot stop conduction.)

The voltage at the output plate of unigenerator 11 has jumped from nearly zero to full B-plus, thus applying a positive pulse through the coupling capacitor to the grid of keying tube 11. The flow of plate current through this keying tube energizes the keying relay. The voltage at the cathode of unigenerator 11 has dropped to a lower value, applying a negative pulse to the input grid of unigenerator 12. This negative pulse, however, has no effect, since the input triode section of unigenerator 12 is completely cut off.

After a recovery time determined by the setting of the speed control, unigenerator 11 reverses, its output plate voltage falls, and its cathode voltage

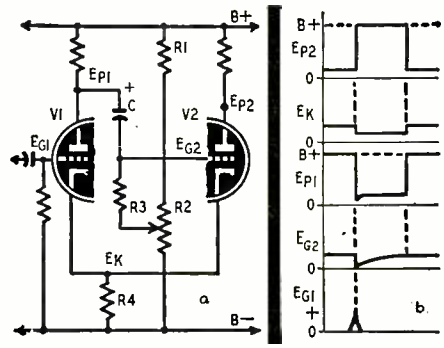


Fig. 1—Basic unigenerator circuit, with waveforms produced by an input trigger.

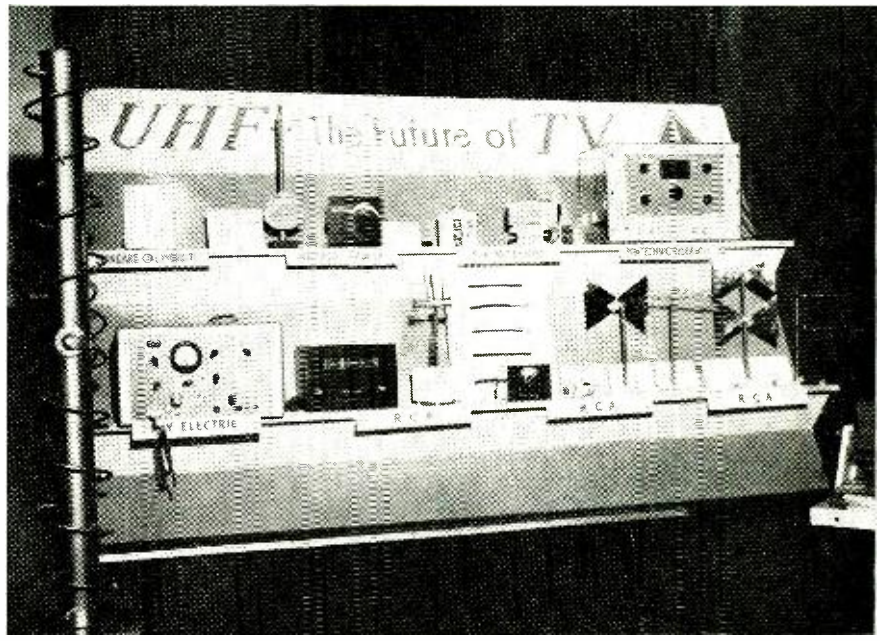
rises to the original value. The rising cathode voltage transmits a positive pulse through the differentiator circuit to the input of unigenerator 12, overcoming the cut-off bias and triggering this stage in the manner described above. Since there is no appreciable delay between the fall in voltage at the plate of unigenerator 11 and the corresponding rise at the plate of unigenerator 12, keying tube 12 conducts and holds the keying relay closed when keying tube 11 is cut off.

The series of pulses continues successively down the chain, keying tube 13 holding the relay closed when keying tube 12 releases. However, keying tubes 14 and 16 have no B-plus voltage, since their sequence-selector thyratrons were not energized, and the keying relay opens during these intervals.

The final positive pulse from the cathode of unigenerator 19 is applied to the grid of the "erase" tube. The resulting flow of plate current energizes the erase relay, and removes B-plus voltage from the sequence-selector tubes. After a short time delay, controlled by the value of the resistor in series with the erase relay coil, the erase circuit recloses. With B-plus voltage again applied to their plates, the sequence-selector thyratrons are reactivated in preparation for the next character to be transmitted.

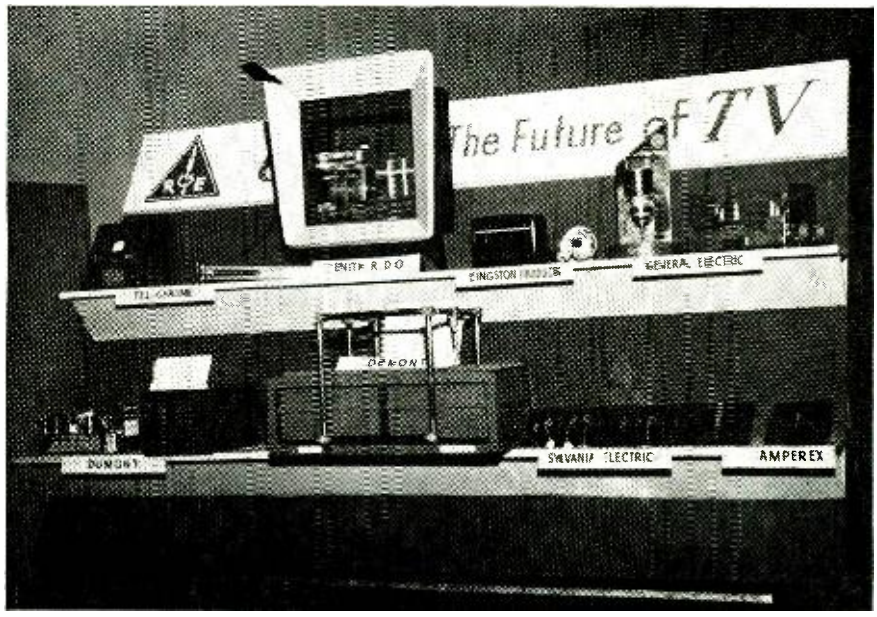
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I. R. E. FACES THE FUTURE

U.h.f. was the dominant feature of this year's I.R.E. meeting



A two-bench display of converters, tuners and other equipment for u.h.f. television.

"I.R.E. Sets the Pace" was the official slogan at the 40th I.R.E. convention, held in New York City March 3-6. Underneath the official slogan, and pervading the whole convention was an unofficial one: "It's u.h.f. again this year—but this time we mean it," which was never put officially into words, but was felt in spirit in most conversations, conferences, papers and displays.

The 40th anniversary convention was the most successful in the history of the Institute. More than 29,000 engineers were registered, as compared to a little less than 23,000 last year. The Radio Engineering Show which always forms a part of the meeting showed a spectacular increase as well, with 356 exhibits against last year's total of 276. Exhibits, which last year occupied three floors of New York's Grand Central Palace, with plenty of room on the third floor, now crowded four floors—a veritable World's Fair of electronics.

The feeling that the freeze on u.h.f. TV broadcasting was about to be lifted did indeed give a mighty impetus and direction to the proceedings. At the preconvention press conference the biggest collection of u.h.f. converters and tuners on record was displayed. These will make it possible to receive the new u.h.f. stations on old receivers, and assure that new sets can be built for the high frequencies without further delay, once there are u.h.f. transmitting stations to send out programs.

U.h.f. played a large part in the technical sessions. Two sessions, at which nine papers were read, were devoted to the subject. G-E announced its new GL-6183, a ceramic 1-kilowatt air-cooled tetrode which gives full output

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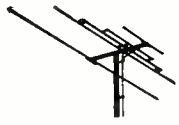
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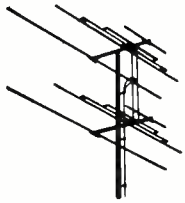
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HOW THE Q-TEE FUNCTIONS

by Sydney E. Warner, VEE-D-X Chief Engineer



The Q-TEE is a new engineering approach to the all-channel TV antenna problem. Entirely new in design, this antenna incorporates a revolutionary feature, Electronic Channel Separators. The result is a unique antenna with better gain and directivity, higher front-to-back ratio, greater ease of assembly, increased mechanical strength and better appearance. Figure 1 shows the basic antenna assembly. On the low channels, elements (A-A) form a half-wave dipole, with elements (B-B) as the reflector. On the high channels, elements (C-C) form a full wave dipole with elements (E-E) as a half-wave director.

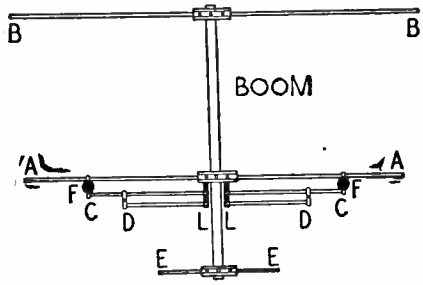


Fig. 1

Isolation filters (F-F) are anti-resonant at the center of the high channels (195 mc) and isolate the low channel dipole (A-A) from the high channel dipole (C-C). The center matching and phasing section performs a dual function and accounts for the unique operational characteristic of this antenna. In the high channels elements (D-D) are "T" match sections which tap the dipole (C-C) and provide a 300 ohm termination at (L-L). The high channel antenna is, therefore, a full wave antenna "T" matched, with a half-wave director. On the low channels the isolation filters (F-F) have a low impedance (inductive) since they operate below resonance. The high channel dipole (C-C) combined with element (D-D) form a double "T" match which taps dipole (A-A) to provide a 300 ohm termination at (L-L).

Fig. 2

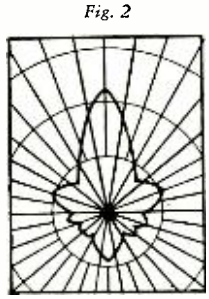


Fig. 3



The close proximity of (A-A), (C-C) and (D-D) provides a driven element with very low "Q". This low "Q" in effect represents a driven element of a large electrical diameter and which in turn accounts for the broad (all-channel) frequency characteristics of the antenna.

Figures 2 and 3 show the horizontal directivity pattern of the Q-TEE. Note that the directivity is quite pronounced. The front-to-back ratio on the low channels will run from 6 db to as high as 12 db. This is an important consideration in those areas where co-channel interference problems exist. On the high channels, the front-to-back ratio is as high as 8 db on the center of the band.

The directional characteristics of the antenna give less noise pickup since signals off the side and back are rejected to a much greater degree than they are in a conical type antenna. Conicals designed for good response on the high channels are poor on the lows, while those designed for the low channels are poor on the highs. Q-TEE does not have these limitations.

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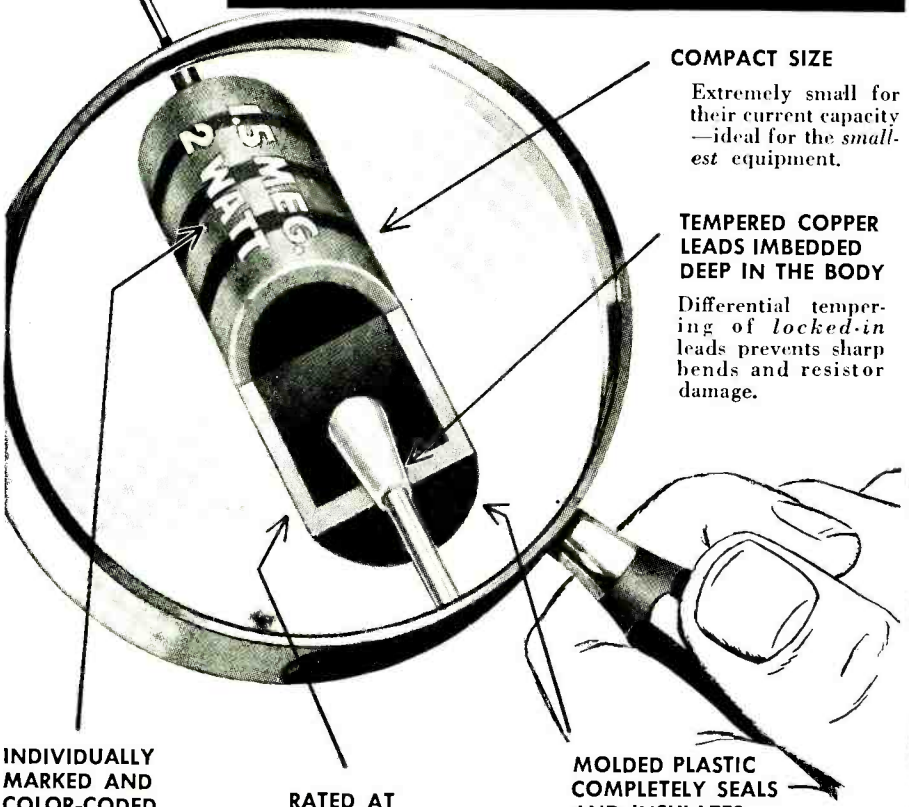
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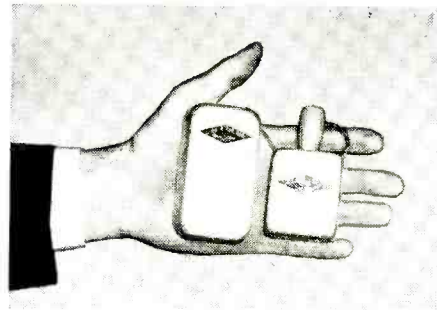
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at 900 megacycles. This is an air-cooled version of the 6039 introduced last year. RCA reported on an experimental triode with a power output of 5 kilowatts. Other transmitter problems of the ultra-highs were discussed, as well as types of antennas for the spectrum.

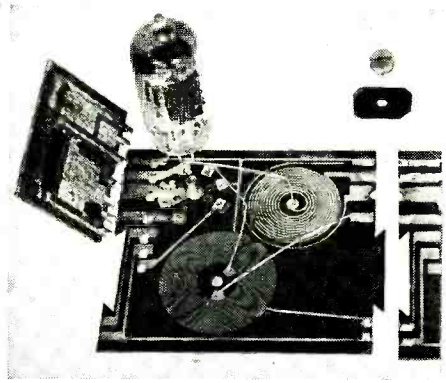
A number of completely new classi-



The Stephens Radio Link transmitter.

fications appeared on the program. One of these was the session *Subaudio Instrumentation*. The name was new but the subjects discussed were vibration testing, oil prospecting by underground sound (and subsound), and other subjects already familiar to the engineer.

A second subject, which had been discussed at previous conventions, occupied two full sessions of this one. The subject was *Information Theory*. Engineers pointed out that by transmitting only those portions of a message—or even a television picture—that could not be predicted in advance, equipment and spectrum space might be used more efficiently. Besides transmitting new material, it would be nec-



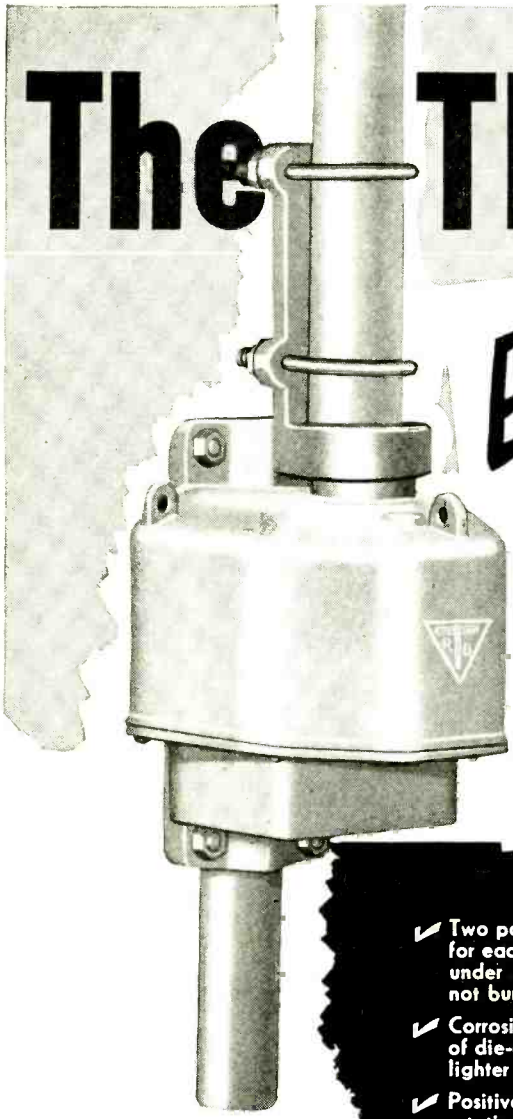
Sylvania appliquéd-circuit unit, with part of second showing snap-in system.

essary to send signals representing the difference between the signal predicted by the receiver and that actually transmitted, when such "error" should occur. This subject borders closely on another important one—that of computers, since a "memory" is necessary to assemble material received and from it to predict what will come.

In spite of the ban on color broadcasting, color was one of the important features of the convention. A complete session and an evening symposium were devoted to it, and the subject was touched on in other papers. One of the most popular exhibits at the show was Columbia's demonstration of an all-electronic CBS color broadcasting sys-

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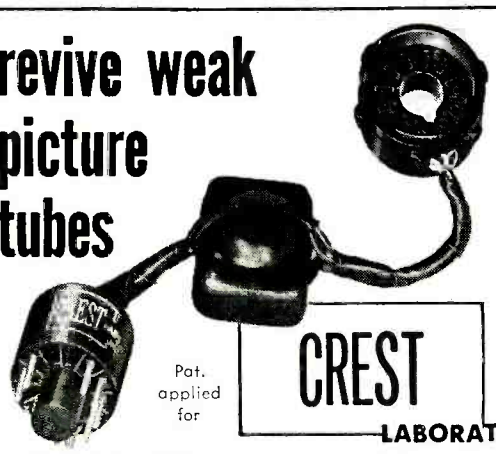
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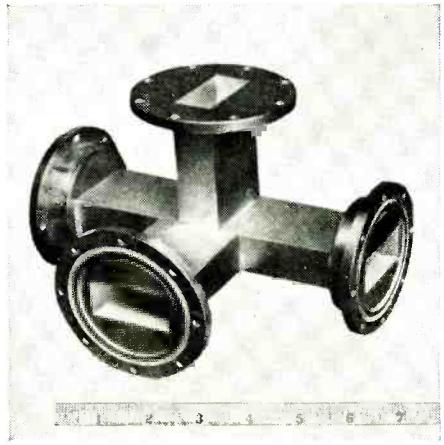
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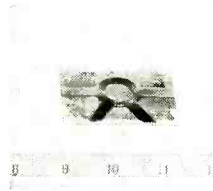
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tem. Though Columbia has always pointed out that its system will work with a three-color tube at least as well as any other, opposition publicity has so linked it with the "mechanical color wheel" that the public was surprised. Even engineers, who should have seen that it was theoretically inevitable, formed long lines to the demonstration room, to see with their own eyes that CBS was an electronic system.

Possibly the most interesting announcement of the convention was that of a new system of microwave wiring. Engineers of the Federal Telecommunication Laboratories described a transmission line consisting of a metal ribbon separated from a larger metal plate or ground plane by a thin layer of plastic. Such ribbons, they stated, could replace waveguides costing many times as much and whose weight and size are so vastly different as to make comparison impractical. The theory is that the strip or ribbon forms an electrical image of itself in the ground plane, and that therefore any irregularity is matched in its image. This makes an absolutely symmetrical line without the careful machining to close tolerances required in waveguide manufacture.





Comparison between standard Magic-Tee and the same unit in Federal's new microwave wiring.

A number of special fittings were shown, including a *magic tee* which was shown along with its waveguide equivalent. The one weighed 15 pounds and cost $200; the latter weighed an ounce and cost less than a dollar.

Bell Laboratories also demonstrated a new type of u.h.f. transmission line which was simplicity itself. Unlike the simple u.h.f. line shown by George Goubau last year (which was just a piece of wire) this was a rod of insulating material. A quartz, polystyrene, or other excellent insulator will guide radio waves at 48,000 mc (48 kmc, as the authors of the paper put it). It has an advantage over waveguides, as even the small guides used at that frequency (a little thicker than a soda straw) are rigid. Where a

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The TV Booster may be considered a dam of power. In ordinary boosters, this power may spill over, thus overloading the tube and setting up noise or "snow." In an attempt to avoid this, ordinary boosters do not make use of maximum possible gain.



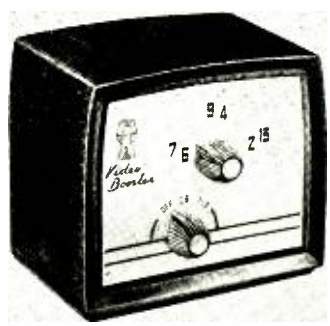
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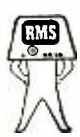
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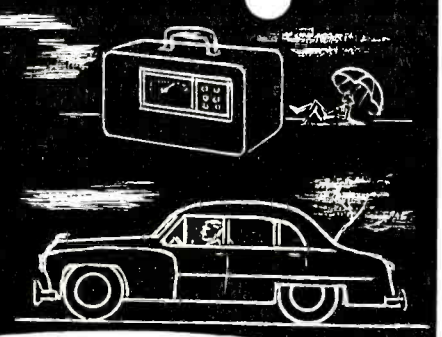
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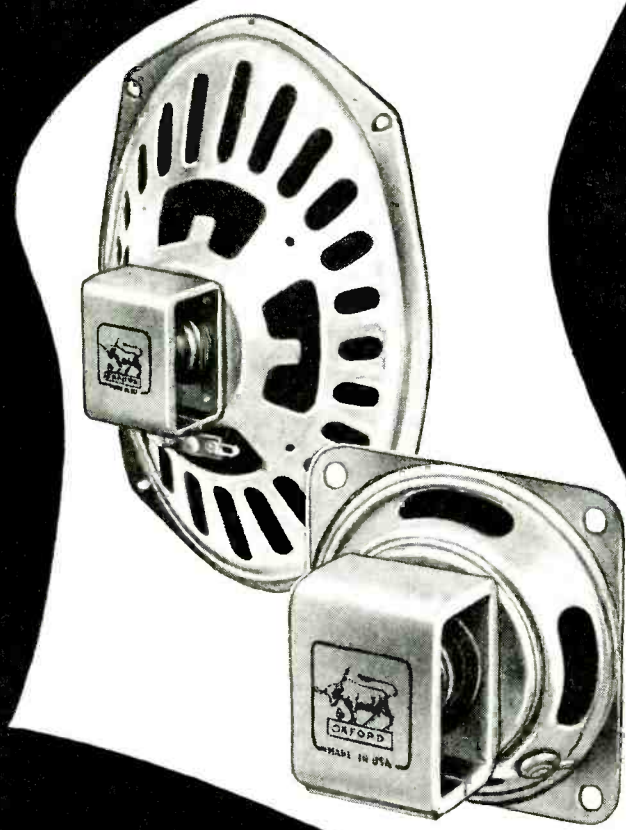


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curved guide is needed, a polystyrene "waveguide" can be bent into the required shape readily.

Another important report by Bell was on work in receiving u.h.f. signals at points far beyond the theoretical line-of-sight. Signals of 500 and 3,700 mc were received *reliably* at a distance of 285 miles. Reliable reception means to a communications engineer that he can be sure of hearing a signal when he turns on the receiver. Weather and frequency seem to have had little effect on reception at these frequencies.

While the signals were very weak, they were very much stronger than predicted by theory. This indicates that our propagation theory is incomplete and that there are factors hitherto unsuspected.

The vest-pocket transmitter came into its own in the Stephens Radio Link, illustrated on page 76. It is an FM transmitter for actors' use on TV or movie stages. Frequency is about 50 mc, and reliable range 30 feet.

Other subjects which received much more attention than at previous conventions were transistors and medical electronics. The latter had a full session devoted to it for the first time. Treatment by microwave diathermy was the subject of one paper. The author pointed out that it is much more easily controlled than ordinary short-wave diathermy. Another paper described the use of color television in connection with ultraviolet microscopy. Since different types of tissues reflect different portions of the ultraviolet spectrum more strongly, the spectrum itself can be divided into three parts, each one of which is assigned a color. Then otherwise barely distinguishable differences show up clearly.

Discussion on transistors was a normal advance on that of previous years, and as such was not dramatic. The crystal diode also received some mention, in a paper describing its action at very low voltages. A paper on a barium titanate amplifier (RADIO-ELECTRONICS, February, 1952, page 92) was read. This device, whose action resembles that of a magnetic amplifier more than of a transistor, is as yet a novelty.

Printed circuits appear to have come into their own. Only one paper on the subject appeared, though some equipment used printed circuits where expedient, without bothering to mention it. The one paper described printed i.f. subassemblies for television. Using both silk-screen and photographic etching, a complete i.f. stage was placed on a card less than two inches square. Some of the resistors and capacitors were appliquéd onto a much smaller card mounted on the edge of the first. The tube was plugged into socket holes in the card, which was so shaped as to snap into preceding and succeeding stages. This system was presented by Sylvania, who, however, have no immediate plans for using it in production models. When that occurs, the service technician's dream of replacing whole defective stages, instead of trying to repair them, will have come true.

—end—

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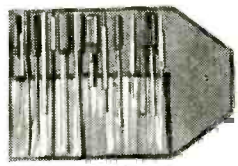
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NEW GLOW LAMP APPLICATIONS

Gas-filled tubes have certain characteristics which make them suitable as pulse counters. Unfortunately, a gas tube with one cathode and one anode can have only two stable states: conducting and nonconducting. Thus a counting decade needs as many as 10 ordinary glow lamps (see RADIO-ELECTRONICS, Dec., 1951, p. 91).

To simplify counter design, tubes are being designed with multiple cathodes (or anodes). Successive pulses trigger the tube from one element to the next. Thus a tube with 10 cathodes does the work of 10 ordinary tubes and can function as a complete decade all by itself. Two promising tubes of this type have been disclosed recently in Patent Office publications.

Fig. 1-a is the basic design of a tube invented by N. B. Wales, Jr.* It has an extended cathode K, a short anode F, and several probe-anodes P. Hydrogen at low pressure is sealed within the glass envelope. R controls the tube current and determines the extent of the cathode glow. Initially, R is adjusted so the glow rises to a height A. Only the KF gap is ionized.

*U.S. Patent No. 2,573,373, assigned to International Business Machines Corp., New York City.

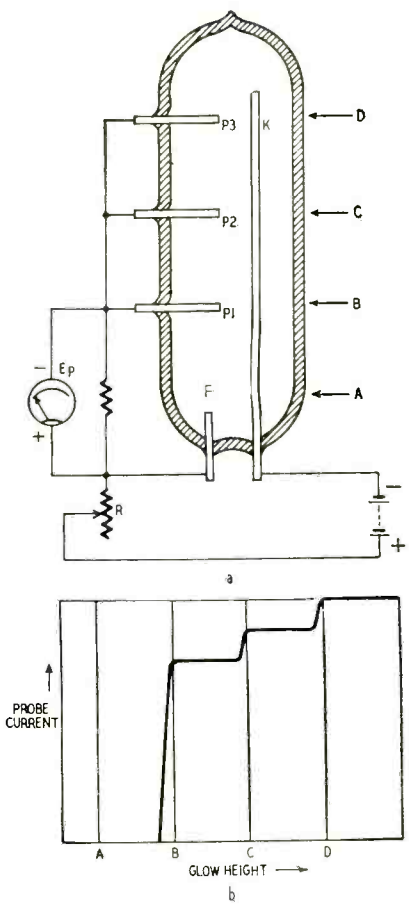


Fig. 1—Multiple-anode lamp and response.

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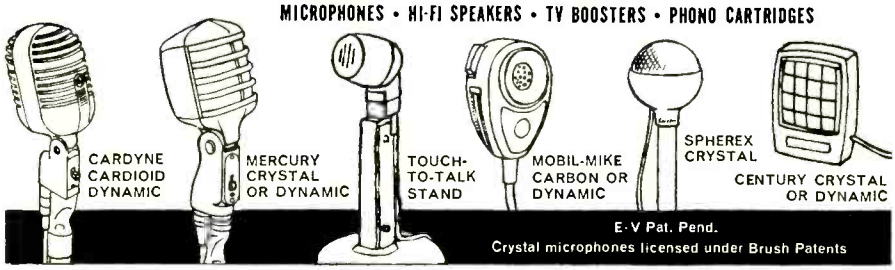
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If the resistance of R is reduced, more current flows between cathode and anode F. The glow spreads slowly and gradually. When it is close enough to P1, electrons can leap from the cathode to this probe-anode. Therefore this gap ionizes. The meter registers this probe current. Further decrease of R increases the glow height until it is close to P2. Then another abrupt change occurs. Fig. 1-b shows the variation of glow height *vs.* probe current. Note the nearly flat plateaus which break sharply near each probe element.

