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This new unit makes use of the high flux density available in the magnet system of the previous H.F. 1016 unit. A curved diaphragm is used with a rigid centre section coupled to the voice coil. The rigid coupling and the design of the cone termination give a balanced response over the whole audio range. The unit is specially suitable for use in the smaller type of enclosure having a volume of approximately $1 \frac{1}{2}$ cubic feet.

| Type | Flux Density | Price | Type | Flux Density | Price |
| :---: | :---: | :---: | :---: | :---: | :---: |
| 8" H.F.816* | 16,000 gauss | ¢6.13.9 | T. 816 | 16,000 gauss | 16.6.9 |
| $8^{\prime \prime}$ H.F.812* | 12,000 gauss | ¢4.1.3 | T. 12 tweeter | 16,000 gauss | £13.4.6 |
| $8^{7}$ H.F.810 | 10,000 gauss | £3.0.6 | T. 10 tweeter | 14,000 gauss | ¢4.8.3 |
| $6^{\prime \prime}$ H.F.610 | 10,000 gauss | 62.10.3 Steel 62.12.3 diecast | $\text { T. } 359$ <br> tweeter | 9,000 gauss | L1.14.0 |

Specification:
Chassis-die cast aluminium; Cone-graded pulp cambric surround; Cone dia.-9 ins: Pole dia.-I in.; Flux density - 16,000 gauss; Total flux64,000 maxwells; Impedance -15 ohms.
Price: $\mathbf{6} 10.0 .0$ (inc. tax)

* Incorporates q universal impedance speech coil.

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## HALF TRACK

8.8.R. TD2 Monarienk, latest model bitin. opool

Deposit g1,0.0 and 9 monthly . . . . . . . . .CA8H
aplifter for B.8.R. deok, printed circuit remdy wired, with
ECC8s, BCL 82 . EM85
Tspe Amplifer for B.8.R. deok, printed circuit remdy wired, with
ECC8s, BCLis2, EM8s and EZ81. Complete with all
plugs, plugs, ecicete, panels, knols, etc. The whole amplifier Deposlt $\{1,0.0$ and 8 monthly. .............
Case with 7 in .14 in . speaker, in two tone grey.
. CABH Kit as above
Deposit 82.4 .0

VAsH Deposit \&2.4.0 and í ${ }^{\prime}$ monthiy
....
The above recorder can be rupplied asaembled, tested and complete with tape and microphone for. . . . . . . . . . . . . CASH Collero

Tape Amplifier for study deck, with ready wired printe................................. control and input panels, mains and output transformera. Complete with valves, knobs, plans, acrews, etc, EF86 ECC\&3, EM84. EZ81. OA81 and 2 ELB4, 8 watts output. Magic eye, radio and mic. inputs, $\mathbf{E X} \mathrm{L} / \mathrm{s}$ eocket, tone and monitor controls. Can be used as an ampllier CABH 81 I.11.0
Deposit 81.4 .0 and 12 monthly
Case for above including 9in, x bin. opeaice
Total IIt as above

To an offer the above reeorder, complete with tape and maiorophone, in a De Luze two tone grey anbinet, agembled for Deposit 88.10 .0 sad 12 monthly
$\$ 8.8 .0$
81.1 .0
48.8.0
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882.0.0
21.18.8
885.0 .0
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this Maohtne it listed at 39 gns. by makers and is a very good bay. . . . . . . . . .
Building Ingtruotions avellable at $2 / 6$ emoh zit (refanded if rit bonght)

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| GRAMOPMONE EOU\|PMENT |  |  |
| :---: | :---: | :---: |
|  | 14 TC8/H cartridge .........................CASH | 27.10 |
|  | Deposit 81.0 .0 and 7 monthly . . . . . . . . . . . . . . . . . . . . | 21.2 |
|  | Deposit | 8.14 |
| Garrerit Antosilm De Lux | Antoalim De Luxe |  |
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Complete $\mathbb{K} i t$, lesm cabinet.
 peaker. no control holes have been drilled. 1deal Eezenoy, etc. ............................................
81.12 .6

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Mallard have reduced the price of many Tranaistorg to: OC44 11/a, OC45 10/OC70 6/6, OC71 6/6, OC72 8/-, OO75 8/-, OC76 8/-, OC81 8/-. These are their new list prices. Why buy surplus, OC72 in matohed pairs only at $16 /-$ pair
(No otber types.)

## QUARTER TRACK

B.8.R. TD2

Deposit 1.4 .0 s.... 12 monthis

CABH 11.11 .0

Tape Ampllfer as over, but quarter track CAB'H
Deposit el.0.0 and 9 monthly $19 \%$

Cene. two tone grey. with ppestier. .....
Complete Kit as above.
Deposit 82.10 .0 and 12 monthiy
madio Deok
Collaro Studjo Deok, 4 track
Depoalt $\$ 1.18 .0$ and 12 tnonthiy
Tepo Amplifer, as over. but 4 track
Cane with 91 n . x Din. Apesker
28.9.0
$\mathbf{8 1 . 1 . 0}$

Completa Kin. x Bin. npesker . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . .


ECLS4, E780 and EM85, Radio and Mic. sockets, givea
Ealf Traols equalised output of $400 \mathrm{mp} /$ Volts
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Marrioti Tape Heads, 4 track type L/RPS/7 and L/EB/9 Record Playback and Erase with mounting bracket for studio
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M.S.S. 2 tresk type DR1 and DE1 Record/pleyback and Erame 31.7 .6
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Brase dial secutcheod is avallable for AF208 and Jubllee. Prioe $7 / 6$ Individual leaffete giving full description and toohnical doteile.

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Osmor rod aerlal 8/6. 1,F.T.s and Onc, colls 8e/-, Osmor driver 8/a. Oemor output $8 /=$, Set transistors and diode $43 /=$, J.B. Rang $12 / 8$, Trimmera $1 / 8$ each. Bet condensers 15/-. Set resiators $8 /-$, Ardente volume oontrol $8 /$ W/C switch 3/8. Spesker 17/10, Hardware $4 /=$, Printed Ciroult 7/6, New case and dial 12/6, Battery PP4 2/3. Leaflet giving full lliugtrated detall $1 / 6$. All the a bove components if orderad at one time . . . . . . . . . . CASH 88.10 .0 Osmor undertake to align thls recelver for 10/-.

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Trensistor Cabiuet for Tin. $\times 4 \mathrm{in}$. 日peaker. Ideal for Weyrad olrcuith two tone grey

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500 mW push-pull output. Ferrite rod aerial. Car serial socket and coil. M.W.
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Type TR3, Fully built. high galn, low noise, printed circuit. Attractive krey and gohi iront panel 13 x lyin.
Heisiat $3 f l$. overall. Front to tack 51 fa . Vol. and onfof tone. Mike radio, monitor snd ext. speaker jacks. Valves ECC33. E'Thes, FZso. Mains trans. Ready to bolt to B.S.R. Deeck. Complete with switch wafer wired. Our I'rlce ONLY 86.2.6. (6/-Parking and Carr.). Nitnilar model without
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6 transistora and diode, 5in. circular speaker, buperhet circuit. Cabinet $13 \times 7 \frac{1}{3} \times \frac{1}{2} \mathrm{in}$., battery included. Fully tunable LW and MW. Polished walnut front.

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Chassis $10 \times 5 \frac{1}{2} \times 4 \mathrm{in}$. front to back. Valves: UBC41, UCH41, UF89, UL84 with metal rectifer. Bin. speaker. Ferrite rod aerial. Tone, vol. and gram. position. Covers L. and M. waves. Limited quantity at only $£ 6$ (5/- carr.) complete with small dial.
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Permeability toned F.M. front end 22/6 (post 2/6), with ECC85. $4 \times 3 \times 3 / 1 n$. $88.95 \mathrm{Mc} / \mathrm{g}$.

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4 watts. Valves ECCB3, ELS4 and EZSO. Contruls, volume, bass and
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 $8 \mathrm{~K}^{2} 2,8 \mathrm{~S} 4$, and SK5 sockets $3 / \mathrm{m}$ ea; ditto pluga
Also many other itemis speulfed. S.A.E. enquiries.