As a decade counter, the tube contains 10 probes. Also, R is replaced by vacuum tubes. See Fig. 2. V1, a pulse amplifier, normally operates near full conduction. V2 is a control tube which is biased near cutoff. The first *negative* input pulse triggers V1 more negative and V2 more positive. The internal resistance of V2 is momentarily reduced. The cathode glow, normally having a height "0," rises to "1." Probe current

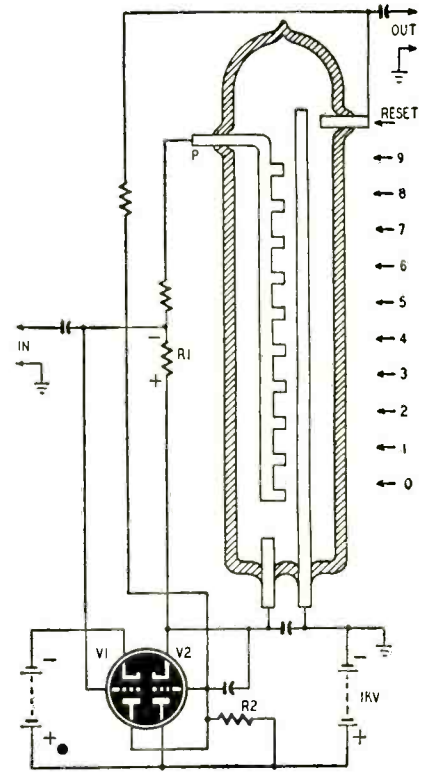


Fig. 2—Typical circuit using multi-anode glow lamp.

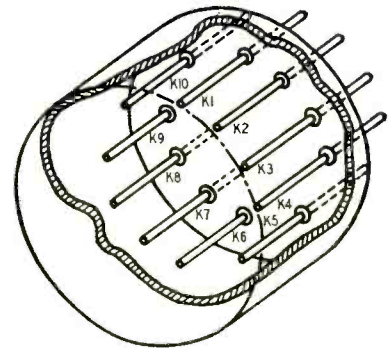


Fig. 3—Multi-cathode type of glow lamp for computer applications.

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through R1 biases V1 to *maintain* the glow at height "1." The next input pulse biases V1 further so that the glow reaches height "2," and so on.

The tenth pulse drives the glow to the "reset" element. Current flows through R2 to bias V2 to nearly cutoff. Probe current nearly disappears and causes the glow to slide down to "0." Now the tube is ready for the next decade of pulses.

Another multielement tube was recently invented by G. E. Hagen.** In several ways it appears to have better possibilities than the previous one. This tube has 10 cathodes arranged in a ring as in Fig. 3. The anode (not shown in this figure) is a circular bar adjacent to the cathodes. The tube is filled with helium. The ionizing voltage may be relatively low because the cathode-anode gaps are small and equal.

Each cathode K is associated with a rectifier D, a resistor R, and a capacitor (see Fig. 4). Electrons can pass downward through each rectifier, from its cathode to its anode.

Initially, assume that the glow discharge is between K2 and the anode. Therefore electrons flow through R2 to this cathode. A smaller current flows through R1, D1 to this same element. Still less current flows through R10, D10 and D1 to reach K2. In a typical case, K2 is 100 volts positive. K1 is 90, K10 is 80, and so on around the circle to K3 which is 10 volts above ground.

With application of a *negative* pulse to the anode, the discharge is interrupted momentarily, and the anode

**U.S. Patent No. 2,575,517, assigned to Northrop Aircraft, Inc., Hawthorne, Calif.

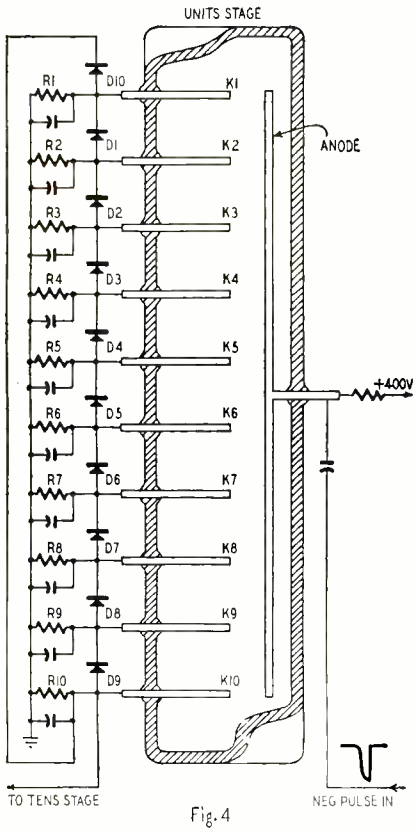
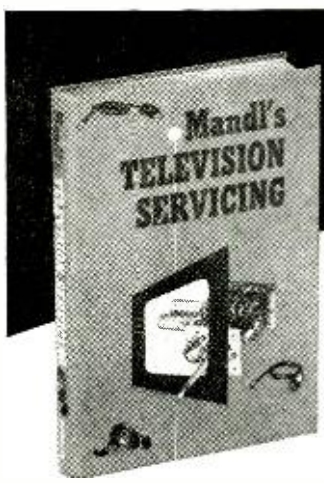


Fig. 4

Fig. 4—Application of multi-cathode lamp to a counter circuit.



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voltage starts to rise. The cathode capacitors maintain their charges for a short time. When the anode voltage is high enough, it ionizes the gap to whichever cathode has the lowest potential. At this time it is K3. After firing, the cathode potentials readjust themselves. K3 becomes 100 volts positive; K2, 90; K1, 80; and so on. In the same way, successive pulses fire K4, K5, and so on, in progression.

The ring arrangement of cathodes eliminates need for a reset element. At the tenth pulse K10 fires and transmits a positive pulse to the next (tens) decade. The eleventh pulse fires the K1 gap and the cycle repeats.

—end—

APRIL FOOL STORY FOOLED EVERYBODY

The printer joined in the fun when we published our annual April Fool story last month, with the result that we were fooled and the majority of our subscribers were badly puzzled.

As most of our old readers have already suspected, the last line of the story "Noise Neutralizer" by Mohammed Ulysses Fips on P. 53 of the April issue should have been: **April 1.** Then it would have followed the model of previous April stories by the same author.

The printer, while trimming some dead matter off the bottom of the page, worked up too far and trimmed off the heavy type at the bottom of the third column, which would have tipped off the reader as to the hoax nature of the story. The error was found and corrected, but only after many of the copies had been printed and shipped out.

Our sincere apologies to any readers who may have been puzzled by the omission. It was just one of those things we couldn't do anything about, as all the proofs were correct up to the very moment the presses began to roll.

CORRECTIONS

Frequency Meter

There is an error in the diagram of the frequency meter in Fig. 1 on page 25 of the February, 1952, issue. There should be a dot indicating a connection between the lead from pin 5 of the 6H6 and the lead between S1-d and the meter. With this connection made, the meter is connected between pin 5 and ground and is shunted by R2-R7, depending on the setting of the range switch.

We thank Mr. John Yannoulis, of Cairo, Egypt, for calling this to our attention.

John E. Pitts, W6CQK

In the article Useful Phone—C. W. Monitor, by John E. Pitts, which appeared in the January, 1952 issue of RADIO-ELECTRONICS, the author's call letters were erroneously given as W6CQP. This call has been assigned to Mr. Raymond Christian, 5543 Gables Street, National City, Calif. Mr. Pitts' correct call letters are W6CQK.

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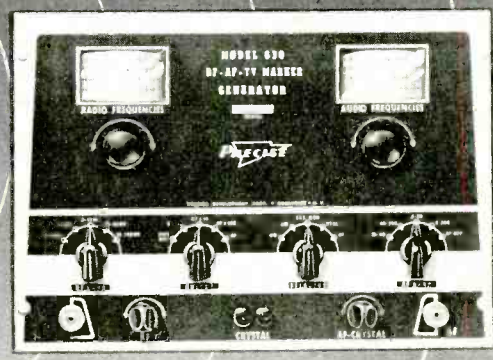
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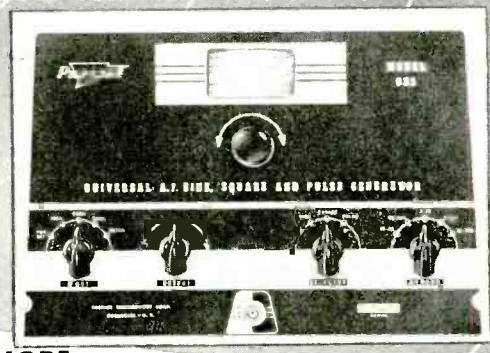
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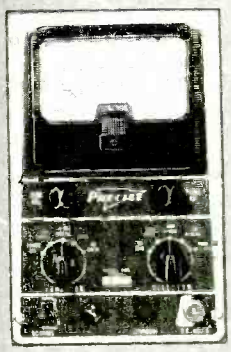


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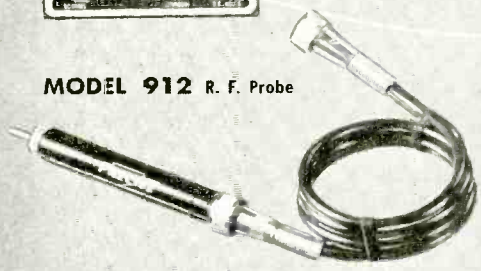
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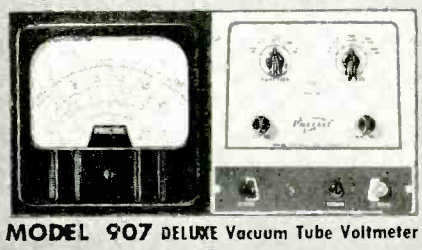




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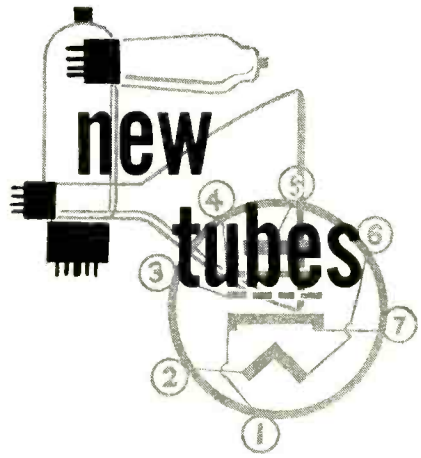
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Both types have screens 14⅜ x 10$^{13}/_{16}$ inches, with slightly curved sides and rounded corners; external conductive coatings; and require a single-gun ion-trap magnet. Maximum voltage ratings are: Ultor, 16,000 volts; grid 2, 500 volts; grid 4 (17LP4 only), 1,000 volts.

In the larger sizes, RCA is producing the 20MP4 and 21MP4 electrostatic focus types. Except for its over-all length and screen size (17¼ x 13¼ inches), the 20MP4 is identical in all respects to the 17LP4 described above. The 21MP4 is a metal-shell tube with a screen 18⅜ x 14 inches. Its electrical characteristics are the same as the foregoing types. All four picture tubes have standard RMA basing.

G-E has announced the GL-5QP4, a cathode-ray view-finder tube for high-accuracy focusing in television cameras. Developed for use with the "Eidophor" system of theater projection color television, the GL-5QP4 will also be used in all G-E-made TV studio cameras.

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Receiving types

G-E's new miniature power-output pentode, the 6BK5, is intended for use with the 6BN6 gated-beam limiter-discriminator (December, 1951, RADIO-ELECTRONICS, page 37). Its high power sensitivity and small grid driving volt-

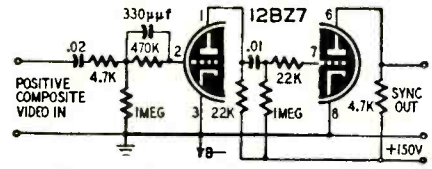


Fig. 1—Sync clipper-amplifier

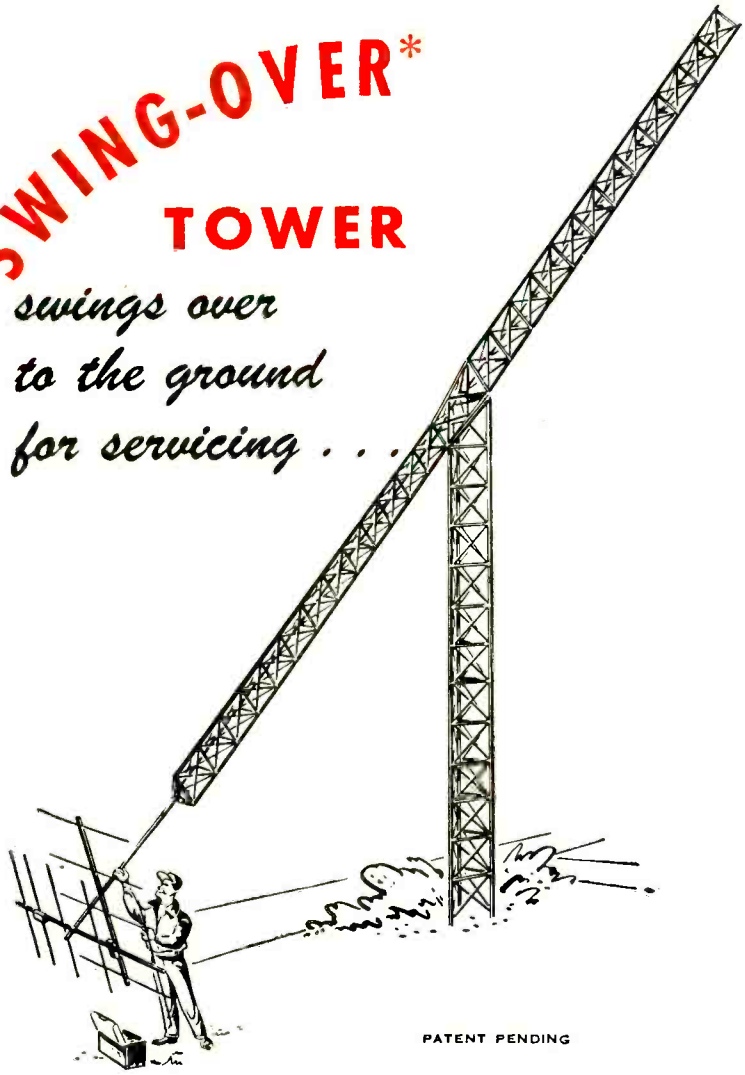
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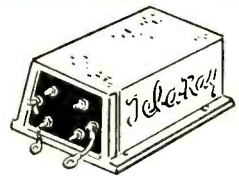
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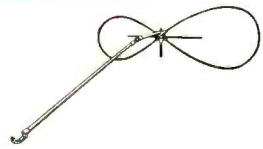
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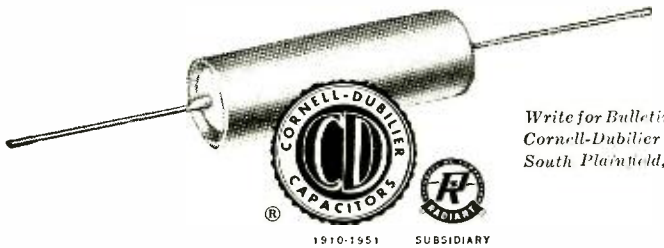
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age requirements eliminate the need for a first audio amplifier tube. The 6BK5 can deliver 3.5 watts output with a grid signal of only 5 volts peak.

Another G-E tube is the 6BX7GT, a twin-triode combined vertical-oscillator and amplifier. It provides improved linearity and high output at reduced B-plus voltages.

CBS-Hytron has announced four new miniature tubes for television. The 12A4 is a high-perveance triode vertical deflection amplifier. Operating data: Heater voltage and current: 6.3 v at 0.6 amp (parallel connection); 12.6 v

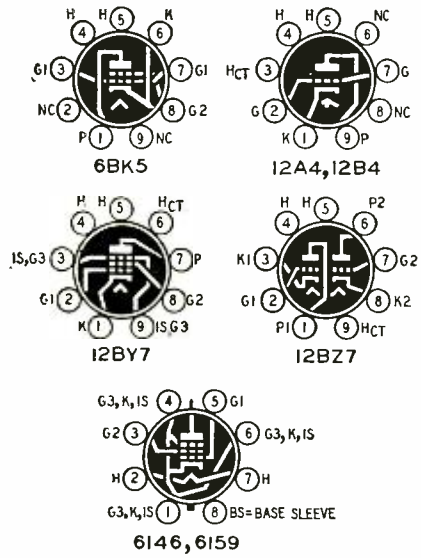


Fig. 2—Basing of tubes described in text.

at 0.3 amp (series connection); plate voltage, 250 v; plate current, 15 ma; cathode bias resistor, 560 ohms; peak-to-peak grid signal, 25 v; peak-to-peak sawtooth current in yoke, 360 ma.

The 12B4 is a triode vertical sweep amplifier with smaller output capabilities than the 12A4.

Type 12BY7 is a high-transconductance pentode video amplifier providing improved contrast linearity. Typical operating conditions for the 12BY7 are: Plate voltage, 250 v; plate current, 24 ma; screen voltage, 180 v; screen current, 5 ma; Gm, 12,000 micromhos; cathode resistor, 100 ohms; suppressor grid connected to cathode at socket. The heater is designed for either series or parallel operation.

Type 12BZ7 is a high-mu dual triode intended for use as a sync separator-amplifier. A typical schematic recommended by the manufacturer for this application is shown in Fig. 1.

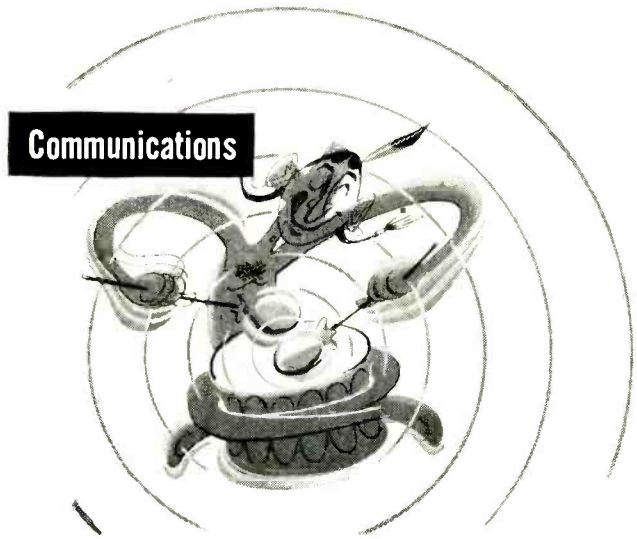
Transmitting and special tubes

RCA has announced the 6146 and 6159, improved beam power tubes for low-power v.h.f. transmitting applications. Differing only in heater ratings (6.3 volts for the 6146 and 26.5 volts for the 6159) their ICAS ratings are 90 watts input up to 60 mc, and 60 watts input at 175 mc.

—end—

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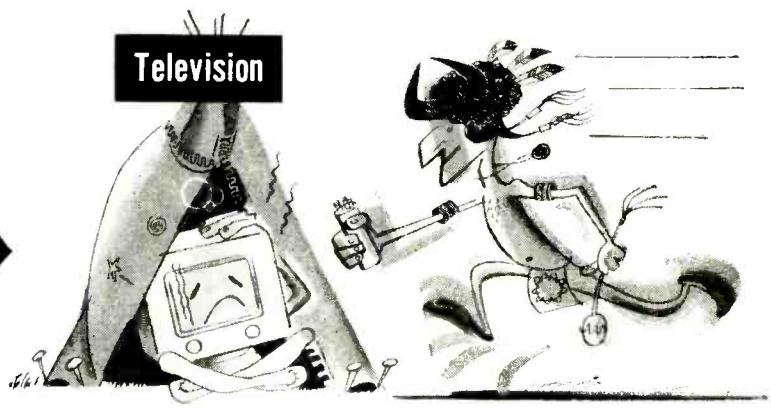




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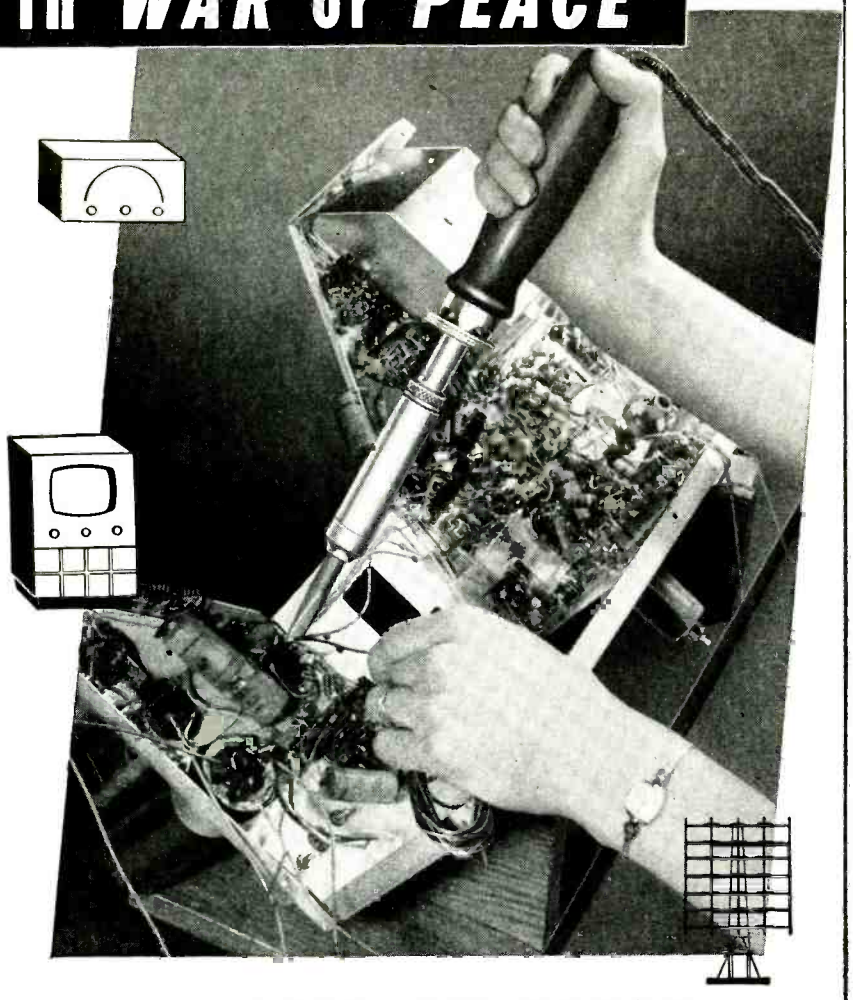
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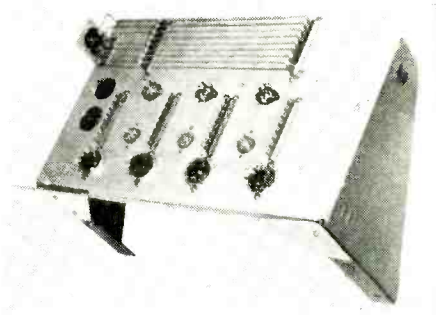


Fig. 1—The assembled breadboard chassis, showing the placement of tube sockets, terminal strips, bus bars, and power connector. The end wings of the aluminum control panel, which is bent outward at an angle of 30°, so that it appears practically invisible in the photo, are seen near the bottom.

EXPERIMENTER'S BREADBOARD

By H. L. REMLEY

A phone call from a friend, asking just what values to use in making a multivibrator with a given pulse width, brought the reply, "Why not set up a simple multivibrator circuit and find out just exactly what you want?" He replied that it would entail a lot of work and he had just wondered if I knew, offhand, the values he sought. At this point he was invited over to see a simple solution to his troubles. We won't go into the multivibrator problem here but will describe one way to make such experimental setups as simple as possible.

Many devices have been described or manufactured to permit rapid assembly of experimental breadboard circuits, but for several reasons they did not appeal to this writer. A survey of recent literature, a search through shelves and junk boxes—and our deluxe breadboard was the result. In its main features, it is a simplified version of a job described in *Electronics* for July, 1949.

The complete breadboard assembly is shown in Fig. 1. The main chassis was made from an 8½ x 12½-inch aluminum panel. A right-angle bend, ¼ inch wide, was made on each edge for rigidity. Two 6½ x 8-inch standard

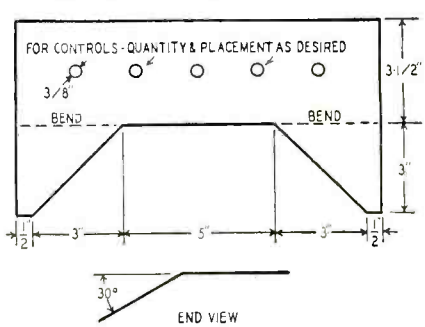


Fig. 2—Details of control panel strip.

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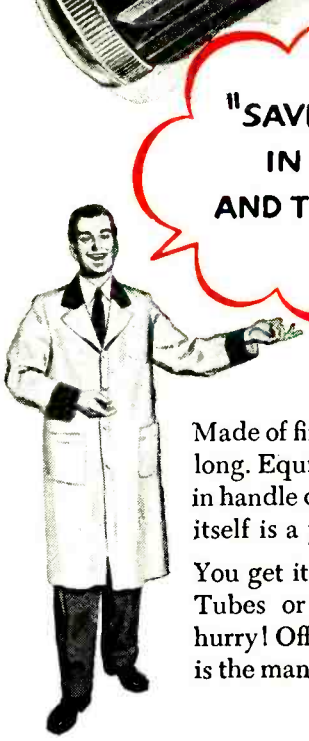
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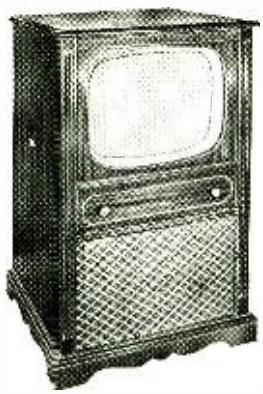
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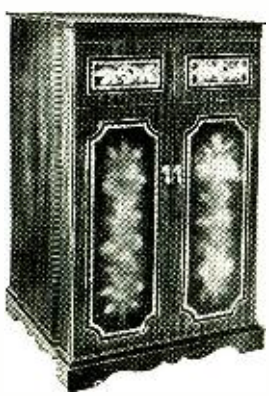
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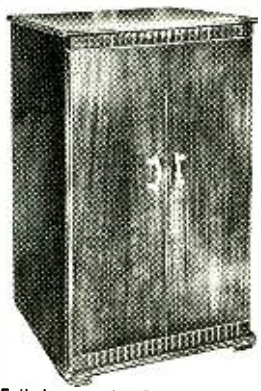
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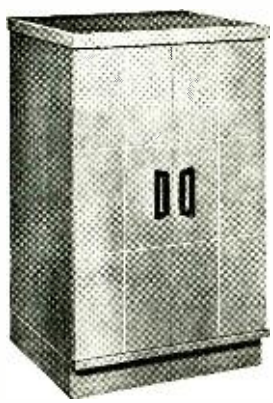
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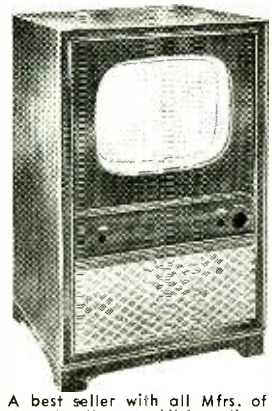


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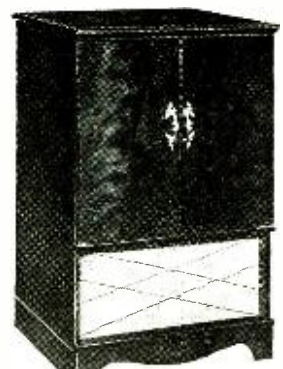
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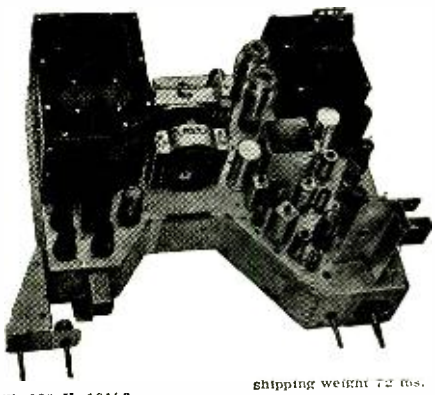
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rack mounting chassis brackets formed the ends of our breadboard, supporting the chassis at a convenient angle, with the low side usually in front when working with the breadboard. Another piece of aluminum, cut, bent, and drilled as shown in Fig. 2, is bolted across the back of the chassis between the two mounting brackets. In addition to strengthening the assembly, this backplate is used to mount controls, with their shafts projecting to the rear. If desired, similar control plates may be mounted at the ends of the chassis.