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| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| ${ }_{\text {ORA }} \mathrm{OR2}$ | 17／8 | 8BQ5 | 7／6 | $6{ }^{\text {G }} 44 \mathrm{CT} 1818$ | 25L6GT11／ | EN（7） | EA | $8 / 6$ | KT6l 12／6 |  |  |  |  |
| $\mathrm{OBL}^{\mathrm{O} 2}$ | 17／8 | 6BQ7A | 15／－ | 6U4GT 12／6 | $25 \mathrm{U} 4 \mathrm{GT1} 18 / 2$ | 15／－ | EAF42 9／－ | ELL2 19／8 | $\begin{array}{ll} K 161 & 1276 \\ \mathrm{KI} 33 & 7 / \end{array}$ | PY800 | $\begin{aligned} & \mathrm{U} 19 \\ & \mathrm{2l} \end{aligned}$ |  | Transisiors and diodes |
| O24 | 51－ | ${ }_{\text {6BR7 }}$ | ＊ $8 /-$ | 6U15G $7 / 8$ | $25 \mathrm{Y} 510 / 6$ | AC／sG 22／8 | EL34 $2 / 6$ | E1．32 5／－ | KTG6 15／－ | PYzo 18／5 | U2\％ | 15／－ |  |
| 143 | 3／－ | ©iB148 | 18／2 | 61＇76 8／6 | $25 Y 501975$ | ACsGVM | EH41 $\quad 8 / 6$ | ELi33 12／6 | к＇下区 43／6 | QP21 |  | $29 / 1$ |  |
| 1A5 | 8／－ | 6 Ba 7 | 25／－ | 6vibu 4／6 | $2624611 / 6$ | 15／－ | EH91 4i－ | E1．34 $10 /$－ | KT101 $3 \% / 4$ | 4 Fr 2 B | U25． | $29 / 1$ | GID4 5／6 |
| 147 | 12／－ | 6BW6 | －10／6 | ${ }^{6 \times 1006} 816$ | 25\％5 10／6 | AC／T F $182 / 4$ | KLC： $23 / 10$ | $\begin{array}{ll}\text { EL35 } & 19 / 6\end{array}$ | KTW01 $6 / 6$ |  | U26． | $17 / 8$ | G115 5／8 |
| 1 Cl | 6／－ | 6HW7 | ＊5／－ | 6X4 4／8 | $2{ }^{2} \mathrm{Z} 6 \mathrm{GT} 19 / 5$ | Ac／TP 32／4 | EВ¢е33 5／－ | EL37 23／11 |  | Q8150／15 ${ }^{\text {d }}$ | $\mathrm{U}^{2} 96^{\circ}$ | $1 / 8$ | GD6 |
| 1 C 2 | 01 | 6BX4 | $5 /-$ | 6X5 | 27AU 19／5 | AC／P1 $15 /-$ | EBC41 81－ | ${ }^{\text {ELL33 }}$ 2511 | KTw63 \％／6 |  | $\begin{aligned} & C 191 \\ & : 83 \end{aligned}$ | 25／11／8 | GD8 |
| 103 | 816 | 604 | 6／－ | 786 20／8 | 2817 \％－ | Ac／V P\％22／8 | EBCS1 8／－ | RL41 | $\begin{array}{ll}\text { KTZ43 } & 8 / 6 \\ \text { KTZ }\end{array}$ | R10 10／6 | $\begin{gathered} 183 \\ 1.36 \end{gathered}$ | $25 / 11$ | GiD9 4／－ |
| 105 | 12／6 | BC5 | 6／6 | 7B7 8／6 | 30Cl ${ }^{\text {c }}$ 7／6 | AP4 7／6 | Eれc90 6／－ | ELAE 10\％－ |  |  | U37 | 2511 | GD10 \＄／－ |
| 108 | 10／6 | 608 | $8 / 8$ | $7 \mathrm{C5}$ 81－ | $30 \mathrm{Cl} 1516 / 2$ | ATP4 5／－ | EBC41 12／4 | $\begin{array}{ll}\text { EL492 } \\ \text { ELS1 } & 10 / 2\end{array}$ |  | $\begin{array}{ll}\text { R12 } & 8 / 6 \\ R 16 & 25 / 11\end{array}$ | U37 | 25／11 | GD12 4／－ |
| 105 | 18／2 | 6 CB | $2 / 6$ | $7{ }^{766}$ | 3055＊6／－ | $\begin{array}{ll}\text { AZ } & 18 / 2\end{array}$ | 1．B1\％${ }^{\text {E }}$－ $8 /$ | $\begin{array}{ll}\text { EL83 } & 1075\end{array}$ |  | $\begin{array}{lr}\text { R16 } & 25 / 11 \\ \text { R17 } & 12 / 8\end{array}$ | U41 | $\begin{gathered} 19 / 6 / 6 \\ 8 / 8 \end{gathered}$ | GD15 81－ |
| 1D6 | 10／8 | fic9 | 13／8 | $7 \mathrm{H7} 81-$ | 30FL1＊10\％ | AZ31 10\％ | KB1＇83 13／7 | EL84＊＊ | ME4 <br>  <br> 1891 <br> $18 / 8$ | $\begin{array}{ll}\text { R17 } & 12 / 8 \\ \mathrm{R18} & 14 / \mathrm{l}\end{array}$ | U43 | 8／8 | $\mathrm{GDET}^{\text {G }}$／－ |
| 1 FL | 76 | ${ }^{\text {AC10 }}$ | $9 / 8$ | 787 8 8／6 | 30FL12 18／2 | A $24113 / 7$ | ELS＇49 9／6 | FL85 13\％ | $\begin{array}{ll}\text { MH9 } \\ \\ \mathrm{MH} & \text { 12／8 } \\ 7 /-\end{array}$ | $\begin{array}{ll}\text { R18 } \\ \mathrm{L} 18 & 14 / 5\end{array}$ | C45 | 13／6 | GET1081 $/ 6$ GET11112／ |
| $1 \mathrm{~F}^{2}$ | 8／－ | ${ }^{6} \mathrm{C} 12$ | 18／7 | $7 \mathrm{Y} 4 \quad 7 / 6$ | 301．${ }^{\text {＊}}$／6 | B36 15\％ | EbLI 30／6 | ELS6 18／10 | MHD4 $12 / 6$ |  | USO | 17／6 |  |
| 1 Fa | 81－ | bCD6G | 35／8 | 8D2 3／6 | 30L15＊9／－ | $\mathrm{BL}_{1} 63$ 7／8 | EBL：${ }^{\text {L }}$ 22／8 | EL91 $51 /$ | ${ }_{\text {MH1／}}{ }_{\text {M }}$ | RG1／240A | Uso |  | GET114 $8 / 6$ |
| $1 \mathrm{F7}$ | 15／－ | 6C19 | 718 | 8183 | 30P4＊15／－ | C1 12／6 | KBL31 22／8 | EL99 10／6 | MHLA ${ }^{\text {M }}$（ ${ }^{7 / 6}$ | RG1／240A | US5 | 4／6 | GET873 9／8 |
| 1 1F9 | $5 /-$ | 8CW4 | $24 /-$ | y ${ }^{\text {c／V6 } 14 / 11}$ | $30 \mathrm{Pl2}$ 7／6 | （10 12／6 | ${ }_{\text {ECSI }}{ }^{\text {R }} 13 / 7$ | ${ }_{\text {ELSH0 }}$ | MHLD ${ }_{\text {MLA }}^{\text {M／6／6 }}$ | सK34 54／－ | UB4 | 19／5 | GET874 9／8 |
| 168 | $17 / 6$ | 61）1 | 2／－ | 91：2 4／－ | 3016816 | cbll $27 / 2$ | Eço $5 / 6$ | ELa： 1812 | $\begin{array}{ll}\text { MLJ } & 8 / 6 \\ \text { M16 }\end{array}$ | $\begin{array}{ll}\text { RK34 } \\ \text { S13 } & 8 / 6 \\ 82 / 6\end{array}$ | U76 |  | GEX13 3／6 |
| $1 \mathrm{H5}$ | $10 / 6$ | n133 | 19／5 | $9 \square^{7} 713 / 7$ | 30P19 19／5 | CB1．31 22／s | ECO3 12／6 | ELR21 25／11 |  | S130 $\begin{array}{r}\text { 22／6 }\end{array}$ | ${ }^{\text {U78 }}$ | 16／6 |  |
| 1L4 | 3／－ | ${ }^{\text {BDB }}$ | 8／8 | 1001 12／6 | 3UPL ${ }^{\text {2／6 }}$ | Cc1435 22／8 | E¢－14 6\％ | E1ヶ＊せ2 19／6 |  |  | C107 | $\begin{aligned} & 1612 \\ & 1672 \end{aligned}$ | ci $\times 36$ 10／－ |
| 1 lab | 16／10 | 6D8 | 16／－ | $10 \mathrm{Cz} 25 / 11$ | 30PL13 10／6 | CK500 6／8 | EC70 12／6 | EM4 17／9 | M1sP4 20\％－ | $\begin{array}{ll}8 P 13 C & 18 / 6 \\ 8 P: 1 \\ 8 / 8\end{array}$ | U191 | $\begin{aligned} & 1612 \\ & 10 / 2 \end{aligned}$ | CiEX45／16／6 |
| 1LD5 | 5／－ | 6ES5 | 12／6 | $10 \mathrm{D1}{ }^{7 / 8}$ | 35 A 5 20／9 | CILA 28／10 | ECs1 27／6 | EM34 9／6 | MX 40 25／11 | \＄P42 12／6 | U251 | 14／－ | 55／1 |
| 1LNS | 5／－ | 6 Fl | 25／11 | 1012 11／8 | 35L6GT 9／8 | CL33 18／8 | Ec40 \％／－ | EM33 12／－ | ${ }^{1} 37{ }^{1}$ | SP42 $12 / 6$ | U281 |  | 15／\％ |
| ivs | 10／6 | 6 F 5 | 12／6 | 10 Fl 25／11 | $35 \mathrm{~W} 4 \quad 7 / 6$ | CV6 2／8 | Ec91 10／6 | EM71 28／10 | N7\％ ¢2／8 | $\begin{array}{ll}\text { 8PF1 } \\ \text { SU25 } & \text { d／6 } \\ \text { 27／2 }\end{array}$ | C281 | 19／5 | K 64 11／6 |
| 1P1 | $7 / 6$ | ${ }^{6 F 6 G}$ | 7／－ | 10F9 11／6 | 3523 18／2 | Cvas 10／8 | Ec92 18／－ | EM＊0 9／－ | Nion 22／8 | $\begin{array}{cc}\text { SU25 } & 27 / 2 \\ \text { SU61 } & 8 / 8\end{array}$ | U428 |  | GEX66 15／－ |
| 1 P 10 | $8 /$. | ${ }^{6 F B 6}$ | 8／－ | 10F18 12／6 | 35846 GT 81. | cve71 10／6 | ECes 181 18／－ | $\begin{array}{ll}\text { EM81 } & \text { 9／6 }\end{array}$ | Nil8 $22 / 8$ |  | C291 | 11／6 | AF102 $27 / 6$ |
| 1 P 11 | 7／8 | 6 F 8 | 12／8 | 10LD3 8／8 | 35259 T 9／－ | $\mathrm{Crl}^{18 / 8}$ | ECY：32 ${ }^{\text {5／6 }}$ | $\begin{array}{ll}\text { EM884 } \\ \text { EM } & \text { 10／8 }\end{array}$ | $\begin{array}{ll}\text { N18 } \\ \text { N151 } & \text { 2／8\％} \\ \end{array}$ | BL2150A | U301 | 22／8 | AFH14 $11 /-$ |
| 1 R 5 | 8）－ | ${ }^{6} 11$ | 17／9 | 10LDll 15／7 | 408CA 18／2 | cYic 18／2 | EC＇33 8／6 | EM85 18／10 | N308 20／1 | T41 87\％ | U329 | 14／－ | AF115 $10 / 6$ |
| $=18.8$ | 9\％ | $6 \mathrm{Fl2}$ | $3 / 6$ | 10P13 15／－ | 418TH25／11 | Cri31 11／－ | ECC34 $23 / 11$ | EN81 53／－ | Nas9 $15 /-1$. |  | U439 | $16 / 2$ | AF116 10／－ |
| 185 | 5／－ | 6 Fl 3 | 10\％ | 10P14 18／8 | $42 \quad 28 / 8$ | D1 3／－ | ECC35 8／6 | $\begin{array}{ll}\text { EN91 } & 53 /- \\ \text { ER／}\end{array}$ | N389 | TDD2 | 4 | 16／2 | $\text { AF117 } 9 / 8$ |
| 1 T 2 | 20／11 | 6F14 | 25／11 | J1E1 1\％1\％ | $43 \quad 10 \%$ | D15 10／6 | ECC40 17／6 | EY51＊8／6 |  | THD＋${ }^{\text {TH21C }}$ | C404 | 6／6 | AF127 12／－ |
| 1 T 4 | 3／－ | 6 F 15 | 14／11 | 11 ES 15／－ | －0A5 21／10 | D42 10／6 | ECく81＊5／－ | EY81 13\％ | PABC80 ${ }^{\circ}$ | TH41 $25 / 11$ | 4801 | 2911 | OA5 $6 /-$ |
| 104 | 12／6 | 6 Fl 16 | 8／－ | 1＇2A6 5／－ | $50 \mathrm{C} 5101-$ |  | ECC8\％8／6 | EYBS 16／2 |  | TH233 84／－ |  |  | OA10 8／－ |
| 11 | $5 / 6$ | 6 F 47 | 12／6 | 1：2A8 16／6 | 20C1）5G35／7 | 1177 4／－ | ECCx3＊\％／－ | EYY4 $14 / \mathrm{l}$ | P＇c9s $18 /{ }^{18 / 7}$ | TH22 $815 /-$ | VMPst | （ 15／－ | OA70 8\％ |
| 2 27 | 1018 | －F18 | 14／11 | 12ACA 14／11 | 50LAGT 101－ | DAC32 10／6 | Ecces ${ }^{\text {－}}$ 9／－ | EXYt， 76 | PCC84＊ 786 |  |  |  | OA78 8／－ |
| 2 C 26 | 4／－ | 6 F 19 |  | 12ado 18／10 | 52KU 14／4 | DAF91 5／－ | モcces \％ 76 | EY91 7／0 | juces ${ }^{\text {8／6 }}$ |  | $V_{P 2}{ }^{\text {P2 }}$ | 14／6 | OAT9 8／－ |
| 21013C | $7 / 6$ | $6 \mathrm{~F}^{2} 3$ | 1016 | 12AF6 13／7 | 63KU 19／5 | DAF96 7／6 | ECCs $18 \%$ | EZ35 $5 \%$ | PCCs5 8 9／6 | TP2620 32／4 | $\mathrm{VP}_{\text {VP4 }}$ | 14／6 | OA81 8／－ |
| 2D 21 | 15／－ | $6 \mathrm{~F}^{2} 4$ | 12／6 | leatit \％／－ | 72 4／6 | DCC90 10／8 | ECl91 5／6 | $\begin{array}{ll}\text { EZ40 } & \text { 8／8 }\end{array}$ | Pcts9＊9\％－ | UABCRO $9 /-$ | VP | $16 \%$ | OA85 8／－ |
| 2 F | 85／11 | ${ }^{6534}$ | 10／8 | 12AH5．12／6 | 77 8\％－ | DD4 $12 / 6$ | ECF80＊10／6 | EZC1 \％／－ | $\mathrm{P}^{\prime} \mathrm{C} F 80^{\circ}$ \％ 78 | UAF42 9／8 | VP4A |  | $\begin{array}{ll} \text { OAB6 } & 4 /- \\ \text { OASI } & 3 / \end{array}$ |
| $2 \times 2$ | 25／11 | 6F33 | 78 | 12AT10 76 | 78 8／6 | $1) 041$ | LCFs： $10 / 6$ | EZ80 6／－ | PCPG2 $10 / 6$ | Ubil $18 /-$ | $\checkmark \mathrm{P} 13 \mathrm{C}$ | 22／8． | $\begin{array}{ll}\text { UA } 491 & 3 /- \\ \text { OA96 } & 3 / 6\end{array}$ |
| ${ }_{3}^{34.5}$ | $\begin{gathered} 8 /- \\ 10 / 8 \end{gathered}$ | ${ }^{\text {6GB }}$ | $8 / 8$ $8 /-$ |  | 30 3 3 | DDT4 12／6 | ECP＇Si $19 / 5$ | EZBl 6／－ | PCFP4 18／2 | UBC41 8／8 | Vpre3 | 8／8 | OA210 9／6 |
| 847 | 12／6 | 6J5G | B／－ | 12AU7＊ $6 / 6$ | 83  <br> 838 $15 /-$ <br> 1985  | ET＂ $2 / 8$ |  | E290 4 4／8 | PCFs6＊9／6 | UBC81 11／－ | VP41 |  | UA211 18／6 |
| 3 D 6 | 5／－ | 6 JdGT | 8\％ | 12AVti 12／4 | $85 A 1$ 42\％－ | DF゙！6 15\％ | ECH8 $25 / 11$ | FC4 $25 / 11$ |  |  | VP133 |  | OC16W 35／－ |
| 344 | $7 / 6$ | 6JA | 5／6 | 12Aス7＊\％\％ |  | $\begin{array}{ll}\text { DFF72 } & 10 /- \\ \text { 13－}\end{array}$ | ECL1 $1120 / 8$ | FC15C $25 / 11$ | PCLE3＊＊${ }^{\text {9／8 }}$ | UBF＇sy ${ }^{\text {g／6 }}$ | V473 | $17 / 8$ | OC19 25／－ |
| $3{ }^{4} 5$ | $8 / 8$ | ${ }^{6} \mathrm{~J} 718$ | 4／6 | 12GA6 8／－ | 90 Al 67／6 | 1F91 8／－ | ECH33 2i／8 | FW4／5008／6 |  | UBLA ${ }^{\text {U }}$ | $\begin{aligned} & \text { YR10S } \\ & \text { VRI } \end{aligned}$ | ${ }^{1 /-}$ | Ocze $28 /-$ |
| 3354 | 8／－ | 6J7GT | 10／8 | $12 \mathrm{BEB} 9 \%$－ | 90av 87／8 | 11986 $7 / 8$ | ECH35 $6 / 6$ | H＇Wi／5008／8 |  | $\begin{aligned} & \text { Uxu4* } 14 / 8 \\ & \text { ucxs } \\ & 7 / 8 \end{aligned}$ | VR150 | 7）－ | $\begin{array}{ll}\text { Oc28 } \\ 0 \text { c28 } & 25 / 7\end{array}$ |
| 3 V 4 | 7／8 |  | 12／6 | $12 \mathrm{BH7} 20 / 8$ | \％ucet 37／6． | DF97 9／－ | ECH42 $9 / 6$ | ＂TlC $25 /$. | PEASDD | $\text { UCFso }{ }^{76 / 2}$ |  | $5 \%$ |  |
| 4D1 | 76 | 6K6 | $8 /-$ | 12 El 30／－ | $90 \mathrm{cv} 37 / 6$ | DH30 15／8 | ECH51 $7 / 6$ | （1550 41／6 | PEN40 ${ }_{\text {O5／11 }}$ | UCH2 ${ }^{\text {U }}$ 28／2 | Yus38 | 5／－ |  |
| $5 \mathrm{R4G}$ | 17／6 | tik7 | 2／－ | $12 \mathrm{H6}$ 3／－ | 90c＇l 16／－ | LH63 6／－ |  | （2\％30 9／－ | PEN25 4／6 | UCH44 9／8 | V 4111 | 80／－ | OC35 18／－ |
| ${ }^{3} \mathrm{U} 40$ | 4／6 | 6K7\％ | T 8／－ | 12550T 4／－ | $150 \mathrm{B2} 218 /$－ | DHi6 $6 \%$ | ECL80 ${ }^{\text {¢ }}$ |  | PENTOD ${ }^{\text {P／8 }}$ | UCH42 ${ }^{9 / 8}$ | VU11 |  | OC38 $0181 / 8$ |
| 5 S 40 | 10／－ | 0 K 86 | 5／－ | 12J76T $8 / 8$ | $150 \mathrm{C2} 217 / 8$ | DH77 6／－ | ECLH3 9／6 | GZ33 19／5 | PRN＋03／－ | UCL8\％${ }^{8 / 6}$ | （133 | 7／6 | Oris 1 9／－ |
| 5 Y | 5／6 | 6 K 8 CT | 10／6 | $12 \mathrm{Ks} 17 / 8$ | 101 10／6 | Dlk $45 / 3$ | ECles3 18／6 | O：834 $19 / 5$ <br> 14  | 34／8 |  | W21 | 12／6 | $00^{0} 44^{9 / 3}$ |
| 5 Y 4 | 12／6 | 0 E 20 | 19／6 | 12K79T 5／6 | 145BT 32／4 | DH10127／11 | E61，86 16／2 |  |  | UF41 ${ }^{\text {U }}$ |  | $22 / 8$ | OC44PM 9／3 |
| 38.3 | 18／5 | 6Li | $22 / 8$ | 12K8sT14／－ | 185BTA32／4 | D11107 13／7 | El＇s $29 / 8$ | （1） | 25／11 | UF42 ${ }^{\text {c／}}$ 12／－ | W61m | 28／11 | $\mathrm{OCHF}^{45} 9$－ |
| 584 | 9／－ | dLfG | 7／8 | 12976T 5\％ | 301 10／6 | 1） 32 12／－ | EF9 22／8 |  |  | UF80．${ }^{\text {¢ }}$ |  | $10 / 6$ | OC45PM 9／－ |
| 6／301 | 10／－ | 61.8 m | 10／8 | 124A7 8／6 | 310210 | DK40 21／10 | EF＇22 $141 /$ | ${ }_{1 / 4 B C 80}{ }^{12 / 6}$ | PEN46 48 |  | W76 | 8／8 | OCdS $82 / 6$ |
|  | 10／6 | 8Litit | 7／6 | 128467 8／8 | $30310 / 6$ | Шкч1 8／－ | EFi3t 4／－ | 13／6 | P13N453DD | U＇88＊${ }_{\text {U }}$ | W77 |  | OC6S 25／－ |
|  | 3 \％－ | ${ }_{5}^{2} 18$ | 13／－ | 12867 8／6 | $30410 / 6$ | lk92 10／8 | EF37A 8\％－ | $\mathrm{Hl}_{1,3}{ }^{13 / 6}$ | PGE40．0D | ＋86 13／6 | Wsim | － | 00770 8／8 |
| $0^{6} \mathrm{AB7}$ | 8i－ | 61．19 | 22／8 | 1281778 | 3051016 |  |  | H1，138 ${ }^{\text {H／6 }}$ | 32／4 | UF＇89 8／－ | W 101 | 1 | 0.718 |
| BAC7 | 4／－ | 6L1）3 | 81－ | 12857 8／6 | 3061018 | DL33 ${ }^{\text {D／6 }}$ | EF10 15／－ | H1：3 1411 | PENA $22 / 8$ |  | W107 | 18／2 | OC72 8／－ |
| 6ACS | $5 / 6$ | 8LL13 | 11／8 | 124k7 7 ／－ | 8107378 | DL35 $12 / 6$ | EF41 8／－ | H1．8a197／6 | 23／1 | 1：L4 40 14／6 | W72 | $18 / 5$ | 0673 16／－ |
| GAG7 | 7／6 | 6LD20 | 18／7 | 128Q7 11／8 | 4039 12／6 | DL63 10／－ | 15F42 10\％ | $11.4112 / 6$ |  | ULS4＊${ }^{14 / 6}$ | 1 | 12. | $\mathrm{OC}^{7} 7581-$ |
| －AJjo | 8／6 | 6x7ct | 8／－ | 125127818 | ＋378 2／－ | 1Lem 1\％／8 | EFSO | HL133DD | 4020 34／－ |  | 18 | $91-$ | $00^{76} 31-$ |
| 6AK5 | $8 /$ | ${ }_{61} \mathrm{Pl}^{1}$ | 18／9 | 12UJG 7／6 | 5763 \％／6 | טLi8 $16 \%$－ | Brit．5／－ | HLS3D ${ }_{\text {12／6 }}$ | 1023 $38 / 8$ | CM4 $17 / 8$ | $\begin{array}{r}411 \\ \times 41 \\ \hline 1\end{array}$ | 25／11 | Ur78 8／－ |
| 6AK6 | 12／6 | P15 | 12／6 | $12 \mathrm{Y} 410 / 6$ | 7193 5／－ | $\mathrm{DLF}^{\text {b }}$ 15／－ |  |  | 1＇Ls6． $15 \%$ | UM80 14／11 | ${ }^{6} 1$ | 12／8． | $00^{81}$ 8／－ |
| afk8 | 9／－ | ${ }_{6} \mathrm{P}^{26}$ | 19／5 | $14 \mathrm{B6} \quad 20 / 9$ | $7475 \quad 76$ | DI．75 30j－ | EF54 5j－ | HVれ2A ${ }^{\text {P／－}}$ | ${ }^{1} \mathrm{~L}^{38} 825 / 1$ | URIC 18／2 | ${ }^{1} 63$ | $9 / 8$ | OC81M 8\％－ |
| 6AL5 | 4／－ | 6P28 | 25／11 | 14H7 22／8 | ACO42 $25 / 11$ | 11．0\％6／－ | EF73 10／6 | HVR2 $10 \%$ | ${ }^{1}$ Lx $\times 1010 / 8$ | UUS 8／ | －64 | 78. | OC82 10\％ |
| 6AMS | 5／－ | 6Q7a | 8／－ | 1487 27／8 | AC044 10／6 | LL94 7／6 | EFs0＊5／－ | 1 W 3107 | PLK2 ${ }^{\text {P／8 }}$ | Uv6 $19 / 5$ | $\times$ | 12／6 | OCk3 8／－ |
| 6AM6 | $3 / 6$ | 6 CT （TT | 11／－ | $18 \quad 23 / 10$ | AC2JPEN | D195 7／6 | $\begin{array}{ll}\text { EFs3 } & 13 / 6\end{array}$ | 1W $4 / 3508 /-$ |  | CU6 $\begin{array}{cc}19 / 5 \\ \text { LU7 } & 16 / 2\end{array}$ |  | 12／6 | $\mathrm{OCS4}^{\text {O }} 8$ |
| GAQS | 7／6 | 6 H 7 G | 10\％ | 19 10／6 | $22 / 8$ | 101．96 7／6 | EFヶ5 $6 /-$ | 1 W $4 / 500$ | PLaq－12／4 | Uv8 $20 / 11$ | X 78 $\times 88$ | 14／－ | OC140 29／－ |
| 6ARG | 20\％－ | 6R7GT | 11／－ | 19AQ5 10／6 | ACPPEN／ | DLS10 10／6 | EF86＊ $9 /-$ | 16／2 |  | U08 0 6／11 |  | 29／8 | 0 Cl 701816 |
| 6ATB | 6／－ | 68.47 | 8／6 | 19BG8G22／8 | DD 12／8 | Dм \％$^{\text {\％／8 }}$ | EFA9 9／－ | К ВС32 20／5 | PM8＊18／10 | UVio 22／8 | ${ }_{\mathbf{X}}{ }_{10}$ | 2218 | 0 C171 10／6 |
| 6AU6 | 10\％． | 6 sc 7 | 7／6 | $19 \mathrm{Hl} 10 \%$ | AC4PEN | DW4／3E08／6 | EF91 3／6 | K F3， 8 8／6 | PT15 10／6 | UU12 $82 / 8$ | ${ }^{\mathbf{Y} 63}$ |  | OCP71 29／6 PXC101 $6 / 8$ |
| ${ }_{\text {6AP }}{ }^{\text {GAV }}$ | 12／4 | 6897 | 8 － | 2012 14／11 | 27／2 | DW4／5008／6 | EF993 4／6 | K1．35 8／6 | PX4 10／6 | UYIN 18／2 | $\times 15$ | 1016 | PXC101 6／6 <br> PXC101A |
| 6.17 688 | $10 / 6$ $3 /-$ | ${ }_{683} 68$ | $88 /$ | 20F＂2： $25 / 11$ | ACEPEN | EK0F E83F E80／－ | EPH5 8／－ | K LL3228／11 | FYill $18 / 2$ | $\mathrm{T}^{\top} \mathrm{Y} 2111612$ | 263 | $7 / 6$ | ${ }_{6 / 6}$ |
| fibas | 6／－ | 68K7 | 81－ | 20 PI ＊ $26 / 11$ | ACDPEN／ | $\begin{array}{lll}\text { F83F } \\ \mathrm{F} 180 \mathrm{~F} & 80 / 6\end{array}$ | ${ }_{\text {EF9\％}}{ }_{\text {EF9 }} 13 /-$ | KT ${ }_{\text {KT8 }}$ 5／－ | PY35＊＊${ }_{\text {PY }}$ | UY41 UY85 | ${ }^{\mathbf{Z} 68}$ | $8 / 6$ | X $410418 /-$ |
| ${ }_{6}^{6 B E 6}$ | 6／－ | 68.7 | 6／－ | 20P3＊22／8 | DD 25／11 | E1148 2／6 | EF183 18／8 | KT33C 8／－ | PY80 7／6 | $\begin{array}{lll}\text { U12／14 } & 8 / 6\end{array}$ |  | 18／8 ${ }^{8 / 8}$ | 15A |
| 6 BCRE | 22／8 | 68N7 | 6／6 | 20P4＊25／11 | AC6PEN $7 / 6$ | EA50 \％／－ | EF184 12／6 | кT3 2811 | PY81 7／6 | U16 10\％ | 7719 | 5 | 90／10P ${ }^{12 /-}$ |
| 6 BH 6 | 81 － | 6SQ7 |  | 20P5＊28／8 | AC／P EN（ 5 ） | EA76 9／6 | EF＇804 22／8 | KT41 22／8 |  |  |  |  | ${ }^{30 / 10 \mathrm{P}}$ |
| 6 | 6／－ | 7 | 12／6 | $10 / 6$ | 22／8 | EABC80 9／－ | EK2 25／11 | KT44 12／6 | PY83 8／－ | U13／20 ${ }^{8 / 6}$ | 2759 |  |  |

[^0][^1]
## STEAIIS KUULLARD DESICHS

Designed by MULLARD-presented by STERN's sirictly to specification MULLARD "5-10" MAIN AMPLIFIER
For use with the MULLARD 2-valve pre-amplifier with which undistorted power output of up to 10 watts is obtained. We supplyspecified componciek in Mains TRANSFORMER and cholce of the latest Ultra-Linear PARMEKO or the PARTMIDGE Output Transformer COMPLETE KIT OF PARTS
\&10.0.0

(PARMEKOOutput Trans.).
\$11.10.0 INCORPORATENG PARTHIDGE OUTPUT Alternatively we supply \$11.10.0 INCORPORATRNG PARKREGE

## MULLARD'S PREAMPLIFIER <br> TONE CONTROL UNIT

Employing two EF86 valves, and designed to operate with the MULLARD MAIN AMPLIFIERS, but also perfectly suitablefor other KIT OF PARTS

## £6.6.0

ASSEMBLED AND TE
 - Equalisation for the latest R.I.A.A. characteristics. - Input for Crystal Pick-ups, and variable reluctance magnetic types Input (a) Direct from High Imp. Tape Head. (b) Froni a Tape Amplifler or Pre-Amplifler. - Sensitive Microphone Channel. Wide range BA SS und TREBLE Controls.

## THE MULLARD "510/RC" AMPLIFIER

The popular complete ' 5 -10' Incorporating Control Unit wroviding up to 10 watts. Specified Components and new MUNL VALVES are supplied including PARMEKO MALio TRANSFORMEIRS and choice or the latest Transformers. KAT OF £11.10.0 ORASSEMBLED $£ 13.10 .0$ Dep. \&2.6.0, 12 months at 17/0. Dep. £2.14.0, 12 months zt $19 / 10$. Dep. \&2.6.0, 12 months at 17/O. Dep. £2.14.


## THE MULLARD " $33 / R C$ "

IDEAL AMPLIFIER FOR A SMALL HIGH QUALITY INOF UP TO 3 WATTS
 OF ASSEMBLED
Ond TESTED
O8.19.6
(plus $6 / 6$ carr. and ins.) Jeposit £2.0.0 and 8 months E1.0.0. Complete to MULLARD'S $£$ PECCIFKO OUTP including Mullard
valves and PARMEKO OUTPUT THANSFOKMER.

## "The TUDOR" AM/FM

 TUNING UNIT A. SELF POWERED PRICE ONLY $£ 19.19 .0$ Rerostt 21.9.4.

Provides full coverage of the VHF/FM band ( $87-108 \mathrm{Mc} / \mathrm{s}$ ) and also the LONG and MEDIUM wavebands. Incorporates Multplex outlet socket for stereophonic purposes and separate consrols for tuning the FM and AM bands. Operates pertectly with the
STERN-MULLARD AMPLIFIERS and contains matching FRONT STERN-MULLARD AMPLI Whis in Black/Gold or White/Black. Also operates equally well with any Amplifer requiring input of 100 to $350 \mathrm{~m} / \mathrm{Volts}$. well with any Amphiner requiring input on 100 to 00 m/volts.

THE "TUDOR" STEREO AMPLIFIER


For Only
£18.18.0
Deposit £3.16.0. $\quad 12$ A self contained Ampvide high quality stereophonic and monophonic reproduction. Each channel provides a rated output of 6 nic reprond for monophonic operation解 DESCAIPTIVE LEAFLET IS AVALLABLE.