The main chassis was drilled and punched for three types of sockets (in this case four octal, three 7-pin miniatures, and three 9-pin miniatures). Saddle-type octal sockets with four ground lugs were used. Multiple tie-point strips provide plenty of terminals to which parts may be fastened. The eight bus wires are used for supply voltages and voltage-divider networks. External connections are made through the socket at the left. A 5-pin tube socket was used because the contacts fit standard banana plugs where individual connections are desired. The common-ground bus (nearest the front) is connected to the chassis at one point.

Also included on the chassis were two cutouts and mountings for FP type capacitors. These capacitors and all tubes, when used, are inserted from the under side of the chassis.

Obviously, the number and arrangement of sockets, tie points and bus bars may be varied to suit any requirements. More effective use of the available chassis space may be made by providing sockets for plug-in circuit units. Suitable components are available from several manufacturers, such as Millen, National, Alden, and Vector. Vector also manufactures turret-type sockets, which are handy space-savers. The breadboard shown was assembled from parts on hand at the time the author felt the need for the device. —end—

DEFINITE DICTUM

The old term "solenoid" has become a source of some confusion to radio technicians. To the r.f. man it means any cylindrical coil (as opposed to the helix, or pancake coil). To the relay manufacturer it tends to mean a magnet winding with a movable core.

The following definition, worthy of any magazine's "How's That Again" department, should relegate all that confusion to the background. It appeared in the *New York Herald Tribune*, under the head "Primary Magnet Form Bears Term 'Solenoid'."

> Solenoid means a primary form of electrical magnet. It consists of a filament which, when inclosed by a spiral-conducting wire properly positioned with its ends brought to the middle, may become a magnet when engaged by a current.
>
> This form of electrical magnet also is called a solenoid magnet.

The whole secret of a successful solenoid, of course, rests in the proper positioning of the wire, with the ends brought to the middle. This is known technically as "ends to a mean."

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Handsome round cornered molded bakelite case 3⅛" x 5⅞" x 2¼" complete with all test leads and instructions.

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Operates on 105-130 Volt 60 Cycles A.C. Hand-rubbed oak cabinet complete with portable cover

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* Uses the new self-cleaning Lever Action Switches for individual element testing. Because all elements are numbered according to pin number in the RMA base numbering system, the user can instantly identify which element is under test. Tubes having tapped filaments and tubes with filaments terminating in more than one pin are truly tested with the Model TV-11 as any of the pins may be placed in the neutral position when necessary. * Uses no combination type sockets. Instead individual sockets are used for each type of tube. Thus it is impossible to damage a tube by inserting it in the wrong socket. * Free-moving built-in roll chart provides complete data for all tubes. * Phono jack on front panel for plugging in either phones or external amplifier detects microphonic tubes or noise due to faulty elements and loose external connections.

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SIGNAL TRACER



The well known model CA-12 is the only signal tracer in the low price range including both meter and speaker ! ! !

SPECIFICATIONS: * Comparative Intensity of the signal is read directly on the meter—quality of the signal is heard in the speaker. * Simple to Operate—only one connecting cable—no tuning controls. * Highly Sensitive—uses an improved vacuum-tube voltmeter circuit. * Tube and Resistor Capacity Network are built into the detector probe. * Built-In High Gain Amplifier—Alnico V Speaker.

Completely Portable—weighs 8 pounds—measures 5½" x 6¼" x 9".

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THROWS AN ACTUAL BAR PATTERN ON ANY TV RECEIVER SCREEN! !

Two Simple Steps

1. Connect Bar Generator to Antenna Post of any TV Receiver.
2. Plug Line Cord into A. C. Outlet and Throw Switch.

RESULT: A stable never-shifting vertical or horizontal pattern projected on the screen of the TV receiver under test.

Power Supply: 105-125 Volt 60 Cycles. Power Consumption: 20 Watts. Channels: 2-5 on panel. 7-13 by harmonics. Horizontal lines: 4 to 12 (Variable). Vertical lines: 12 (Fixed). Vertical sweep output: 60 Cycles. Horizontal sweep output: 15,750 Cycles.

TV Bar Generator comes complete with shielded leads and detailed operating instructions. Only ....

$39.95 NET

Superior's New Model 660—AN AC OPERATED
SIGNAL GENERATOR

Provides Complete Coverage for A.M.-F.M. and TV Alignment

Generates Radio Frequencies from 100 Kilocycles to 60 Megacycles on fundamentals and from 60 Megacycles to 240 Megacycles on powerful harmonics. * Accuracy and stability assured by use of permeability trimmed Hi-Q coils. * R.F. available or modulated by the internal audio oscillator. * Built in 400 Cycle sine wave audio oscillator used to modulate the R.F. signal also available separately for audio testing of receivers, amplifiers, etc.

Oscillator Circuit: Uses a miniature high frequency type of acorn triode in a Hartley circuit to insure a high degree of stability. By using the same type of triode as a buffer amplifier, complete and positive isolation between the R.F. oscillator and the attenuator is attained. * Attenuator: a 3 step ladder type of attenuator is used. Each step of the attenuator is controlled by a separate attenuator control thus providing intermediate level steps. * Tubes used: 955, as R.F. Oscillator, 955 as Modulated Buffer Amplifier, 6SN7 as Audio Oscillator and Power Rectifier.



The Model 660 comes complete with coaxial cable test lead and instructions.

$42.95 NET

NEW TIME PAYMENT PLAN
ORDER BLANK

Moss Electronic Distributing Co., Inc.
Dept. B-25, 38 Murray Street, New York 7, N. Y.

Please send me the units checked below. I am enclosing the down payment with order and agree to pay the monthly balance as shown. It is understood there will be no carrying, interest or any other charges, provided I send my monthly payments when due. It is further understood that should I fail to make payment when due, the full unpaid balance shall become immediately due and payable.

- ☐ JUNIOR SUPER METER ..... Total Price $21.40
  $5.40 down payment. Balance $4.00 monthly for 4 months.
- ☐ MODEL TV-11 ..... Total Price $47.50
  $11.50 down payment. Balance $6.00 monthly for 6 months.
- ☐ MODEL CA-12 ..... Total Price $33.95
  $9.95 down payment. Balance $4.00 monthly for 6 months.
- ☐ TELEVISION BAR GENERATOR ..... Total Price $39.95
  $9.95 down payment. Balance $5.00 monthly for 6 months.
- ☐ MODEL 660 ..... Total Price $42.95
  $12.95 down payment. Balance $5.00 monthly for 6 months.
- ☐ I enclose $_____ as down payment.
- ☐ Ship C.O.D. for the down payment.

Signature_____

Name_____

Address_____

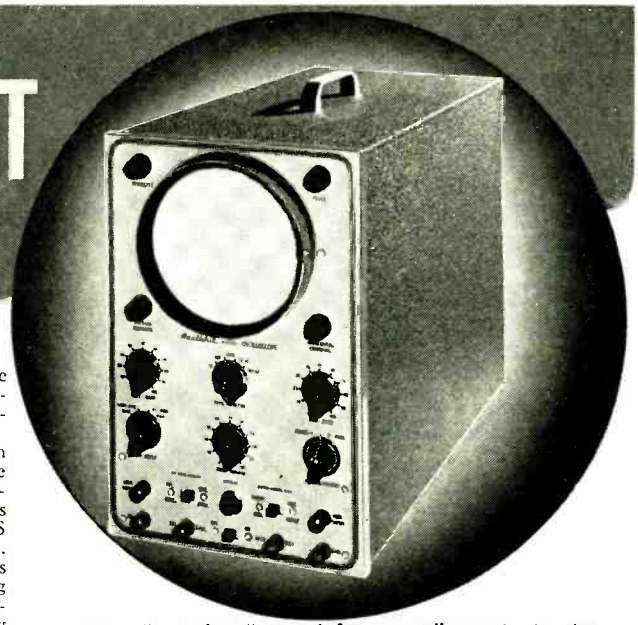
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The NEW 1952 Heathkit OSCILLOSCOPE KIT

MODEL O-7
SHIPPING WT. 29 LBS.

$43.50



The Heathkit 0-7 Oscilloscope with its 10 tube lineup (including CR tube) and carefully engineered circuit using highest quality components is truly the most outstanding scope value on the market today.

The "spot shape" (astigmatism) control working in conjunction with the focus control assures clear, sharp focusing . . . extended sweep range and faster retrace time permits the study of high frequencies . . . step-attenuated frequency-compensated cathode follower vertical input contributes to the excellent frequency response of the vertical channel . . . .03V RMS per inch vertical sensitivity makes weak input signals easy to study . . . push-pull operation of both vertical and horizontal deflection plates reduces pattern distortion . . . specially designed extra-wide CR tube mounting bracket places vertical cascade amplifier, vertical phase splitter, and deflection amplifiers near base of CR tube to reduce distributed wiring capacity and increase high frequency response.

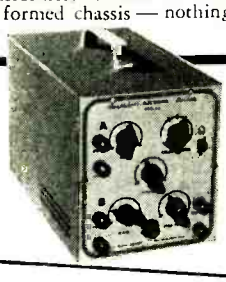
Ideal for TV servicing — steep wavefronts encountered in TV work are easily handled. Fine for production line testing — rugged quality components can stand up under continuous hour-after-hour use. Excellent for laboratories — electrical performance comparable to scopes costing 4 and 5 times as much.

You'll like the complete instructions showing all details for easily building the kit — includes pictorials, step-by-step construction procedure, numerous sketches, schematic, circuit description. All necessary components included — transformer, cabinet, all tubes (including CR tube), completely punched and formed chassis — nothing else to buy.

- **New "spot shape" control for spot adjustment — to give really sharp focusing.**
- **A total of ten tubes including CR tube and five miniatures.**
- **Cascaded vertical amplifiers followed by phase splitter and balanced push-pull deflection amplifiers.**
- **Greatly reduced retrace time.**
- **Step attenuated — frequency compensated — cathode follower vertical input.**
- **New mounting of phase splitter and deflection amplifier tubes near CR tube base.**
- **Increased frequency response — useful to 5 Mc.**
- **Tremendous sensitivity .03V RMS per inch Vertical — .6V RMS per inch Horizontal.**

Heathkit ELECTRONIC SWITCH KIT

MODEL S-2



SHIPPING WT. 11 LBS.

$19.50

The companion piece to a scope — Feed two different signals into the switch, connect its output to a scope, and you can observe both signals — each as an individual trace. Gain of each input is easily set (gain A and gain B controls), the switching frequency is simple to adjust (coarse and fine frequency controls), and the traces can be superimposed for comparison or separated for individual study (position contol).

The kit is complete with tubes, switches, cabinet, power transformer and all other parts, plus a clear detailed construction manual.

NEW Heathkit AUDIO FREQUENCY METER KIT

MODEL AF-1
SHIPPING WT. 15 LBS.



$34.50

The ideal instrument for determining frequencies from 20 cycles to 100 KC. Set the selector switch to the proper range — feed the signal into the input terminals — and read the frequency from the meter — completely simple to operate, and yet dependable results.

Quality Simpson 200 microampere meter has two plainly marked scales (0-100 0-300). These scales read in conjunction with the seven position selector switch, give full scale readings of 100, 300, 1000, 3000, 10,000, 30,000, and 100,000 cycles. Convenient ranges for fast and easy readings.

For greatest accuracy, the 1-3-10 ratio of ranges is maintained and each range has an individual calibrating control.

A signal voltage anywhere between 2 and 300V can be fed directly into the instrument and a change in signal voltage between these limits will not affect the meter reading. In addition, input wave shape is not critical (the unit will read the frequency of either sine wave or square wave input).

The tube complement consists of a 6SJ7 amplifier and clipper, 6V6 amplifier and clipper, 6H6 meter pulse rectifier, 6X5 power supply rectifier, and OD3/VR150 voltage regulator.

Construction is simple, and quality components are used throughout.

Heathkit INTERMODULATION ANALYZER KIT



MODEL IM-1
SHIPPING WT. 18 LBS.

$39.50

Intermodulation testing of audio equipment is rapidly being accepted by more and more engineers and audio experts as the best way to determine the characteristics of audio amplifiers, recording systems, networks, etc.

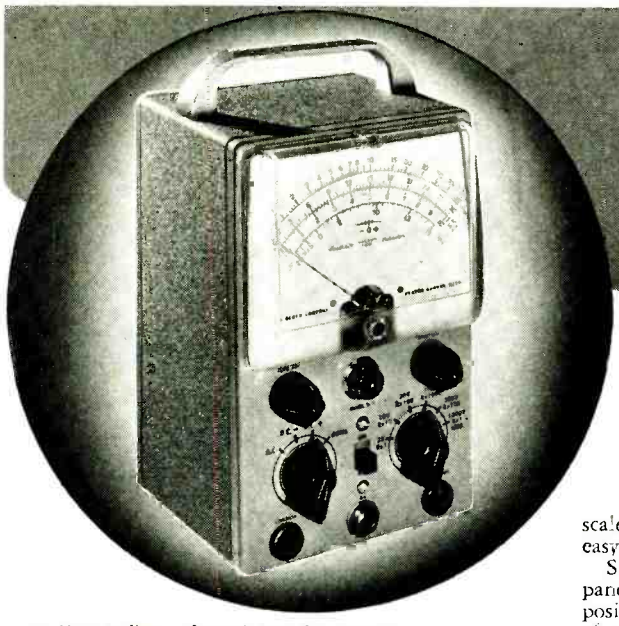
The Heathkit Intermodulation Analyzer supplies a choice of two high frequencies (approx. 3000 cycles and 7000 cycles) and one low frequency (60 cycles). Both 1:1 or 4:1 ratios of low to high frequencies can be set up for IM testing, and the ratios are easily set by means of a panel control and the instrument's own VTVM. An output level control supplies the mixed signal at the desired level with an output impedance of two thousand ohms. The Analyzer section has input level control and proper filter circuits feeding the instrument's VTVM to read intermodulation directly on full scale ranges of 30%, 10% and 3%. Built-in power supply furnishes all necessary voltages for operating the instrument.

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THE *New* 1952 *Heathkit* VTVM KIT

MODEL V5-A
SHIPPING WT. 7 LBS.

$24.50

- New styling, — formed case for beauty.
- New truly compact size. Cabinet 4⅛" deep by 4-11/16" wide by 7-3/8" high.
- Quality 200 microamp meter.
- New ohms battery holding clamp and spring clip — assurance of good electrical contact.
- Highest quality precision resistors in multiplier circuit.
- Calibrates on both AC and DC for maximum accuracy.
- Terrific coverage — reads from ½V to 1000V AC, ½V to 1000V DC, and .1 to over 1 billion ohms resistance.
- Large, clearly marked meter scales indicate ohms, AC Volts, DC Volts, and DB — has zero set mark for FM alignment.

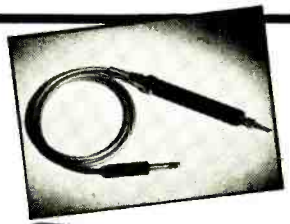
Designed to take up a minimum of space, yet designed to be the most important and useful instrument on your workbench. Really handsome looking — note the rounded edges on front panel and rear cover. New compact size has cabinet dimensions of only 4⅛" deep x 4 11/16" wide x 7⅜" high.

Tremendous coverage — will read from ½V to 1000V AC, ½V to 1000V DC, .1 to over 1 billion ohms resistance, and Db. Meter scale has zero-set mark for FM alignment — all scales clearly marked for easy and fast readings and Db scale is in red for easy identification.

Simple to operate. Ohms adjust and zero adjust controls located on front panel along with selector and range switches. Selector switch has four positions: AC, DC—, DC+ and Ohms to set up the instrument for type of reading desired. DC— position allows negative voltages to be taken without reversing test prods. AC and DC voltage ranges are full scale 3V — 10V — 30V — 100V — 300V — 1000V and resistance ranges are RX1, X10, X100, X1000, X10M, X1 Megohm. Convenient ranges for fast and accurate readings.

Strictly highest quality components used throughout — 1% precision resistors in multiplier circuit, Simpson 200 microampere meter movement, sturdy cabinet, excellent positive detent smooth acting switches, etc. New miniature tube used in meter balancing circuit and new battery holding clamp and spring clip assure good contact to ohms string of resistors.

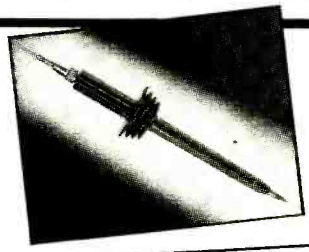
Kit comes complete — and the instruction manual with its step-by-step instructions, pictorials, figures, and schematic makes assembly a pleasure.



Heathkit R F PROBE KIT

Extends range of Heathkit VTVM to 250 MC ± 10%. Designed for taking RF measurements. All parts furnished including probe housing and crystal diode detector. Shipping Weight 1 lb.

$5.50



Heathkit 30,000 V DC PROBE KIT

For taking readings up to 30,000 V DC when used with the Heathkit VTVM (or any standard 11 megohm VTVM). Comes with two color molded plastic probe body and all parts. Shipping Wt. 2 lbs.

$5.50

Heathkit A. C. VACUUM TUBE VOLTMETER KIT



Now — as a Heathkit — at a price anyone can afford, an AC VTVM. Makes possible those sensitive AC measurements required by audio enthusiasts, laboratories, and experimentors. The kit audio men have been looking for. Ten ranges consisting of full scale .01, .03, .1, .3, 1, 3, 10, 30, 100, 300 volts RMS assure easy and more accurate readings. Ten ranges on DB provide for measurements from −52 to +52 DB. Frequency response within 1 DB from 20 cycles to 50 KC.

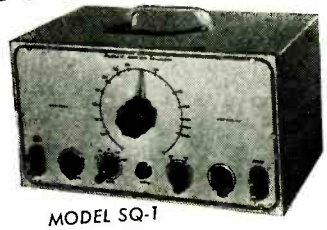
The ingenious circuitry incorporates precision multiplied resistors for accuracy, two amplifier stages using miniature tubes, a unique bridge rectifier meter circuit, quality Simpson meter with 200 microampere movement, and a clean layout of parts for easy wiring. A high degree of inverse feedback provides for stability and linearity.

Extremely compact, cabinet size — 4-1/8" deep x 4-11/-16" wide x 7-3/8" high. Newly designed cabinet makes this the companion piece to the VTVM.

MODEL AV-1
SHIP. WT. 5 LBS.

$29.50

Heathkit SQUARE WAVE GENERATOR KIT



The Heathkit Square Wave Generator is an excellent square wave frequency source with features you won't want to be without. Especially notable is the wide range of the instrument — 10 cycles to 100 kilocycles continuously variable. This wide range makes it useful for television and wide band amplifier work as well as audio experimentation. The output impedance is low, and the output voltage is continuously variable between 0 and 20 volts. Because a multivibrator stage cannot be accurately calibrated, terminals on the front panel can be used for synchronization to an external source should it be desired.

The circuitry consists of a multivibrator stage, a clipping and a squaring stage, and a cathode follower output stage. The power supply is transformer operated and utilizes a full wave rectifier tube with 2 sections of LC filtering.

For a good, wide range, and low priced square wave generator, the SQ-1 just can't be beat.

MODEL SQ-1
SHIP. WT. 14 LBS.

$29.50

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Heathkit SIGNAL GENERATOR KIT

Model SG-6
Shipping Wt. 7 lbs.



The new Heathkit Signal Generator Kit has dozens of improvements. Covers the extended range of 160 Kc to 50 megacycles on fundamentals and up to 150 megacycles on useful calibrated harmonics; makes this Heathkit ideal as a marker oscillator for TV. Output level can be conveniently set by means of both step attenuator and continuously variable output controls. Instrument has new miniature HF tubes to easily handle the high frequencies covered.

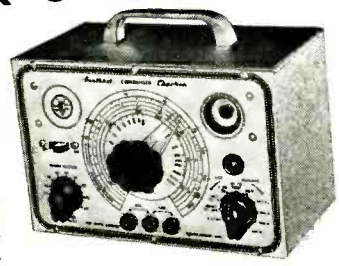
Uses 6C4 master oscillator and 6C4 sine wave audio oscillator. The kit is transformer operated and a husky selenium rectifier is used in the power supply. All coils are precision wound and checked for calibration making only one adjustment necessary for all bands.

New sine wave audio oscillator provides internal modulation and is also available for external audio testing. Switch provided allows the oscillator to be modulated by an external audio oscillator for fidelity testing of receivers. Comes complete, all tubes, cabinet, test leads, every part. The instruction manual has step-by-step instructions and pictorials. It's easy and fun to build a Heathkit Model SG-6 Signal Generator.

Heathkit CONDENSER CHECKER KIT

Only **$19.50**

Model C-2
Shipping Wt. 6 lbs.



Checks all types of condensers — paper — mica — ceramit — electrolytic. All condenser scales are direct reading and require no charts or multipliers. Covers range of .00001 MFD to 1000 MFD. A Condenser Checker that anyone can read. A leakage test and polarizing voltage for 20 to 500 V provided. Measures power factor of electrolytics between 0% and 50% and reads resistance from 100 ohms to 5 megohms. The magic eye indicator makes testing easy.

The kit is 110V 60 cycle transformer operated and comes complete with rectifier tube, magic eye tube, cabinet, calibrated panel and all other parts. Has clear detailed instructions for assembly and use.

NEW Heathkit SIGNAL TRACER AND UNIVERSAL TEST SPEAKER KIT

$19.50

Model T-2
Shipping Wt. 7 lbs.



The popular Heathkit Signal Tracer has now been combined with a universal test speaker at no increase in price. The same high quality tracer follows signal from antenna to speaker — locates intermittents — finds defective parts quicker — saves valuable service time — gives greater income per service hour. Works equally well on broadcast, FM, or TV receivers. The test speaker has an assortment of switching ranges to match either push-pull or single output impedances. Also tests microphones, pickups and PA systems. Comes complete: cabinet, 110V 60 cycle power transformer, tubes, test probe, all necessary parts, and detailed instructions for assembly and use.

Heathkit TUBE CHECKER KIT



Model TC-1
Shipping Wt. 12 lbs.

$29.50

The Tube Checker is a MUST for radio repair men. Often customers want to SEE tubes checked, and a checker like this builds customer confidence. In your repairing, you will have a multitude of tubes to check — quickly. The Heathkit tube checker will serve all these functions — it's good looking (with a polished birch cabinet and an attractive two color panel) — checks 4, 5, 6, 7 prong Octals, Loctals, 7 prong miniatures, 9 prong miniatures, pilot lights, and the Hytron 5 prong types. AND IT'S FAST TO OPERATE — the gear driven, free-running roll chart lists hundreds of tubes, and the smooth acting, simplified switching arrangement gives really rapid set-ups.

The testing arrangement is designed so that you will be able to test new tubes of the future — without even waiting for factory data — protection against obsolescence.

You can give tubes a thorough testing — checks for opens, shorts, each element individually, emission, and for filament continuity. A large BAD-?-GOOD meter scale is in three colors for easy reading and also has a "line-set" mark.

You'll find this tube checker kit a good investment — and it's only $29.50.

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NEW 1952 *Heathkit*

BATTERY ELIMINATOR KIT



Model BE-3
Shipping Wt. 17 lbs.

- Can be used as battery charger.
- Continuously variable output 0 - 8 Volts — not switch type.
- Heavy duty Mallory 17 disk type magnesium copper sulfide rectifier.
- Automatic overload relay for maximum protection. Self-resetting type.
- Ideal for battery, aircraft and marine radios.
- Dual Volt and Ammeters read both voltage and amperage continually — no switching.

The new Heathkit Model BE-2 incorporates the best. Continuously variable output control is of the variable transformer type with smooth wiper type contacts.

There are no switches or steps and voltage between 0 and 8 Volts is available at 10 Amperes continuous and 15 Amperes intermittent. Maximum safety from overloads and shorts provided by automatic overload relay which resets itself when overload is removed.

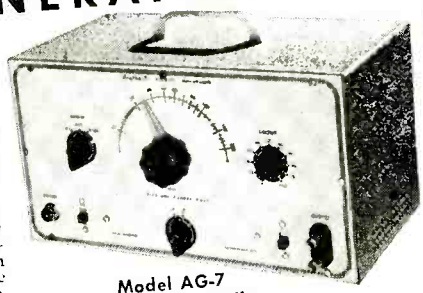
The new rectifier is a 17 plate Mallory magnesium copper sulfide type. This is the most rugged type available for long trouble-free use.

Output is continuously metered by both a 0 - 10 Volt Voltmeter and a 0 - 15 Amp Ammeter. Shorted vibrators indicated instantly by ammeter.

Equip now for all types of service — aircraft — marine — auto and battery radios — this inexpensive instrument vastly increases service possibilities — better be ready when the customer walks in.

NEW *Heathkit*

SINE AND SQUARE WAVE AUDIO GENERATOR KIT



Designed with versatility, usefulness, and dependability in mind, the AG-7 gives you the two most needed wave shapes right at your fingertips — the sine wave and the square wave.

The range switch and plainly calibrated frequency scale give rapid and easy frequency selection, and the output control permits setting the output to any desired level.

A high-low impedance switch sets the instrument for either high or low impedance output —on high to connect a high impedance load, and on low to work into a low impedance transformer with negligible DC resistance.

Coverage is from 20 to 20,000 cycles, and distortion is at a minimum — you can really trust the output wave shape.

Six tubes, quality 4 gang tuning condenser, power transformer, metal cased filter condenser, 1% precision resistors in the frequency determining circuit, and all other parts come with the kit —plus, a complete construction manual — A tremendous kit, and the price is truly low.

Model AG-7
Shipping Wt. 15 lbs.

$34.50

THE NEW *Heathkit*

HANDITESTER KIT



A precision portable volt-ohm milliammeter. Uses only high quality parts — All precision 1% resistors, three deck switch for trouble-free mounting of parts, specially designed battery mounting bracket, smooth acting ohm adjust control, beautiful molded bakelite case, 400 micro-amp meter movement, etc.

DC and AC voltage ranges 10 - 30 - 300 - 1000 - 5000V. Ohms range 0 - 3000 and 0 - 300,000. Range Milliamperes 0 - 10 Ma, 0 - 100 Ma. Easily assembled from complete instructions and pictorial diagrams.

$13.50

Model M-1
Shipping Wt. 3 lbs.

NEW *Heathkit*

T.V. ALIGNMENT GENERATOR KIT

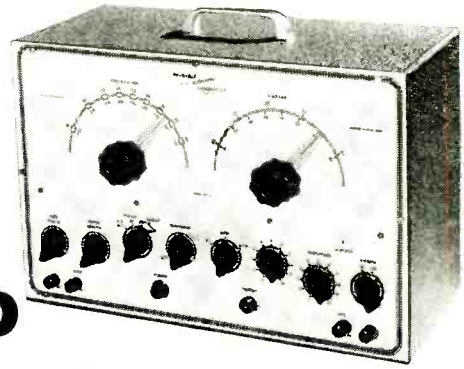
Here is an excellent TV Alignment Generator designed to do TV service work quickly, easily, and properly. The Model TS-2 when used in conjunction with an oscilloscope provides a means of correctly aligning television receivers.

The instrument provides a frequency modulated signal covering, in two bands, the range of 10 to 90 Mc. and 150 to 230 Mc. — thus, ALL ALLOCATED TV CHANNELS AS WELL AS IF FREQUENCIES ARE COVERED.

An absorption type frequency marker covers from 20 to 75 Mc. in two ranges — therefore, you have a simple, convenient means of frequency checking of IF's, independent of oscillator calibration.