## -

 with a good quallty (iRA and P.M. SIPAKER A 2 stage Amplifier incorporating 3. modern B.V.A. valves and has separate BASS and TREBLE CONTROLS. The Case will also accommodate almost any make of Autochanger and is WE SUPPLY SEPARATELY-Self powered with Cathode Tollower output. Incorporates
TWO inputs for MICROPHONES One for CRYSTAL PICK-UP and a fourth for RADIO or TAPE Kit of Parts

## Assembled and Tested $£ 10.0 .0$

ONLY 88.7 .6 (Plus 7/6 Carr attractively finished in Mushroom Grey Rexine.

## PRICE REDUCTIONS

(a) The KIT OF PARTS to build both the "5-10" Main Amplifier and the 2-valve PRE-AMP CONTROL
H.P. Dep. £3.7.0 and 12 § $15,15,0$ H.P. Dep. £3.7.0 and $12 £ 15.15 .0$ months at $£ 1.2,9$ and the 2-stage PRE AMP both ASSEMBLED and TESTED H.P. Dep. £3.16.0 and 12 \&18.18.0 Months of £1.7.8...o.iout Transformer £1.6.0 extra.

## 1 RECORD PLAYERS

THE GARKARD "AK'TO-SLIM" | 4-speed Autochanger with 88.10 .0 Crystal Pick-up .
GARRARD "AETO-SLIM DELiXXE" 4-speed Autochanger incorporates transcription Pick £12.14.6 COLLARO "4JUNTOR" 4 SPEED SINGLE RECOHD PLAY- £3.15.0 ER with separate Crystal 23.15 .0 Pick-up. Above Pick-up separately for £1.6.6.
The COLLARO C60 4-speed Auto-
 B.S.R. MODEL UA14. A 4-speed mixer Autochanger with $\quad 87.19 .6$ Crystal Pick-up …........ TA/Mk.II $4^{-}$ speed Player fitted high $\$ 8.10 .0$ output Crystal Pick-up.. PIIIIIPS MODEL AGI016. A $4-$ speed Player which can be operated both for Mono or Stereo opera- \&13.13.0 tion
Carr. and Ins. on each 5 - extra.
This attractive PORTABLE AMPORTABLE AM-
PLIFIER CASE (a) The 2-stage (plus Rectifer) AMPLIFIER
£4.2.6 (b) The PORTABIE CARRYING CASE $£ 3.17 .6$ (c) $6+$ in. P.M. SPEAKEK 18/9. Carr. and Ins. 4/-extra.

## MULLARD FOUR CHANNEL MIXER UNIT

 £8.8.0

Alternatively MODEI 1.1 . provides for one microphone Input matched for moving coll or Ribbon Mike. £1.17.0 extra.

## STERN'S INTER-COMM BABY ALARM

Employing the new MULLARD ECL86 valve to provide two (or three) way conversation up to 200 to 250 volts.
200 PHICES. MATCER UNTT
PRICES
and ONE FXATERSION


KIT OF PARTS £6.17.6 ASSEMBLED AND TESTED $£ 8.8 .0$ Consists of a MASTER UNIT. size only $8 t \times 5 \frac{2}{2} \times 61 n$. and ONE EXTENSION (a second extension may be added to any time). WE WELCOME ENRTMRIES and our technical staft will with picasure assist with choice of suitablo equipment.

## -momos <br> Stereaphanic Saund by Stern's

THE "STP-1" STEREO TAPE PRE-AMPLIFIER incorporating TAPE HEADS

- PUSHPULLOSCILLATOR CIRCUIT
4-SPEED EQUALISATION
- FERROXCUBE OSCILLATOR TRANSFORMER
- SENSITIVEMETER FOR SIGNAL LEVEL
SEPARATE GAIN CONTROLS IN EACH CHANNEL
MULLARD VALVES
(a) The BRENELL Mk, V $\frac{1}{2}$ TRACK DECK with the

b) The COLLARO "STUDIO" t-TRACK DECK with the KIT to bulld the STP-1 Deposit £\%.16.0. 12 months of $£ \dot{8} 17.3$.


## dESIGNED TO OPERATE WITH

 incorporating the latest :TRACK
TAPE HEADS.
OVERALL SIZE CASE $131 \times 31 n$. FRONT PANEL (choice of Black or White) $14 \times 3$ in. PRICES Ktt of c220.0 Deposit eq.8.0 12 Parts 022.0 .0 months of $£ 1.12 .3$ Assembled 828.0 .0 Deposit $_{\text {months of }} 5.12 .012$
and 'ested

## COMBINED PRICE SCHEDULE

## STEREOPHONIC RECORD PLAYER UNIT8 ARE AVAILABLE FROM STOCK

## STEREO AMPLIFIER <br> A high fldelity deslgn provides up to 10 watts (per channel) Superb reproduction. Frequency response flat to within 3 dib Trome/s. to $60 \mathrm{kec} / \mathrm{s}$ at 50 Mis Total Harmonic Distortion at10 watts 0.1\%.

MULLARD'S "10 PLUS 10"

(a) ASSEMBLED AMPLIFIER, including CONTROL UNIT (as illustrated..............ion
£21.0.0
(b) A complete KIT of PARTS.
£18.10.0
 with the DUAL CHANNEL PRE-AMPLIFIER, this provides for a more versatile instanlation and is essential if a low output Magnetic Pick-Up is to be used.
(a) THE ASSEMBLED AMPLIFIER and DUAL

(b) A KIT of PARTS for both Units..................
830.0 .0

Deposit 85.4 .0 , 12 months at $\mathfrak{i l i} 18.2 . \quad$ \&26.0.0 Hustrated and Descriptive 1srochure available. Please enclose S.A.i.

## ARMSTRONG RADIOGRAM CHASSIS

FULIL RANGE IN STOCK. Dlease enclose S.A.E. for leaffets.
STEREO 12 Mk. 2 £43.10.0


STEREO 55 £32.15.0
Deposit £6.15.0
12 months at $£ 2.7 .8$ watts watts from each amplitler. Covers the VHF and Medium wavebands.
JUBIIEE MK.2 \&30.12.0 Deposit. £6.4.0
A. Ki-Fi mono chassis giving eight watts push-pull at $£ 2.4 .9$ A. Ki-Fl mono chassis giving elght watts push-pull output and covering VHF. medium and long bands. Tape Record and RC play inputs.
AF208 £22.18.0
Deposit £4.18.0
An AM/FM chassis provioing 5 watts output months at 12 1.13.0 VHF and medium wavebands. Tape Record and RC play inputs. TVB VHF TUNER 221.18 .0 Deposit play in
A self-powered high-fidelity tuner of outstanding destgn. incorpors-
ting features which are normally found only in the most expensive tupers. The full VHF band ( $87-108 \mathrm{M} / \mathrm{cs}$ ) is covered and an output control enables the output to be varled between 0 and 500 mV
"HI-FI' LOUDSPEAKERS WEHAVEIN STOCK A COMPLETE RANGE BY GOODMANSMWIIARFEDALE-WH.

TIIE MQLLARD "10 + 10" AMPLIFIER (described below) DECKS provide a complete sTBAEOPHONIC IN Details are readily avallable.

## DUAL CHANNEL PRE-AMPLIFIER

Two Mullard 2-valve Pre-ampli-
flers combined into a Single unit enabling it to be used for both STERJOPIONIC or MONOPHONIC operation. It is designed primarily to operate with our range of MLLLAMD MANF AMPLIF1ERs but whll also operate equally well with any make of Ampli-
 fiers requiring an input of up to $250 \mathrm{~m} / \mathrm{vol}$ ts
KIT PARTS \&12.10.0 ASSEMBLED \&15.0.0 OF PARTS \& 12 mths . at $18 / 4$. H.P. AND TESTED \& $£ 15.0 .0$ \& 12 mths , at $£ 1.2 .0$ STEREO "TWIN THREE" AMPIIFIER ASSEMBIES and TESTED
 Based on a recent design by MULLARD LTD. Ideally suited for use in PORTABLE RECORD offer a specially designed Portable Case. Incorporates MULLARD
ECL86 valves. separate BASS and TREBLE CONTROLS. and produces excellent reproduction of up to 3 watts per channel. Frequency response is $40 \mathrm{c} / \mathrm{s}$ to $30 \mathrm{Kc} / \mathrm{s}$. Size Ill $\times 3 \times 51 \mathrm{n}$.
To construet a sirikeo Por TABLA: RECORD PLAYER Assembled AMPLIFIER with two ROLA $8 \times 5 \mathrm{in}$. 1400 LOUDSPFAKERS and the PORTABLE CASE for
(Carr. \& Ins.. lo/- extra). Deposit $£ 2.16 .0$. 12 months of 1.0 .0. SUITABLE RECORD PLAYERS FROM $\mathbf{8 8 . 1 4 . 0}$ An alternative "TWWN IHILEB"' can be supplled tor DUAL CHANNEL MONOPHONIC operation producing output of 6 watts. PRICE AS ABOVE.

## THE "MONO GRAM" AMPLIFIER



A small Amplifier ol genuine high quality performance. It ECL86 Valve, separate BASS and TREBLE CONTROLS and when driven by the standard Crystal Pick-up a power output of 3 watts is achieved without dietortion. PRICE... READY FOR USE
84.19.6 Carr. \& Ins. 5/case finished in two tone Rexine is avallable to accommodate the amplifer-speaker and a variety of record changers. Price £4.0.0. The $8^{\circ} \times 5^{\circ}$ matching speaker $£ 1.0 .0$.
Constructors (an Buili a Really Firstachass Rccord Player. Comblete in all resbects, for approx. e14. This will compare with known Record Players currently offered at much higher prices.

## GIERN TADIO PREMIER RADTO <br> mall ordens and all postal evguiaiss to

## BUILD A HIGH QUALITY TAPE RECORDER Like this for

FOR THIS WE SUPPLY
Deposit £7.0.0 and 12 months of £2.11.4. $\star$ Complete Kit of Parts to Build $\star$ The Latest Collaro "Studio" $\star$ Portable Carrying Caso (as
the HF/TR3 Tape Amplifier. Tape Deck.
$\star$ Rola/Celestion $10 \times 6$ in. D.m. Loudspeaker.

A ACOS Crystal Microphone and
(2.200 ft. Spool E.M.1. Tape.

ALTERNATIVELY WE SUPPLY THE COMPLETELY ASSEMBLED
and GUARANTEED TAPE RECORDER FOR
£39.10.0
H.P. Terms: Deposit £7.18.0 and 12 months of $£ 2.17 .11$.

HF/TR3MKII TAPE AMPLIFIER (Mullard Type_"A" design)


A very high quality Amplifer Incorporating 3-speed treble FEROXCUBE POT CORE INDUCTOR. FOR COLLARO-
TRUVOX - BRENEL WEARITE Tape Decks. has GILSEN Output Transformer. Includes separate Power Supply Unit. KIT OF $£ 13.13 .0$ PARTS 12 months at £1.0.0.
and TESTED

## 12 months at \&1.4.11. \&17.0.0

SPECIAL "COMBINED ORDER" PRICES
For Constructors with their own cabinet-WE OFFER-
KIT to buld the HF/TR3 Amplifer together with the COLLARO "STUDIO" DECK...............i.. As above but with the HF/TR3 supplied ASSEMBLED and TESTED Deposit £5.18.0. 12 monthiy payments of £ 2.4 COMPLETE KIT to build the HF/TR3 AMPLIFIER with the BRENELL MK. V TAPE DECK. Deposit £8.8.0. I2 monthly payments of £3.1.7
d) As above but with HF/TR3 supplled ASSEMBLED and TESTED Deposit $£ 9.2 .0$ i2 monthiy payments of 33.6 .9 (e) THE ASSEMBLED AND TESTED HF/TR3 AMPLIFIER with the WEARITE MODEL 4A DECK, $\& 60.100$ Incorporates Wearite Head Lift Transformer etc. Deposit £12.12.0. 12 monthly payments of $£ 4.8 .9$
£26.0.0
£29.10.0
£42.0.0
£45.10.0 (Carriage and Insurance on each above is iof- extra).

The MODEL HFG/2R PORTABLE TAPE RECORDER (Original price 833.0 .0 ) FOR ONLY 22 gis.
Deposit £4.14.0. 12 months £1.13.9 Crystal Microphone $£ 1.0 .0$ extra. Cart. and Ins. 10/-extra) incorporates THE GARRARD "MAGAQUAL TAPE DECK and a HIGH the very successful MULLARD TYPE "A" DESIGN and specifically developed to operate the GARRARD DECK. Price CLUDES THE GARRARD TAPE MAGAZINE and 4in. SPOUL OF DOUBLE PLAY TAPE. Comprises a Twin Track Recorder operating at $3\{1 \mathrm{n} / \mathrm{sec}$. speed and providing up to 1 hour 10 mins. playing time. Truly Portable - welghs only 22 lbs .
The TRUVOX "TOUCH" With the New "SERIES $60^{\circ}$ Recorders
Two Models are available R6:. A Twin Track Recorder with speeds of 16 and 32 i.p.s.
1164. A Four Track Recorder with speeds of 34 and ? $1 . \mathrm{p} . \mathrm{s}$.
PRICE FOR 840.19 .0 Deposit \&8.4.0, 12 months They offer full of s3.0.1. MON offor tull and SUPER-
 IMPOSING AUTOMATIES. STOP, a REV. COUNTER and a storage compartment for 7 inch spools tape.


ADD "HI-FI" TAPE RECORDING TO YOUR
EXISTING AUDIO INSTALLATION WITH
MLLLARD TYPE "C" MAPE PRL lhe "Hi-Fi" link to add full tape recording facllities to H1gh Fidelity home installations. In-
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Gns. parts with tully punched chassis and point-to-point
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 | $250-0-250 v$ | $70 \mathrm{~mA}, 6.3 \mathrm{v}, 2 \mathrm{a}, 0-5-6.3 \mathrm{v} .2 \mathrm{a} 17 / 9$ |
| :--- | :--- |
| $350-0-350 \mathrm{v}, ~$ | $10 \mathrm{~mA}, 6.3 \mathrm{v} .2 \mathrm{a}, 5 \mathrm{v}, 2 \mathrm{a} \ldots$ |
| $18 / 9$ |  | $\begin{aligned} & 350-10-350 \mathrm{v}, 60 \mathrm{~mA}, 6.3 \mathrm{v}, 2 \mathrm{a}, 5 \mathrm{v}, 2 \mathrm{a} \\ & 250-0-250 \mathrm{v}, 100 \mathrm{~mA}, 6.3 \mathrm{v}, 2 \mathrm{a}, 6.3 \mathrm{v}, 1 \mathrm{a}\end{aligned} \ldots 21 / 9$

 $250-0-250 \mathrm{v}, 100 \mathrm{~mA}, ค .3 \mathrm{v}, 4 \mathrm{a}, ~(6-5-6,3 \mathrm{v}, 3 \mathrm{a} 25 / 9$ $300-0-300 \mathrm{v} .130 \mathrm{~m} \mathrm{~A}, 6.3 \mathrm{v} .4 \mathrm{a}, 6.3 \mathrm{v} .1 \mathrm{a}$, for Mullard 510 Amplifier $300-0-300 \mathrm{v} .103 \mathrm{~mA}, 6.3 \mathrm{v}$. 4a. 0-5-6.3v. 3à $29 / 9$ $350-0-350 \mathrm{v} .100 \mathrm{~mA}, 6.3 \mathrm{v} .4 \mathrm{a}, 5 \mathrm{v}$. 3a, $28 / 9$ $425-0-305 v, 150 \mathrm{~mA}, 6.3 v, 4 \mathrm{a}, 0-5-6.3 \mathrm{v}$. 3 a 2 $29 / 9$
 $250-0-250 \mathrm{v}, 60 \mathrm{~mA}, 6.3 \mathrm{v}, 2 \mathrm{a}, 0-5-6.3 \mathrm{v}$. 2 a .

 4a C.T.. 5 v. . 3 55/
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Fush-Full 8 watts, ELB4, or $\ddot{6}$ vg to $3 \Omega$ or matelied to $15 \Omega$
Push-pulj $10-12$ watts to match 6 V 6 Or FI 84 to 3-5-8 or $15 \Omega$ Followine types for 3 and $15 \ddot{\circ}$ speu Push-Pı11 10-12 watts 6 VG or F.L. 84 wsh-Pull $15-18$ watts, $61 \beta$, KT6 $\cdots 28 / 9$ Push-Puli Mullard 510 Uitra Linear. $22 / 9$ Push-Pull 20 watts, sectionally
wound, $6 \mathrm{~L}, \mathrm{KT66}, \mathrm{EL} 34$, etc.

Midzet tVpe 2!-3-3in.
$250-0-250 \mathrm{v}, 100 \mathrm{~mA} .6 .3 \mathrm{v} .4 \mathrm{a}, 0-5-6,3 \mathrm{v}, 3 \mathrm{q} 2 \% / 9$ $300-0-390 \mathrm{v} .100 \mathrm{~m} \mathrm{~A}, 6.3 \mathrm{v} .4 \mathrm{a}, 5 \mathrm{v}, 3 \mathrm{a}, 27 / 11$ 1a. for Mullard Amplifier ... $33 / 9$ $\begin{array}{lll}350-0-350 v . ~ & 100 \mathrm{~mA}, 6,3 v, 4 a, 5 v, 3 a & 2 / 11 \\ 350-0-350 \mathrm{v} .150 \mathrm{~mA} .6 .3 \mathrm{v}, 4 \mathrm{a}, 5 v .3 a & \ldots 35 / 9\end{array}$

```
MIDGET MAINS Primari \(50 \mathrm{c} / \mathrm{s} .250 \mathrm{v} .60 \mathrm{~mA}, 6.3 \mathrm{v} .2 \mathrm{a}\) Both above size 2 i \(\times 24 \times 24\) ins.
``` Both above size 2 X \(x \not x 2\) xins. All with \(200-250 \mathrm{v} .50 \mathrm{c} / \mathrm{s}\). primaries 6.3 v . All with \(200-200\) v. \(5 / 9 ; 3 \mathrm{v}, 2 \mathrm{a}, 7 / 6 ; 0-4-6.3 \mathrm{v}, 2 \mathrm{a}, 7 / 9 ;\) 12 v. 18, \(7 / 11 ; 6.3\) v. 3 a, \(8 / 11 ; 6.3\) v. 6 \&. 17/6: 12 v. 1.5 a. twice, \(17 / 6\). SHOGTIING CHOKES
\(150 \mathrm{~mA} 7-10\) H H 250 ohms \(100 \mathrm{~mA}, 10 \mathrm{H} 200 \mathrm{ohms}\) \(80 \mathrm{~mA}, 10 \mathrm{H} 350 \mathrm{ohms}\)
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Quality Quality Remorder Motor Fobly shrouded
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 Special Offer!
TV Remote Control Uait By well known manufacturer, on/off, brightness and valume box with 15 feet of muiti 7 way screened cable. (itrey.) Liated at e2/2/\(\underset{\text { Special Price }}{\text { Post }}|4 /| |\)

\section*{HUGE PURCHABE}

CRYSTAL PICK-UP CARTRIDGES. LOWEST PRICES EVER, some are lees than half thst price.
ALL COMPLETE WITH STYLI L.P. \& STANDARD (AND/OR GTEHEO WHERE BHOWN), FULIY GUARANTEED BTANDARD FITTITU. WLLL FIT MOST P.J. ARMS AND HEADS. Postage \(1 /\) - each extra. TYPE C.T.1. By well known manuacturer. With 2 sapphire atyli. 18/8
 Ronette studjo \(0 . \ldots . . . .\). Acos GP.gs/3 ............ 15/ Acon GP.61/1 ........... 1B/STEREO
Acostereo 73/1. With 2 sapphlres 25/-,
Acostereo 78/8. With Diamond L.P./Btereo and aspphire 8td. 29/4,
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Ronette Stereo type 105 35/6.
Ronette Btereo type 106, with Diamond L.P./atereo and sepphire std. \(\mathbf{3 g y}\) Ronette Stereo type 106
Ronette Stereo type 106 with Diamond L.P./Btereo and sapphire std. ...................................

\section*{: TECHNICAL : TRAINING in radio television and electronics}

Whether you plan to have your own business, to become an electronics engineer, to take up a career in industry, or to brush-up your knowledge and study new developments, transistors, etc., an I.C.S. Course will help you to success. You learn at home in your own time, under expert tuition. Moderate fees include all books.
EXAMINATION COURSES FOR:-
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A basic course in radio electronic and electrical theory backed by thorough practical training. You build radio receivers, signal generator and multimeter.


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}


\section*{I5 Amp Thermostat}

You can make yourself a thermostat similar to the above using a "Sunvic" unit which we can offer at 9/6. This is adjustable over the same range as the amount of heating. We can also offer a crackle finished callbrated case which can be used for containing the Sunvic. Price two items together 14/6, plus 1/-Postage.