Sweep width is controlled from the front panel and covers a sweep deviation of 0-12 Mc. — all the sweep you could possibly need or want.

And still other excellent features are: Horizontal sweep voltage available at the front panel (and controlled with a phasing control — both step and continuously variable attenuation for setting the output signal to the desired level — a convenient instrument stand-by position — vernier drive of both oscillator and marker tuning condensers — and blanking for establishing a single trace with base reference level. Make your work easier, save time, and repair with confidence — order your Heathkit TV Alignment Generator now!



Model TS-2
Shipping Wt. 20 lbs.

$39.50

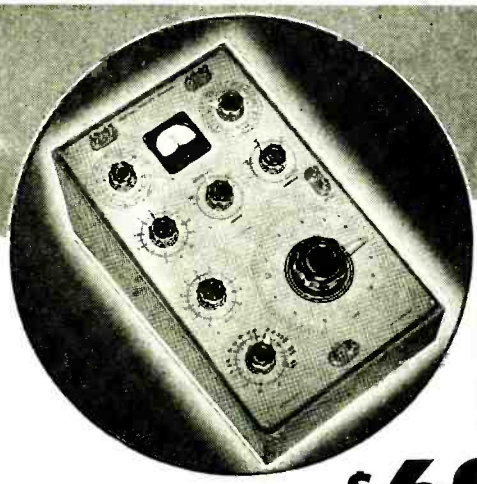
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Heathkit IMPEDANCE BRIDGE KIT



Model 1B-1B
Shipping Wt. 15 lbs.

$69.50

This Impedance Bridge Kit is really a favorite with schools, industrial laboratories, and serious experimenters. An invaluable instrument for those doing electrical measurements work. Reads resistance from .01 Ohms to 10 meg., capacitance from .00001 to 100 MFD. inductance from 10 microhenries to 100 henries, dissipation factor from .002 to 1, and storage factor from 1 to 1000. And you don't have to worry about selecting the proper bridge circuit for the various measurements — the instrument automatically makes the correct circuit when you set up for taking the measurement you want. Bridge utilizes Wheatstone, Hay, Maxwell, and capacitance comparison circuits for the wide range and types of measurements possible. And it's self powered — has internal battery and 1000 cycle hummer. No external generator required — has provisions for external generator if measurements at other than 1000 cycles are desired. Kit utilizes only highest quality parts. General Radio main calibrated control. Mallory ceramic switches, excellent 200 microamp zero center galvanometer, laboratory type binding posts with standard ¾ inch centers, 1% precision ceramic-body type multiplier resistors, beautiful birch cabinet and ready calibrated panel. (Headphones not included.)

Take the guesswork out of electrical measurements — order your Heathkit Impedance Bridge kit today — you'll like it.

Heathkit LABORATORY RESISTANCE DECADE KIT



$19.50

Shipping Wt. 4 lbs.

An indispensable piece of laboratory equipment — the Heathkit Resistance Decade Kit gives you resistance settings from 1 to 99,999 ohms IN ONE OHM STEPS. For greatest accuracy, 1% precision ceramic-body type resistors and highest quality ceramic wafer switches are used.

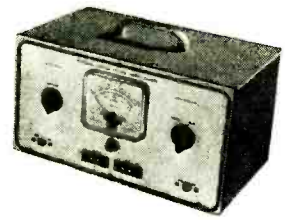
Designed to match the Impedance Bridge above, the Resistance Decade Kit has a beautiful birch cabinet and attractive panel. It's easy to build, and comes complete with all parts and construction manual.

Heathkit LABORATORY POWER SUPPLY KITS

Limits:

No load	Variable 150-400V DC
25 MA	Variable 30-310V DC
50 MA	Variable 25-250V DC

Higher loads: Voltage drops off proportionally



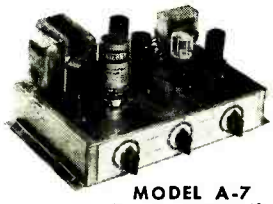
$29.50

Model PS-1.....Ship. Wt. 20 lbs.

Every experimenter needs a good power supply for electronic setups of all kinds. This unit has been expressly designed to act as a HV supply and a 6.3 V filament voltage source. Voltage control allows selection of HV output desired (continuously variable within limits outlined), and a Volts-Ma switch provides choice of output metering. A large plainly marked and direct reading meter scale indicates either DC voltage output in Volts or DC current output in Ma. (Range of meter 0-500V D.C., 0-200 Ma. D.C.). Instrument has convenient stand-by position and pilot light.

Comes with power transformer, filament transformer, meter, 5Y3 rectifier, two 1619 control tubes, completely punched and formed chassis, panel, cabinet, detailed construction manual, and all other parts to make the kit complete.

Heathkit ECONOMY . . . 6 WATT AMPLIFIER KIT



MODEL A-7
Shipping Wt. 8 lbs.

$14.50

- **Choice of 4-8-15 ohm output impedances.**
- **Response flat ± 1½ db from 20—20,000 cycles.**
- **6 watts output.**
- **Good fidelity at low cost.**
- **Output tubes working in push pull.**
- **Volume, bass, and treble controls.**
- **Two separate inputs.**

The purpose of this kit is to provide to the kit builder a low cost amplifier with excellent fidelity. The circuit consists of four tubes with following functions: a 12SL7, one section working as an amplifier and one as a phase splitter, two 12A6 output tubes working in push pull, and a 5Y3 rectifier in a full wave rectifier circuit.

The unit operates from a husky power transformer, and has good output transformer with a choice of 4—8—15 ohm output impedances. (Speaker not included).

The kit provides excellent listening pleasure and the price is really low. Compare it with all others. You won't find a better buy.

MODEL A-7: For tuner and crystal phono inputs. Has two position selector switch for convenient switching to type of input desired.

Model A-7-A: Has a 12SH7 preamplifier stage with special compensation network for operation with reluctance phono input.
Shipping Wt: 8 lbs.....**$16.50**

Heathkit HIGH FIDELITY 20 WATT AMPLIFIER KIT



MODEL A-8
Shipping Wt. 18 lbs.

$33.50

The A8 (or A-8A) is a high quality amplifier for those who want high fidelity output at moderate cost. Frequency response within ± 1db from 20—20,000 cycles. Distortion at 3db below maximum power output (at 1,000 cycles) is only .8%. Kit has a Chicago power transformer in drawn steel case and a Peerless output transformer with output impedances of 4—8—16 ohms. Bass and treble controls permit listener to select output with tonal qualities of his own liking.

The tube lineup is composed of a 6SJ7 voltage amplifier, a 6SN7 amplifier and phase splitter, two 6L6's in push-pull output and a 5U4G rectifier. All parts furnished (speaker not included) and the construction manual makes assembly easy.

MODEL A-8: For tuner and crystal phono inputs. Has two position selector switch for convenient switching to type of input desired.

MODEL A-8A: Features an added 6SJ7 stage (preamplifier) for operating from variable reluctance cartridge phono pickup, mike input, and either tuner or standard crystal phono pickup. A three position selector switch provides flexible switching. Shipping Wt. 18 lbs.....**$35.50**

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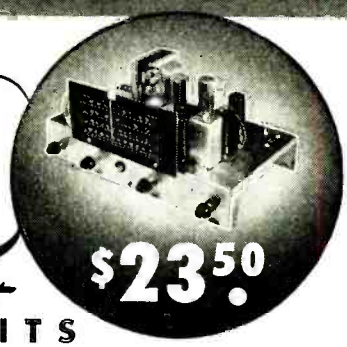
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Heathkit RECEIVER & TUNER KITS for AM and FM



Model BR-1 Broadcast Model Kit covers 550 to 1600 Kc. Shipping Wt. 10 lbs.

Model AR-1 3 Band Receiver Kit covers 550 Kc. to over 20 Mc. continuous. Extremely high sensitivity. Shipping Wt. 10 lbs.



TWO HIGH QUALITY Heathkit SUPERHETRODYNE RECEIVER KITS

Two excellent Heathkits. Ideal for schools, replacement of worn out receivers, amateur and custom installations.

Both are transformer operated quality units. The best of materials used throughout — six inch calibrated slide rule dial — quality power output transformers — dual iron core shielded. I.F. coils — metal cased filter condenser. The chassis has phono input jacks, 110 Volt output for phono motor and there is a phono-radio switch on panel. A large metal panel simplifying installation in used console cabinets is included. Comes complete with tubes and instruction manual incorporating pictorials and step-by-step instructions (less speaker and cabinet). The three band model has simple coil turret which is assembled separately for ease of construction.



Model FM-2
Ship. Wt. 9 lbs.

$22.50

TRUE FM FROM Heathkit FM TUNER KIT

The Heathkit FM Tuner Model FM-2 was designed for best tonal reproduction. The circuit incorporates the most desirable FM features — true FM.

Utilizes 8 tubes: 7E5 Oscillator, 6SH7 mixer, two 6SH7 IF amplifiers, 6SH7 limiter, two 7C4 diodes as discriminator, and 6X5 rectifier.

The instrument is transformer operated making it safe for connection to any type receiver or amplifier. Has ready wound and adjusted RF coils, and 2 stages of 10.7 Mc IF (including limiter). A calibrated six inch slide rule dial has vernier drive for easy tuning. All parts and complete construction manual furnished.



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	Heathkit VTVM Kit — Model V-5			Heathkit R.F. Signal Gen. Kit — Model SG-6	
	Heathkit FM Tuner Kit — FM-2			Heathkit Condenser Checker Kit — Model C-2	
	Heathkit Broadcast Receiver Kit — Model BR-1			Heathkit Handitester Kit — Model M-1	
	Heathkit Three Band Receiver Kit—Model AR-1			Heathkit Power Supply Kit — Model PS-1	
	Heathkit Amplifier Kit — Model A-4			Heathkit Resistance Decade Kit — Model RD-1	
	Heathkit Amplifier Kit — Model A-6 (or A-6A)			Heathkit Impedance Bridge Kit — Model IB-1B	
	Heathkit Tube Checker Kit — Model TC-1			Heathkit A.C. VTVM-KIT — Model AV-1	
	Heathkit Audio Generator Kit — Model AG-7			Heathkit Intermodul. Analyzer Kit—Model IM-1	
	Heathkit Battery Eliminator Kit — Model BE-2			Heathkit Audio Freq. Meter Kit — Model AF-1	
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MARKER-CALIBRATOR

The Hickok Electrical Instrument Co., 10514 Dupont Ave., Cleveland 8, Ohio, has introduced the new model 680 TV r.f. marker generator and crystal-controlled calibrator. Accurate to .05%, the unit is a crystal-calibrated standard for use in checking oscillators, generators, and front-end and over-all response curves of TV sets. A built-in heterodyne detector and electron-ray tube zero-beat indicator are provided to insure accurate calibration.



The unit has the following features:

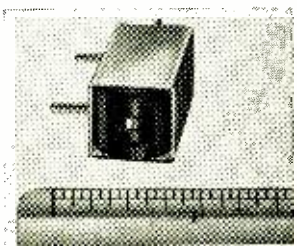
1. An r.f. signal generator covering from 52-89 and 174-217 mc on fundamentals, and to 868 mc on harmonics.
2. A 2.5-mc crystal to beat with the v.f.o. to provide accurate check points at 2.5-mc intervals throughout the range.
3. Two additional crystal sockets are provided for calibrating signal generators and other equipment. If a 4.5-mc crystal is used, dual markers may be obtained.

The unit is housed in an 11½ x 6 x 9-inch portable steel case and draws 20 watts from 105–125-volt, 50–70-cycle lines.

RECORDING HEAD

Shure Brothers, Inc., 225 West Huron St., Chicago 10, Ill., announces the new TR-16 magnetic tape recording head which features excellent frequency response, compactness (0.765 inch wide, 0.845 inch long, and 0.609 inch thick), track widths from .025 to 0.1 inch, and flexible mountings which provide for vertical and angular adjustments.

The unit may be used for multiple-track applications and is recommended for dictating or low-cost playback machines. Mu-metal shielding minimizes hum pickup.



NEW TUBE TESTER

Electronic Measurements Corp., 280 Lafayette Street, New York, N. Y., has announced the addition of a new tube tester to the EMC line of electrical testing equipment. Model 205 is designed to give test readings for all tubes, including noval and subminiatures from 0.75 to 1.17 filament volts through the standard emission method of testing. This instrument, using four-position lever-type switches and individual sockets for each tube base type, is available in either stationary or portable oak cases.



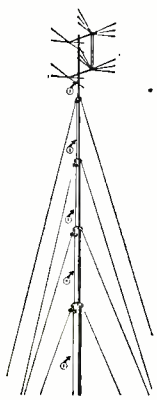
GEIGER KIT

Allied Radio Corp., 833 W. Jackson Blvd., Chicago, Ill., announces that its new "Super Scout" Geiger counter is available in kit form. The unit provides effective radiation detection for schools, laboratories, civil defense applications, and prospecting use. It detects the presence of gamma rays and medium-to-high energy beta rays, as well as cosmic and X-rays. It instantly spots radiations from uranium, pitchblende radium, and other radioactive sources. Clicks heard in headphones and flashes of a neon lamp increase in frequency as the source of radiation is approached.

The unit includes a built-in vibrator-type power supply powered by two flashlight batteries, a sensitive G.M. tube, and a 1T4 tube used as a rectifier. It weighs 3 pounds and has a sturdy leather handle and a belt clip for convenient carrying. It is supplied with easy-to-read instructions, a pictorial diagram, and all parts except headphones.

TELESCOPIC TV MAST

JFD Manufacturing Co., Inc., 6101 16th Ave., Brooklyn 4, N. Y., is distributing the new *Zoom-Up* telescoping tower-type mast in seven models. The masts



are constructed of 10-foot telescoping sections of zinc-plated seamless steel tubing with heavy-duty nuts and bolts to lock the sections firmly in position. Guy rings, clamps, and all other necessary hardware are supplied with each antenna. The units are erected simply by installing the antenna on the uppermost section and then pushing the lower sections into place.

The masts are available in three models for 20 feet, two for 30 feet, and one each for 40 and 50 feet. For a given height, the models differ in the outside diameters of the sections.

CARBON MICROPHONE

The Astatic Corporation, Conneaut, Ohio is distributing its new model 10M5 single-button, hand-held microphone which is designed for maximum



clarity of speech. Response is from 100 to 4,500 cycles. Sensitivity is rated at 1 volt for 100 microbar signal (100-ohm load).

The mike includes a built-in d.p.s.t. push-to-talk switch with microphone and relay contacts normally open. It is recommended for mobile transmitter and sound installations and similar applications. When used with a step-up transformer, it will work directly into power-output stages without using a preamplifier. A hang-up bracket is provided for holding the mike on a wall, panel, or dashboard.

It is supplied with a 4-conductor, self-coiling, oil-resistant rubber-covered cable. The retracted length of the cable is 12 inches. The extended length is 5 feet.

CHANNEL SEPARATOR

Technical Apparatus Corp., Sherburne, N. Y., announces that the new Tacoplex channel separators are now available. These units separate TV channel signals traveling along a common transmission line and feed the

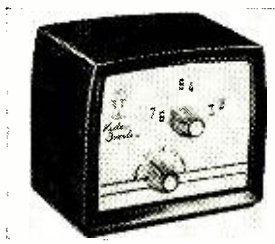


separated signals through individual outputs to separate boosters or amplifiers. Such units are employed at all booster stations in a community TV distribution system. They terminate the transmission line properly and make it possible to amplify one channel without amplifying adjacent ones. (Simultaneous amplification of adjacent-channel signals often results in distortion of both video and sound.)

The two-channel model is the 1512 and the three-channel model is the 1513. They are available for any combination of two or three low-band channels, not including adjacent channels, except 4 and 5.

TV BOOSTERS

Radio Merchandise Sales, Inc., 1165 Southern Blvd., New York, N. Y. has added two new TV boosters to the



RMS line. The model SP-6 is a pentode-tube booster with an external gain control which permits operating the unit at maximum gain in extreme fringe areas and with reduced gain in areas where full gain causes overloading of the set.



The SP-6J triode-tube booster features an extremely low noise level, high gain, and a full 6-megacycle bandwidth.

Both units are approved by Underwriters Laboratories and carry a full guarantee with standard RMA warranty on tubes and parts.

LIGHTNING ARRESTER

Insuline Corp. of America, 36-05 35th Avenue, Long Island City, 1, N. Y. has announced its new 6113 and 6114 lightning arresters for TV antennas. Approved by Underwriters Laboratories, the new molded phenolic units are designed to withstand all extremes of weather. The 6113 has a binding post for ground wire, and the 6114 has a grounding strap which fits around the



usual metal pipe of the TV mast. Either type can be installed without cutting the lead-in. Contact to the lead-in conductors is made through cup-shaped washers with serrated teeth.

PRECISION RESISTORS

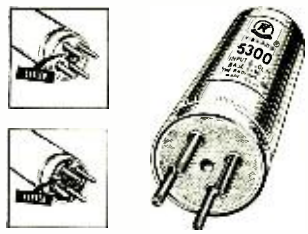
International Resistance Co., 401 North Broad St., Philadelphia 8, Pa. has introduced two new types of precision resistors. The deposited-carbon (DDC) and boron-carbon (BOC) types are



physically alike except for color. Both provide higher resistance values in less space and at lower cost than precision wire-wound units. Both are rated at ½ watt and are available with tolerances of 1, 2, and 5%. The body length is 9/16 inch and maximum diameter is 5/32 inch. The BOC type is recommended for applications where stability and accuracy are required under widely varying temperatures.

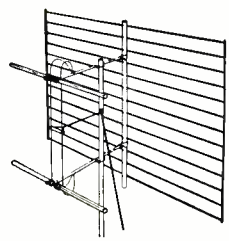
VIBRATORS

The Radiart Corp., Cleveland 2, Ohio, announces its Red Seal line of replacement auto radio vibrators which have a vent built into the base. This vent is wax-sealed at the factory to prevent oxidation of the points before the unit is put into use. When the vibrator is operated, the temperature rise melts out the wax and permits air to circulate inside the unit, thus providing longer life and better performance.



NEW TV ANTENNA

Davis Electronics, 3047 West Olympic Blvd., Los Angeles 6, Calif., has just announced the new Super-Vision TV antenna. It is recommended for fringe-area and dx reception and where high-gain performance is desired on all channels. Ghosts are reduced or eliminated by the sharp pattern in the forward direction. High vertical and horizontal directivity are obtained by the use of stacked dipoles, together with a "bedspring" type reflector. Aircraft flutter, diathermy, FM, and other sources of TV interference are substantially reduced. Gain is 10 db or more on high channels.



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TAPE RECORDER

TapeMaster, Inc., 13 West Hubbard St., Chicago 10, Ill., is producing the new model PT-121 professional-quality tape recorder designed for operation with the user's own audio amplifier and speaker. The unit includes a tape-transport mechanism and matching self-powered preamplifier with push-pull supersonic bias-erase oscillator, fully wired and ready to plug in.

The PT-121 has a tape speed of 7.5 inches per second; maximum speed variation 2% with line variation from



95 to 125 volts. Dual-track head, for ¼-inch tape. Fast forward and fast rewind (20:1 ratio). Inputs for both radio-phono and microphone. High input impedance. Output impedance 17,000 ohms. Audio output to 4 volts. Response 70–8,000 cycles plus or minus 3 db. Equalization provides high- and low-frequency compensation for recording and playback.

Fitted into a 12 x 12½ x 9½-inch leatherette-covered portable case, the unit is supplied with a 5-inch reel of tape and a 7-inch take-up reel. Mike, amplifier, and speaker are to be supplied by the user.

TUBE CADDY

Argos Products Co., Genoa, Ill., has introduced the "Tube Caddy Junior," a new, smaller, companion-piece to the larger "Television Tube Caddy." The new unit (model TC-2) measures 15½ x 13 x 8 inches and holds up to 143 receiving tubes. The larger model (TC-18) is 20 inches long, 13½ inches high, and 9 inches wide, and carries up to 249 tubes.

Both models have two drawers at the top for miniature and medium-size tubes and space at the bottom for larger tubes. Drawers have removable partitions. Small tools and a meter also may be carried.



LIGHTNING ARRESTER

Brach Mfg. Corp., 200 Central Ave., Newark 4, N. J., announces the production of the model 4004 lightning arrester for open-wire transmission lines. The unit does not distort the line spacing nor introduce mismatch at any TV frequency. It incorporates a rare-gas tube which dissipates the charges before they can enter and destroy delicate TV receiver equipment. The 4004 is waterproof, with all parts protected against corrosion. It is listed by Underwriters' Laboratories.

—end—

All specifications given on these pages are from manufacturers' data.

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with easy-to-install

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Distribution Amplifier
8 TV Set Outlets
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Commercial Antensifier (30 Times Gain) Use As Pre-Amplifier, Line Amplifier or de-luxe Booster
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Fully licensed under RCA and Hazeltine patents. The photo shows the Espey Model 511-C, supplied ready to play. Equipped with tubes, antenna, speaker, and all necessary hardware for mounting.

NEW FEATURES—Improved Frequency modulation circuit, drift compensated • 12 tubes plus rectifier, and pre-amplifier pick-up tubes • 4 dual purpose tubes • High quality AM-FM reception • Push-pull beam power audio output 10 watts • Switch for easy changing to crystal or variable reluctance pick-ups • Multi-tap audio output transformer supplying 4—8—500 ohms.

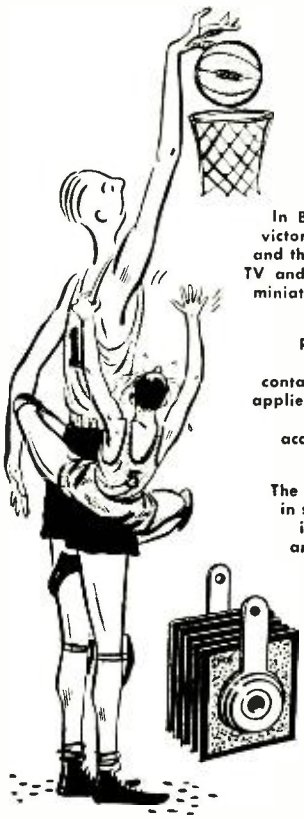
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say TV owners of the *vertical black* bars which appear when Barkhausen Oscillation occurs in the horizontal sweep output tube (such as the 25BQ6, 6BQ6, 6EV5, 25EV5, 6AU5, or 25AU5, etc.).

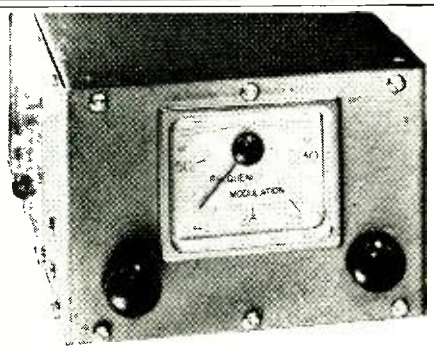
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Model M-51

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NEW COAST GROUP

A new organization, the Society of Radio and Television Technicians, Inc., is reported from the San Fernando Valley, California. Dell Davis, chairman of the public relations committee, informs us that it is an outgrowth of the old Radio Technicians Association, San Fernando Valley Chapter, which has been disbanded.

Dinner meetings are held twice monthly, with the programs aimed directly at the practicing technician. Routine business is confined to a 15-minute period, the remainder of the meetings being entirely technical, and operated in "typical service club style."

An ingenious method has been adopted to insure maximum member attendance at all meetings. Members who interrupt a speaker or engage in crosstalk are fined one dollar. The fines are placed on a clothesline strung across the hall as they are levied.

At the end of the meeting a member's name is drawn from a hat. If he is present he "takes in the wash." If not, the money is held and goes toward next meeting's jackpot.

PHONE BOOK PUBLICITY

The Associated Radio-Television Service Dealers of Columbus, Ohio, have decided to have a master cut made of the organization's insignia, to be used for the telephone directory listings of members who may wish to use it.

The new president, Fred Colton, in a special message, urged all members to display the Association's emblem, not only in their places of business, but in the phone book, on trucks, on their letterheads and in all other places where it might further the public's recognition of the emblem and the competent, ethical, business operations for which it stands.

FIRST LADIES NIGHT

The Mid-State Radio Servicemen's Association of Harrisburg, Pennsylvania held its First Annual Ladies Night with sixteen members and wives in attendance on February fifth, 1952. The affair was held at Shelley's Restaurant, Steelton, with a "family style" meal.

After dinner many pictures were taken by Vance Beechley, with his Polaroid "picture-in-a-minute" camera. After this a color movie entitled "Historic Old New England" was shown. Without exception, it was acclaimed as excellent by all present.

The wives were especially enthusiastic about this event and immediately asked that plans be made to hold an annual affair. On second thought they asked, "Why wait another year to get together? Why not have a clam-bake or a wiener roast for members and wives during the summer or early fall months?"

Mid-State members cite the success of this affair in recommending that other associations follow their example.

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RIDER HONORED BY FRSAP

John F. Rider, publisher of service manuals and other books for the service technician, was honored March 16 by the Federation of Radio and Television Servicemen's Associations of Pennsylvania, as the person who, in the opinion of the Federation, had contributed most to the welfare of the service technician during 1951.

Mr. Rider was presented with a plaque at a luncheon meeting in the Harrisburger Hotel, Harrisburg, Pa. The meeting was attended by delegates from the member associations of FRSAP and by visiting delegates from New Jersey and New York, as well as by representatives of other branches of the radio and television industry.

Mr. Rider spoke briefly on receiving the plaque, and at greater length later in the meeting. He called particular attention to the strides organized service technicians have made during the past three or four years, pointing out evidence of the increased attention and respect shown them by manufacturers and manufacturers' associations. Only the "grave setback" of internal dissension could negate this progress, Mr. Rider declared. He also attacked the "professional" philosophy common among radio technicians. "Knock the 'profession' philosophy out of this business!" he said. "Service is a business—it's a technical business, but all the more a business." He then pointed out that engineering firms—every member of which might be a licensed professional engineer—conduct their affairs on a commercial, not a professional, basis, and suggested that TV and radio repair organizations could profit from their example.

Dave Krantz, chairman of the Federation, in his presentation speech, also referred to the great strides made by the industry in cooperating with the technicians. "Although," he said, "There are still many who would ignore the issue and believe that someone else will do the job for them." He gave particular praise to the RTMA, which "has made great strides in forming a program for the set manufacturers, and although we don't agree with some of its features, we still want to cooperate with the RTMA in solving any or all of the problems confronting us." He also paid tribute to some of the distributors and local chapters of the National Electronic Distributors Association, at the same time regretting that the national office of the N.E.D.A. had made "little or no effort to meet with the servicing industry to formulate a cooperative program for the technicians."

Others present who spoke briefly were Albert Coumont, service manager of the RTMA, Ed. Cahill, vice-president, and Dan Creato, legal counselor, of the RCA Service Co., Max Liebowitz, president of NETSDA, officers of FRSAP, Sandy Cowan, editor of *Radio Service Dealer*, and Fred Shunaman, managing editor of RADIO-ELECTRONICS.

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TUBE & TOOL CARRIER
with Detachable Mirror for Observing Pix Tube

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We interviewed hundreds of Servicemen like yourself to tell us the features *you* want in a professional carrier. Model CP embodies *all* your practical suggestions. That's why Servicemen say it's today's truly unbeatable carrier value!

Other Grayburne Tube Carriers available:
Model CL: for the "long haul". Holds 200-225 tubes. $13.50 net.
Model CJ: for the "short haul". Holds 60-70 tubes. $9.95 net.

SERVICEMEN: For name of your nearest Grayburne distributor, write to us NOW!

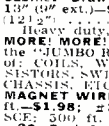
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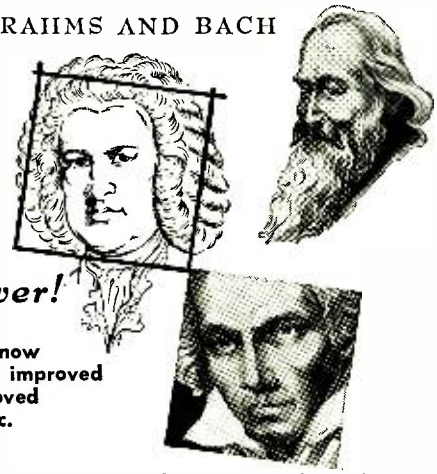
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Yes, Bach, Beethoven and Brahms are now better than ever—we don't mean we've improved their music, but we *do* mean we've improved the reproduction of their *recorded* music.



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constant stylus contact with the record grooves over the entire audio spectrum (20-20,000 cps) • full frequency response • full transient response • no resonances • no mistracking • no grinding of groove walls

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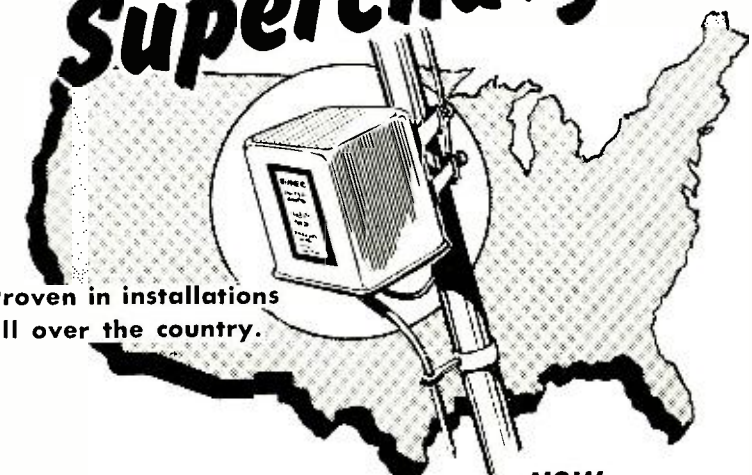
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NETSDA'S MARCH MEEING

The most recent meeting of the National Electronic Technicians' and Service Dealers' Associations was held at the Harrisburger Hotel, Harrisburg, Pa., March 2. Several important pieces of business were attended to. The National Headquarters was moved to 165 East Broadway, New York, N. Y., from its former Washington address. The attorney for the New York member of the Association was instructed to file application for a charter as a non-profit corporation in New York State. The membership application of the Radio and TV Technicians Guild of Florida was accepted.

The annual election of officers also took place. Max Liebowitz, New York City, was elected president; Roger Haines of Haddonfield, N. J., vice-president; Richard Devaney of Philadelphia, Pa., recording secretary; David Van Nest of Trenton, N. J., corresponding secretary; T. L. Clarkson of Harrisburg, Pa., treasurer; and Jack Wheaton of East Williston, Long Island, Sergeant-at-Arms.

The next meeting was set for Sunday, May 4, in New York City.

FRSAP HAS PAPER

We have received the first issue of the *FRSAP News Letter*. An eight-page paper produced by a standard duplicating process, it is an excellent job and full of news of the Pennsylvania organizations. The art work is also worthy of note. Cover design, inside heads and borders, and the cartoon are well done and interesting.

The little magazine does not confine itself to the Pennsylvania technicians' associations, but prints news of other organizations, from New York to Florida. There is also a note on community antenna systems, which are more common in Pennsylvania than in any other state.

FIX-IT-YOURSELF BOOKS

RADIO-ELECTRONICS has received letters from Frank Moch, President of NATESA, and from the Federation of Radio Servicemen's Associations of Pennsylvania commending the article "Fix It Yourself" in the March issue.

Frank Moch says "We wish to congratulate RADIO-ELECTRONICS for taking such fast and forthright action on the 'fix-it-yourself' books. Our thinking on this subject is very much akin to yours. We believe these books will lead to greater income for the service technician since it is obvious that much damage will be done by unqualified tinkering. Unfortunately, the tinkerer who does the damage won't assume the responsibility for his stupidity and will in turn pass it on to the service operator. In the meantime these books add more fuel to the fire of condemnation and derision which is burning out the souls of the legitimate operators. . . ."

The Pennsylvania Federation, while expressing no opinion as to the "material and the methods of presentation in the books," stated that "We have gone on record to investigate and have ap-

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pointed a committee to obtain transcriptions and copies of all commercials used in broadcasts, and advertising in local dailies, to study for further action. These books and the methods used to sell them, plus the unfavorable publicity the TV technicians have received in the public press, are doing much to lower consumer opinion and confidence in the servicing industry."

Meanwhile, RADIO-ELECTRONICS has information that some broadcast stations have declined to handle this type of advertising, and reports of cancellation of newspaper advertising due to protests from local bodies have been received from several points. It appears that local service organizations, in cooperation with local Better Business Bureaus and other interested bodies, are in a position to make the most effective protests against any untrue or misleading advertising which may appear in connection with these books.

SYLVANIA BACKS SERVICE

Sylvania will expand its national promotion of TV-radio service technicians during 1952, according to a statement made by Terry P. Cunningham, director of advertising. The company will use such national publications as *Life*, *Colliers*, *The Saturday Evening Post*, and *Better Homes and Gardens* to promote the cause of the service technician "displaying the Sylvania seal," and tell the public that he does a good job. "They will also tell the public how to select a reliable service technician," he stated. The campaign will also be supported on the company's "Beat the Clock" program on CBS-TV every Saturday night.

N. H. COMMITTEE FORMED

Service technicians of the Manchester, N. H., area have formed an "investigative committee" to check on all customer complaints of incompetent or dishonest TV servicing. According to Frank Lavoie, chairman of the local service association: "Many TV owners have had a scalping. For example, some television dealers never sold radios. Now they sell—and service—TV sets. . . . This leads to a lot of people having to pay for labor which cannot be done competently."

Mr. Lavoie is attempting to contact other organizations and independent service technicians in the Manchester area with the view of exchanging ideas, educating the public to the problems of TV service, formulating a code of ethics, and defining guarantees more precisely.

KINGSTON CHANGES NAME

A notice received from the Kingston (New York) Radio Servicemen's Association states that henceforth that organization will be called the *Ulster Electronic Technicians' Association*. The change is apparently meant to broaden the activity of the association to cover service technicians throughout Ulster county, instead of confining it to the city of Kingston.

—end—

New WILLIAMSON TYPE

Heathkit AMPLIFIER KIT

AMPLIFIER Features

- First Williamson Type Amplifier supplied with matching preamplifier
- Uses Altec Lansing Peerless output transformer.
- Practically distortionless — Harmonic and intermodulation distortion both less than ½ of 1% at 5 watts output.
- Frequency response ±1 db from 10 cycles to 100 kc.
- Output impedance 4, 8, or 16 ohms.

The new Heathkit Williamson Type Amplifier kit is the best obtainable in amplifiers today—the choice of the really discerning listener. You can hear the difference and measurements actually bear out the superb performance. Frequency response ± 1 db from 10 cycles to 100 kc allow you to hear the highs and lows with equal crispness and clarity. Harmonic and intermodulation distortion both less than ½ of 1% at 5 watts output eliminate the harsh and coarse-at qualities which contribute to listening fatigue.

The circuit is similar to the one published in Audio Engineering Magazine for November, 1949, and is considered by engineers throughout the audio field as one of the best ever developed. The Main Amplifier (which may be purchased separately) consists of a voltage amplifier and phase splitter using a 6SN7 a driver stage using a 6SN7, and a push-pull output stage using a pair of 807 tubes. The output transformer is manufactured by the Peerless Division of Altec Lansing, and is built to their highest standards. Output impedances of 4, 8, and 16 ohms are available. The power supply uses a separate chassis with husky Chicago Transformer power transformer and choke and 2 5U4G rectifier is used. Mallory filters for long, hum-free operation. A 5V4G rectifier is used.

The main amplifier and power supply are each on a chassis measuring 7" high by 9½" wide by 11" long.

PREAMPLIFIER AND TONE CONTROL UNIT KIT

The preamplifier kit consists of a 12AX7 (or 12AY7) dual triode first amplifier stage with a turn-over control for LP or 78 record types, and a 12AU7 amplifier stage with individual bass and treble tone controls which each provide up to 17db of boost or attenuation. A switch on panel selects either magnetic, crystal, or tuner inputs. Preamplifier also is well suited to custom installations—it will operate in either vertical or horizontal position, and special ganged shafts at the controls and switches allow a variety of shaft lengths to be selected. Dimensions: 2¼" high by 14¼" wide by 7¼" deep.

WA-A1 Amplifier kit — Combination 1 — (Main Amplifier and Power Supply) complete with WA-P1 Preamplifier kit. Total Ship. Wgt. 31 lbs. (Shipped Express only) $69.50

WA-A1 Amplifier kit only — Combination 4 — (Main Amplifier and Power Supply). Less WA-P1 Preamplifier. Total Ship. Wgt., 29 lbs. (Shipped Express only) $49.75

WA-P1 Preamplifier Kit only. (less power supply) (Tubes included). Total Ship. Wgt., 7 lbs. (Shipped Express or Parcel Post) $19.75

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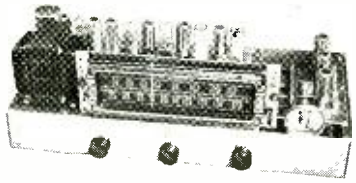
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Above: Collins FM-AM Pre-Fab Tuner After You've Assembled It. Total Kit Cost, $69.

Join thousands developing a fine radio hobby with inexpensive COLLINS FM-AM Pre-Fab Tuners — best buy in radio tuners since the crystal set! Thrilling experience in economical way to high fidelity radio reception. Radio building's a snap with COLLINS wired and tested components! Buy direct from COLLINS factory and POCKET THE SAVINGS!

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FM Tuning Unit 88-108 MC $15.25 ☐



U.C-2 Universal Chassis Kit $14.75 ☐



AM Tuning Unit (Includes IF & Audio Amplifier) $19.25 ☐

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FM-IF Amplifier 10.7 MC $19.75 ☐

Tuning Eye Kit 6U5-G $2.85 ☐



All Pre-Fab units assembled, wired, tested and aligned at factory. Prices include tubes. Chassis Kit includes all necessary parts, nothing else to buy. Instruction Manual with detailed step-by-step procedure, pictures and schematic diagrams included. Chassis measures 8" x 17"-x2½". Overall, tuner assembled measured 8"x17"x6". Expertly engineered for utmost satisfaction.

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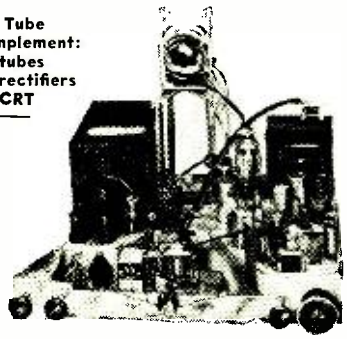
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28 tubes
3 rectifiers
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All Channel ↕ Booster

• Broad band single knob control pre-amplifier built in to eliminate long leads which may cause regeneration and attenuation of signal.

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When you buy from Mattison you need only one source of supply! You can buy a Mattison Chassis, a Mattison Cabinet or a complete Mattison TV Set!

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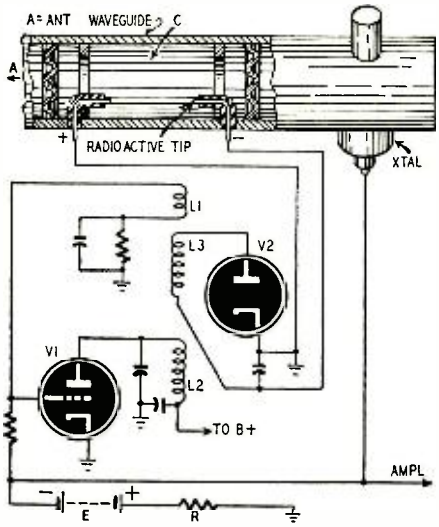
Mattison Television & Radio Corp.
893 Broadway, Dept. E2, N. Y. 3, N. Y.

R.F. ATTENUATOR

Patent No. 2,570,893

Gilbert Wilkes, Chevy Chase, Md.
(Assigned to the U. S. Government as represented by the Sec'y of the Navy)

This attenuator performs double duty. It is an effective a.g.c. device and acts as a T-R switch to protect a crystal rectifier. As described here, the invention applies especially to pulse control of a guided missile.



The figure shows a portion of the missile. Signals from the antenna pass through a wave guide to the crystal detector. The guide includes a sealed chamber C filled with gas at low pressure. The gas ionizes when a sufficiently strong current (d.c. or r.f.) flows through it. Ions act like a conductor in that they reflect r.f. waves. When ionization is complete, little or no r.f. signal can reach the crystal from the antenna because of the reflection.

The a.g.c. functions as follows. When the crystal rectifies a signal, d.c. flows through R. This produces a positive bias which tends to overcome voltage E of the battery. It raises the r.f. output of oscillator V1. L1 and L2 are the oscillator coils. The r.f. is stepped up in L3 and rectified by diode V2. Then the d.c. appears across C. With a larger antenna signal, there is more d.c. output from V2 so C is ionized to a greater degree. This, in turn, reflects more of the signal back to the antenna. This action tends to keep the crystal input at a steady value and protects it from heavy surges or pulses.

To minimize the output required from V2 for ionization, a radioactive cathode tip is used as shown. This keeps C partly ionized at all times so less d.c. is needed.

EXPANDED R.M.S. METER

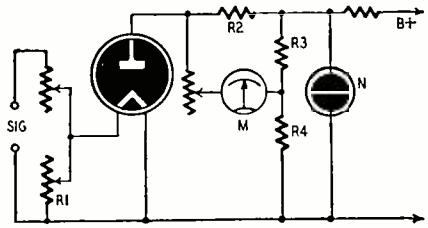
Patent No. 2,575,996

Adolph Bunblasky, New Canaan, Conn.
(Assigned to Sorensen & Co., Inc. Stamford, Conn.)

This r.m.s. volt meter is sensitive to small percentage changes above or below some pre-determined normal level.

R1 feeds a portion of the signal to the filament of a diode. The plate voltage is above the saturation value so that the total emission reaches the anode. Plate voltage is stabilized by a neon lamp N. R2, R3, R4 and the diode are arranged in a bridge network which is balanced when the input signal is normal. M is a center-zero instrument.

When the signal varies from its normal level, the bridge is unbalanced in one direction or the other. Therefore the meter indicates the increase or decrease. The unbalance is proportional to the



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HIGH FREQUENCY UNIT*

make a 3-way system from your coaxial *or a 2-way from a single speaker*

Improve the realism of your sound reproduction by adding this new compact advanced-design h-f unit to your present coaxial or extended range speaker. Sits atop cabinet or mounts flush on baffle or panel. Gives smooth, clean highs from 4,000 cycles to limits of audibility. List Price, $56. Write for free illustrated folder EA, with complete installation data.

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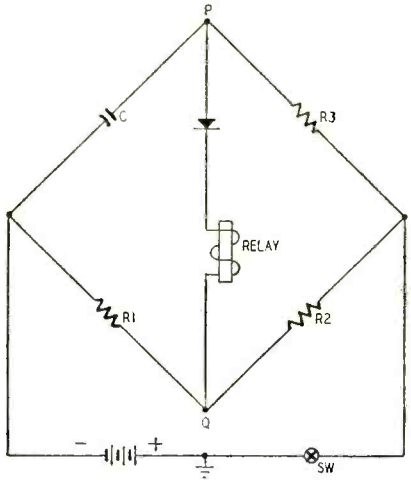
change in filament voltage. For convenience the meter may be calibrated with sine wave input, but it remains accurate regardless of wave shape.

RELAY TIMER

Patent No. 2,577,137
Frank K. Low, Orange, N. J.
(assigned to Bell Telephone Labs., Inc.)

This is a delayed action relay circuit. It eliminates the need for special copper slug relays or other expensive timing equipment. An R-C timing network is used, but timing accuracy is much better than usually obtained by this method.

The components form a bridge. The timing interval begins when the switch is closed. The flow of current through R1 and R2 establishes point Q at a predetermined positive potential. Since capacitor C had no initial charge, point P is at zero



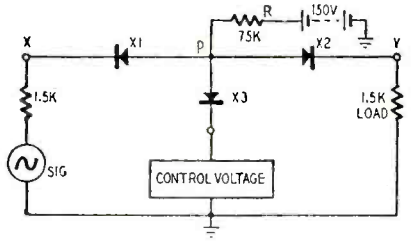
voltage. The rectifier will not conduct as long as its anode terminal P is less positive than its cathode terminal Q.

As capacitor C charges through R3, the potential at P increases and eventually becomes more positive than Q. At this instant the rectifier begins to conduct through the relatively low series resistance of the relay winding. The transition from rectifier cutoff to conduction is quite rapid and the relay is quickly energized.

ELECTRONIC SWITCH

Patent No. 2,576,026
Larned A. Meacham, New Providence, N. J.
(assigned to Bell Telephone Labs., Inc.)

This gating switch is effective up to v.h.f. It consists of a T network of germanium crystals. A d.c. control voltage biases the rectifiers to cutoff or to full conduction as required. This new circuit is more effective than previous ones. It requires relatively low control voltage to control fairly large signals. Practical component values are shown in the diagram.



If a sufficiently large *negative* control voltage is applied in the middle branch, X3 is biased to conduction. X1, X2 are cut off. The high resistance of the latter units impedes signal current flowing to the load. X3 has low resistance so it tends to short out the signal. Accordingly, very little signal can reach the load. Attenuation may be as high as 110 db, for example. When the control voltage is *positive*, X3 is blocked. The other rectifiers conduct. Therefore maximum signal reaches the load.

The signal must not be permitted to control the gating action. With components shown, its peak must be less than 3 volts. The control voltage peak must be at least 3 volts: positive to attenuate the signal, negative to transmit it.

PUZZLED?

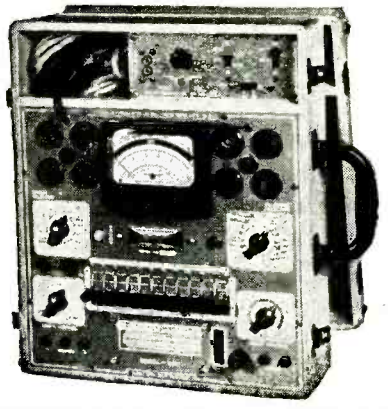


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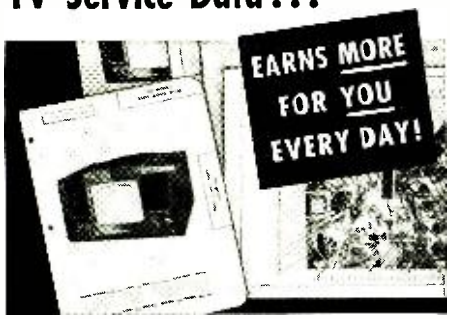
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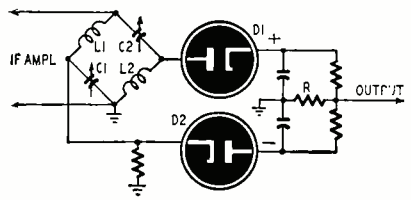
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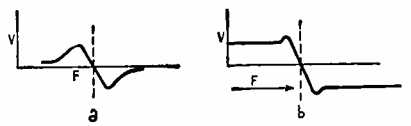
Patent No. 2,581,968
Clyde J. Norton, Braintree, Mass.
(Assigned to Sylvania Electric Products, Inc.)

This discriminator has the advantage of being tunable. Also, it supplies a voltage output even when the signal is swept far from its average value. This voltage may be used for a.f.c., for example.

Two series-resonant networks are connected as a bridge. L1, C1, are tuned to the center i.f., as are L2, C2. The bridge output is rectified by diodes. Diode D1 has a positive voltage output, since electrons flow from ground, through R, and back to the tube. D2 is oppositely connected and has negative output.



As long as the signal is unmodulated, the bridge is balanced. Each inductor has the same reactance as the capacitor which tunes it. Thus the diodes rectify equal and opposite voltages and the output is zero. When the i.f. sweeps to a higher value, L1 has more reactance than C1. Also, the reactance of L2 is greater than that of C2. From the schematic it is evident that the output from D1 will be greater than the output from D2. Thus the output is positive. During the next half-cycle of modulation, the i.f. is swept to a lower frequency and the discriminator output will be negative.



Figs. (a) and (b) show the frequency vs. voltage characteristics of conventional and the new type discriminators. Dotted lines indicate the center i.f. The new circuit (b) provides output even at frequencies far removed from the center value. This voltage can be used to control an oscillator.

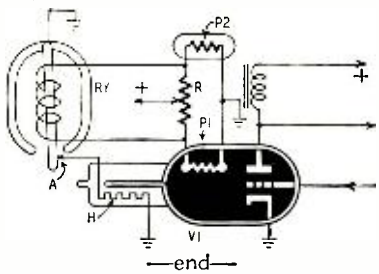
GAS SUPPLY FOR THYRATRON

Patent No. 2,582,282
Jerome Rothstein, Belmar, N. J.
(Assigned to the United States of America as represented by the Secretary of the Army)

A thyratron gradually loses its gas due to absorption or "cleanup" with the tube. Eventually the tube must be discarded because the pressure is too low. This invention provides an auxiliary gas supply. Gas is admitted to the gas tube as needed to replenish it.

An elongated glass reservoir is shown at the left of thyratron V1. The reservoir holds gas at a pressure higher than that inside the envelope of V1, and it is separated from the main tube by thin glass. V1 also includes a Pirani filament P1, which may be of tungsten. Its resistance varies with the gas pressure. A second Pirani gauge, P2, is connected to P1 and R to complete a bridge. The variable arm is adjusted for balance when a new thyratron is installed.

As gas is lost from V1, the resistance of P1 becomes lower. P2 is not affected, however. Therefore the bridge is unbalanced and relay RY operates. Contact A closes, and completes an a.c. circuit through heater H (inside the reservoir). Some of the heated gas diffuses through the thin wall into V1 until bridge balance is restored.



—end—

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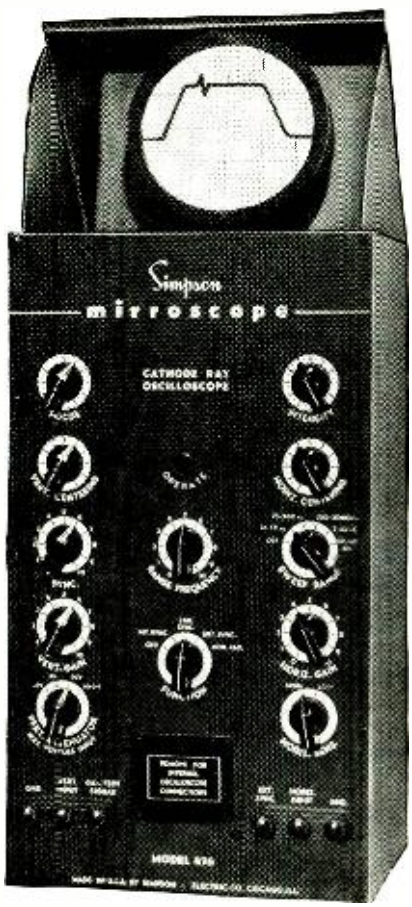
Frank J. Moch

president of the National Alliance of Television and Electronics Service Associations, says:

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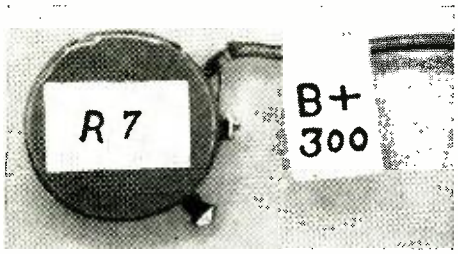
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MARKING TABS

Where tabs are required for the identification of wires and circuit components, they may be made easily with common adhesive plaster. The photograph shows the application of this material to a potentiometer and to a wire lead.

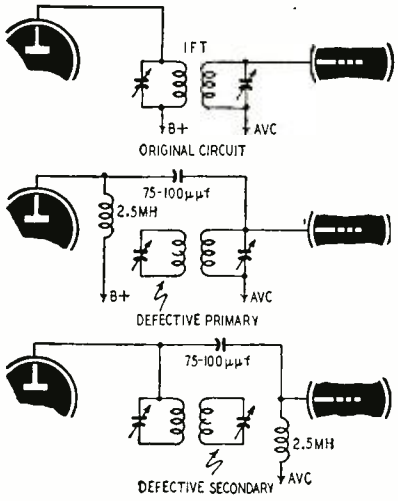


The cloth surface of the plaster takes marking well in either pencil or ink and if it is exposed to the weather, a protective coating will keep the lettering clear indefinitely. Polystyrene cement painted over the tab will provide excellent weatherproofing.—*Milton White*

SUBSTITUTE FOR OLD I.F.'S

Occasionally, a set lands on the service bench with an open i.f. transformer and the age and general run-down condition of the set do not justify the cost of a new replacement.

The circuit can be converted to use impedance-capacitance coupling as shown in the diagrams. An r.f. choke of about 2.5 mh is substituted for the open or shorted winding and the signal is carried over to the next stage through

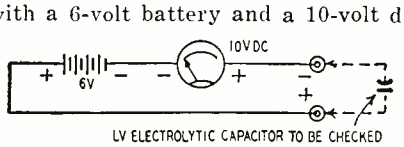


a mica capacitor of about 75 or 100 μμf. The choke can be used to replace a defective primary or secondary.

The modified circuit will not be quite as efficient as the original, so take care to align the i.f. and r.f. circuits on the nose.—*Robert M. Mayo*

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I find this circuit handy and accurate for checking *low-voltage* electrolytic capacitors for leakage. In it, the capacitor to be checked is connected in series with a 6-volt battery and a 10-volt d.c.



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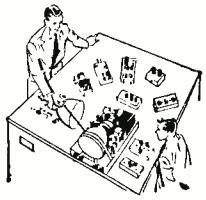
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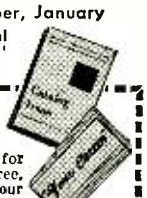
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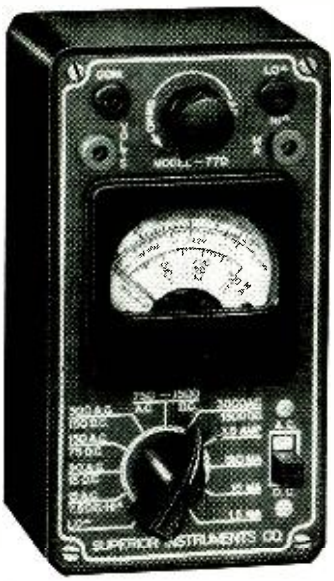
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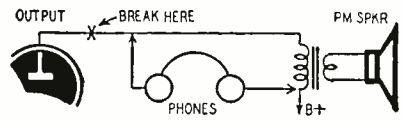
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meter. On a good capacitor, the meter will read zero or close to it. Discard the capacitor if the meter shows more than 2 volts. The units can be checked for capacitance on a standard capacitance checker.—*A. von Zook*

CHECKING RUBBING SPEAKERS

It is often difficult to locate the source of distortion or scratching sounds which occur when an amplifier or radio is played at high volume. The trouble may be in the amplifier or it may be a rubbing voice coil in the speaker. I have a sure-fire method of detecting a rubbing voice coil. Try it the next time you have



reason to suspect the speaker.

With the set disconnected from the line, disconnect the plate lead to the output tube and connect a pair of high-impedance headphones across the primary of the output transformer. Press slightly on the cone while wearing the phones. A rasping sound indicates a rubbing voice coil. The voltage step-up in the transformer and the use of phones provides a sensitive test.—*John Newall*

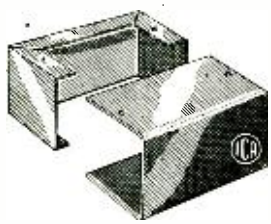
LEADS FOR R-14 PHONES

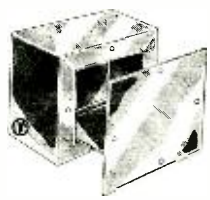
Many surplus headphones such as the popular type R-14 have special tip sockets which do not fit the tips on the replacement-type phone cords. When the cord must be replaced, this difficulty can be bypassed by purchasing phone cords with *spade lugs*. Break off the ears of the spade lugs close to the sleeves. The sleeves alone will make a neat fit in the pin sockets on the headphones.—*J. Sareda*

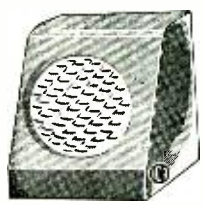
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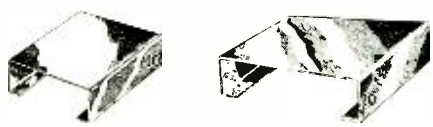

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INCREASING SENSITIVITY IN A.C.-D.C. RECEIVERS

Small table model a.c.-d.c. radios usually use loop antennas. While adequate for nearby stations, they seldom have sufficient sensitivity for satisfactory reception in rural areas.