\section*{Ice-Stat}

This is a small thermostat which cuts on and off at around freezing point. Has many uses, one of which could be an ice warning device to Price 7/6. Post 1/-
Morganite Potentiometers
Single and
types avallable. types avallable.
standard slze with good length spindle. all
newand boxed. new and boxed. Single types. each, values avallable: \(50 \mathrm{~K}, 10 \mathrm{~K}, 25 \mathrm{~K}, 25\).
Gange tyne, , Gange type \(3 /-\) each-values avallable: \(5 \mathrm{~K} \pm 5 \mathrm{~K}, 100 \mathrm{~K} \pm 100 \mathrm{~K} \$ \mathrm{meg} . \pm\) meg. 2 meg. \(\pm 2\) meg.

\section*{Component Storage} Drawers


Stout board construction, these drawers are ideal for small parts. Supplied complete with simple erec-
tion instructions-1/6 each or 12 tion instructions-1/6 each or 12
drawers each \(6 \times 2 / \times\). 6 in., \(13 / 6\). drawers
post \(2 /=\).

\section*{Hi Fi Speakers}
E.M.I. Ceramic magnet 12.000 lines, size \(13 \times 8 \sin\). (roughly equivalent to 10 watts. Price \(33 / 6\). plus \(5 /\)-carriage 10 watts. Price 33/6. plus s/-carriage ohm or 3 ohm. Similar model but spectally designed and hand made for very low frequencies ( 40 to 55 cycles). Price £"10.0.
Miniature Transistor Sets Cheaper than you can posslbly make them, we are able to offer these made up. ready to work. complete with leather carrying cas and earphone. Astra 7 uses transistors, covers
\(535-1065 \mathrm{kc} / \mathrm{s}\), sensi. \(535-1065 \mathrm{kc} / \mathrm{s}\). sensi-
tivity 300 micro tivity 300 micro
volts/M, output 150 volts/M, output 150
mW , ferrite slab merial. Size appx 1ins. Price £6.19.6. Post \& Ins. \(3 /-\)

 Zephyr 6 , very similar specification Price 55.19 .6 with leather case and earphone plus Post \& Ins. \(3 /\)-. earphone plus Post \& ins. 3 --.秕*

The 'Good Companion'
Mk.ll using

\section*{Transfilters}

In the 'de-luxe' cablnet as illustrated it costs £10.19.6 to build-but What a set!
Scan these pages: you will find nothing to compare with its specification. It uses transfilters instead of I.F transformers, has variable feedback as well as
 all the usual features. A.V.C., Push-pull output, Ferrite Aerial, Slow Motion Tuning, etc., etc., and is a very poweriul Medium \& Long Wave set, conservatively rated at 750 mW . Every component used is by a famous maker, such as American Philco MADT R.F. transis-tors-Mullard A.F. transistors-Jackson Brothers' tuning condensers-Rola-Celestion loudspeakers-Dubilier-T.C.C.-Morganite resistors and controls. Also full after sales service available.
tou wif definitely be doing the right thing if you buy a Good Companion.
"A jolly fine set but deserving a better case"
 This is a comment Which many constructhers have voiced and de-luxe version of the Pocket Companion. This uses a solid hide case of very pleasant red with gold lettering and our Pocket Compandon now has the 15 gulnea look. The most up-to-date its type it uses a transfilter in conjunction with Philco R.F. translstors and Mullard output transisPhilc R.jolete buiding costs with plastic case \(£ 6.15 \mathrm{~s}\). or with solid hide cast, \(\mathbb{E}^{2} \% 15 \mathrm{~s}\).
If you have already built and want to change your case, then return the plastic case with a postal order for \(\mathbb{E} 1\) or if you wish to retaln the plastic case then send \(28 /\)-s, plus \(1 / 6\) Post and Ins. for the hide case only.

\section*{Infra-Red Heaters}

Make up one of these
latest type heaters
ideal for bathroom,
They are simple to make
from our easy to follow
Instructions-uses silica enclosed
elements designed for the correct
infra-red wavelength (3 microns). Price
for 750 watt element and instructions \(15 / 6\), plus 218 post and insurance.

\section*{Battery Charger Bargain}

Components Would Cost More Car Battery Charger-ready-made high output battery charger in stove enamelled sheet steel louvred case. Rated at 12 ete and ready to work. rate selector for tiv. and variable also seleter to show che charging. Suitable for \(2 x 0 / 250\) charking rate. Special snip price of \(65 \%\), plus \(3 / 6\) post and ins.


\section*{LIMITED QUANTITY ONLY'}

Waterproof heater wire. 16 yds. length. 70 watts. Self regulating temperature control. \(10 /\). Post Free.

\section*{THIS MONTH'S SNIP!!}

Slient running mains motor by very famous maker. Ideal for gramophone, tape recorder, fan, etc., etc. \(200-250\) volts, A.C., shaded pull start. Size approximately \(2 I \times 24 \times 18 \mathrm{in}\). \(2.750 \mathrm{r} . \mathrm{p} . \mathrm{m}\). Spindle diameter \(5 / 32 i n\). Spindle length inn. Brand new guarantee. Price 12/6, plus 1/- post.

"Starlux 208"
Solderless ' 3 ' TRANSISTOR. Ideal for home and holidays as no Aerial or Earth
assembling an Our solderles. Terminals ensure perfect connections using first grade Transistors and all biece tor privat receive Luxembourg (the station of the stars) and other stations on both Medium and Long waves. Penlight Battery operated. 37/6. Post and insurance, \(2 / 6\).

\section*{Building A 'Scope?}


3in. osctlloscope tube. American made type No. 3FP7, 6.3 v. 0.6 amp . heater. electrostattc deflection, brand new and guaranteed with circuit diagram of scope, 15/- each, plus 2/6 post and insurance.

Tape Recorders


One of the easlest ways to learn anything, is to then keep playindustrious Japanese have really rone to town on tape recorders this year and many bargains are on offer. it is the writer's opinion that there is bound to be a big demand for them as Christmas presents so there is a good reason why you should buy your tape recorder immediately. Prices range as follows:
Child's Model : Assemble Yourself Model \(\mathrm{E}^{6.19 .8}\)
 The "Treasurer "Hocket secretary"." s14.14.0 The first two are not really good enough for music but they are quite good for speech. The last three are reasonable also or music. Alt have a cost Try this pew learning techcost. nique- you will be amazed.

\section*{"Dipyt" Automatic HeadIamp Dimmer}

hands and feet free for emergency, could easily avoid an accident. We now offer such a device ready made and tested. The unit measures \(5 x\) very easy to wire into the circuit and can also be used to control side lamps for parking. Price of unit is £10.18.6. Carr, paid, Diagram and instructions free with unit or separate \(2 / 6\), (Agents wanted.)
Fluorescent Light Bargain
Kit of parts comprising: choke, two 1 a mp holders. holder and starter. 0 watt.

watt. \(23 / 6\). Plus \(2 /\)-post and insuranca
 Heater Just screw it together. Uses 1250 watt copper cladelement which glves off black heat. Will last a lifetime. oom, it's so safe. Complete in crackl Anished case. 23.19.6. easily worth double. Carriage and insurance, 6/6.

\section*{Flood Lamp Control}

Our dim and full switch is ideal for controlling photo flood lamps: it gives two lamps in serles, two lamps full brilliance and lamps off. Similar control of other appliances can be arranged where used in pajr or where eircuit can be split exactly in half.


Technically the switch is 5 known as a double-pole change over with off. Our price 3/6. plus post and nsurance 1/-.

noculars originally part
the "see in the dark", equipment ontain many lenses, and two compete systems suitable for closed circuit T1th cameras may be made from each (1ons). The binoculars are instructhey also contain 2 infra-red cells, but these are sold without guarantee. Offered at a really bargain price of e2.1\%.6. plus 5/-carr. and ins.
Transistor Set Cabinets


Very modern cream cabinet, size \(5 \downarrow \mathrm{x}\) \(3 \times 14 \mathrm{in}\). with chrome handle. tuning knob and scale. Price \(7 / 6\), plus 1/6 postage and packing. Special quotations for quantities.

\section*{Miniature Microphone} American made. Dynamic type. reai bargain at 2/8, plus 6d. postage.

\section*{Power Unit}

A useful source of D.C. for experimenting, energising instruments, esectroplating, reactivating batteries etc. This power unit can be made in a of hours and due to the availabinity price, we can supply the complete kit pice, we can supply the complete hit reto any box for \(9 / 6\). plus \(1 /\) - post and insurance.


\section*{Cabinet \&ick-up}

Made for a famous Company intending to make a Battery Record Player but changed their minds. This is an extremely fine looking cabinet, must have cost at least \(£ 2\) to make. It is complete with handle and fasteners as illustrated. Also included in the parcel is a Cosmocord pick-up with crystal cartridge and sapphire stylus. Both items new and perfect. Price 1916, plus 4/6 Post \& Ins.

\section*{DO YOU EVER FORGET?}

\section*{This Pocket Secretary collda} eliminate the trouble (often emburrassment) your forgrtfulness catuses you-she will stay in your jacket pocket and as fast as you can think slie uill capture and slore-ideas notes-formulae-appoint-ments-anything you can say or sing! then at your demand she will play them whl back to you.
Undoubtedly one of the smallest precision tape re. corders made. Entirely controlled by push buttons. you can record ard play back with the instrument in your pocket. It is a full function machine using standard \(\frac{1}{2}\) tape and easy to replace batteries. Speaking and playing back is from the same (crystal) microphone.
Sperifications: Dimensions: \(6 \frac{1}{4} \times 2 \frac{1}{2} \times 18\), weight: 14 oz. recording time: le mins. rewinding time 4 mins. recording system: D.C. Bias, erasing system: Magnetic erasing, wow and flutter within \(2^{\prime \prime}\). and frequency
response: \(500-1,200 \mathrm{~s} / \mathrm{s}\) (within- Gdb .
Prier £14.14.0. Cimplete ready to work.
Bargain for Service Engineers You often come up against the old set that won't be parted with. For these we can offer bargain parcel of rectifiers MU12 replacement and forsiacement. ex-government paid.

\section*{Parcel of Mica Condensers} 50 all very useful values. Total list prlce over 25 . Yours for \(5 /\).

\section*{Simmerstat Heater Regulator} A device for controlling the quantity of heat delivered from an element, boiling ring, heater. soldering iron (anything up to 2,500 watts). Completely adjustable from zero to max. Normally these are \(55 /-\) each. Special snip price 15/- each. Plus \(1 / 6\) post and nsurance.

\section*{Zener Diodes}

Latest invention for voltage control and stabilisation. Complete with and stabilisation.

\section*{MULTI-METER BARGAINS!}

MODEL ITI/2 (Filus. on right). 20,000 ohms per volt, 20 ranges comprising A.C. volts, 5 ranges up to 1,\(000 ; D . C\). volts, 6 ranges up to 2.5 KV ; C.C. current, 3 ranges up to 26 ohms; resistance, 2 ranges up to 6 meg.; capacity 2 ranges up to 0.1 ; decibels- 20 to +22 . Scale cornerwise to the equivalent of 4 in . movement is pocket size instrument measuring \(4 \frac{1}{2} x\) \(3 \frac{1}{3} \times\) lin. Complete with test prods, battery and operating instructions, price \(£ 5.5 .0\), post free.
MODEL EPIOK. Similar in size and appearance to ITI/2 exsept that this is 10,000 ohms per volt and maximum D.C. volts 1,200 instead of 2.5 K , also no capacity range. Price £5.19.6. Post free.


\section*{ALL METERS BRAND \\ NEW AND FULLY GUARANTEED}


MODEL TP5S. (IIlus. on left). 20,000 ohms per volt; D.C. volts, 5 ranges up to 1,\(000 ;\) A.C. volts, 5 ranges up to 1,000 ; resistance, 2 ranges up to 10 meg.; capacity 2 ranges up to 0.1 ; decibels- 20 to +26 . 'One switch control, really beautifully made precision instrument, size only \(3 \frac{1}{4} \times 5 \frac{1}{2} \times 1 \frac{1}{3}\) in., price only E5.19.6. Post free.
MODEL TPIO. Similar in size and appearance to TP5S, but sensitivity 2,000 ohms per volt, price \(£ 3.19 .6\). Post free. MODEL U1. A robust instrument of 1,000 ohms per volt sensitivity. A.C./D.C. volts up to \(1,000, D . C\). current up to 500 , resistance up to 200 K , size \(5 \frac{1}{4} \times 3 \frac{1}{5} \times 2 \frac{3}{4}\) ins. complete with test prods, single switch control, large easily-read scale, price only \(£ 2,19.6\). Post free.

\section*{ELECTRONIC}
post orders are dealt with from Eastbourne, so for prompt attention please post your orders to 66 Grove Road, Eastbourne, marked Department 7. Callers may use any one of the Companies below.
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\hline 286 London Road, &  & 520 Iliert strext North & 42-46 Windmill llilt, & 246 Iimh Streett \\
\hline ('rovdon. & Finsbury Park. N.4. & Mantor Patk. E. 12. & Rnishith, Mididx. & Harleaden, N. W'10. \\
\hline Phone: CRO 6558 & Phone: ARChway 1049 & Phone ILFord 1011 & Phone: RUIsllp 5780 & Phone: ELGar 4444 \\
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* Full VHF Band ( \(87-108 \mathrm{Mc} / \mathrm{s}\) and Medium Band, 187-570M) \(\star 7\) Valves \(\star 5\) Watts Output \(\star\) 15ab Negative Feedback \(\star\) Separate wide range bass and Treble Controls \(t\) 2 Compensated Pick-up Inputs \(\star\) Frequency Response \(30-22,000\) c.p.s. \(\pm 2 \mathrm{db} \star\) Tape Record and Playback Facilities \(\star\) Continental Reception on Good Programere Send S.A.E. for leaflet

PRICE \(£ 22.18 .0\) Cart. Free


\section*{BARGAIN SALE PRICES}

New Boxed VALIVES \(50=1\) ay (iuarantee
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\hline 024 & 6/15K7 & & EABU80 8/ & 8/-1 PCTA \({ }^{\text {d }}\) & 0/- \\
\hline 1 RS & 6/.6K86 & 5/ & F.B91 4/ & 4/- PC'L d \(^{\text {d }}\) & 101. \\
\hline 1,45 & 6/- 4L61: & 8/- & EBC'll 8 & 8/- P1, 1 & 101- \\
\hline 1'4 & 3/-6N7M & 6/- & EBCAI 81 & 8/- PL×3 & 8/- \\
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\hline 3 3 4 & \(7 /\) +13 7 & 6/- & EClid2 9 & 9/-PY81 & 8\% \\
\hline 3 V 4 & 7/-0V6G & 6/. & ECH81 9 &  & 7- \\
\hline 3 U & 7/6. 6.4 & 5/- & EH5S 6 & 3/- PY83 & 81 \\
\hline 5 U 4 & \(6 / \mathrm{m} \times 5\) & 6/- & Ev89 8i & \(8 /-4 \mathrm{P}^{2} 5\) & 71 \\
\hline 5 Y 3 & 6/.12AT7 & 61. & EL3: 5 & 5-- \(\mathrm{SP}^{\text {d }} 1\) & /- \\
\hline 5 L 4 & 9/-12AU7 & 8\% & E1.84 7 & Ja MP61 & \(3 /=\) \\
\hline \(0 \mathrm{AC7}\) & 4/112AX7 & 71 & EY51 9 & 9/-1522 & 7 \\
\hline 6АM6 & 4/-12 \(\mathrm{SH}^{\text {H7 }}\) & \(71 \%\) & EYS 9 & 9/-UBC41 & 8/- \\
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\hline 6BW6 & 7/-125 Y 6 c & 9/- & E1148 1 & 1/- UCLS & 10/- \\
\hline \(6 \mathrm{C4}\) & 8/-35 L6 & 9/- & HABC8010 & 0/- UCL8 & 12/- \\
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\hline 6G6 & 4/-807 & & КT33C 8 & 8/- U L41 & , \\
\hline 6H6 & 3/-954 & & KI76 8 & g-UY41 & 710 \\
\hline 6.55 & 5/- DAF96 & 8/- & MU14 7 & 7/- UY85 & 7/- \\
\hline 636 & 5/- Lト96 & & PCCN 8 & 8/-UU9 & \(7 /\) \\
\hline 637G & 6/- DK90 & & PCFs0 8 & 8/-VR150 & 7/- \\
\hline 6 K 8 & 5/- D L98 & \(8 /\) & PCP82 8 & 8/.1W81 & 6/. \\
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\end{tabular}

\footnotetext{
I.F. TIRANSFOLRMERS 7/6 pair \(465 \mathrm{~K} / \mathrm{a}\) Slag Tuning Miniature Can, \(2 \times \frac{4}{4} \mathrm{fin}\). High Q and good bandwidth. Data shoets. NEW
ELECTROLXTICS
TUBULAR TUBULAR

FAM1OLS
MAKES TUBOLAR TUBULAR CAN TYPES \(1 / 350 \mathrm{~V} \quad 2 /-150 / 350 \mathrm{~V} \quad 5 / 6 \mid 16 / 450 \mathrm{~V} \quad\) 5 \(\begin{array}{llll}2 / 350 \mathrm{~V} & 2 / 3 & 300 / 25 \mathrm{~V} & 3 /- \\ 4 / 450 \mathrm{~V} & 2 / 3 & 32 / 350 \mathrm{~V} & 4 /- \\ 100 / 270 \mathrm{~V} & 5 / 8\end{array}\) \(4 / 450 \mathrm{~V} \quad 2 / 3 / 250 / 25 \mathrm{~V} \quad 3 /-2,00016 \mathrm{~V}\) \(8 / 450 \mathrm{~V} \quad 2 / 31500 / 12 \mathrm{~V} \quad 3 /-8,000 / 6 \mathrm{~V}\) \(16 / 450 \mathrm{~V} \quad 3 /-18+8 / 450 \mathrm{~V} \quad 3 / 632+3 \cdot 2 / 350 \mathrm{~V}\) \(32 / 450 \mathrm{~V} 3 / 88^{8+8 / 450 \mathrm{~V}} \quad 3 / 632+3 \cdot 2 / 450 \mathrm{~V} \quad 6 /-\) \(25 / 25 \mathrm{~V} \quad 1 / 98+18 / 450 \mathrm{~V} \quad 3 / 9 \quad 32+32+32 / 350 \mathrm{~V} 7 /-\) \(60 / 25 \mathrm{~V} \quad 2 /=16+10 / 450 \mathrm{~V} \quad 4 / 3\) \(50 / 50 \mathrm{~V} \quad 2 /-32+32 / 350 \mathrm{~V} \quad 4 / 6 / 100+200 / 275 \mathrm{~V} \quad 12 / 6\)
}

\section*{COMPLETE RADIO CHASSIS £5.19.6. post free}

4 Mullard valves. \(51 n_{\text {Bi speaker. }}{ }^{\text {superhet }}\) Clreult.
Superhet Clreult. BRANI) NEW.
Size \(9 \times 6\) x 5 in. high. Tested by us ready Slze \(9 \times 6 \times 5 t i n\). high. Tested by us
for use. \(200 / 250 \mathrm{v}\). A.C.-D.C. Mains.


DE LUXE MODEL as Illustrated with Mliuminated dial. Fully tunable over Medium
antee.

MAINS TRANSFORMERS 200/250 จ. A.C. Postage \(2 /\) earh transformer.
STANDARD, \(250-0-2500,80 \mathrm{~mA}, 6.3\) v. 3.8 a.
tapped \(4 v .4\) a. Rectifler \(13.3 \mathrm{v} \cdot 1 \mathrm{~A}, 3 \mathrm{~F}\). 2 a. or 4 v .2 a a. 22/6, ditto. \(350 \cdot 0.350\).. 29/6
 MIDGET, 220 v. 45 mA .6 .3 v. \({ }^{2}\) a. \(\quad 1 \mathrm{~J} / 6\) \(\begin{array}{llllll}\text { SMALL, } 220-0-220, & 50 \text { tiAA, } & 6.3 & \text { v. } & 2 \text { a. } & 17 / 6 \\ \text { STD. } 280-0-250 & 85 \\ \text { nuA } & 6.3 & \text { v. } 3.5 & \text { n. } & 17 / 6\end{array}\)
 Ditto, tapped sec. \(2,4,6.3\) v., 1/ smp. 8/8 Ditto, rec. 6.3 v. 3 amp. GENERAL PURPOSE LOW VOLTAGE, 2 gmp. \(\begin{array}{llll}3.4,5,6,8,9,10, & 12,15,18,24,30 & \mathrm{~F} . & 22 / 8 \\ \text { AUTO TRANSFORMER, } 150 \mathrm{w} . & \therefore . & 22 / 6\end{array}\) \(0,120,200,230,250 \nabla ., 500 \mathrm{~W} . \quad \therefore 8_{82 / 8}\) MULLARD " 510 " Mains transioner wion PARMEKO MAINS TRANSFORMER. Made for gpecial contract, the ratings can bafely be \(210-230-250\) v. H.T. \(300-14-300\) v. 50 mA . Lar. T . 6.3 v. 1.8 amp . Size \(\mathrm{i} \times 3 \mathrm{k} \times 3 \mathrm{k} \mathrm{in}\). Weight AIb.