The obvious solution is to use an outside antenna to increase the signal pickup. Usually an attempt to attach an outside aerial to the loop antenna results in the receiver starting to oscillate and squeal. Coupling the outside antenna to the receiver through a capacitor produces the same result.

One method which I have employed to couple an outside antenna to the receiver loop antenna is: With the outside antenna located as desired, take the free end of the antenna wire and wind several turns completely around the loop antenna. This effectively transformer-couples the outside antenna to the set with the loop acting as the secondary. Four or five turns usually proves adequate. A little experimenting will easily indicate the optimum number of turns. Grounding the free end of the antenna winding may give added gain.

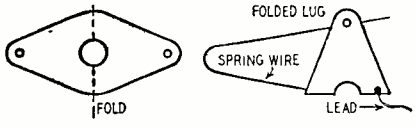
An a.c.-d.c. receiver so modified has much greater sensitivity and a better signal-to-noise ratio than a similar receiver using only the loop antenna.—*James J. Skiles*

PLASTIC PARTS BOXES

Plastic boxes sold by hardware and five-and-ten-cent stores make neat chassis and cabinets for small code oscillators, amplifiers, and similar devices. The partitioned containers are handy to have around for storing resistors, capacitors, and other small components. But be sure to select *fire-resistant* or *noninflammable* plastic! A short circuit, a hot soldering iron, or a carelessly dropped cigarette can easily start a fire if the box is made of a highly inflammable plastic.—*O. C. Vidden*

CLIPS FOR ACORN TUBES

Clips or connectors for plate and grid leads of acorn tubes such as the 956 are often difficult to obtain. In an item in *Break-In*—a New Zealand amateur magazine—ZL2QH shows how you can make your own. He takes a double-ended soldering lug and bends it double so the two end holes will slip over the grid or plate lead of the tube. A short length of thin spring steel or brass wire—about No. 24 will do—is bent into a V of about 45°, and one end is soldered into the bend of the lug.



To use the clip, press open ends of the V together and slip the clip over the tube lead. When the spring is released, it presses against the lead, holding the clip in place and insuring a good electrical contact.

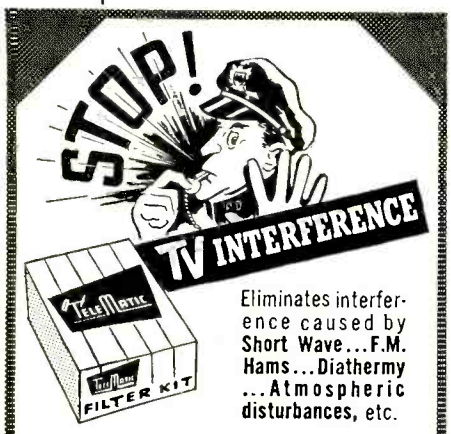
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1U4	.60	6J6	.73	12BE6	.49
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1X2A	1.25	6K6	.65	12J5GT	.50
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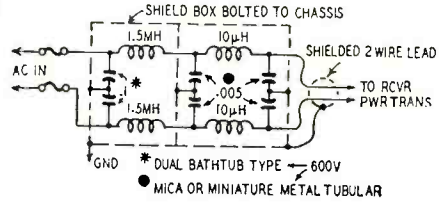
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place for the filter is in the power line feeding the device producing the noise. When this is not possible, the alternative is to place the filter in the line at the input of the receiver.

The filter shown in the diagram is designed to handle receivers drawing up to about 100 watts from the line. The input half of the filter—the 1.5-mh inductors and the 0.1-μf capacitors—attenuate the lower frequencies of the noise while the pi-section filters in the output half handle the high-frequency components. The unit is constructed in a 6- x 3- x 2-inch metal shield box with cover and dividing compartment.

The inductors are wound with No. 26 single-cotton-covered enameled wire. The 1.5-mh units consist of 300 turns

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pie-wound on a ½-inch form. These will be difficult to wind by hand, so single-pie r.f. chokes rated at 150 ma or more will suffice. The high-frequency chokes consist of 30 turns of enameled wire close-wound on a ¼-inch form. Heavier wire should be used for the coils if the set draws much over 100 watts.

The author stressed the following precautions when describing this filter in *Short Wave News* (London, England):

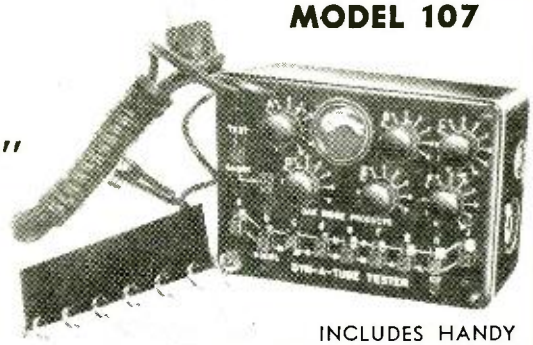
1. Keep leads on the 0.1-μf capacitors short because the capacitance and the inductance of the leads may resonate in the interference band and accentuate the noise rather than suppress it. If the physical arrangement of the components requires long leads, shunt a .005-μf mica capacitor across each 0.1-μf unit.
2. Bolt the filter case firmly to the chassis of the set. Scrape away any paint or oxide on the chassis and filter box to get a good metal-to-metal contact. Use short shielded leads to connect the output of the filter to the input to the power supply of the set.
3. *Use a good ground on the set.* Failure to ground the receiver may result in a nasty shock from the current passed by the large input filter capacitors.

RECTIFIER TESTER

This is the circuit of a handy tester for selenium rectifiers. To operate: Connect the rectifier to the Rectifier

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	39.95	24AP4 Round-Metal	69.95

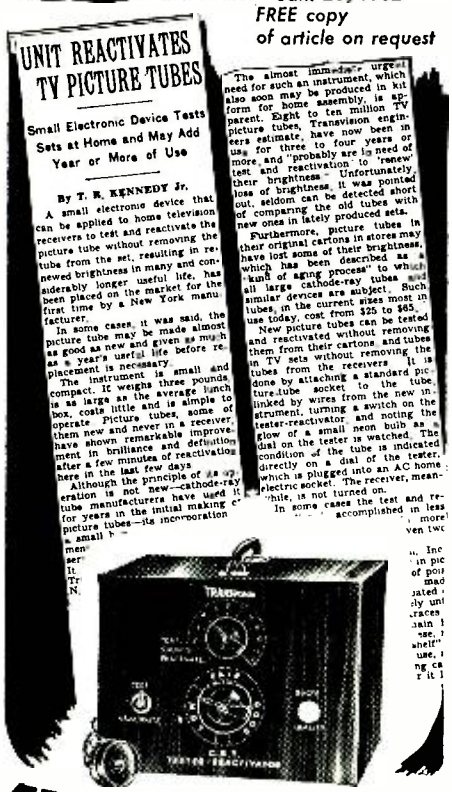
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performs 2 vital functions:

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Without removing picture tube from set, you apply this precise instrument to:—

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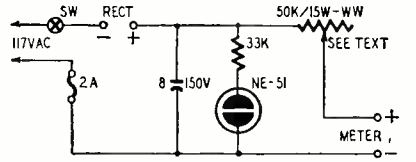
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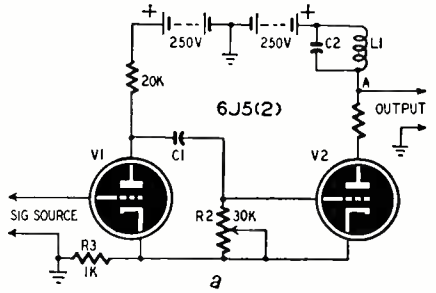
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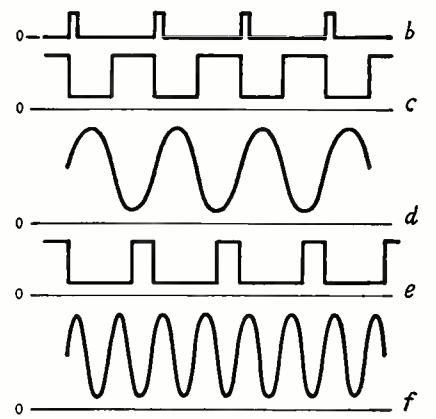
pin jacks. Be sure to observe the proper polarity. Turn on the power momentarily and watch the NE-51 neon lamp. If both electrodes glow, turn off the power at once because this indicates that the rectifier is shorted. A shorted rectifier may damage the filter capacitor if power is left on. If the lamp does not glow, the rectifier is open. If only one electrode glows, connect a milliammeter to the METER terminals and adjust the 50,000-ohm control for the rated current drain through the rectifier to test for excessive heating. Be sure that the meter polarity is correct and that its full-scale rating is higher than the current rating of the rectifier under test.—*O. C. Vidden*



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In radar, television, and similar electronic applications, it is sometimes desirable to generate a sine wave which is synchronized by pulses or other non-sinusoidal recurring signals. A simple





circuit which eliminates the a.f.c. and components needed to develop the sine wave and lock it in with the pulses is described in patent No. 2,559,144, issued to A. J. Baracket.

The circuit shown at *a* generates a sine wave at the fundamental or an integral multiple of the pulse repetition rate.

The equipment is set up with V2 drawing sufficient plate current to create enough cathode bias across R3 to cut off V1. Under this condition, the voltage on the plate of V1 equals the supply voltage (250 volts) so C1 is charged to a voltage equal to the difference between the supply voltage and the cathode bias.

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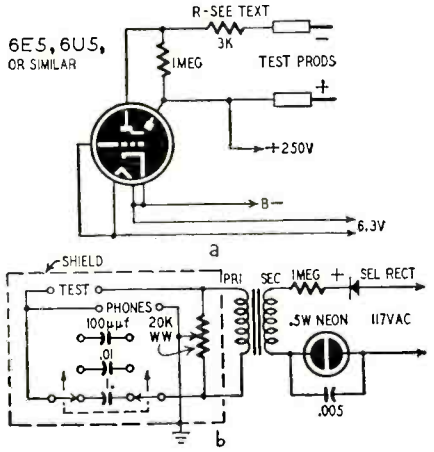
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CAPACITOR TESTERS

The capacitor checker shown at *a* and the capacitance bridge at *b* are two of a number of capacitor checkers described in an article in *Short Wave Listener* (London, England).

The checker tests mica, paper, and ceramic capacitors for excessive leakage and breakdown. It requires a 6E5 or similar electron-ray tube, two resistors, a pair of prods, and a source of operating voltage. The value of R may have to be determined experimentally. Its value should be adjusted so the shadow on the indicator tube just closes when the test prods are shorted.

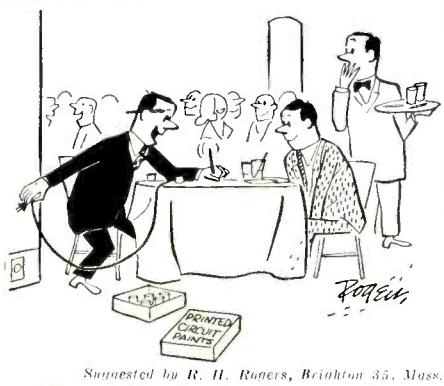


Connect the prods across the capacitor to be tested. The shadow closes if the capacitor is shorted and flickers if it is leaky or intermittent.

The capacitance bridge measures capacitance and checks capacitors for opens. The capacitors at the left are standards and should have the highest accuracy obtainable. Other values may be used if desired.

A neon-tube relaxation oscillator supplies a note of approximately 1,000 cycles to the bridge. Operating voltage is taken from the a.c. line through a selenium rectifier. The transformer is a standard audio interstage unit.

Calibrate the bridge by connecting known values of capacitance across the TEST terminals and marking the values on a scale under the pointer on the 20,000-ohm potentiometer when it is adjusted for a null in the phones. Use a separate scale for each capacitance range.



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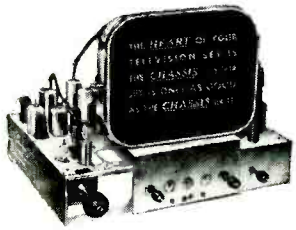
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RECEIVER-TRANSMITTER QUERY

? *I have a model 11-UF-ED-6 Link receiver and a model 32-UFM-ED-2 transmitter. Both are crystal controlled on 39.46 mc. I want to shift the frequency to 33.86 mc. The transmitter crystal is at 1,233.125 kc. The receiver uses two crystals: one at 5.456 and the other at 6.892 megacycles. What crystals must I use for the new frequency? —G. F. B., College Park, Md.*

A. The transmitter output is on the 32nd harmonic of the crystal frequency. Therefore, the new crystal frequency is 33.86/32, or 1.05925 mc. (1,059.25 kc).

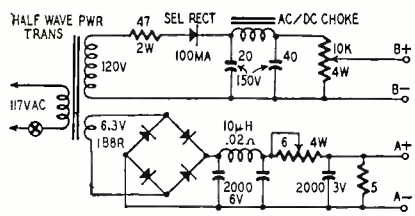
The receiver is a double superheterodyne with the first i.f. at 5 mc and the second at 456 kc. The 5.456-mc crystal is in the oscillator circuit of the second converter and is not changed. The heterodyning frequency for the first converter is 5 mc below the signal frequency and is the fifth harmonic of the 6.892-mc crystal. Therefore, at the new frequency, the heterodyning signal is 33.86 minus 5, or 28.86 mc. Since the 5th harmonic of the crystal is used, the new crystal for the receiver must be 28.86/5 or 5.772 mc.

Some of the tuned circuits may not have sufficient range to tune down to the new frequencies, so you may have to shunt the coils with small padders or add a few turns to the coils. A grid-dip meter will be helpful in checking the tuning range of the coils and in making sure that you don't pick up the wrong harmonic of the crystal.

BATTERY ELIMINATOR

? *I have a 4-tube battery-operated portable receiver which draws 11 ma at 90 volts and 250 ma at 1.5 volts. Please print a diagram of an a.c. operated battery eliminator for this set.— E. K. W., Greensboro, N. C.*

A. The power supply shown in the diagram will supply B-voltages up to 120 and A-voltages up to 3 volts, depending



on the current drain. The low-voltage rectifier may be a Mallory 1BR8 or equivalent, and the low-voltage filter choke may be a 10-μh, .02-ohm filament choke, of the type used in auto radios. The 10,000- and 6-ohm controls may be adjusted to give the desired output voltage.

AMPLIFIER MODIFICATION

? *I have an amplifier which consists chiefly of a pair of push-pull 41's operated with fixed bias and driven by a pair of 76's as voltage amplifier and phase inverter. The power transformer delivers 650 volts center-tapped to the plates of the 80 rectifier. Bias for the 41's is developed across a 985-ohm resistance in the negative lead of the supply. I want to replace the 41's*

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with 6L6's to provide higher output. Please tell me what changes are needed. —J. P., Pinales, Calif.

A. You will have to double the power output of the amplifier to get a noticeable increase in volume level. From your description of the amplifier, we gather that its maximum power output is about 10 watts, so you will have to raise the output to at least 20 watts to produce a noticeable increase in the volume level.

Since the output tubes draw about 75% of the current from a power supply in the average amplifier, we feel that the power transformer is probably rated at 100-110 ma. A pair of 6L6's delivering about 20 watts draw about 160 ma. Allowing another 30 ma for the voltage-amplifier tubes, the power transformer would have to be rated at about 190 ma. This drain would most certainly overload your power transformer.

If you feel that you need more power output, it may be that you are not supplying enough voltage to the 41 grids. The peak signal voltage applied to the grids of the 41's should be equal to the d.c. bias on the grids. Thus, if the 41's are biased at 25 volts, the r.m.s. signal should be approximately 17.6 volts. If the voltage amplifiers do not deliver this voltage with normal input signals, we suggest adding another voltage amplifier or making a modification which will cause a normal input signal to drive the amplifier to full output.

We don't think that it will be practical to try to double the output of your amplifier.

G-E 17C101

? *I have a G-E 17C101 TV receiver which does not have as much brightness as the 17C103 and similar later models. On my set, I have to turn the brightness control up full. On later models, there is plenty of reserve brightness. Which resistors should I change to increase the brightness?—A. L., South Swansea, Mass.*

A. The circuits of these two sets are identical at most of the points most likely to affect the brightness. We would be willing to bet that when your set was new, its picture was as bright as in the new sets just off the assembly line. It is normal for the picture brightness to fall off gradually as the set ages in use.

Low-voltage rectifiers decrease in efficiency, filter capacitors lose capacitance, and resistors may change value so as to lower the B-voltage and reduce the output from all circuits. Aside from the reduction in B-voltage, the loss in light output may be caused by weak tubes or changes in the values of components in the horizontal output and high-voltage circuits.

Even if the electronic circuits of the receiver are in top-notch condition you will still lose some light because the light-output of the picture tube drops off with age. Don't forget that the face of the picture tube and the surfaces of the safety glass or mask pick up an even accumulation of dirt and



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grime which is not noticeable until you start to clean it off. You can lose a lot of brightness here.

The loss in brightness is probably due partially to all of the items which we have mentioned. Start by cleaning the safety glass and tube face and replacing the low-voltage rectifiers. The next step would be to replace the high-voltage rectifier and horizontal output tubes and touch up the setting of the drive control. Of course, you could continue this process of replacing components until you end up with a new set, but why do it? You will only have to start all over again when the 1953 models come off the assembly line!

SUPERHET COIL DATA

? *I am constructing a superhet receiver for 10 to 160 meters, and need winding data for the antenna and oscillator coils The i.f. is 456 kc, the converter tube is a 6SA7, and the tuning capacitors are 140-μμf units. I want to use 1-inch coil forms.—G. F. S., Chicago, Ill.*

A. The information you requested is given in the table. The 1-3-mc antenna coil is close-wound with No. 30 s.s.c. wire. Its primary is wound over a layer of thin paper wrapped around the grounded end of the grid coil. The oscillator coil for this band is close-wound with No. 26 enameled wire.

COIL WINDING TABLE

Ant. coil (No. of turns)	1.0-3.0 mc	2.5-6.5 mc	6.3-13.8 mc	13.5-27 mc	23-47 mc
Pri.	18	12	10	9	3
Sec.	150	31	18	11	3
Osc. coil					
Full winding	70	28	16	9	3
Cathode tap	25	10	10	5	2

The antenna transformer primaries for the 2.5-, 6.3-, and 13.5-mc bands are close-wound and spaced about 1/16 inch below the secondaries. In these ranges, the secondaries are all wound with No. 26 wire spaced to occupy approximately 1 inch.

For the 23-47-mc band, the secondary of the antenna transformer is space-wound with the primary interwound with the bottom turns of the secondary. The oscillator coil is initially close-wound, then the turns are spaced as required to cover the desired tuning range.

Tracking is always a major problem when using homemade coils, so we recommmend that you use separate tuning capacitors for the antenna and oscillator circuits. A vernier dial should be used on the oscillator capacitor for tuning and logging. The antenna tuning capacitor is set to peak each signal after it is tuned in with the oscillator capacitor.

Tuning may be made easier on the higher frequencies by using a band-spread control. This should be a 30 μμf variable capacitor connected in parallel with the oscillator tuning capacitor.

—end—

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In some 1951 Motorola TV combinations such as the 17F1, 17F2, etc., a.c. speaker hum may be noticed even when the a.c. power switches on both radio and TV chassis are turned off. The remedy is to reverse the leads at the speaker pin jacks.

If the AM-FM chassis has been removed for servicing, when reinstalling it plug the speaker leads in so the ground wire from the radio chassis plugs into the pin jack which is tied to terminal 2 on the socket for the speaker plug from the TV chassis. This terminal corresponds to the ground connection on the TV chassis.—*Motorola Installation and Service Bulletin*

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Whistles throughout the broadcast band can be caused by radiation from the horizontal sweep circuit of a nearby TV receiver. This trouble originates most frequently in sets having metal picture tubes. Conductive coatings of most glass tubes minimize radiation.

The trouble can be reduced or eliminated in sets having metal picture tubes by connecting a 500-μμf, 20-kv filter capacitor between ground and the high-voltage lead running directly to the second anode. The connection to the high-voltage lead should have smooth soldered joints to avoid corona discharges. A further reduction in 15.75-kc radiation can be obtained in some instances by connecting a 0.1-μf, 600-volt capacitor from each side of the a.c. line to ground.—*Admiral Radio & TV Service Bulletin*



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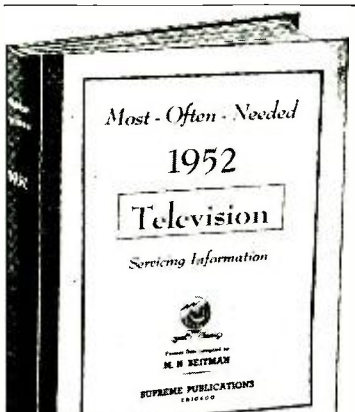
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PHILCO 51-T1443 SERIES

The filament protective fuse consists of a length of No. 26 copper wire in series with one of the filament-supply leads (black) from the power transformer. This fuse wire is connected between pin 3 of the 5AX4-GT (low-voltage rectifier) and pin 6 of the chassis power socket, J101. Always use No. 26 copper wire when replacing this fuse.—*Philco TV Service Manual*

EMERSON 661-B

If the complaint is horizontal instability or loss of horizontal sync, check for a shorted capacitor in the a.g.c. line. The short or intermittent occurs most frequently in the 200-μμf mica capacitor in the grid circuit of the second video i.f. amplifier.—*James Moudry*

PILOT CANDID TV (TV-37)

To clear up a complaint of sound bars in the picture, realign the sound trap at 21.25 mc. The sound trap is in the can with the detector coil.—*Wilbur J. Hantz*

CROSLEY 321 AND 331 CHASSIS

If it is necessary to increase the width of the picture beyond the range of the width control on models using chassis 321, 321-1, 321-2, 331, 331-1, and 331-2, remove the 15,000-ohm resistor (R24) and connect a wire between lugs 2 and 3 of the flyback transformer. Also connect a 220-μμf, 2,000-volt capacitor (part No. 137498-62) between lugs 6 and 8 of the transformer.—*Crosley Service Dept.*

DU MONT 12-INCH TV SET

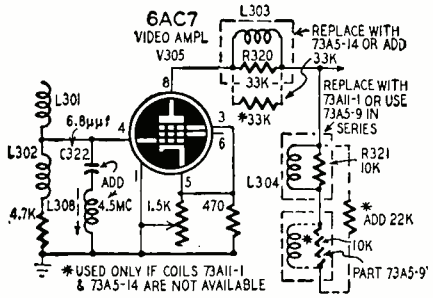
A band approximately 2 inches wide traveled upward from the bottom of the screen after the set warmed up. Tubes and voltages checked O.K. The trouble was finally traced to a hot short in one of the 6AG5 video i.f. amplifier tubes. The trouble was localized by tube substitution. The short did not show up on a tube checker.—*Jacob Dubinsky, W2LVR*

ADMIRAL 21B1 CHASSIS

Picture smear or poor definition have been reported on some of these chassis. The trouble has been traced to 4.5-mc interference in the picture when the set is tuned for best picture. When the set is tuned to eliminate the interference, it is not properly tuned for best picture.

To eliminate or reduce the interference, make the following changes while referring to the partial schematic:

1. Remove peaking coil L304 (part 73A5-9) and replace it with peaking coil, 73A11-1 which has a three-pie winding.



If part 73A11-1 is not available, use two 73A5-9 peaking coils connected in series, with short leads, so that the coils are not more than ¾ inch apart. Connect a 22,000-ohm, ½-watt resistor across this assembly.

2. Remove peaking coil L303 (part 73A5-13) and replace it with peaking coil, part 73A5-14, coded with a blue dot.

If part 73A5-14 is not available, leave part 73A5-13 in the receiver and wire across it a 33,000-ohm, ½-watt resistor.

3. Connect a series resonant trap L308, part 72B99-3 (used in 20T1 receivers), between pin 4 of V305 (6AC7) and chassis ground.

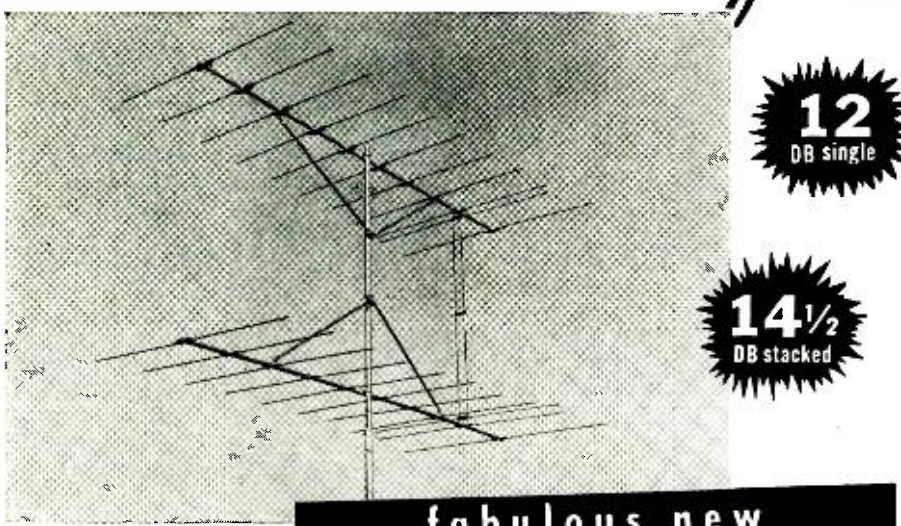
Mount the trap in the chassis hole located between tubes V305 (6AC7) and V403 (12AU7), with the 6.8-μμf capacitor C322 connected to pin 4 of V305.

4. Tune the trap by watching the picture and adjusting the slug for minimum 4.5-mc interference. If greater accuracy is required, the trap should be adjusted in the following manner:

(a) Using clip leads, short-circuit pin 1 of V201 (6AU6) to chassis ground and connect a 50-μμf capacitor between pin 8 of V305 and pin 7 of V201.

(b) Set the channel selector to a TV station having the strongest signal. Tune the fine tuning control for loudest sound. Using a non-metallic screwdriver, carefully

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adjust the trap slug for minimum sound. Warning: Do not attempt to adjust the 4.5 mc trap by using a grid-dip meter, since the reading will not be correct. *Admiral Service Bulletin*

DELCO 957582 AUTO RADIO

If this set is dead, the trouble may be traced to an open 200,000-ohm, ½-watt resistor between the plate of the 6SQ7 and the filter capacitor. This resistor is mounted with its leads clipped short. They often snap off or pull out. Replace this resistor with a 1-watt unit, leaving the leads longer than on the original.

This trouble may occur in other sets and in different parts of the circuit whenever the leads are so tight that vibration or expansion of components with heat will cause the leads to pull out.—*O. C. Vidden*

RCA 65AU

If this set is dead or intermittent, resolder all connections to the oscillator coil before looking elsewhere for the trouble. We've had several of these sets with cold solder joints on the oscillator coil.—*Clarence C. Lewis*

NOISE IN AUTO SETS

Stubborn cases of ignition noise may be caused by leakage between the antenna and the body of the car. A deposit of metal salts, caused by corrosion of the brass in the antenna, forms under the insulating washer. This leakage is too high to be measured with an ordinary ohmmeter. The noise can be cleared up by removing the antenna and cleaning its base and insulator.

In cases where noise is being picked up through the 6-volt supply—noise comes in with the antenna disconnected—one simple remedy is to run the hot lead from the set direct to the battery. Keep this lead dressed close to the body of the car.—*Frank Greene*

STANDARD COIL TUNERS

A weak, snowy picture may be caused by an inoperative r.f. stage in sets using these tuners. A common cause of this trouble (other than tube failure) is a shorted screen bypass capacitor. The best way to check for this is to remove the r.f. amplifier tube (6AG5, 6BC5 or 6CB6) and check the screen voltage from the top of the chassis. If this voltage is low or zero it will be necessary to remove the turret and replace the defective component.

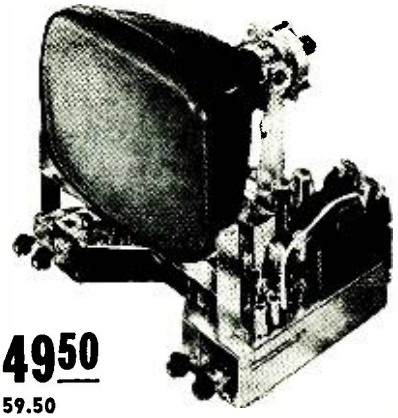
If the set has been in operation for an extended period of time with the capacitor shorted, it is advisable to replace the two resistors between the r.f. amplifier screen and B-plus point, since they probably will have been overheated by the short. Since the short lowers the B-voltage to the 6J6 oscillator-mixer tube it may also not function (unless the resistor connected to the screen has opened because of overheating). In these cases the trouble is apparent because the resistor often breaks in two.—*DeLoss Tanner*

—end—



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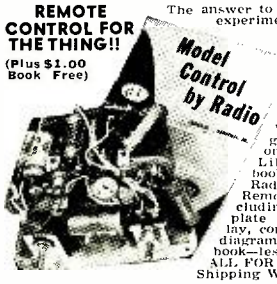
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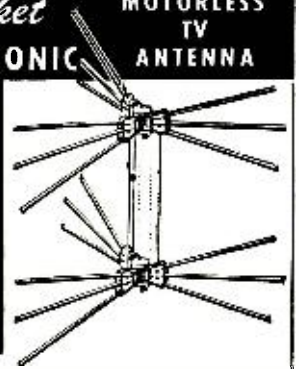
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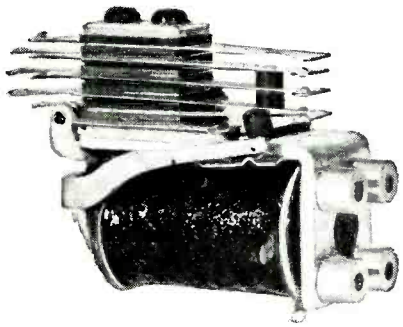
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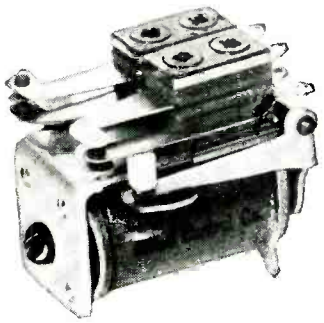
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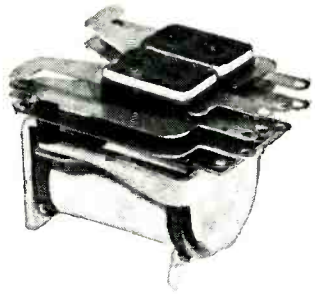
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R-850	12 VDC.	450	1A @ 1.5 AMP.	ADVANCE 1601	1.50
R-379	19/27 VDC.	250	2A @ 1.5 AMP.	ADVANCE 1605	1.65
R-694	24 VDC.	300	1A @ 5 AMP.	ADVANCE 1601A	1.50
R-935	28 VDC.	1000	1C @ 1.5 AMP.	ADVANCE 1603S	1.65
R-572	24 VDC.	256	1C	AIRCRAFT RADIO CORP.	1.25
R-857	24 VDC.	260	1 MAKE BEFORE MAKE	AIRCRAFT RADIO CORP. 9453	1.75
R-912	4/5 VDC.	20	3A-1C CERAMIC	ALLIED TKX50	1.45
R-291	6 VDC.	5	1A	ALLIED .73A71	1.25
R-921	6.7 VDC.	18	1A Dbl. Brk. @ 10 amp.	ALLIED CRX-11	1.45
R-738	12 VDC.	60	3A	ALLIED TX3A	1.20
R-922	12 VDC.	75	1A Dbl. Brk. @ 10 amp.	ALLIED CRX-13	1.45
R-144	12 VDC.	228	1A	ALLIED D-283486	1.45
R-696	24 VDC.	230	1A @ 8 AMP.	ALLIED 55837	2.00
R-145	18/24 VDC.	250	2A CERAMIC	ALLIED 7252	1.45
R-723	24 VDC.	280	1C	ALLIED 7251	1.50
R-298	21 VDC.	300	1A	ALLIED CB-5	1.25
R-296	21 VDC.	300	1A	ALLIED CA-5	1.25
R-586	21 VDC.	300	1A & 1C	ALLIED 73A-69	1.25
R-142	24 VDC.	400	2C	ALLIED 73A50	1.50
R-785	24 VDC.	200	2C @ 10 AMPS.	AUTO. ELECT. ZH-37169-1	2.00
R-375	24 VDC.	200	2A heavy duty	AUTO. ELECT. H-87063-1	1.75
R-373	12/20 VDC.	225	1A split	AUTO. ELECT. SQA	2.50
R-370	12 VDC.	75	1C	AUTO. ELECT. MANKATO R-25	2.30
R-607	24 VAC.	INT.	1A	AUTO. ELECT. MANKATO R-45-D	1.20
R-606	24 VAC.	INT.	1A & 1B	AUTO. ELECT. MANKATO R-45-F	1.20
R-605	24 VAC.	INT.	3A	AUTO. ELECT. MANKATO R-45-G	1.20
R-374	24 VDC.	300	2A heavy duty	BETTS & BETTS RAC-15AS	1.75
R-728	6 VDC.	30	1A	CLARE.....A-26690	1.25
R-149	6/8 VDC.	45	1B	CLARE.....A-20545	1.50
R-732	12 VDC.	120	1A	CLARE.....A-25454	1.45
R-281	12 VDC.	126	2A	CLARE.....A-13415	1.25
R-347	18/24 VDC.	300	1A	CLARE.....A-19469	1.10
R-376	24 VDC.	300	1A	CLARE.....K	1.25
R-818	18/24 VDC.	300	1B	CLARE.....A-8058	1.30
R-133	24 VDC.	300	NONE	CLARE.....A-20388	.75
R-348	18/24 VDC.	300	2A	CLARE.....A-16734	1.15
R-138	24 VDC.	300	4A	CLARE.....A-16280	1.45
R-349	18/24 VDC.	300	1C	CLARE.....B-16947	1.25
R-377	24 VDC.	300	1C	CLARE.....B-22441	1.45
R-132	24 VDC.	300	2C	CLARE.....	1.50
R-731	24 VDC.	300	2C	CLARE.....A-16265	1.55
R-492	24 VDC.	300	4C 1A	CLARE.....	1.95
R-626	24 VDC.	400	1A @ 5 AMPS.	CLARE.....A-22717	1.55
R-786	60 VDC.	1300	2C	CLARE.....A-12408	2.00
R-415	60/85 VDC.	1800	2A	CLARE.....K	1.95
R-371	2 VDC.	30	1C Ceramic	COOK.....418	1.75
R-755	24 VDC.	300	1A	COOK.....55340	1.45
R-150	6 VDC.	30	1A	E-Z ELECTRIC	1.50
R-893	14 VDC.	150	1A, 1C	G. E.....55526	2.50
R-895	14 VDC.	150	2A, 1B, 1C	G. E.....55531	2.50
R-896	24 VDC.	260	2A	G. E.....55589	2.50
R-959	24 VDC.	747	2C	GUARDIAN....36761	1.50
R-693	2/6 VDC.	125	1C @ 3 AMP.	LEACH.....P-501424	1.20
R-947	12/24 VDC.	320	1C @ 3 AMP.	LEACH.....P-3	1.25
R-692	6/24 VDC.	1280	1C @ 3 AMP.	LEACH.....P-3	1.35
R-856	18/24 VDC.	300	1B	PAUL HENRY 1010	1.45
R-913	6 VDC.	20	3A, 1C CERAMIC	PRICE BROS.	1.45
R-915	12 VDC.	70	1A Dbl. Brk. @ 10 amp.	PRICE BROS.	2.00
R-148	12 VDC.	100	2C & 1B	PRICE BROS.	1.85
R-222	12 VDC.	100	2A	POTT. & BRUM.	1.00
R-834	6 VDC.	20	3A, 1C	RBM	1.45

OTHER RELAY TYPES IN STOCK

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- telephone Relays
- Voltage Regulators
- Differential Relays
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Form C—"Break-Make" (Double-Throw)

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ELECTRONIC LITERATURE

Any or all of these catalogs, bulletins, or periodicals are available to you on request direct to the manufacturers, whose addresses are listed at the end of each item. Use your letterhead—do not use postcards. To facilitate identification, mention the issue and page of RADIO-ELECTRONICS in which the item appears. All literature offers void after six months.

SYLVANIA LITERATURE

Sylvania offers a number of useful booklets to the engineer and service technician. Following are a few which may be obtained without cost:

No. 211: "Radio Tube Characteristics." Standard receiving tubes, subminiature types, and germanium rectifiers are listed with characteristics and base diagrams.

No. 213: "Transmitting Tube Characteristics." Characteristics and base diagrams of tubes used in commercial and amateur transmitters are given.

No. 216: "Television Picture Tubes and General-Purpose Cathode-Ray Tubes." Technical and physical data on all types of cathode-ray tubes.

No. 217: "Electronic Tubes." Electrical specifications on Strobotrons, flash tubes, glow modulators, thyratrons, Pirani tubes, selenium rectifiers, and silicon and germanium diodes.

No. 229: "Tube Substitution Manual." Lists possible substitute tubes for TV, radio, and electronic equipment with electrical and physical alterations which may be necessary.

Available from Sylvania Electric Products, Inc., Electronics Division, 1740 Broadway, New York 19, N. Y.

RADIO & TV REPAIRS

The Feiler Engineering Co. is distributing its new revised edition of "How to Simplify Radio and TV Repairs." Helpful general facts on radio and TV servicing and the advantages of the signal-tracing technique.

. Available upon request to Feiler Engineering Co., 8026 N. Monticello Ave., Skokie, Ill.

HALLDORSON CATALOG

Catalog No. 20 is a transformer replacement guide for TV and home and auto radios produced by leading manufacturers as well as a listing of the Halldorson line of transformers, chokes, vibrators, deflection and focus coils, and Varivolt adjustable-voltage isolation transformers.

Available gratis from The Halldorson Co., 4500 Ravenswood Ave., Chicago, Ill.

TUBE TESTER CHART

A new tube roll chart for Hickok tube testers is now available. Dated January 1, 1952, this chart includes all the new tubes on which data was available at the time of printing.

Price $1.00 from The Hickok Electrical Instrument Co., 10531 Dupont Ave., Cleveland 8, Ohio.

—end—

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Radio Thirty-Five Years Ago

In Gernsback Publications

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Modern Electrics	1908
Wireless Association of America	1908
Electrical Experimenter	1913
Radio News	1919
Science & Invention	1920
Television	1927
Radio-Craft	1929
Short-Wave Craft	1930
Television News	1931

Some of the larger libraries still have copies of ELECTRICAL EXPERIMENTER on file for interested readers.

MAY, 1918
ELECTRICAL EXPERIMENTER

Television and the Telephot, by H. Gernsback

The Phenomena of Electrical Conduction in Gases, by Rogers D. Rusk, M.A.

Capt. E. H. Armstrong "Over There"

External Grid Vacuum Valve Construction, by R. U. Clark, 3rd

Microphone "Howler" for Code Practice, by Cecil A. Rich

The How and Why of Radio Apparatus, by H. Winfield Secor

Design for a Panel Transmitting Set, by James R. Hopkins

Theory of Tuning, Wave Lengths and Harmonics, by Prof. F. E. Austin

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Seeking vital combustion data in the flaming interiors of modern turbo-jets, G-E engineers have developed a "curved light" probe. A filament of fused quartz transmits light from flaming gases inside the jet around corners to an external photocell amplifier.



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Silver-plated, spring alloy, preformed finger stock especially suited for electrical "weather-stripping" for TVI-proofing cabinet access doors, etc. Also ideal for making coaxially constructed tube connections and many other uses. Available in 17/32", 31/32", and 1⅞" widths.

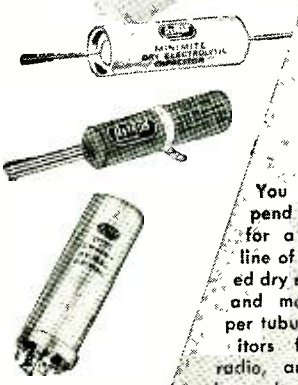
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375	408	484	509	440	466	6370	2045	2442
377	409	485	511	441	468	6450	2105	2532
378	411	487	514	442	470	6470	2125	2545
380	412	488	515	446	472	6497	2145	2557
381	413	490	516	447	474	6522	2155	3202
383	414	491	518	450	475	6547	2220	3215
384	415	492	519	452	476	6610	2258	3237
385	416	493	520	461	477	7350	2280	3250
386	418	494	522	462	479	7480	2282	3322
387	419	495	525	463	480	7580	2290	3510
388	420	496	526			7810	2300	3520
390	422	497	530			7930	2305	3550
391	423	498	531				2320	3580
392	424	503	533				2360	3945
393	425	504	537				2390	3955
394	426	506	538				2415	3995
395	427	507						
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5485	6906	7940	2045	5825	6340	6600	7573	8240
6040	7740	7973	3735	5840	6373	6606	7606	
6073	7773	8273	5305	5850	6406	6625	7640	
6106	7806	8306	5677	5873	6440	6640	7650	
6125	7840		5706	5875	6450	6673		
6140			5725	5906	6473	6706		
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Less than half the original price. Built for America's leading dep't store chain, whose name we cannot mention because of this low price. Consists of master station, remote station and 20 ft. of 3 conductor wire. Can be used as a private or non-private system. 115V AC or DC. Brand New. Now only $17.95. Additional wire per ft. .05.

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SPECIAL PURCHASE Record Changer
Gen. Instruments 3-speed Automatic

Reg. $34.95
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With all purpose cartridge & needle. Plays 33⅓-45 and 78 RPM records automatically.

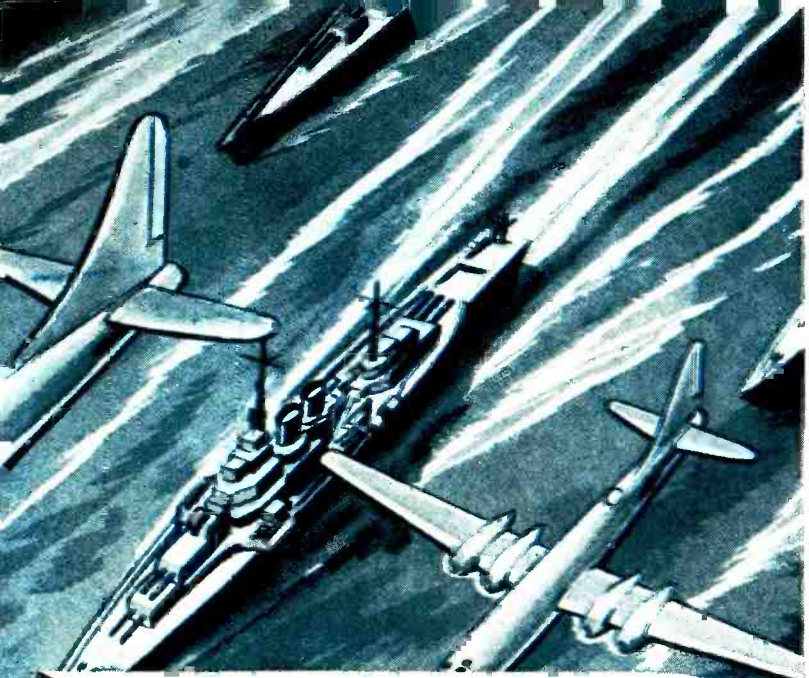
HAMS! Sun Radio is headquarters for most of the famous lines of ham gear—like National, Hallicrafters, Hammarlund, B&W, Bud, etc Write our ham department for availability and prices. W3PPQ—"Pick" is at your service.

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McMurdo 911 Sweep Gen...	78.50	44.95
McMurdo 909 Sweep Gen...	48.50	29.95
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McMurdo 700 144/240 MC XMTR less tubes	36.95	21.95
Vision TSW50 Sweep Gen. & TM10 Marker	89.50	45.00
Philco 507 Cross Hatch.....	49.95	17.50
Garrard RC 70 78RPM Record Changer	49.50	24.50
Reiner La. Model #450 VTVM	135.00	75.00
Hickok 288 XTAL Sig. Gen. (Used—Good Cond.)	186.00	125.00
Hickok 505 Scope W/Sweep (Used—Good Cond.)	208.70	140.00
Precision 10-54P Tube & Set Tester (Used — Good Cond.)	135.00	90.00
Triplett 3296 Modulation Monitor (Used — Good Cond.)	110.00	65.00
Electronic TV Magnifier....	24.95	9.95
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Current well known Tube Tester Kit	32.50	22.50
Arkay AM Sig. Gen. Kit....	19.95	14.95
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G. E. UM3 Multimeter 20,000 OHMS per volt (discont. model)	39.50	27.50
Well known make HI-FI AMP. Kit	25.80	17.95
Rauland 1825 A-HI-FI AMP.	93.06	62.50
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. . . and TV ANTENNAS too!

Amphenol has long been recognized as one of the world's leading manufacturers of radar and communications antennas for civilian and military use. When Amphenol's famed team of engineers originated the Inline Antenna, they incorporated into their design the best in mechanical and electrical characteristics that years of antenna research had developed.

In the almost four years since the Amphenol Inline Antenna was originated, many other types of antennas have come into the TV market. Comparison with the manufacturers' own test data and reports reveal that the Amphenol Inline is still the superior all-channel TV antenna.

AMERICAN PHENOLIC CORPORATION
1830 SOUTH 54th AVENUE • CHICAGO 50, ILLINOIS

AMPHENOL INLINE*



People

Dr. W. R. G. Baker, General Electric vice-president and general manager of the G-E ELECTRONICS DIVISION at Syracuse, N. Y., was awarded the Medal of Honor of the I.R.E. at its annual convention in New York City. The medal, the highest honor of the Institute, was presented to Dr. Baker for distinguished service rendered in the science and art of radio communication.



DR. W. R. G. BAKER

William J. Doyle, for many years general sales manager of the ASTATIC CORP., Conneaut, Ohio, was appointed vice-president in charge of sales, according to an announcement by L. D. Cahoon, president of Astatic.



W. J. DOYLE

Bruce E. Vinkemulder was appointed distributor sales manager of the Capacitor Division of SANGAMO ELECTRIC CO. Mr. Vinkemulder was formerly in charge of engineering publications for electronic equipment manufactured by Sangamo. He will make his headquarters at the Sangamo capacitor plant in Marion, Ill.



B. E. VINKEMULDER

Matthew D. Burns was appointed general manager of the Radio Tube Division of SYLVANIA ELECTRIC PRODUCTS, INC. His headquarters will be at Emporium, Pa., home of the Division. Mr. Burns was formerly general manufacturing manager of the division. Walter A. Weiss, formerly manager of the division's receiving tube plant in Burlington, Iowa, succeeds Mr. Burns as general manufacturing manager.



M. D. BURNS

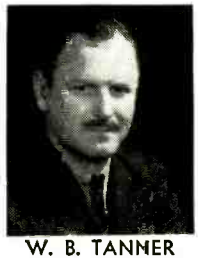
Sylvania also announced the appointment of its vice-president, C. A. Haines, as head of a new exchange department to supervise the planning of plant expansion. Mr. Haines was formerly in charge of operation of the Radio and Picture Tube Division.

Ray Whitmore, district sales manager at Syracuse for the AMERICAN PHENOLIC CORP., Chicago, was placed in charge of the company's new offices in the Empire State Building, New York City. The office will handle industrial sales only. Walter B. Wasson, formerly of the Chicago office, was placed in charge of the Syracuse office.



R. WHITMORE

William B. Tanner was appointed director of advertising, in charge of an enlarged Advertising Department formed by AEROVOX, New Bedford, Mass. The new department will handle all advertising and publicity for Aerovox, including the Hi-Q division and Wilker Products, Inc., a subsidiary. Mr. Tanner was formerly advertising and personnel manager for the Hi-Q Division of Aerovox. He will transfer his headquarters from Olean, N.Y., to New Bedford, Mass. Fred P. Donati, advertising manager of Aerovox will assist Mr. Tanner in handling the advertising of all the company's divisions and subsidiaries.



W. B. TANNER

Louis H. Niemann was appointed eastern sales manager of HYTRON RADIO & ELECTRONICS CO., Salem, Mass. He succeeds Fred Garcelon who was promoted to assistant to John Q. Adams, Hytron vice-president in charge of sales. Mr. Niemann comes to the company from Sylvania Electric Products, Inc.



L. H. NIEMANN

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Personnel Notes

. . . **Paul A. Walker** was named chairman of the FCC. Robert T. Bartley was appointed to fill the vacancy on the commission created by the resignation of Wayne Coy.

. . . **William L. Rollins** was named vice-president in charge of industrial sales for CRESCENT INDUSTRIES, INC., Chicago. Mr. Rollins has been with Crescent for over 13 years. The company also announced the appointment of Edward M. Gietl as manufacturing manager. He will be in complete charge of the production of speakers, record changers, and allied products.

. . . **R. W. "Bill" Woodbury,** a veteran West Coast parts distributor, joined the field staff of SPRAGUE PRODUCTS Co., North Adams, Mass. He will call on Southern California distributors.

. . . **Don E. Larson,** advertising manager of HOFFMAN RADIO CORP., Los Angeles, and chairman of the Publicity and Publication Committee for the 1952 Western Electronic Show and Convention, appointed the following committeemen: James L. Fouch, Cinema Engineering Co.; Byron Cole, Packard-Bell Co.; and Lloyd Sigmon, KMPC.

. . . **James A. Sullivan,** a veteran in sales and engineering positions in the electronics field, joined the sales staff of OXFORD ELECTRIC CORP., Chicago speaker manufacturer. He will work directly under Hugo Sundberg, vice-president and manager.

. . . **Joseph Maresca** was appointed assistant to Bernard L. Cahn, general sales manager of the INSULINE CORP. OF AMERICA, Long Island City, N. Y. He will continue to act as manager of the Sales Order Department.

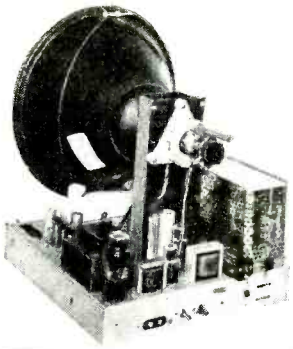
. . . **Leslie E. Woods,** director of industrial relations at RAYTHEON MANUFACTURING Co., Waltham, Mass., was ap-

Finest TV CHASSIS complete with TUBE!

12½" picture tube with complete chassis including:

- beautiful bronze metal mask
- permanent magnet 12" speaker
- all tubes aligned perfectly
- ideal for fringe areas . . . works better than other receivers and where others can't
- ultra-sensitive fringe area tuner
- standard 90 day guarantee on all tubes and parts
- full band reception and output
- gated AGC—finest automatic gain control
- COMPLETE . . . READY TO OPERATE

complete, including the picture tube, licensed by RCA $89.50



Fringe Area Double "V" TV ANTENNA . . . complete with all hardware, 300 ohm line and 9 ft. mast $7.95

16" picture tube with complete chassis including:

- gated AGC—finest automatic gain control
- full band reception and output
- standard 90 day guarantee on all tubes and parts
- ultra-sensitive fringe area tuner
- ideal for fringe areas . . . works better than other receivers and where others can't
- all tubes aligned perfectly
- permanent magnet 12" speaker
- beautiful bronze metal mask
- COMPLETE . . . READY TO OPERATE

complete, including picture tube, licensed by RCA $129.50

CUSTOM-BUILT CABINETS



Beautifully designed console cabinets with luxurious mahogany finish . . . dimensions: 38" High x 22¼" w. x 18¼" d. Fits 12½" and 16" tube (specify size when ordering)

ONLY $44.95

20% deposit with order; balance C.O.D.; Ship F.O.B. Chicago; SATISFACTION GUARANTEED; Illinois residents add 2% sales tax.

THERE IS A LIMITED QUANTITY . . .
ORDER TODAY!

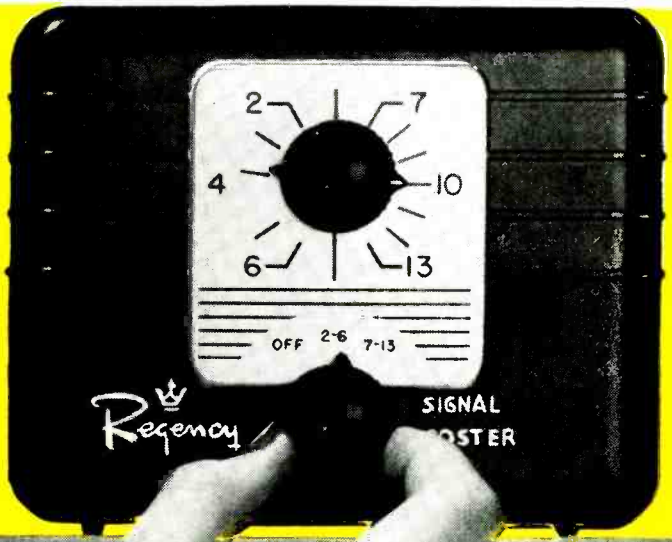
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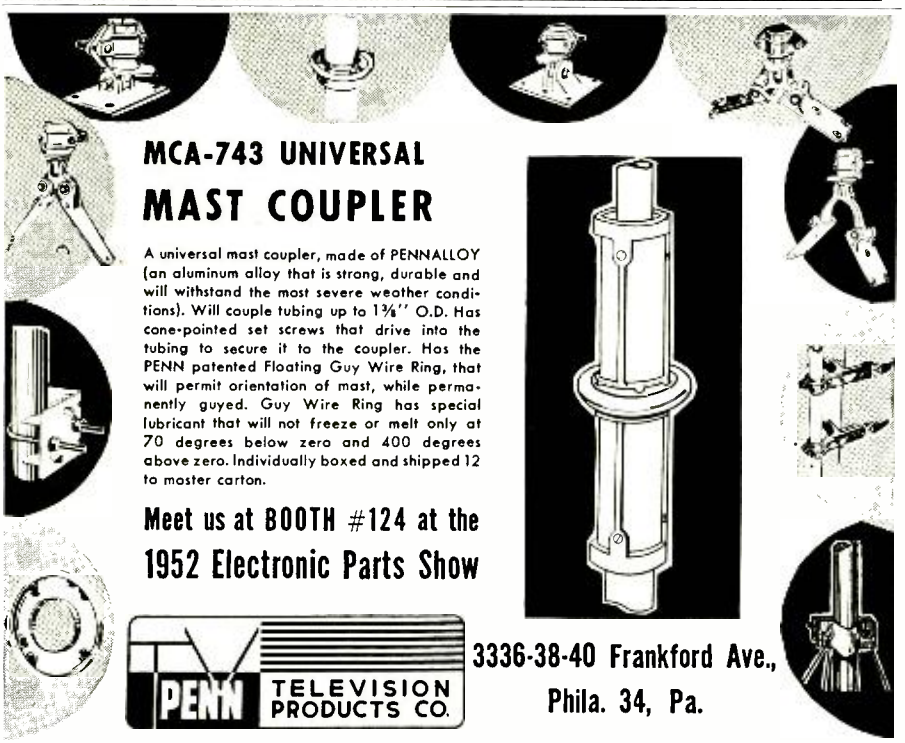
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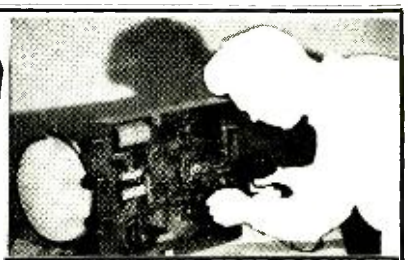
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pointed a member of the New England Regional Labor-Management Committee for Defense Manpower.

. . . **M. R. Fieldman**, connected with transformer sales operations for several years, was appointed sales manager of THE HALLDORSON CO., Chicago.