MAINS POWER PACK Size 3 a \(\times 4 i^{\circ} 17 / 6\) with mains tranoformer, metal rectulter and cundensers to provide smoothel H.T. nutput 220 v. 46 mA . D.C., I...T. is. 3 v. 2 a. centre brand New. Bargain. Post \(2 / 6\).. .. \(29 / 6\)

INTERVALVE TRANSFORMERS 3:1 or \(5: 1,8 /\) O.P. TRANSFORMERS. Heavy Duty 50 mA , \(4 / 6\). Mulliratic push-pull, 7/6. Ditto, \(10 \mathrm{ws}, 15 / 6\). Miniatire, 384 m ete., b/9. L.F. CHOKES 15/10H. 60,60
 FULL WAVE BRIDGE SELENI NM R CAI RR: CHARGER TRANSFORMERS. Tapped input 2001 250 v. for charsing at 2,6 or \(12 v_{\text {vt }} 11\) amps., \(15 / 6\). 2 amps. meter Leads, Fume ' 'aue. itc., for \(t\) w. or \(1: v_{1}\), \(69 / 9\)

\section*{BOOKS list S.A.E.}

40 Clrcuits for Girmanium Diodes 3/-. "W, W." Radio Valve Data, \(8 / \%\).
High Fldelity Speaker Enclosure, 5/-. Vave and TV Tube Equivalents, g/6 TV Fault Findint, 5/-,
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Transistor Superhet Recelvers, \(7 / 6\) Prattical Radio Inslde Out, \(3 / 6\). Master Colour Code Chart, 1/6.
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\section*{4 TRANSISTOR PUSH-PULL AUDIO}
size \(3 \times 1 \frac{1}{4} \times\). AMPLIFIER
A ready bullt miniature pusb-pull amplifier with loput and output transformers, 4 transleturs. Ideal for use with record players, intercoms, etc.
Complete with full instruetions and elreult.
Price 52/6 9\% Ratt. 2/3, 2ifa. Speaker 15/-
C.R.T, BOOSTER TIRANSFORMERS for heater cathode short circult or tubes with laling emlssion. Full instructions supplied, mains input. Type A optional \(25 \%\) and \(50 \%\) boost.

LOUDSPEAKERS P.M. 3 OHM, 21, 3, 4in., \(19 / 8\). sin. Hola, 17/8; 8in. Pleasey, 19/8; 7in. x 4in. Rola 18/e; 日lin. Rola, 18/6; \(10 \geq 6 \mathrm{in} .27 / 6 ; 10 \mathrm{in}\). Rola \(30 /=: 4 \mathrm{in}\). Tweeter, \(20 /-; 12 \mathrm{in}\). A.A. \(80 /-\); 13 i I 8 in .
Double Cone E.M.1. 45/:
STENTORIAN BFID12. 10 n. 3 to 15 ohmm, \(10 \mathrm{w.93/-}\) \(35 \mathrm{ohm}, 7 \times 41 \mathrm{n} ., 25 / \mathrm{m}\); \(51 \mathrm{n} ., 22 / 6 ; 8\) in. \(0,18 / 6\).

\section*{BAKER SELHURST LOUDSPEAKERS}

Detaile S.A.E.
12In. laker lisw. stalwart c.p.s. l2in. Ntereo; Foam Buspensi
 l2in. Baker Cltra Twelve \(20 \mathrm{e} . \mathrm{p}, \mathrm{s}\), to \(25 \mathrm{kc} / \mathrm{s} .217 .10\) Fin. Auditorium, 35 W. \(\overline{\text { Detailg and Enclogur }}\) plans B.A.E.
TWIN GANG TUNING CONDEMSERS. 365 pF nimiature lin. x 1 fin . \(x\) Ifin. \(10 / \mathrm{f}, 500 \mathrm{pF}\) Standard with trimmers, \(9 /-\); midget, \(7 / 6\); with trimmers, \(9 /=\) 500 pF slow motion tuning, atandard or midget, \(9 /\) SMALL 3 gang \(500 \mathrm{pF}, 17 \%\).
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10 watt \(\left\{\begin{array}{c}\text { WIRE-WOUND RESISTORS } \\ 10 \text { otmons- } 10,000 \text { ohins }\end{array}\right\} \begin{aligned} & \text { Witto } 5 \%, 10 \Omega \text { to } 22 \text { nieg., } 9 \mathrm{~d} . \\ & 1 / 3 \\ & 2 /-\end{aligned}\) 10 watt \(\left\{\begin{array}{c}\text { WIRE-WOUND RESt } \\ 10 \text { obmas }-10,000 \text { ohins }\end{array}\right\}\) 12.5 K to 50 K 10 m.


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\section*{Practical Wireless}

Vol. XXXYIII No. 670 DECEMBER, 1962


\section*{The Final Link}

THIS month we present the last in the current series of free, double-sided blueprints and we feel we have produced two designs of widespread appeal and interest.
The first is the Luxembourg Tuner which, as the name implies, has been specifically designed for peak performance on 208m. This tuner incorporates some novel features which will appeal to those wanting to try something a little different, it is easy to build and is strongly recommended to readers who want better-than-normal reception of Radio Luxembourg.

The reverse side of our blueprint also breaks new ground, so far as Practical Wireless is concerned. It is probably true to say that of the thousands of enthusiasts who take the trouble to build good quality receivers and amplifiers, a good many make do with inferior or indifferent arrangements for the final link in the audio chain.

One can, of course, mount a loudspeaker on a solid baffle or insert it into a box of any convenient shape and size and get reasonable (even superb) results. Much depends, naturally, on the predominating acoustics and the degree of audio discernment in the ears of individual listeners.

But this hit-or-miss approach, while capable of relatively good results can lead to disappointment and, in any case, it seems odd to carefully design the electronics and take the acoustics for granted.

In general, then, a well-designed enclosure is the only real housing for a loudspeaker and the only acceptable device for disseminating high quality audio.

We feel it is appropriate, therefore, to conclude this series of blueprints with The Berkeley-a specially designed bass reflex speaker enclosure which is suitable for use with P.W. or other high quality amplifiers and which will give added pleasure to your record, radio or tape listening.

\section*{Our Query Service}

0NCE again we must remind our readers of the rules of our Free Query Service. The following points should be carefully noted:
(i) We cannot undertake to answer technical queries over the telephone
(ii) All queries must be accompanied by the query coupon from the current issue
(iii) If a postal reply is required a stamped and addressed envelope must be enclosed with the query.
We must also point out that we cannot design circuits to readers' specific requirements. Nevertheless we shall continue to help readers as far as possible but it should be remembered that all information necessary for answering the query should be sent to us.
||||||||||||!|||||||||||||||||||||||||||||||||||||||||||||||||||||||||||||||||||||||||||||||||||||||||||||||||||||
Our next issue dated January will be published on December 7th.

standby basis. One particular feature of the S264A equipment is that. being crystal controlled. it can be switched into operation from "cold" if necessary.

Marconi 50 cm radars are currently in operation at many British airports. Service establishments and airfields.

\section*{Conference on the Design and Use of Microwave Valves}

THE Electronics Division of the Institution of Electrical Engineers is organising a threeday national conference in September, 1963, on the design and use of microwave valves. This has been timed to fall between international conferences on microwave valves which are held every other year and the programme will be complementary to these conferences.

The forthcoming conference will review present techniques and developments and will cover fundamental valve design, present performance and the use of valves in systems, including matching system characteristics with achievable valve performance.

It will be of particular interest to engineers in this country who do not attend international conferences and among the subjects to be covered will be "signal amplification and physical measurement ", "communications and industrial applications " and "radar".

\section*{New Headquarters Installation for R.A.F. Radio Amateurs}

THE new headquarters of the R.A.F. Amateur Radio Society was opened recently at No. 1 Radio School, R.A.F. Locking.

The society, which was formed in 1939. includes a large number of professional wireless operators. both R.A.F. and ex-Service, in its membership and most local R.A.F. amateur radio clubs are affiliated.

A grant of \(£ 660\) from the Nuffield Trust for the Forces has paid for the most expensive of the new installation which is used in conjunction with a beam aerial which can be directed to any part of the globe. A standby transmitter also capable of top band communication has also

High-power Radars for Ministry of Aviation
CONTRACTS by the Ministry of Aviation have been awarded to Marconi's for the provision and setting to work of three dual installations of \(500 \mathrm{~kW}, 50 \mathrm{~cm}\) radars, type S264A. These will be sited at St. Annes (near Black pool), Ash (near Sandwich, Kent) and Ventnor (Isle of Wight). These are the first radars ordered by the Ministry for the United Kingdom Airways System.

The dual installations consist of the complete transmitting/ receiving and ancillary equipment in duplicate, feeding a common aerial head on a main/


A Marconi 50 cm surveillance radar of the type recently ordered by the Ministry of Aviation.
been installed in addition to a 2 m VHF set which is restricted to United Kingdom use.

\section*{Recording Noise}

IONDON is the first city in the world to be systematically surveyed for noise. The information obtained will be useful for town planning generally and especially to architects when making provision for insulation in new buildings of all kinds in the central area.

Information about noise levels at selected sites throughout central London is also being recorded for use in particular town planning problems such as assessing the noise effects of elevated motorways and heliports and for siting hospitals and other buildings where noise may be detrimental to their use.

The London Noise Survey is being conducted by the Building Research Station of the Department of Scientific and Industrial Research and the London County Council. Two vans with equipment which includes TR 52/2 professional tape recorders supplied by EMI Electronics Lid. are sampling noise levels for 100 seconds once an hour over a 24 -hour period at each of 540 points, distributed at 500 yd . intervals on a rectangular grid over central London. The work has continued since early in 1961 and more than 350 sites have already been monitored.

Noises are automatically recorded on magnetic tape every hour on the unattended tape recorders. At the end of the 24-hour period the tape is taken to the Building Rescarch Station at Garston for analysis.

\section*{New T.I.M. Recording}

THE Post Office is to make new recordings for T.I.M., the Speaking Clock.

The present Speaking Clock, which has been in use since 1936, is to be replaced early next year. While the timekeeping of the present clock is as good as it was a quarter of a century ago some parts of it are obsolete.

The new clock. which has been designed and built by Post Office engineers at the Research Station at Dollis Hill. London, will, with the new techniques employed. be cheaper to instal, maintain and operate. The quality of the recordings will also be improved.


A member of the LCC staff is seen here switching on an EMI tape recorder in a van at an Albert Embankment site, in Landon, to record sample noise levels (see "Recording Noise").

The Great German Radio Exhibition
O VER 100 firms to date have registered for the Great German Radio Exhibition to be held at the Berlin Funhturm from August 30 to September 8 , 1963. Final figures can only be estimated at the commencement of next year. However, it can already be determined that once again all halls and pavilions of the exhibition area occupied in 1961 will also be in demand for the Radio Exhibition of 1963.

The studios of the broadcasting stations will again participate with demonstrations in the exhibition. Formerly only one hall of the exhibition grounds was required to house the Channel 1 television programme; however, in the coming year a further hall is planned for the Channel 2 programme.

Temporary VHF Station on the Isle of Skye
'THE BBC's plans for extending and improving reception of
its sound and television broadcasting services in the West of Scotland and the outlying islands provide for several new transmitting stations, including a combined television and VHF sound station for the Isle of Skye. As the completion of this station and of the necessary radio links to connect it with the BBC's Scottish programme networks will take some time a temporary low-power VHF sound relay station has been brought into service at Penifiler to serve the town of Portree. This station is now transmitting the Scottish Home Service on \(93.9 \mathrm{Mc} / \mathrm{s}\) with horizontal polarisation, which means that VHF receiving aerials should be mounted horizontally.

It is hoped to complete the television station for the Isle of Skye and the permanent VHF sound station, which will radiate the Light and Third programmes as well as the Scottish Home Service, early in 1964.

\title{
A HIGH QUALITY BASS REFLEX CABINET
}

\author{
By R. Edwards
}

\section*{The BERKELEY Loudspeaker}


\(\mathcal{J}\)HE bass reflex type of loudspeaker enclosure has been popular for many years on account of its ability to provide good smooth output down to the lowest frequencies normally reproducible by the particular moving coil unit employed.

In this type of enclosure, which is also known as a "vented enclosure" or "phase inverter cabinet", use is made of the sound waves radiated from the rear of the loudspeaker cone, and these waves are allowed to emerge at the front of the cabinet through an aperture or "vent" close to the loudspeaker opening. The interior of the cabinet forms a resonant cavity and its resonant frequency is determined by the volume of air enclosed and the area of the vent. It is usual practice for the enclosure to be tuned to the bass resonant frequency of the loudspeaker unit.

Due to the loading provided by the enclosure, the characteristic peak in the loudspeaker speech coil impedance curve at bass resonance resolves into a pair of peaks, one just above the enclosure resonant frequency, and the other just below. The amplitude of both peaks is considerably less than that of the original single bass resonant peak, con-

\section*{Enclosure}
sequently there is less mismatch with the amplifier at this frequency than there would be normally. and so more power is delivered to the speech coil.

Furthermore, in the region of resonance, greater air loading is offered to the cone resulting in improved efficiency of the system together with a reduction of amplitude distortion.

For sound frequencies equal to and just above the enclosure resonant frequency sound waves radiated from the rear of the cone undergo a \(180^{\circ}\) phase change and appear at the vent in phase with the radiation from the front of the cone, thus the effective sound output is the combined output of these two sources.

When the sound frequency is lowered below resonance the phase of the air in the vent changes abruptly and tends to oppose that from the front of the cone. The response of the system therefore falls off just below the enclosure resonant frequency.

On the other hand, as the frequency is raised above the enclosure resonance the enclosed volume of air becomes increasingly capacitive and the sound waves from the rear of the cone tend to become absorbed within the cavity, until eventually at high frequencies there is practically no output from the vent and the system performs as an infinite baffle.

\section*{Design Features}

Optimum size for a bass reflex cabinet is governed by the particular loudspeaker to be used, the cone diameter and fundamental resonance being key factors in this respect. The Berkeley bass reflex enclosure is intended for use with a high power amplifier, such as the Strand Amplifier (described in the October issue of Practical Wireless), and has been designed around a 12in. dia-


Fig. 1-A half-section, constant-resistance network; parallel connection.
meter moving coil unit having a power handling capacity of 15 W . Provision is also made for the fitting of a H.F. tweeter unit.

The loudspeaker specified is WB Model H.F. 1216. This is a full range unit, covering 20c/s to \(16,000 \mathrm{c} / \mathrm{s}\) and has a fundamental resonance of \(37 \mathrm{c} / \mathrm{s}\). A second choice would be the WB Model H.F. 1214. This is a less expensive unit and has a frequency coverage from \(25 \mathrm{c} / \mathrm{s}\) to \(14,000 \mathrm{c} / \mathrm{s}\), while the bass resonance is at \(39 \mathrm{c} / \mathrm{s}\).

A corner style enclosure has been adopted as this allows full advantage to be taken of the walls as reflecting surfaces and these improve the low frequency sound distribution. A triangular cabinet has good acoustical properties and is, of course, likely to prove the most convenient shape for installation in a room.
The dimensions of the Berkeley have been chosen to provide a volume of 9 cu . ft . which is about ideal for the type of loudspeakers specified, and it is tuned to just below \(40 \mathrm{c} / \mathrm{s}\) approximately by a plain vent. A smaller cabinet would result in inferior bass response and would also prove more critical in respect of tuning. The effects of standing waves are less serious in a large enclosure and can usually be dispelled by the use of only a small amount of lagging material.
To ensure rigidity and so prevent resonance effects from any of the surfaces, all panels are 1 in . thick and are built up from equal thicknesses of blockboard and chipboard and glued together. All joints must be glued and must be air tight since
any air leakage other than through the two apertures in the front panel will impair the proper functioning of the enclosure as a "bass reflex".

The small aperture to the right of the large loudspeaker opening is for an H.F. tweeter unit, but the fitting of such a unit is quite optional. It is certainly advisable to try the enclosure with only the 12 in . unit in position before incurring further expenditure which, subsequently, may not perhaps appear fully justified.
The question of what is correct tonal balance is very much a matter for the individual to decide, and it is possible that due to the efficient bass response there may seem to be some deficiency in the upper register. In such a case the incorporation of a tweeter unit should restore the balance satisfactorily by adding the necessary brilliance to the reproduction.
It is considered prudent to carry out this drilling and to fit the four screws during construction, or at any rate before the covering material is fitted to the front panel, since it would obviously be an inconvenient task to perform once the cabinet has been completely finished.

If a tweeter is not to be installed initially this hole must be covered by means of a piece of \(\frac{1}{2} \mathrm{in}\). plywood about 6 in . x 4in. This should be drilled to accept the four captive screws, and then clamped tightly against the inside surface of the cabinet with nuts.
The drilling details given on panel \(F\) (Blueprint) are for the W.B. Model T. 12 Tweeter Unit. Details of this unit and suitable crossover networks are given later.


Fig. 2-A half-section, constant-resistance network; series connection.

\section*{Lagging the Enclosure}

Sound waves from the rear of the loudspeaker cone at middle and upper frequencies produce standing waves in the cavity, and these are sometimes of sufficient severity to disturb the smooth response characteristic of the system and so to "colour" the output. It may be necessary to lag the interior with absorbent material in order to eliminate such effects. The amount of lagging needed can be determined only by experiment.
Critical listening tests should be made with the completed (but unlined) enclosure installed in its final location. Such tests must be of fairly lengthy duration and should involve the reproduction of both music and speech, to permit a proper assess-
ment of the loudspeaker enclosure performance to be made. Dry, unnatural colouration or tendency to boominess or ever accentuation of the lower frequencies may be cured by partially lining the inside of the enclosure with felt or fibreglass blanket material \(\frac{1}{2}\) in. to 1 in. thick.

It is suggested that only two interior surfaces be lined, preferably the underside of the top panel and one of the side panels. An alternative and possibly better scheme is to suspend a curtain of the same material from the top panel so that it hangs diagonally across the interior of the cabinet.

The application of absorbent material must be carried out discriminately, since excessive damping of the enclosure can have an adverse effect on the high frequency response. The inspection panel must always be replaced firmly in position before resuming listening tests.


\section*{H.F. Tweeter Unit}

The H.F. tweeter W.B. Model T. 12 is a hornloaded pressure driven moving coil unit. It has a frequency range of 3.000 to \(17.000 \mathrm{c} / \mathrm{s}\), an impedance of 152 , and a power handling capacity of 15 W .

When using the tweeter, a crossover or dividing network is also required in order to restrict the range of frequencies applied to each loudspeaker. The type of crossover network recommended is that known as a half-section constant-resistance network. This particular kind of crossover can take two forms, either "parallel connecticn" as shown in Fig. 1 or "series connection", 广ig. 2. Actually there is very little to choose between these two forms. The series connection is often considered as being somewhat better in performance than the parallel arrangement: however, the latter circuit uses smaller value capacitors and so is cheaper and perhaps easier to make up.

A crossover frequency of \(3,000 \mathrm{c} / \mathrm{s}\) should be used, and the appropriate component values are given in the circuit diagrams. That part of the circuit feeding the L.F. unit forms a low-pass filter, and has an attenuation rate of 12 dB per octave above the crossover frequency. The H.F. unit is fed from a high-pass filter, this having a similar rate of attenuation below the crossover frequency.

The input impedance of the crossover network is \(15 \Omega\) and the matching to the amplifier is not altered at all by the addition of the tweeter, although a slight loss in the total output does occur in the region of the crossover frequency.


Above-The enclosure ready for the finishing touches. Left-A view inside the cabinet.
A suitable crossover unit (type CX300-series connection) can be obtained from the manufacturers of the loudspeakers. For those who may wish to construct their own networks details are given below.

Paper, or metallised plastic film type capacitors should be used and these should have a voltage rating of \(50-100 \mathrm{~V}\). Electrolytic capacitors are not suitable. It will be necessary to use capacitors in parallel in order to obtain the values specified.

The coils can be easily constructed by winding 16s.w.g. enamelled wire on a cardboard or plastic former lin. diameter and 1 tin. long. Cheeks about \(3 \frac{1}{2}\) in. diameter should be fitted at either end of the former. The 1.125 mH coil requires 210 turns (about 16 layers) and the 0.56 mH coil 145 turns ( 11 layers). All turns must be close wound and the layers even. Terminate the completed coil by passing each end of the wire through a pair of holes in the end cheeks then bringing out about lin. of wire to provide the connection.

For convenience the filter components should be assembled on a small wooden panel and, after the wiring has been completed, this can be
mounted on the floor of the cabinet. In order to avoid inductive coupling it is advisable to arrange the two coils so that there axes are at right angles to one another, and to space them about 3 in . apart.

Since there is a \(180^{\circ}\) phase shift through the crossover network, the two loudspeakers must be connected in what would be normally anti-phase. Correct phasing can be established by reversing the two leads to one loudspeaker speech coil and observing which arrangement gives best sound output.

\section*{The Finish}

Regarding the finish to the cabinet, use has been made of applied "Vinyl" or "Fablon" to the sides, and wood or plastic veneer to top and edges. This eliminates the necessity of polishing to great extent. The front is covering with approved loudspeaker fabric. It is suggested that the cabinet should be first made up "dry", then dismantled and finally glued up after any needful adjustments have been made.

Start by cutting all the blockboard panels to drawings on the Blueprint,, plane all edges square,

Fig. 3 (right)—An exploded view of the Berkeley.


The units undermentioned in this article are manufactured by Whiteley Electrical Radio Company Ltd., Mansfield, Notts., England.

\section*{Building the Cabinet}

The construction of this corner cabinet is quite simple, complicated joints being eliminated entirely. A little care and attention to planing edges square and true will be well repaid when finally assembling.

Two types of board are used, both of half an inch thickness. The inside is of chipboard (Weyroc) and the outer of blockboard or laminated blockboard. This latter material is a superior board and is well worth the extra expense. Owing to the acoustic requirements regarding cubic volume of the inside of the cabinet it will be found that a \(9 f t\). x \(4 f\). board of each material will be needed. Stock sized boards are usually 8 ft . x 4 ft ., so enquiries should be made concerning the availability of material of suitable size.
and where required at \(45^{\circ}\). Gauge a line to mark the boundary of the chipboard all around the inside face of each panel. Care must be taken to get these marks the right distance in from the edges. They vary, due to the overlapping.

Now cut the chipboard panels to fit the markings and screw each parr together with \(\frac{3}{3}\) in. \(x\) No. 8 csk. screws at 1 ft . centres. Having proceeded this far all sections should correspond to details on the Blueprint. Assemble the cabinet by screwing through the edges of the blockboard with 1 in. \(x\) No. 6 csk. screws, making any adjustments to the meeting. rabbeted edges, etc.

\section*{Glueing}

Having checked for squareness and tight joints, dismantle and glue and screw the respective panel sections together. These should be placed one on top of each other on a flat surface and weighted on top. Leave for a day to thoroughly set. This
(Continued on page 749)

\title{
transistor
}
tunerreceiver

\author{
By A. Sydenham
}

\(D\)ESPITE many criticisms of transistorised receivers one must acknowledge the high sensitivity of the superhet form-the distinction immediately being drawn between it and the TRF configuration.

A simple TRF receiver employing regeneration might perform well enough in an area of high signal strength but when used under less favourable conditions cause disappointment due to the low reserve of gain and limited tuned circuits.

The superhet holds pride of place for reliability, stability, sensitivity and general performance and no TRF receiver can be made to equal it without becoming equally expensive. Beginners in particular are well advised to realise this for it is easy to become misled.

Criticism of the audio quality emitted by transistor receivers and which is often considered inadequate for home use, is, however, frequently justified and is the price that must be paid for
using small loudspeakers in small cabinets driven by Class \(B\) output stages from depreciating batteries.

But listening to a radio programme on a mains powered A.M. receiver-where good quality audio is available-is, in many areas, rather unsatisfactory, due to the characteristic whistle caused by neighbouring TV receivers and/or the sundry bangs and pops due to radiated interference.

It is an interesting project therefore to construct a transistor superhet tuner-which can be kept physically small-and feed its output to a good quality amplitier or, alternatively, to the "Gram" sockets of a suitable receiver. In this way much of the radiated interference is avoided for no external aerial is needed and at the same time an adequate reserve of audio gain becomes available.

Details of a suitable tuner are presented here of a model recently constructed. When fed to the input sockets of a 10 W mains powered audio amplifier similar to the " \(5-10\) " the unit gave an excellent performance equalling that of the 2 -valve superhet tuner it displaced. the quality obtained being considered superior to that of the model using


Fig. 1-Gircuit diagram of the transistor tuner-receiver.
valves-which also had to have an aerial connected.

The unit has also been tested in connection with the "Gram" sockets of a standard broadcast receiver and it was further proved that the unit could be used as a complete headphone, or personal, receiver if so desired.

\section*{The Circuit}

This is on conventional lines, reliability being the aim-see Fig. 1. No claims to originality are made; the circuitry is familiar and easily recognised. Practical problems arise, however, in converting a circuit diagratm to a working model and a good layout is not always easily obtained. Here the difficulty is resolved.

Both the medium and long wavebands are covered, the switching being arranged so as to minimise the chance of the unit being left switched on accidentally. A standard 3 -way, 4 -pole rotary switch is employed: SIA and SIB selecting the waveband coverage, and the other two sections performing on/off duties and ensuring that the battery is completely disconnected at position " 2 ". The central switch position is "oft"; it is thus impossible to change from one band to the other without going through the "off" position.

TR1 (OC44) functions as the frequency changer with TR2 and TR3 (OC45) as intermediate frequency amplifiers. Following the demodulator diode, DI, is an additional transistor, TR4 (OC71) which is used to drive the subsequent amplifier. The average emitter current of TR4 is \(400 \mu \mathrm{~A}\) and the whole tuner consumes less than 4 mA , thus making battery replacement only a minor problem.

If higher gain is required TR4 may be operated under common emitter conditions but the output impedance will be lowered to approximately \(5 \mathrm{k} \Omega\). The necessary rearrangement of the stage is shown in Fig. 2 and if the unit is to be used as a headphone receiver this is the best method. to adopt.

A minor economy can then also be effected by omitting the \(5.6 \mathrm{k} \Omega\) collector resistor together with the output capacitor connecting instead high impedance phones between the negative rail and TR4 collector. It might also become necessary to experiment slightly with the \(100 \mathrm{k} \Omega\) base feed resistor to obtain optimum results.

If the circuit of Fig. 2 is used to feed a valve amplifier it might also become necessary to vary the value of the upper base feed resistor, \(100 \mathrm{k} \Omega\), since the collector resistor is, as specified, a little
on the high side. Only a sma!l emitter current is required - about 0.5 mA .

Referring again to Fig. 1 it will be noted that all transistors are stabilised by the familiar potentiometer, emitter resistor form, and this together with the neutralising circuitry makes the unit completely stable.


Fig. 2-Alternative circuit for Tr4 in common-emitter mode.

\section*{Mechanical Details}

The whole tuner is constructed on a standard 18-way tag-board, the tags having been given imaginary numbers to assist correct identification. Although the appropriate figures can be marked on to the board it will usually be sufficient to locate No. 1 and No. 19 and count from there as required.

The oscillator coil and the three I.F. transformers are mounted so that their pins project through the tag side of the board and although a separate hole may be drilled for each pin it is generally simpler to use a single hole-just large enough for all the pins to pass through togetherfor each component. This also makes the cores available from either end of the can. An array of small holes lies along the centre of the tag-board when it is purchased and it is only necessary to enlarge as required.

\section*{Panel}

The wavechange switch, twin gang tuning capacitor and outlet insulator are mounted on a metal panel affixed to the tag-board in such a way that the tags come at the bottom as may be seen in the appropriate illustration. For dimensions of this panel see Fig. 4. Because it is made of metal the \(\frac{1}{s}\) in. fixing holes must be arranged to coincide with tags 3 and 11 on the board as shown and


Fig. 3-Drilling details for the component tag board.
prior to bolting it in position \(\frac{1}{16} \mathrm{in}\). thick paxolin washers must be placed over the bolts before they are passed through the board to prevent the underside of the "L" from short circuiting all the tag eyelets it hides.

A very simple bracket will also be needed to hold the ferrite aerial (which should be left to one side at this stage) and this will be bolted to tag 28 on the same side as the panel.

\section*{Constructional Notes}

Actual wiring construction should commence by fixing the canned transformers by letting their fixing lugs pass through small holes drilled for them. Care should be taken to check that the orientation agrees with that shown. These lugs are then pressed out flat and soldered as shown in Fig. 5.

Before proceeding further it is advisable to plug each core hole on the transformers with sleeving or something similar to prevent any blobs of solder accidentally spilling in and locking the cores which are rather fragile.

The remainder of the tag side of the board can then be wired as indicated in Fig. 5. The transistors should be left until last. Check that electrolytic capacitor C12 and diode D1 are connected in the correct sense as shown. The taut layout allows for all component lead-out wires to be snipped off short.

When wiring of the tag side of the board is complete (except for the transistors) the other side can be tackled and all wiring is illustrated in Fig. 6 where the panel is shown pressed out flat for


Fig, 4-Urilling details of wavechange switch panel.
clarity. C13 actually lies flush with the top of the board and must be slender enough not to foul the aerial (see illustration).

When the capacitors are in position-observe polarities-the transistor wires may be sleeved and passed through existing small holes on the board. Provided thin sleeving has been used the set of leads on each transistor will fit firmly yet not overtightly. The transistor shells thus remain on the top side of the board whilst their wires pass below and are soldered using the normal techniques.

The aerial may now be fixed in position as shown and wired allowing the connecting leads


Fig. 5-(a) Details of fixing transformer lugs. (b) Detoils of tog board wiring.


Fig. 6-Wiring diagram for top side of the tag board.
(which should be of stranded conductor) just loose enough to permit free movement of the two coils along the ferrite rod.

\section*{The Switch}

Each of the four central "pole" tags control three of the "way" tags disposed around the rim of the switch and visual check is initially required to identify them correctly. It is then advisable to press flat alternate "way" sections as shown to obviate incorrect connections being made. If the battery flex leads are left until all the wiring has been checked over chances of damaging the transistors will be minimised.

When satisfied that all is well a black flexible lead approximately 6 in . long is soldered to S1C rotor and a similar, but red, lead connected to S1D rotor. 'The switch should then be set to position " 2 ", the central position, and the appropriate stud connectors affixed to the free ends of the flexible leads which may then be twisted together neatly.

\section*{Setting Up}

A length of suitable cable (coaxial will do if not very long) should be connected to the stand-off insulator " 1 " (Fig. 6) the far ends being equipped suitably ," and connected to an amplifier or to the "Gram" sockets of a suitable broadcast receiver which may then be switched on and adjusted to normal three-quarter volume level setting. Alternatively high impedance phones may be used.

Control knobs are then fitted to the tuner spindles and a battery connected. The rotary switch should then be turned to position " 3 " (M.W.) and the vanes of the ganged tuning capacitor fully enmeshed.
The modulated output from a signal generator tuned to \(470 \mathrm{kc} / \mathrm{s}\) is now applied to the fixed vanes connection of VC1. The cores of T5, T4 and T3 should be adjusted for maximum output in that order, the generator output being kept at a low level.

Next the generator is set to \(600 \mathrm{kc} / \mathrm{s}\) and the oscillator coil core adjusted to receive the signal which is then further strengthened by sliding the medium-wave coil along the ferrite rod until best results are obtained.

If the ganged capacitor is now rotated towards the other end of its travel the note should reappear again at \(1.200 \mathrm{kc} / \mathrm{s}\). before the vanes are fully disengaged, to which frequency the generator may now be set before the aerial and oscillator trimmers TC1 and TC2 respectively, are carefully adjusted for best results.

Should the aerial trimmer need to be set fully home and the signal is still not considered correctly peaked then unscrew the oscillator trimmer slightly until the signal disappears. Now adjust \(\mathrm{VC1}\) to slightly fuller capacity when the signal will reappear; it should now be necessary to unscrew the aerial trimmer TC1 slightly to obtain a peaking point. The adjustments should then be made
all over again, viz at \(600 \mathrm{kc} / \mathrm{s}\) and \(1,200 \mathrm{kc} / \mathrm{s}\), until no improvement is possible.

\section*{The Long-wave Band}

The rotary switch is next turned to position " 1 " and an attempt made at receiving the Light programme on \(200 \mathrm{kc} / \mathrm{s}\) with the vanes of VCl approximately one-half enmeshed. It is quite possible that C 4 will need padding a little and is located in such a way as to be easily accessible for this purpose. Values as small as 30 pF connected in parallel make a good deal of difference. Experiment by temporarily connecting various small value capacitors ( \(50-150 \mathrm{pF}\) ) across VC 2 in

turn at the same time swinging the vanes over full travel.

Another quick method is to connect a 90 pF trimmer across VC2 temporarily. Immediately the signal is received the long-wave coil should be slid gently along the ferrite rod to obtain best results in association with VC1, and an assessment made of the precise value of capacitance needed for C 4 .

\section*{Warning}

The unit must not be used under any circumstances in connection with a receiver or amplifier of the A.C./D.C. class nor with a so called A.C. receiver that derives its H.T. from the mains direct. It may be used with a transistorised amplifier, however. if required.

Comparable results are not likely to be obtained if alternative components, or transistors of another make, are utilised; the use of any sub-standard items is almost certain to ensure disappointment.

\section*{Cabinet}

Dimensions of a suitable easily made cabinet constructed are shown in Fig. 7. It is made from hardboard held together with internally glued reinforcement strips, little weight being involved.


Fig. 7-Dimensions of suggested cabinet.
To avoid defacing the cabinet front the tuner can be locked by creating a sub-panel of hardboard through which four 4B.A. bolts may be passed and countersunk to coincide with holes in the metal tuner panel. This sub-panel can then be glued--with the bolts projecting-to the inside of the cabinet. When dry the tuner is placed in position and the four 4B.A. nuts applied and screwed home.

The actual cabinet front is cut \(\frac{1}{4}\) in. smaller than the dimensions given in Fig. 7, a frame of \(\frac{3}{8} \mathrm{in}\). quadrant beading being allowed to overlap by \(\frac{1}{x}\) in. all round to form a rebate for the sides, top, etc.

As mentioned earlier the unit can be used as a completely self-contained headphone receiver if required and in this case a phone outlet can be provided on the panel.

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\section*{By E. McLoughlin}

\section*{A MASTER CONTROL UNIT FOR AN AUDIO INSTALLATION}
(Continued from page 630 of the November issue)

YT must be stressed that voltages from the power supplics must be up to the full specified values. Slight deficiencies were found to produce immediate huge reductions in power in the prototype in both amplifiers, leading to inferior performance. If the H.T. is down by only 50 V below specified value there is almost \(40 \%\) power loss from the EL84. If the L.T. D.C. supply is down by only 1 V at the points shown in the circuits, below the specified values, the available output power can be halved!

But do not use voltages in excess of those specified. Excesses (or deficiencies) can be cured to some extent by changing tappings on the mains transformer primaries (but watch the valve heater voltage!) or by altering the values of reservoir or smoothing capacitators or by using suitable droppers. The power unit must be trimmed to the specified voltages, using appropriate measures with the particular power supply components obtained. Rule-of-thumb methods using any old lash-up are here particularly likely to lead to such poor results as to make the whole unit rather disappointingly weak.

\section*{Inputs}

The amplifier input is switched at will to "Laboratory" or "Line" by means of S4 (Fig. 2). In the position "Line" any signal on the line from apparatus at other stations can be fed into the amplifier and listened to in the laboratory/den on the internal loudspeaker in this unit provided that S3 is set to position "receive". In this position S3 breaks the mains feed to the L.T. power-pack on contacts A , breaks the base-drive on contacts B (so that the transistors are not damaged by receiving base-drive without emitter-collector voltage), breaks the connection of T5 to the line on contacts \(C\) (so that other signals are not fully or partially shorted, as explained above) and. finally, on contacts D . switches the incoming signals on the line through to R2 and R7 and hence to the amplifier input.

In the position "Laboratory" on S4 the amplifier input is connected to both of two sources within the laboratory simultaneously via the
decoupling and impedance-transforming resistance network R3, 4, 5, 6 . This network assures that both sources transfer virtually all of their signal voltage into the amplifier, but negligible amounts mutually to each other. Which of the sources actually feeds the amplifier then must be decided simply by switching the desired source on and the others off at their own switches. If both are on they will mix in the amplifier without otherwise interfering with each other.

Now, with S4 in the position "Laboratory", S3 may be ,"at either position. The "position "Receive" is then used as a "dummy" if the signal is merely to be listened to on the internal loudspeaker, confining it to the laboratory (e.g., when using the oscilloscope/signal tracer source for internal work in the laboratory-see belowand possibly somebody else in the flat or house has other apparatus feeding other signals on to the rest of the line). Such other signals on the line will. of course, not then be actually received until S4 is also switched to "Line".

If the signals from a laboratory source ( S 4 at position "Laboratory") are now required to be sent on to the whole line-with suppression of any other signals possibly present-then S3 is switched over to "Send". This switches mains on for the L.T. power-pack and connects the transistor amplifier input and output appropriately, also shorting R2 to prevent any possibility of instability.

The combination S3 at "Send" and S4 at "Line" serves no useful purpose, neither does any damage nor causes instability.

The internal loudspeaker can be switched on or off independently. If S 3 is at "Send" and all loudspeakers in the system are of the same type the volume on the internal loudspeaker is a true replica of the volume on any other loudspeaker on the line when the series-resistors used as individual local volume controls on the line loudspeakers are cut out of circuit (maximum volume).

\section*{Mains/Distribution/Power Supplies}

The unit described in this article contains all its own power supplies, which are built in tier fashion on to one side panel of the cabinet body, details of which will be given later.

Fig. 1 (last month) gives details of the mains distribution wiring. This follows the principles and general scheme sketched in the initial general article. Great care is essential in carrying out this wiring, which should be checked, checked, and rechecked before switching on mains power. Wrong connections or insecure, untidy connections could lead to highly dangerous conditions or to destruction of valuable equipment.

Note carefully the arrangements for the mains isolation transformer. This item is generally too heavy and bulky and has too great a stray magnetic field for inclusion within the cabinet of the present unit. It is thus attached via a four-core mains power cable of suitable length and quality and mounted separately at a suitable safe position in a proper and secure manner. The reasons for requiring this transformer were fully discussed in the introductory article. Take great care not to confuse the connections; errors could lead to dangerous conditions.

\section*{Cabinet Construction}

This unit is to be considered as a fixed item of electrical installation. As such it will most easily satisfy supply company regulations regarding mains wiring.

If the laboratory/workshop wall is of good dry wood at the location where the unit is to be installed, as was the case for the prototype, then the wall itself may be used directly as the rear of the cabinet, of which sides are formed by wooden slats screwed on internally with angle-iron. The distribution tags and cables can then be screwed directly on to the rear wall, according to the drawings, using appropriate regulation fixtures available in the electrical trade. It is advisable to consult an electrician at the start of the whole
for theit valves EF86 and EL84. Ample publication has occurred elsewhere, so that only brief comment on essentials is necessary here.

It is essential to mount the two valveholders such that R13 can be mounted as direct and short between the relevant pins as possible (Fig. 3). Furthermore, R10 must have its wire cut off very short and soldered direct on to pin 6 at the valveholder of V1. Failure to observe these conditions will cause treble-performance loss.

High gain is obtained in V1 by means of the unusually large anode load R10. D.C. coupling via the anti-parasitic R13 to V2 grid avoids one source of low-frequency phase-shift and losses. The positive D.C. thereby fed to V2 grid requires the unusually high cathode bias resistor R16 to


Fig. 2-The circuit of the "lid-unit".
project if one is not conversant with wiring regulations oneself.
The amplifier unit itself is seen, in the drawings and illustrations, to be built in more or less conventional form of construction on to a panel of wood forming the "lid" of the vertical cabinet. A good 12 -pin connector, rated at \(500 \mathrm{~V} / 2 \mathrm{~A}\) on all pins relative to all other pins, is used to connect the "lid-unit" to the body. This enables rapid removal and replacement for servicing, especially if the take-off hinge and latch type of fixture is adopted.

\section*{The Amplifier}

This is an excellent "hi-fi" circuit of low expense but fine performance specifically developed by Mullard engineers some time ago
compensate. The value of R16 is critical and a close-tolerance resistor is specified. The cathode voltage resulting for V2 is then sufficient for the screen of V1. which is thus D.C.-coupled to V1 cathode. This also represents D.C.-negativefeedback, which stabilises the operating points of the valves-otherwise such a circuit would drift. C11 is also critical. Too low a capacity causes bass loss, whereas too high a capacity causes pure lowfrequency phase-shift oscillation at some or all settings of YR4, especially if inadvertently too high a ratio is used for T6. This oscillation may be of such a pure note and frequency that it can be mistaken for severe mains hum.

If the amplifier howls uncontrollably at full power, whatever settings of the controls are undertaken, reverse connections to the output transformer primary, T6, m and 1.


Fig. 3-The "lid-unit" and sub-chassis wiring diagram.