. . . **Dr. P. S. Christaldi**, former engineering manager of the Instrument Division of ALLEN B. DU MONT LABORATORIES, Clifton, N. J., was promoted to the post of assistant division manager. Other promotions included G. Robert Mezger to engineering manager, Emil G. Nichols to technical sales manager, and Melvin B. Kline and William G. Fockler to assistant engineering managers.

. . . **Roy Steele** was appointed advertising manager of WELLS SALES, INC., Chicago.

. . . **Roy W. Augustine**, research engineer for the MUTER COMPANY, Chicago, was presented a certificate of appreciation by the Department of the Army for his European electronic research conducted during the last year of World War. II.

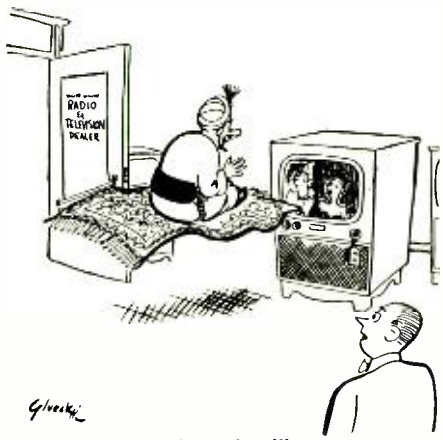
. . . **Caywood C. Cooley** and **Carl W. Schmelzle** were appointed sales manager and assistant sales manager, respectively, of the JERROLD ELECTRONICS CORP., Philadelphia. Mr. Cooley was formerly chief field engineer, and Mr. Schmelzle was associated with Philco.

. . . **I. L. Brandt** joined TAYLOR TUBES, INC., Chicago, as chief engineer. He was previously with Continental Electric Co.

. . . **Arthur J. Costigan**, vice-president in charge of communications of the RADIOMARINE CORP. OF AMERICA, New York City, was presented the Marconi Memorial Medal of Achievement at the 27th Anniversary Dinner of the Veteran Wireless Operators Association held in New York City.

. . . **Willis C. Toner** was appointed manager of SYLVANIA ELECTRIC PRODUCTS' Television Picture Tube Division plant at Seneca Falls, N. Y. He was formerly plant manager at the Ottawa, Ohio, plant where he was succeeded by Gordon L. Fullerton, formerly manufacturing superintendent there. Homer D. Broker, former plant manager at Seneca Falls, was transferred to Boston as staff assistant to the divisional manufacturing manager.

—end—



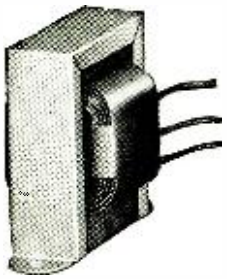
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TV DX IN LARAMIE

Dear Editor:

I feel that I owe you a note of thanks for your articles on TV dx. They were interesting enough to cause me to go out and see if I could find a receiver. The local music store had two Admiral 20X1 chassis stored upstairs. They had received them in a shipment of combinations and had taken the TV chassis out, converting the space to record compartments. No one wanted them, so I took home both for only $50 each. All they needed were speakers (which the junk box promptly furnished).

The same night I hooked up one receiver to a two-bay folded-dipole-and-reflector array cut for the FM band. I didn't even know what all the controls were for, but 20 minutes later I heard San Francisco on channel 4, though I got no picture. That was around 7 p.m. and it lasted for about 30 minutes.

This took place in January, and for the next two months I kept the set on from 9 a.m. till midnight. I got frequent bursts of voice and music but never got a picture. Finally the little woman made me take the apparatus out of the house.

I dug up back issues of RADIO-ELECTRONICS and started studying TV circuits and antennas in earnest. After reading your dx reports and articles, I told my friends to sit tight; that along about June or July I would show them some pictures via sporadic-E.

June 8 I lugged the set back into the house and hooked it up to a channel-4-and-5 twin Yagi.

The next morning after breakfast I turned on the set and sat down to read the Sunday paper. As soon as the set warmed up all hell broke loose—all channels were full of music and pictures! They were the first TV pictures I had ever seen and in the next hour the house was full of people all wanting a look.

In the next two months there was hardly a day when one or more TV programs were not received. Altogether 30 stations were picked up, from as far east as New York City and Richmond, Virginia and from the west coast as well as the central states.

All stations had to show a picture for 5 to 10 minutes or they were not considered as logged. The West Coast, Texas, Chicago, Tennessee and Michigan stations usually gave programs from 30 minutes to several hours with very powerful signals. In fact the contrast had to be turned way down to bring out any detail. All stations were in the low band, with the greatest number on channel 4.

Laramie is down in a valley, with Sherman Hill 12 miles to the east at about 7,850 feet elevation, and the Snowy Range 30 miles to the west. The nearest TV station is in Salt Lake City, about 400 miles west. The antennas used for most of the reception were: a stacked channel 4 folded dipole with reflectors, and a single-channel 2-dipole and reflector, both on the same mast. One Admiral was hooked to each array using separate transmission lines.

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SPECIAL OFFER: Additional 5% discount on all shipments of 100 tubes or more assorted!

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1F5G .49	6AB4 .69	6H6 .59	7C4 .69	12SQ7GT .69	45 .69
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Mfd.	W.V. DC	Net each	Mfd.	W.V. DC	Net each
16	150	.29	40 x 40	150	.45
24	150	.35	50 x 30	150	.45
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40	150	.39	8 x 8	450	.49
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3" PM	.68 oz. $1.09
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6" PM	1.0 oz. 1.59
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8"x8" PM	3.16 oz. 3.49
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10" PM	6.8 oz. 5.95
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7¼" 4-ohm dynamic less output $2.19
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List $32.50
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500 Mmfd @ 20 KV **ONLY 59¢**

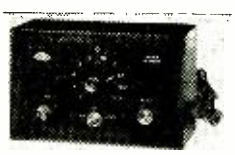
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Very simple to hook up, instructions included. Special, while they last! ..

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That way we could check antenna results and also receive two channels at the same time.

The twin-driven Yagi was taken down, as I felt it was not broad-band enough to cover channels 2 to 6. However, at times it gave excellent reception on all channels. A rhombic was also tried, and at times it would pick up signals when the others wouldn't even show a bar. For dx work I think that you can't beat the plain folded dipole and reflector.

One of the sets was completely out of alignment. We followed the Photofacts procedure and re-aligned it with an inexpensive AM generator and a v.t.v.m. The generator only went to 30 mc so we had to use harmonics for aligning the tuner, but it worked out swell. Then we tuned in a weak signal and peaked the tuner slugs, then the picture i.f.'s for best picture; then the sound i.f.'s were peaked for best sound that would still leave the best picture. This might sound screwy but it's what we did, and it resulted in a set that would bring in a faint signal and lock it perfectly. We then checked this set against the other and also against another set that someone else had brought to Laramie when he moved here from a TV area. The realigned set would consistently show pictures when the other two wouldn't make a bar.

Also built several boosters and gave them a good try, but found out that if the d.x. is there it's there, and if it isn't a booster don't help a bit. They would help out on the very weak signals but even then they always boosted the noise and snow so you didn't gain enough to bother with them.

Our latest addition is a Mattison Silver Rocket with a built-in Bogen booster. It is a modernized 630TS and is particularly adaptable to dx work, since the bottom of the chassis can be reached without taking the set out of the cabinet. By drilling a couple of holes under the sound take-off i.f. and one under the sound-discriminator transformer, you can reach in and realign the set any way you wish. All the other transformers can be reached through the cutout portion of the panel on which the chassis rests.



The picture is one of my brother—who helped me stand watch on sporadic-E dx and to compile lists—sitting beside the older Admiral chassis.

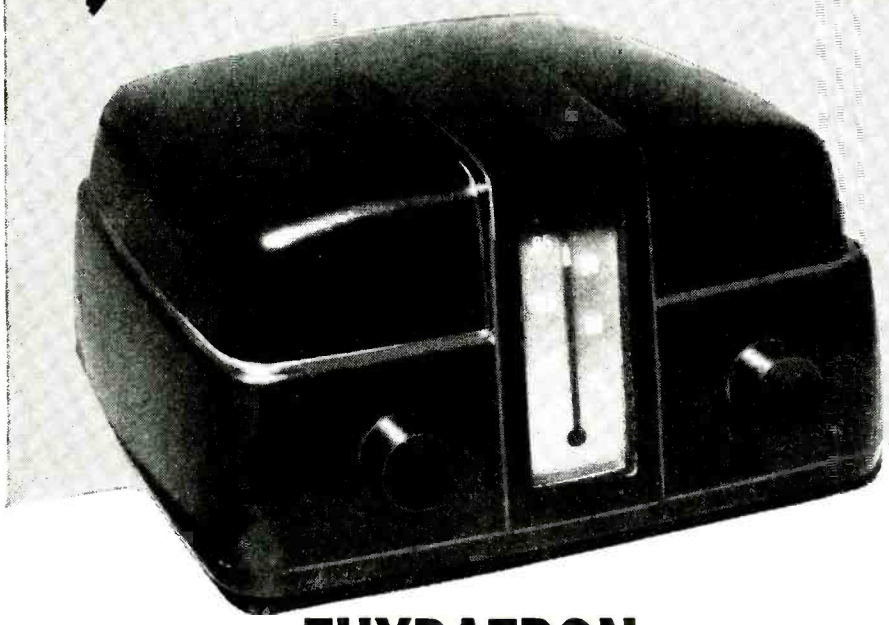
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Your own ingenuity and inventiveness can devise many more interesting and practical uses which this remarkable unit can control for you. A complete schematic is furnished with each control.

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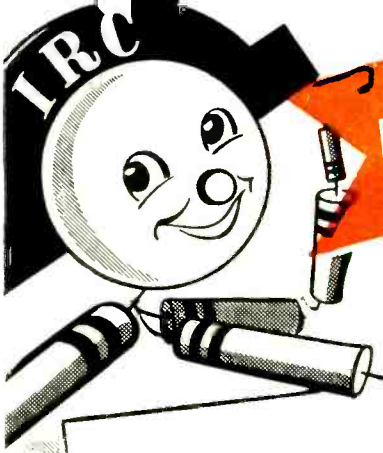
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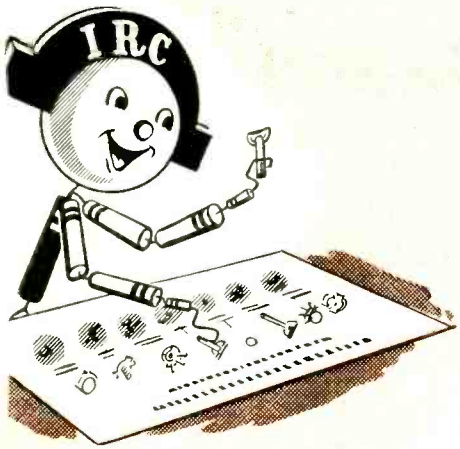


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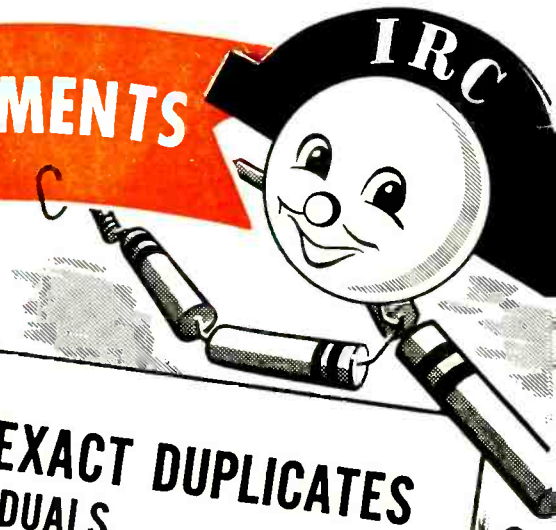
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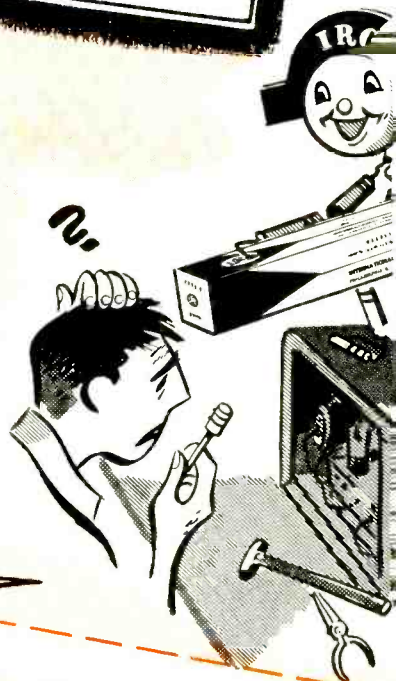
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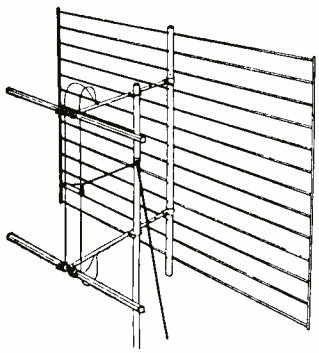
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ELECTRICAL MEASUREMENTS, by Forest K. Harris. Published by John Wiley & Sons, Inc., New York, N. Y. 6 x 9 inches, 784 pages. Price $8.00.

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Preliminary theory of measurements includes various systems of units, error calculation, and availability of standards. This is followed by chapters on meters. The author describes their construction and use, and gives the mathematical theory to analyze motion, damping, sensitivity. In addition to the magnetic type, we learn about electrostatic, thermoelectric, electronic, rectifier, and others. Besides electrical measurements, information is provided on measuring waveform, frequency, power and magnetism. The use of instrument transformers is shown.

The last chapter deals with bridges for a.c. Detectors, oscillators, stray admittance and bridge transformers are described in addition to the bridges themselves.—*IQ*

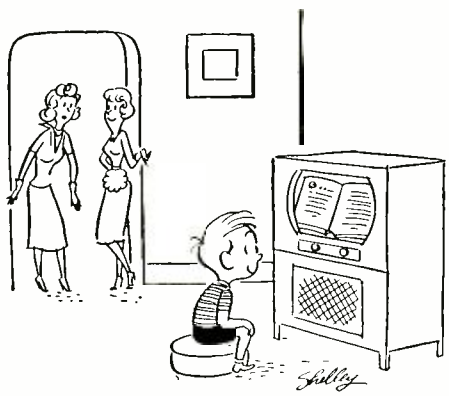
MOST-OFTEN-NEEDED 1952 TELEVISION SERVICING INFORMATION (Volume TV-6), compiled by M. N. Beitman. Published by Supreme Publications, 3727 West 13th St., Chicago 23, Ill. 8¼ x 10½ inches. 192 pages. Price $3.00.

The latest edition of the Most-Often-Needed series contains chassis drawings, diagrams, voltage and resistance measurements, alignment data, waveforms, and other valuable servicing information on well over 500 different models and chassis produced by about 30 TV manufacturers.—*RFS*

DESIGN OF SWITCHING CIRCUITS, by William Keister, Alistair E. Ritchie and Seth H. Washburn. Published by D. Van Nostrand Co., New York, N. Y. 6 x 9 inches, 556 pages. Price $8.00.

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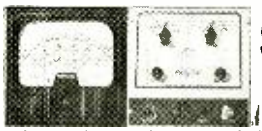
transistors, multivibrators, and other switching elements. Of special interest is a chapter on Boolean (switching) algebra. Other chapters deal with relays in combination and sequence, electronic switching, counting, selecting, timing, pulse generating, checking, registration, and calculating. Problems accompany each chapter. Tables, diagrams, and practical examples are added.—*IQ*

AMERICAN STANDARD GRAPHICAL SYMBOLS FOR SINGLE (ONE) LINE ELECTRICAL ENGINEERING DIAGRAMS. Published by American Institute of Electrical Engineers, 33 West 49th Street, New York 18, N. Y. 8½ x 11 inches, 42 pages. Price $1.40.

Single-line diagrams are useful for indicating the path of a circuit and the functions of its components. Unlike conventional schematics, actual conductors and connections are not shown. For example, an amplifier is shown merely as a triangle pointing in the direction of transmission. Tube elements, power supplies, etc., may be omitted. A single line is drawn for the amplifier input, another for the output. This type of diagram is easy to prepare. At a glance it shows how a system operates and the general arrangement of the parts.

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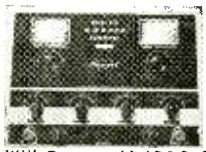
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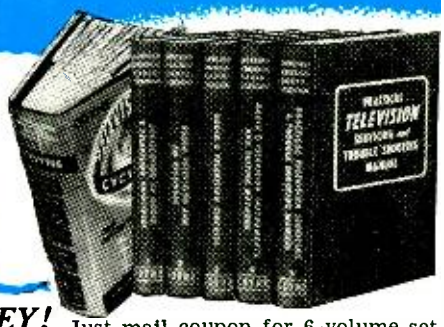


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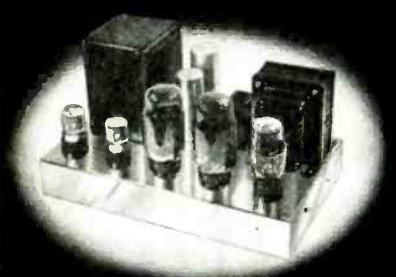
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12 Amps.	8.50	16.00	25.50	52.50
20 Amps.	13.25	24.00	36.00	.....
24 Amps.	16.00	31.00	48.00	.....
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1A7GT	1.00	6BE6	.50	12AU7	.75
1B3GT	.85	6BG6G	1.20	12AV6	.55
1AE4	1.10	6BH6	.80	12BA6	.70
1N21	.80	6BK7	1.40	12BA7	.90
1N21B	3.50	6BQ6GT	.70	12BD6	1.25
1N23	1.45	6BY5G	1.10	12BE6	.70
1N23A	2.50	6C4	.65	12SA7	.75
1N23B	3.75	6CB6	.85	12SF5	.70
1N34	.65	6CD6G	1.75	12SH7	.95
1N34-A	.88	6F6M	.95	12SJ7	.75
1N54	.90	6F7	.98	12SK7	.75
1R5	.65	6F8G	.98	12SL7	.75
1U4	.65	6G6G	1.10	12SQ7	.75
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2B7	.75	6J5GT	.55	25BQ6GT	.98
2E24	3.95	6J6	.75	25L6GT	.65
2E26	3.25	6J7	.95	35C5	.60
2E30	2.35	6K6GT	.79	35Z5GT	.55
3A4	.85	6L7	.98	50C5	.60
3D6	.50	6R8	.80	50L6GT	.60
3Q4	.55	6S7M	.98	80	.60
3Q5GT/G	1.00	6SA7	.75	211	.75
3S4	.90	6SF5	.85	304TL	8.95
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5U4G	.59	6SH7	.70	717-A	.98
5V4G	1.05	6SJ7GT	.75	807	1.65
5X4G	.85	6SJ7M	.80	GE872-A	4.50
5Y3GT	.49	6SK7	.65	955	.45
5Z3	.95	6SL7GT	.75	1280	.80
6AB4	.75	6SN7GT	.65	1603	4.95
6AB7	.98	6T8	1.25	1616	.75
6AC7	.98	6U4GT	.80	1624	1.40
6AH6	1.50	6V6GT	.60	1625	.40
6AJ5	1.65	6W4GT	.60	1626	.40
6AG5	.85	6X4	.45	1629	.30
6AG7	1.50	6X5GT	.45	2050	1.50
6AK5	.95	6Y6G	.95	5608-A	3.95
6AK6	1.30	7A6	.65	5910	.75
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The last page provides an index to all symbols.—*IQ*

RECORDING AND REPRODUCTION OF SOUND (second edition), by Oliver Read. Published by Howard W. Sams & Co., Indianapolis 5, Ind. 6 x 9 inches, 790 pages. Price $7.95.

An excellent reference work on audio for the practical man. It should find a prominent place in libraries of audio technicians, home recordists and hi-fi hobbyists.

The volume is packed with data on recording and reproducing, especially on disc and magnetic tape and wire. Many commercial instruments are described in detail. Adequate space is devoted to accessories and circuits, microphones, speakers, filters, attenuators, tuners. Charts provide filter data, db information, circuit responses, etc. Math is held to a minimum. In spite of the wide coverage and unusual size of the book, few technical errors and misleading statements were noted.

An extensive appendix will be found useful. It includes a glossary of terms, a bibliography, color codes, filter design tables, logs, R-C amplifier data, and other information.—*IQ*

FUNDAMENTALS OF ELECTRONICS AND CONTROL by Milton G. Young and Harry S. Bueche. Published by Harper & Brothers, New York, N. Y. 6 x 9 inches, 525 pages. Price $6.00.

This is a first course in electronics which stresses both the theoretical and practical viewpoints. It is unusual in its completeness, readability and logical arrangement. It is recommended for those who intend to specialize in the field, as well as for students of other branches of engineering.

The first chapter explains electron theory. The next covers circuits for a.c., d.c., and transients. In addition to R, C, and L, other circuit components are treated. These include thyrite, varistors, thermistors, saturable reactors, and other components found in modern circuits. The third chapter describes the principles of emission.

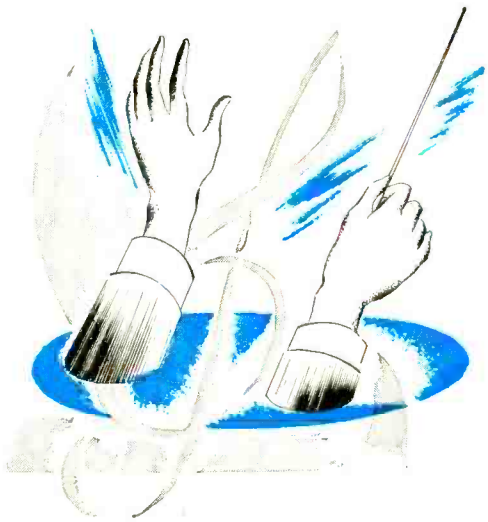
Succeeding chapters elaborate on the basic fundamentals of the first three. There is a chapter on vacuum tubes, another on gas tubes, and one dealing with mercury-pool tubes. These are followed by circuit chapters: amplifiers (tube, transistor, magnetic, rotating); oscillators for l.f. and h.f.; modulators; rectifiers. Equations are given where needed to aid the reader, but this is not a mathematical book.

Each chapter is followed by problems (with answers) and a reference list. MKS units are employed.—*IQ*

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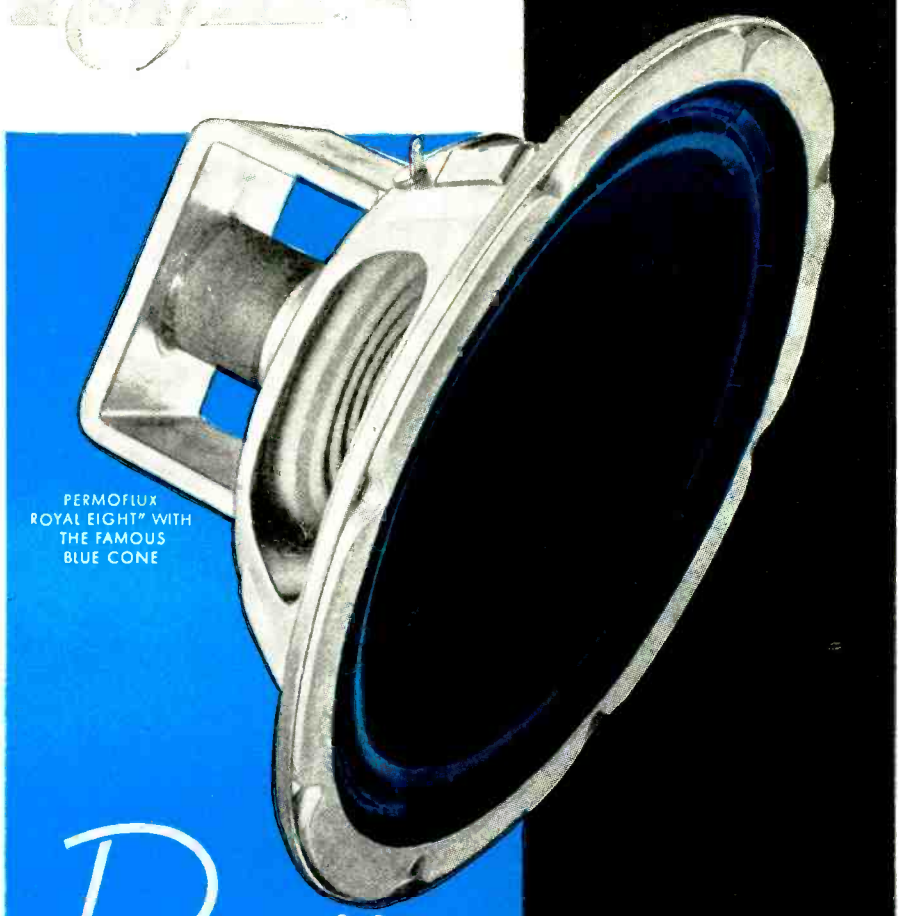
CORRECTION

The price of the book, *Audio Amplifiers and Associated Equipment*, Vol. 3 (Howard W. Sams & Co.), was incorrectly given in the book review on page 137 of the March, 1952 issue. The correct price of this book is $3.95.



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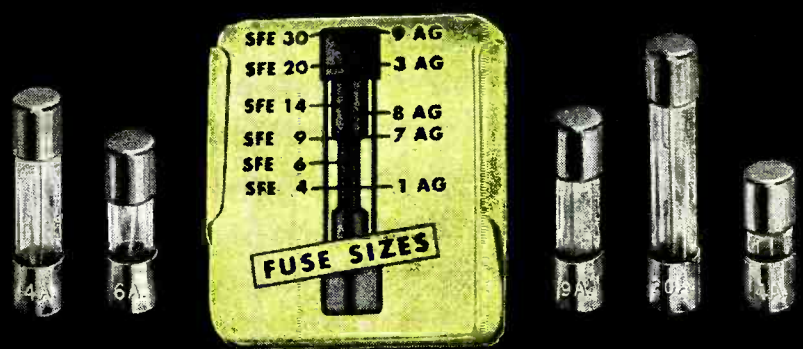
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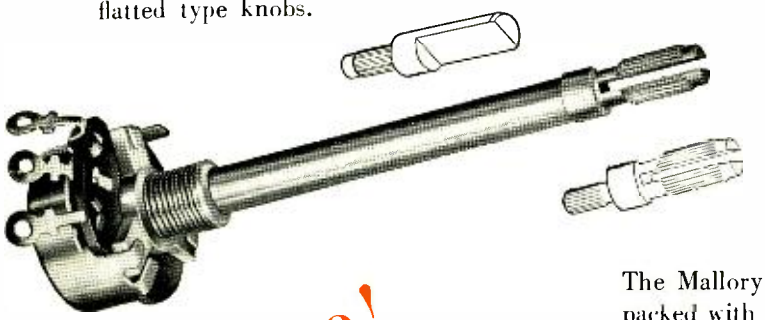
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The Mallory Midgetrol is shown with the two shaft ends packed with every control to permit easy use of split-knurl or flatted type knobs. The Mallory Midgetrol line, in addition to round shaft standard controls, includes dual concentric controls that offer fast, easy assembly in five steps *without* special tools. Front and rear sections are factory assembled and inspected. AC switch attachment is easy.

P.R. MALLORY & CO. Inc.

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How we spot "shady characters"

before they can damage your business

THE instrument you see is working for *you*. A sensitive light-measuring device, it is used like a doctor's stethoscope, to explore the surface of a picture tube for screen imperfections the unaided eye would fail to detect.

Employing a photosensitive surface and color filters, this device does two jobs. It checks not only the uniformity of brightness, but also the *color* values from center to edges of the faceplate.

Why is this important? It is important because RCA has learned, through long experience in the manufacture of picture tubes, that the best picture—the picture having superior quality—calls for unusually rigid processing controls of the phosphor and its application. The light-measuring device spots any departure from RCA's established brightness and color standards. Result? "Shady characters"—those tubes that would produce pictures lacking in fine quality—*never reach your shop*.

This constant vigilance and *quality control* at *all* stages of manufacture assure that RCA standards will be met. In this way, RCA guards its own reputation for quality . . . and *yours as well*.

With RCA Receiving Tubes, as well as RCA Kinescopes, TOP-QUALITY CONTROL makes the difference.



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