Use low-capacity coaxial cable for the leads shown screened in the wiring diagram, Fig. 3. 10 avoid treble loss. Note that all screens are bonded together and joined to chassis at only one point. This is highly important as hum is casily introduced if screens are earthed at several points because they can then carry random chassiscurrents, which may be partially A.C. Use suitable
sleeving or other measures to prevent the screening from touching the chassis at unwanted points. Note in this connection also the separate earthbusbar for VR2, 3, 4. connected locally to chassis at the earth-feed from the 12 -pin plug and not connected to the earth-ring-busbar under the amplifier components.
(To be continued)

\section*{DX on MEDIUM WAVES}

\begin{abstract}
As a change from shortwaves try for some M.W. broadcast band \(D \times\) this season. This article tells you how.
\end{abstract}

\author{
By S. A. Money
}

\(m\)ANY radio enthusiasts will probably be surprised to learn that DX signals from many parts of the world can be heard on the medium wave broadcast band. In the early 1930's many transAtlantic stations were heard on quite simple domestic radio sets. With modern receivers it is possible to achieve quite remarkable results despite the great rise in the level of interference since those early days.
During the past two years the writer and a number of other enthusiasts have listened for DX stations on this band. Many stations from both North and South America were regularly heard and others from the more remote parts of Africa and Asia were also logged.
Optimum conditions for long distance reception on the medium waves occur in the winter during the hours of darkness. In the evening reception of DX signals is extremely difficult due to the high level of interference from the very strong European signals. After midnight most of the European stations have closed down and reception of the weaker DX stations is possible. During the summer a high level of "static" noise makes DX reception more difficult and less frequent.

Sunspot activity is well known to have a considerable influence on short wave reception conditions. In the case of medium waves it has been found that the best conditions for DX reception occur during the years around the sunspot minimum. With the next sunspot minimum due to occur around 1963/64 conditions should be excellent for the next few years.

\section*{Receivers and Aerials}

Under favourable conditions it should be possible to receive the regularly heard North American stations on any good domestic receiver provided that a good aerial system is used.

For serious DX listening a communications type receiver with its high sensitivity and selectvity is almost essential. Ex-Service receivers such as the R1155 have proved to be very good in this respect.

Long wire aerials seem to be the best for DX reception. They should be mounted as high as possible and should be outdoors for the best results. Indoor aerials mounted in the loft or around the picture rail in an upstairs room can give very good results. In order to erect the necessary length of wire it may be necessary to bend it into the form of a square or rectangle. A wire 60 to 90 ft long is suitable.
Ferrite rod aerials are not usually sensitive enough for DX reception. A good earth connection is usually needed with domestic radios and will often improve reception on a communications receiver.

\section*{North America}

Reception from North America usually occurs for a period of from three to five days at a time every two or three weeks, in mid-winter however, the opening may last for as long as two weeks with the exception of one or two poor nights. On many nights there may be heavy "static" interference from thunderstorms over the Atlantic.

Generally reception is possible from just after midnight until about \(5 \mathrm{a} . \mathrm{m}\). when interference from local European stations starts to build up, although some trans-Atlantic stations can be heard as late as 7 a.m.

Programmes from North America are for local entertainment and are in English with the exception of a few French-speaking Canadian stations. Identification of stations is fairly easy since they all give their call-signs regularly, often during the breaks for "commercials".

\section*{East Coast, U.S.A.}

Those stations located in the eastern coastal region of the U.S.A. are the most frequently heard here in Britain. There are no less than 16 radio stations in New York City and of these 14 were known to have been logged in England last winter.

Four of the stations in New York carry the major network programmes. The A.B.C. network broadcasts over station WABC on a frequency of \(770 \mathrm{kc} / \mathrm{s}\). Further along the band on \(880 \mathrm{kc} / \mathrm{s}\) is WCBS, owned by the Columbia Broadcasting System. Both of these stations are regularly heard at excellent strength. Station WNBC ( \(660 \mathrm{kc} / \mathrm{s}\) ), operated by the N.B.C. network, is not too well received here since its aerial is directed away from Europe. The fourth regularly heard station is WOR on \(710 \mathrm{kc} / \mathrm{s}\) run by R.K.O. and carrying the Mutual Network programme.

Of the independent stations in New York, WHN ( \(1050 \mathrm{kc} / \mathrm{s}\) ), WINS ( \(1010 \mathrm{kc} / \mathrm{s}\) ) and WNEW ( \(1130 \mathrm{kc} / \mathrm{s}\) ) can be heard with very good signals on almost every opening to the U.S.A. These three stations broadcast popular music and newscasts. The New York equivalent to our Third Programme is provided by \(W Q X R\) on \(1560 \mathrm{kc} / \mathrm{s}\).

Two stations frequently heard from New York State are WPTR ( \(1540 \mathrm{kc} / \mathrm{s}\) ) at Albany and WKBW ( \(1520 \mathrm{kc} / \mathrm{s}\) ) at Buffalo. Other stations which give good signals from the New England states are WTIC ( \(1080 \mathrm{kc} / \mathrm{s}\) ) Hartford, Conn., WEGP ( \(1390 \mathrm{kc} / \mathrm{s}\) ) Presque Is., Maine, WTOP ( \(1500 \mathrm{ks} / \mathrm{s}\) ) Washington D.C. and WMEX ( \(1510 \mathrm{kc} / \mathrm{s}\) ) at Boston, Mass.

Hill-billy music and songs heard on \(1530 \mathrm{kc} / \mathrm{s}\) will probably be from station WCKY at Cincinnati, Ohio. Pennsylvania state can usually be heard over stations WCAU ( \(1210 \mathrm{kc} / \mathrm{s}\) ) at Philadelphia and KDKA ( \(1020 \mathrm{kc} / \mathrm{s}\) ) at Pittsburgh.

Those stations in the southern states which are near the coast, such as WAVY ( \(1250 \mathrm{kc} / \mathrm{s}\) ) at Portsmouth, Virginia, WBT ( \(1110 \mathrm{kc} / \mathrm{s}\) ) Charlotte, N. Carolina, WCSC ( \(1390 \mathrm{kc} / \mathrm{s}\) ) at Charlston, \(S\). Carolina and WLCY ( \(1380 \mathrm{kc} / \mathrm{s}\) ) at St. Petersburg, Florida, are frequently heard at good strength.

The state of Georgia can sometimes be heard over station WSB in Atlanta which operates on \(750 \mathrm{kc} / \mathrm{s}\). Some of the other stations which have been logged from time to time are, WHAS at Louisville, Kentucky, on \(840 \mathrm{kc} / \mathrm{s}\), WSM ( \(650 \mathrm{kc} / \mathrm{s}\) ) at Nashville. Tennessee, and WALA ( \(1410 \mathrm{kc} / \mathrm{s}\) ) at Mobile, Alabama. Most of these stations can be difficult to receive but, with improving band conditions, they should be more frequently logged this coming winter.

\section*{Central U.S.A.}

What might be considered to be the cream of the DX signals from the United States are those stations located in the central and mid-western states. The nearest and thus most frequently noted stations are WOWO ( \(1190 \mathrm{kc} / \mathrm{s}\) ) Fort Wayne, Ind., WJR ( \(760 \mathrm{kc} / \mathrm{s}\) ) Detroit, Michigan and WCFL ( \(1000 \mathrm{kc} / \mathrm{s}\) ) Chicago, Illinois.

Station KXEL at Waterloo, Iowa can sometimes be heard through WPTR's signal on \(1540 \mathrm{kc} / \mathrm{s}\) and usually peaks up at around 0300 GMT. Another station which is often noted at about this time is KMOX at St. Louis, Missouri operating on \(1120 \mathrm{kc} / \mathrm{s}\).

Texan stations which have been frequently logged here in Britain are WFAA at Dallas and WOAI at San Antonio using frequencies of \(820 \mathrm{kc} / \mathrm{s}\) and \(1200 \mathrm{kc} / \mathrm{s}\) respectively. Perhaps the most distant U.S. stations noted recently are WCCO ( \(830 \mathrm{kc} / \mathrm{s}\) ) at Minneapolis, Minnesota and KOMA ( \(1520 \mathrm{kc} / \mathrm{s}\) ) at Oklahoma City, Oklahoma.
Reception of these more distant stations does require quite a bit of patience since they are usually weak signals and are often only audible for five to ten minutes at a time.

\section*{Canada}

The Canadian Broadcasting Corporation, which runs the main network, is a public body similar to the BBC. Station CBA at Sackville, New Brunswick ( \(1070 \mathrm{kc} / \mathrm{s}\) ) is the most consistent of the CBC stations heard in this country. CBA can usually be heard at excellent strength just before midnight whenever the band is open to North America and is useful as an indicator of band conditions.

Other CBC stations which are often heard in England are CBC Montreal ( \(940 \mathrm{kc} / \mathrm{s}\) ), CBI Sydney. N.S. ( \(1140 \mathrm{kc} / \mathrm{s}\) ) and CBE Windsor, Ontario, on \(1550 \mathrm{kc} / \mathrm{s}\).

Of the independent stations CJON ( \(930 \mathrm{kc} / \mathrm{s}\) ) at St. John's, Newfoundland is usually an excellent signal from midnight and like CBA can be used to indicate the state of the band. Other Canadian stations which usually give good reception are CHNS ( \(960 \mathrm{kc} / \mathrm{s}\) ) Halifax, N.S., CFNB ( \(550 \mathrm{kc} / \mathrm{s}\) ) Fredericton, N.B. and CFCY ( \(630 \mathrm{kc} / \mathrm{s}\) ) Charlottetown, Prince Edward Island.

Generally Canadian signals are not as frequently heard as those from the U.S.A. but reception will normally occur on the same nights as for the U.S.A.

\section*{South America}

Most of the South American stations broadcast in either Spanish or Portuguese and can usually be heard on any night when the North American stations are not audible. Brazilian stations are the most frequently heard with programmes in the Portuguese language. Radio Globo on \(1180 \mathrm{kc} / \mathrm{s}\), R. Tupi on \(1280 \mathrm{kc} / \mathrm{s}\) and \(R\). Jornal on \(780 \mathrm{kc} / \mathrm{s}\) are three stations which are usually excellent signals.
Other countries which are frequently logged are Argentina (Radio Nacional, \(870 \mathrm{kc} / \mathrm{s}\) ), Venczuela ( \(R\). Ondas del Lago on \(1120 \mathrm{kc} / \mathrm{s}\) ) and Uruguay with stations CX6 ( \(650 \mathrm{kc} / \mathrm{s}\) ) and CX14 ( \(810 \mathrm{kc} / \mathrm{s}\) ).

Progranımes in English can be heard from Radio Demarara (ZFY 760kc/s) in Georgetown British Guiana, which usually gives fair to good reception in the early morning.

Central American stations have been heard from Mexico, Cuba, Jamaica and Trinidad. Generally reception from this area is limited to a short period when the conditions change from the North American area to South America.

For details of these and other South American stations the reader is referred to the World Radio Handbook which lists the frequencies, operating times and addresses of nearly every broadcast station in the world.

\section*{Asia and Africa}

North African stations can usually be heard during the evenings in the winter months and are often stronger signals than the more local European stations.
South Africa has been heard in the early mornings on frequencies of \(1268 \mathrm{kc} / \mathrm{s}\) and \(1286 \mathrm{kc} / \mathrm{s}\). Other countries logged from Africa have been Kenya, Somalia, Nigeria and Senegal.
Middle East countries such as Syria, Iraq and Iran are best heard during the period of the feast of Ramadan when they operate all night with programmes in Arabic.
Indian, Pakistani and Chinese stations have been heard just after midnight with programmes in their native languages.
The Voice of America stations at Okinawa and in the Philippines Islands have been heard in the afternoon on \(1140 \mathrm{kc} / \mathrm{s}\) and \(1180 \mathrm{kc} / \mathrm{s}\). Reports have been received of the reception in Scotland of stations from the Pacific islands such as Guam and Fiji but so far nothing has been heard from that area by listeners in England.

The BBC have however, received reports of reception of their Home Service stations in New Zealand so it would seem that reception of Pacific stations in England should be possible if conditions improve as expected.


\section*{Electronic Organ Keying}

SINCE there are now very many different makes of American electronic organs available in this country, a study of some of the techniques involved is very interesting, and although no all-transistor instruments appear to have arrived there are many interesting features to be seen which have hitherto not been used in any English designs.

One of the sections which has always interested me is that concerned with the keying of the instrument, not only from the electrical, but from the actual mechanical point of view. As most of my readers know, the depression of a key actuates some form of electrical contact; in its simplest form two metallic points being brought into contact, or opened, and in its most complicated form, 10 or more contacts being operated, all being opened or closed, or various combinations of them being operated.

Many organs suffer from defects in this part of the instrument, the contacts being very prone to oxidisation or the action of dust or fluff, and it is interesting to note the various methods of overcoming these defects.

The use of mixed metals for the contacts, or the introduction of some form of wiping or slight scraping action are well known, but the most interesting is, I think, that employed by the Baldwin Company, where a printed circuit resistance element is so arranged that when a key is operated a spring strip is lowered and travels across the resistance element, thereby gradually cutting it out of circuit.

In addition to getting rid of the difficulties of dirt, corrosion, etc., this also gives a gradual attack effect, and results in the note being sounded in a similar manner to a standard pipe instrument, but I still feel that there are better ways of doing the job.

\section*{Any Ideas?}

Again, I wonder if any of my readers have spent any time on this aspect and have any ideas of their own they would like to air. Incidentally, the use of the scheme mentioned above does not restrict the instrument to sounding a single note, as the resistance elements can be stacked and practically any number can be operated by a single key.

Of course, the difficulties of suggesting or designing a keying system are restricted, as keys may be of two types, balanced or rear-hung, and thus the contact mechanism must be in the front of the instrument or at the rear, and may present difficulties in accommodating the mechanism.

\section*{A Salvage Tip}

I know that many of my readers are interested in hints and tips such as are accumulated by the keen serviceman, and I am always anxious to pass on anything which is really worth while. I was recently shown a tip which, although originally used to salvage a valve, is also applicable to transistors. Here it is.

In the case of the valve it relates to the older type with a top cap, which often becomes loose and eventually pulls away leaving the merest piece of wire projecting from the glass. In the case of the transistor, a wire may break and leave a similar short stub of wire projecting. In both cases, the application of a soldering iron being impracticable.

The hint is to obtain a two or three inch length of suitable replacement wire, and to tin one end and then carefully to add solder to this end, holding it end downwards so that a fairly large "blob" of solder is formed.

Now hold the piece of wire at its opposite end in a pair of pliers and lower the "blob" end until it nearly touches the protruding end of the wire you are repairing. Place the soldering iron on the wire being held, at a point midway between the pliers and the solder and as soon as the solder is seen to begin to run, lower it so that it touches the protruding end, and then quickly remove the soldering iron.

Provided that you can keep everything steady the two ends will unite, and the soldering iron will carry off the extra heat so that no damage will arise. You need a very steady hand, however, and will soon see how much solder to leave at the "blob".

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\section*{THE} known as the MINISCOPEsee footnote)

(Continued from page 599 of the November issue)

AMILLER-TRANSITRON oscillator is a special form of multivibrator, in which, loosely speaking. the grid and anode function as one triode and the screen and suppressor , as the other triode. The fact that both "triodes" are in one electron-path gives the new characteristics.

The action of one cycle is as follows, starting at the end of a timebase-run. This is reached when the grid voltage has risen to that value for which anode current ceases to show further rise, a condition known as pentode bottoming. (This has nothing to do with anode current saturation.)

All increase of total cathode current then resulting from further rise of the grid voltage (on the charging-curve of the capacitor selected on S5b, via VR9. etc.) is therefore suddenly diverted to the screen-grid at this point, which therefore suffers a sudden rise in current, i.e. fall in voltage. This sudden fall in voltage, at the end of the linear anode run-down, shown in the second lines of waveforms in Figs. 6 and 7 (last month), and shaped in V7 to blank out the flyback as already mentioned. is coupled to the suppressor grid via the capacitor selected on \(\$ 5 \mathrm{a}\), and thus reduces anode current.

But this reduction of anode current causes a rise of anode voltage. which is fed as a further sharp rise to the grid, via the capacitors on S 5 b , causing
far that less volage suppressor grid-base, a tiny bit of anode current can flow. This causes a few volts drop at the anode, immediately, which are of the order of the normal grid-base of the valve and are fed to the grid via the capacitor selected on \(S 5\) b.

The result is that all cathode-current is immediately almost cut off, giving a sharp rise of screen voltage, fed as a similar sharp rise to the supressor, so that the valve is now fully "open" again for any further anode current that wants to flow.

But the anode current at first remains at the very low value giving a drop across VR10 no larger than the grid-base, because any further increase would cause a drop across VR10, fed to the grid via the capacitors on \(\$ 5 \mathrm{~b}\), large enough to cut the valve off, i.e. such increase could not take place. At any rate, it can only take place slowly at a rate such that the charge on the capacitors on \(\mathbf{S} 5 \mathrm{~b}\),

\section*{THE "MINISCOPE"}

The General Electric Company Led. have drawn our attention to the fact that the name "Miniscope" is a registered G.E.C. erade mark. In view of this we have changed the name of our inserument to "The Auditron". We apologise to G.E.C. for the unwitting infringement of their trade mark.
charging through VR9, R35, etc. can follow, thereby avoiding the checking-feedback at the grid.
This gives the relatively slow and very linear rise of anode current, and consequent fall of anode voltage, used for the timebase-sweep of the spot on the CRT. This terminates when the anode current has increased with slowly rising grid voltages up to the point where further rise of grid voltage has no further effect on anode current (bottoming), and we are back where we started.
Current is suddenly diverted to the screen, resulting in total cut-off of anode-current at the suppressor, the flyback takes place, is " caught " by D5, waits until anode current cuts on again at the suppressor, the value is almost cut off at the grid suddenly, a new linear timebase-run takes place, and another cycle is then complete, and so on repeatedly.

\section*{Speed-Influencing Elements}

It is clear that each cycle consists primarily of two portions, as in any multivibrator, associated with independent CR-time constants, which may be influenced independently.
Thus we have here firstly the linear timebase run, determined by the time constant given by VR9 and R35 together with the selected capacitor on S 5 b , and secondly the anode-current cut-off time. determined by the time constant set by R \(40 /\) R41/S6 together with the capacitor selected on S5a.
Each time-constant can, in principle, be controlled fully independently from the other, but a purposeful ganging is in practice desirable, and has been adopted.

\section*{Ganging of Time Controls}

S5 constitutes the ganged coarse speed-control for the timebase. This is a three-position switch selecting capacitors of equal values for both timeconstants simultaneously, in steps of \(10: 1\) in capacity, and thus \(10: 1\) in speed-ratio. VR9 is the time-base-run fine-speed control.

It has no effect on the anode current cut-off period including the flyback, but as a continuously -variable range of \(20: 1\) for the timebase-run speed, because R35 has one twentieth the resistance of the full track of VR9. This gives sufficient overlap of all ranges for all purposes.

It is not the flyback-time, which determines the time from the end of one timebase-run until the circuit commences the next run, but rather the time for which the capacitors on 55 a and R40 (and R41, if in circuit) hold the anode blocked at the suppressor. If the latter is shorter than the true flyback, the new run starts before DS operates, resulting in decreased amplitude of the sawtooth and higher overall frequency. If the suppressor cut-off time is much longer than the true flyback, the anode simply waits resting at C 18 -potential until the suppressor is ready again (Figs. 6 and 7 respectively).

These two conditions can be selected by means of S6. In the position "short", for S6, only R40 is in circuit for the "recover" time constant. so chosen as to match the flyback proper, i.e. when the flyback has reached the C18/D5 catching-level, the suppressor is then just ready for the next run
too.


Fig. 8-The layout of the front ponel.


Fig. 9-The main chassis drilling.

In fact, the given value of \(47 \mathrm{k} \Omega\) for R 40 is such that the suppressor is ready a little sooner than the flyback would be caught by D5, i.e. D5 never operates in the "short" setting of S 6 , and the timebase consequently runs at slightly reduced amplitude, with the advantage of the higher overall frequency.

However, constructors can trim R40 as they wish, using a \(100 \mathrm{k} \Omega\) preset potentiometer here, and adjusting it to the point where further reduction of resistance causes the length of the horizontal trace on the CRT just to begin to decrease. This is then the true matched condition, where D5 just starts to operate, i.e. flyback is just complete, when the suppressor gives the anode free for the next run. without any waiting time. Fig. 7 shows this condition. A new run starts immediately the flyback from the previous one is over, without any delay.

Switching S6 to "long" increases the "recovery" time-constant by a factor of about ten, so that now flyback is over long before the suppressor is ready for the next run, giving considerable waiting times seen in Fig. 6. The advantage of this form of operation is apparent when desiring to display very asymmetric signal waveforms, where the portion of interest is only a fraction of a cycle.

It is seen that, in the "long" setting. increasingly towards the faster end of the range of \(V R 9\),
the aotual timebase run (which is all that is displayed, across the whole CRT screen) is only a fraction of each cycle of the timebase oscillation, yet it is the latter which is locked to the signal frequency by means of the synchronisation.

Consequently a stationary display of a magnified version of the interesting portion of the asymmetric signal is possible, selected by suitable setting of polarity on the synchronisation switch on the signal amplifier. This arrangement gives similar effects to "triggering", though of course not successful in all cases of asymmetric signals, whereas true triggering is always successful.

\section*{Triggering}

An oscilloscope may be operated, basically, in two modes: "sync" in which the timebase is allowed to oscillate, the sync signal merely forcing the frequency into step with the signal frequency, and "trigger" in which the timebase is never allowed to oscillate, but is "kicked" into singleresponses.

Trigger operation frees one of the need to have the timebase run slowly enough to have at least one cycle of the signal frequency included in the timebase frequency "period, which is the basic condition for "sync".

However, triggering is of far less importance for audio work than for TV or pulse work, and so sync facilities only have been provided in the

Auditron. The sync facilities incorporated, together with the "long/short" function, will satisfy all normal needs of the radio and audio experimenter.

\section*{Synchronisation}

The Miller-Transitron timebase is synchronised by setting VR9 such that the overall frequency is somewhat lower than the signal frequency, when left to run uncontrolled. The positive pulses, in step with the signal frequency, amplified and shaped by V4 and V5, then jerk the suppressor to cut-on just that little sooner to bring the two frequencics into step.
The gain of V 4 and the arrangements for extracting a sync signal from the signal amplifier are such that good strong sync is possible for all signals having at least \(10 \%\) of the screen-size vertical amplitude, at all frequencies of operation for which the instrument is intended.

VR8 serves as gain-control for the sync signal, to control the strength of the effect with stronger signals, or to remove all sync if desired. VR8 carries a D.P. switch. S4, which switches over to \(50 \mathrm{c} / \mathrm{s}\) mains sync (for frequency-comparisons against the mains) if turned beyond the point of "no sync". The mains-sync signal is obtained from the heater-line via R23 and R24.

\section*{Calibrations for the Timebase}

A special feature of the Auditron is that the conventional calibration of the timebase controls in terms of basic frequency has been abandoned in favour of a "time per centimeter" of CRT-screen display calibration, which is vastly more useful. A frequency-calibration is relatively useless, as the flyback and wait times are indefinite fractions of a timebase cycle, and thus even if exact number of cycles of the signal appear stationary in the display. the interpretation in terms of signal-frequency is very often rather ambiguous, because it is not clear how much is located on the invisible flyback.

The "time-per-centimeter", in conjunction with a centimeter-grid of lines on the perspex window in front of the CRT. represents a form of calibration removing every ambiguity. S6 has no effect whatsoever on the speed of the timehase run, which is controlled solely by VR9 and S 5 b . Fully unambigunus calibration of VR9 from 12 to 250 micro-seconds per centimeter was thus possible in the prototype, with the three positions of S5 labelled approximately X1, X10, X100. Thus all times from 12 microseconds to 25 milliseconds per centimeter are covered. This enables time measurements to be read off direct. and frequency measurements to be made as follows.

The signal waveform is syncronised stationary, and the length of one cycle read off against the centimeter lines on the perspex window in front of the CRT, which is then multiplied by the time-
per-centimeter readings on the timebase-controls. The result is the time for one cycle of the signal waveform, whose reciprocal gives the frequency.
lt might be asked why here a once-and-for-all direct calibration of the timebase controls has been adopted, whereas for the signal voltage calibration an independent Zener-standard calibrator was used instead of direct calibration of the Y -gain control. The reason is that in the timebase our time-deternining elements are largely the capacitors C 22 to C 27 , and valve-ageing or voltage fluctuations can act only on the single stage V6, resulting in no drifts greater than tolerable for normal workshop standards of accuracy.

\section*{The Flyback-Blanking Circuit}

In order to black-out the flyback of the spot on the CRT-screen we need to cut-off the CRT at its grid during all times except the linear timebaserun used for the display. This requires an


Fig. 10-The cabinet details.
accurately-timed squarewave, whose negative portion coincides with the "flyback and wait" portion of the timebase cycle. and whose positive portion coincides with the linear timebase run.

In order to perform the blanking function properly, this must be as good a squarewave as possible. Furthermore, the D.C. level of this squarewave must be such that the positive part of the wave is coincident with the voltage set on the manual brilliance control, and the negative part goes negative to this level by an amount equal to the amplitude of the wave, the latter needing to be sufficient to cut the CRT off, even for the brightest setting of the manual brilliance control. In other words, the amplitude of the squarewave must be just a little more than the grid-base of the CRT, and 30 V was thus found to be satisfactory.

The circuitry round V7, with associated diodes

D6, D7, D4, was devised to meet all these requirements to within sufficient limits of accuracy for all normal amateur purposes.

\section*{Shaping of the V6-screen Waveform}

Figs. 6 and 7 show that the screen-grid waveform of V6 is already of the required form, very roughly, for the flyback-blanking function. Thus the screen goes negative during the flyback and wait time, because anode-current is then cut-off and heavy current diverted to the screen. During the timebase run, the screen is much more positive, because anode-current is flowing, and thus screen current is low or normal.

Yet the original screen waveform is anything but a good squarewave. At the fastest settings of VR9 the positive-going transition takes about the same time as the timebase run. so that at least half the trace on the CRT would still he dark, and the other half would increase progressivly in brightness. were this waveform used directly to bias the CRT grid.

At the slowest settings of VR9 the screen wave rises fairly soon to a maximum positive, and then gradually falls as the anode and screen draw increasing current during progression of the tine-base-run. This wave, if applied to the CRT grid, would have the undesirable result of giving a trace which starts dark, rises fairly soon to maximum intensity, and then gradually tails off in intensity towards the end.

However, looking at this screengrid waveform of \(V 6\), it is apparent that both positive and negative transitions commence with steep portions having at least the desired final amplitude of 30 V , and pretty accurately coincident, in time, with the start and end of the timebase run. It is thus the purpose of V7, D6, D7, D4 to cut out this portion of the wave, and reject all else.

The D.C.-level of the screen waveform shifts with the setting of VR9, on account of the symmetry - changes thereby involved. It is therefore necessary to clamp the wave to a definite potential prior to introduction of clippers at the desired relative D.C. levels. The combination of C21, D6, R42 performs this function, clamping the wave to -18 V (derived from the Y -amplifier bias circuit) as its most negative limit under all circumstances. R31 merely serves the purpose of reducing loading thereby imposed at the screen-grid of V6. which would otherwise react back to distort the timebase action. The function of such a clamp-circuit is identical to a peak-rectifier circuit.
The output waveform at V7 cathode is now clamped at chassis potential and is positive-going from there. All that is needed is to retain the first 30 V . and chop off the rest, which is performed by the simple diode-limiter circuit D7. which is returned to the desired potential of plus 30 V on R36. C19. D7 and C19 thus short-out all portions of the waveform lying above plus 30 V .

We are now left with the desired waveform for flyback blanking. It is merely necessary, as a final step, to give this the desired D.C. level, i.e., to change over from positive-going-to-chassis to negative-going-to-brilliance-control-setting.
This is performed by another clamp-circuit, whose principles of operation are identical to those of the first. A coupling-capacitor C29 first of all removes all D.C., D4 is a negative peak rectifier, and the series-added D.C. is whatever voltage is present at the slider of VR1, the brilliance-control. R37 and C30 were introduced as an equaliser, to make the action of this clamp circuit slightly fre-quency-selective, speeding it up at the higher frequencies of operation to compensate for slight delays in rise of the original wave there.

The specified value of C30 should be found satisfactory, but if the trace on the CRT is found not to have a clean sharp start at the highest possible timebase-speed setting, slighly larger values should be tried.

\section*{Diodes}

Although silicon diodes are less critical than germanium diodes, heat shunts should nevertheless be used when soldering these diodes. If diodes are unwittingly damaged during soldering,


The Miniscope as it appears in on advanced stage of construction.
this circuit can give a variety of forms of erratic performance. Take care, also, to wire all diodes with the correct specified polarity. It is NOT permissible to use normal germanium diodes of the RF or low-voltage types anywhere in the Auditron, as the voltage ratings of such are far too low, and they would suffer immediate destruction. The peak inverse voltages appearing on the diodes in the Auditron amount to some one or two hundred volts in some cases. and thus the single type number specified throughout is a silicon diode of 350 V peak inverse voltage rating.
(To be continued)


\section*{n} OWADAYS most people have an F.M. tuner to give them high quality interference-free reception from their local BBC stations but there are numerous occasions when the programmes transmitted are not of the more popular light music type and an alternative is required.

Without doubt the most popular station for light entertainment particularly among the younger generation is Radio Luxembourg on 208 m .

In order to receive this station it would normally be necessary to have a complete medium wave tuner but this novel design shows how a high gain and selective tuner pre-set to the Luxembourg frequency can quite easily be constructed.

\section*{The Design}

The original idea for the circuit came from experiments carried out with a \(1.6 \mathrm{Mc} / \mathrm{s}\) I.F. amplifier strip when it was found that by adding a small fixed capacitor to each winding of the I.F. transformers it was quite simple to bring the tuning point down from \(1.6 \mathrm{Mc} / \mathrm{s}\) to \(1.439 \mathrm{Mc} / \mathrm{s}\) which is the exact frequency for Radio Luxembourg.

As miniature \(1.6 \mathrm{Mc} / \mathrm{s}\) I.F. transformers are available from all the component shops they provide a ready made perfectly screened band-pass coil unit adjusted for optimum coupling which can be easily tuned to 208 m .

The circuit which is shown in Fig. 1 on the Blueprint is quite simple but has proved to be very sensitive and yet perfectly stable over long periods. It consists of two straightforward R.F. amplifiers followed by a germanium diode which provides detection and negative bias for non-delayed AVC. In practice the use of a miniature group-board to mount all the small components makes it both very easy to construct and at the same time gives the tuner a neat professional appearance
It will be noticed that no audio amplifying stage has been included as it was found that feceding
trom the detector into a standard Mullard 3W amplifier sufficient signal was always available to overload the input and in fact a preset output control was included, which is normally set at about the halfway position. Good reception has been obtained with this tuner in various locations in and around London and also in parts of South East England using only 4 ft of wire as an aerial, however in view of the characteristic fading that does occur from time to time on Luxembourg it is considered that the best aerial possible should always be used.

When the first prototype was completed a considerable amount of experiment was carried out with various different input circuits from the aerial including winding small coupling coils on to the first I.F. transformer to give a step-up ratio but the difference in results was so slight that it was not considered worth the additional time and trouble.

As a precaution against the possibility of some instability due to the high gain with two R.F. stages small screens were fitted across the centre of each valveholder but it would appear that these are not absolutely essential and some constructors may prefer to build on a try-it-and-see basis and only fit them afterwards if needed. The position occupied by the screens is shown dotted in the under chassis wiring diagram Fig. 3 but it should be noted that they were removed for the photograph (at the top of this page) in order to provide a clearer view of the wiring and components.

\section*{Construction}

The chassis used was an aluminium type with reinforced corners and it measured 8 in . \(x 3\) in. \(x\) \(2 \frac{1}{2}\). Actually a chassis having a depth of only 1 in . Would have been sufficient but the deeper one was chosen as it appeared to be a standard ready made component that was stocked by most of the well-known component shops.
There is comparatively little metal work or drilling to be carried out as will be seen from the chassis drilling diagram Fig. 4. To simplify the

marking out of the I.F. transformers a small paper template should be used and if desired this can be lightly stuck on to the chassis before drilling.

Having drilled all the holes in the chassis the various components can be fitted into position according to the diagrams Fig. 2 and Fig. 3 hut care should be taken to ensure that the valveholders are the correct way round. This also applies to the I.F. transformers and these can be checked quite easily by reference to the small numbers moulded on the base of the formers, 1 and 3 being primary and 4 and 6 the secondary.

\section*{Component Group-board}

The secret of the clean layout and the easy assembly lies in the 18 -way miniature group-board which takes practically all the small components, and by wiring up the various tags on the back first the majority of the work can be done before this item is fitted into the chassis.

The two views of this group-board given provide all the necessary information for carrying out the wiring, but in view of the ease with which it is possible to become confused when constantly turning this component over while working it is strongly advised to positively mark one end with a dab of paint or a small " \(V\) ", notch as shown. It is recommended that all the wires on the rear of the group-board should either be PVC insulated or covered with 1 mm sleeving to avoid the possibility of short circuits.

It is also essential that an insulated backing plate should be fitted between the group-board and the chassis or if preferred it can be mounted just clear of the chassis by two spacing nuts. It will be noted that the two pairs of tags in positions 4 and 13 have been removed and this was done to allow the screens across the valveholders if fitted to be taken close to the chassis.

\section*{Power Supply}

No mains on/off switch has been included as it was thought that in most cases this unit would

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}
probably be controlled from the main amplifier, but this is a matter of personal requirements.

The mains side consists of a conventional double wound transformer T4 of the type used in most Band IlI convertors giving 200 V half-wave H.T. and 6.3 V for the heaters; this type of transformer also effectively isolates the chassis from mains to ensure complete safety. The H.T. is rectified by means of the usual contact-cooled rectifier MRI which must be fixed to the chassis so that the smooth side makes good contact all over for cooling.

One side of the H.T. winding on the transformer goes to chassis together with one side of the \(6 \cdot 3 \mathrm{~V}\) winding. The other side of the H.T. winding then goes to the tag on the rectifier marked -ve while the \(+v e\) tag is taken to the \(16 \mu \mathrm{~F}\) reservoir capacitor and through to the H.T. positive line.
Having completed the actual construction and wiring and carefully checked each part in turn against the diagrams the unit should be connected to the mains and switched on. If a testmeter is available it is a good idea to check at the various valve pins to make sure that there is H.T. on the screens and anodes (pins 5 and 7), and also a small positive on the cathodes (pin 2).

\section*{Setting Up}

The output socket SK2 should now be connected to an amplifier input and the controls turned to near maximum to start with. If a signal generator is available then the adjustment is very simple and routine.

First of all set the signal generator to about \(1440 \mathrm{kc} / \mathrm{s}\) and feed the modulated signal into pin 1 of V2, then adjust the cores of T3 for maximum sound from the loudspeaker. Now transfer the generator to pin 1 of VI and adjust both cores of T2 for maximum signal and then connect the signal generator to the aerial socket and finally adjust \(\mathrm{T}_{1}\) cores for the best output.

This will bring the tuner fairly close to the Luxembourg programme and if desired a short aerial can be fitted and the final adjustment carried out on the actual transmission. A better way if
(Continued on page 749)

\section*{An AUIDID ARSORPTION WATTMETEIR}

\(\mathcal{J}\)

\author{
By K. BERRY
}

HIS wattmeter was developed to enable the power output of audio amplifiers to be measured. It is suitable for use with amplifiers having output impedances of 3 or \(15 \Omega\), and will measure powers of between 1 and 20 watts. A feature of this design is the fact that the meter has a nearlinear scale as opposed to the more usual "squarelaw" scale associated with instruments of this type.

\section*{Theory}

The power dissipated in a resistor is given by the expression \(P=\frac{-}{R}\) watts, where \(R\) is the value of the resistor in ohms, and \(V\) is the voltage developed across it in volts. Thus if it is desired to measure the output power of an amplifier, a resistor, whose value is the same as the output impedance of the amplifier, should be connected to the output terminals of the amplifier and an A.C. voltmeter connected across it to measure the voltage developed. The power dissipated in the resistor can then be calculated. If, however, the meter was so calibrated, then the power developed could be read off directly thus obviating the need for calculations. This is the basis of the absorption wattmeter.

If the voltmeter used has a linear scale, the power calibration tends to be cramped at the "top" end of the scale as shown in Fig. 1. In this design, the voltage applied to the rectifier bridge which feeds a moving coil meter has been



The finished instrument.
deliberately kept as small as possible. Consequently the diodes are being worked over the nonlinear portion of their characteristics and since this approximates to a "square law" curve this largely cancels the cramping effect normally found at the top end of the scale as can be seen by comparing the scale in Fig. 2 with that in Fig. 1.

\section*{Circuit Description}

The circuit diagram of the wattmeter is given in Fig. 3. The appropriate load resistor, \(3 \Omega\) or \(15 \Omega\), is chosen by SW1A. The voltage developed across the load resistor is applied to one of four potentiometer networks, the required network being selected when the impedance and power range switches are set. The output from the selected potentiometer network is fed to the bridge rectifier, Mrl-4, and thence to the meter M1. A
\begin{tabular}{|lc|}
\hline & Specification \\
Impedance & \(3 \Omega\) or \(15 \Omega\) \\
Power range & 5 watts or 20 watts \\
Frequency response & \(\pm 0.5 \mathrm{~dB} 10 \mathrm{c} / \mathrm{s}=100 \mathrm{kc} / \mathrm{s}\) \\
\hline
\end{tabular}
\(250 \Omega\) rheostat VR5 is connected in series with the meter. This has been included to enable an adjustment to be made to the linearity of the scale since this will vary slightly depending on the exact type of diodes used in the rectifier bridge.

The use of four separate potentiometer net-

Table I
\begin{tabular}{|c|c|c|c|c|c|c|c|}
\hline \multicolumn{8}{|c|}{Impedance} \\
\hline \multicolumn{4}{|c|}{\(3 \Omega\)} & \multicolumn{4}{|c|}{\(15 \Omega\)} \\
\hline Voltage & Power & Voltage & Power & Voltage & Power & Voltage & Power \\
\hline 3.87 & 5 & 7.75 & 20 & 8.66 & 5 & \(17 \cdot 32\) & 20 \\
\hline \(3 \cdot 46\) & 4 & 6.93 & 16 & 7.75 & 4 & 15.5 & 16 \\
\hline 3 & 3 & 6 & 12 & \(6 \cdot 7\) & 3 & 13.42 & 12 \\
\hline 2.45 & 2 & \(4 \cdot 9\) & 8 & \(5 \cdot 5\) & 2 & 10.95 & 8 \\
\hline 1.73 & 1 & \(3 \cdot 46\) & 4 & \(3 \cdot 87\) & 1 & \(7 \cdot 75\) & 4 \\
\hline 1.23 & \(0 \cdot 5\) & \(2 \cdot 45\) & 2 & \(2 \cdot 74\) & 0.5 & \(5 \cdot 5\) & 2 \\
\hline
\end{tabular}
works instead of the more usual series (multiplier) resistors is explained by the necessity to keep the resistance in series with the bridge, low, and comparable. on all ranges. This results in a common calibration for all ranges.

\section*{Components and Construction}

The choice of components is quite straightforward. The load resistors, R1 and R2, must, of course, have an ample power rating, but the use of 20W resistors is, perhaps, not essential. Provided the meter is not used to absorb a continuous 20 W , there is no reason why. say, 10 W resistors should not be used. The \(3 \Omega\) board is made up of 3.3! 1 and \(47 \Omega\) resistors in parallel \((=3.06 \Omega)\). The germanium diodes used in the prototype were Mullard type OA70, these are general purpose poirt-contact diodes and any similar diodes should prove suitable. The meter is a \(3 \frac{1}{2} \mathrm{in} .0-1 \mathrm{~mA}\) movement with a D.C. resistance of \(50 \Omega\), but any \(0-1 \mathrm{~mA}\) meter should be equally satisfactory for this purpose.

The prototype wattmeter was housed in an "Eddystone" die-cast case of size \(7 \frac{3}{8} \times 4 \frac{1}{8} \times 2\) inches (approximately) with four small rubber feet fitted



Fig. 4-The calibration arrangement.
to the underside to prevent damage to the paint finish if placed on a rough surface.

\section*{Calibration}

When the instrument has been assembled and wired, it is necessary to calibrate it by adjusting the potentiometers RV1-5 inclusive. This, fortunately, is quite a simple matter and requires only the use of an accurate D.C. voltmeter. This meter is used to measure the voltage applied to the terminals of the wattmeter. Before commencing calibration, the lead to SWIA should be unsoldered so that the load resistors R1 and R2 are disconnected. A variable D.C. voltage is then applied to the wattmeter as shown in Fig. 4. This can be obtained from a battery and poten(Continued on page 754)

Fig. 3-The circuit of the instrument.

\title{
Radio Components
}
(Continued from page 605 of the November issue)

\title{
and their Functions
}

\author{
By K. Royal
}
one for which the experimenter may well find applications.

The rest of VI is wired in the usual manner. Grid bias for the valve is obtained from the voltage dropped across the cathode resistor R3, and this is of the order of 6 V , as measured between cathode (positive) and chassis on a \(1,000 \Omega / \mathrm{V}\) meter. The anode is loaded by the loudspeaker transformer T1, whose turns ratio is selected to match the low impedance loudspeaker to the high anode impedance of the valve. C3 across the primary winding gives further tone correction and damps harmonic resonances which may otherwise be set up in the loudspeaker transformer.

The screen grid of the valve is fed through R4 and heavily decoupled (or smoothed) by C4. It is worth noting that the anode of the valve is fed straight from the output of the rectifier V2 without a smoothing choke or resistor. When this is done on a single-stage circuit the screen grid of the valve must have an almost ripple-free voltage, which is accomplished by the decoupling mentioned above. R4. then, can be considered as the smoothing resistor and C4 the smoothing capacitor. C5, at the cathode of the rectifier, is, of course, the ordinary reservoir capacitor. There is no negative feedback in this simple circuit, for even the cathode of the valve is heavily decoupled by C2.

A fully isolated power supply is employed. T2 being the mains transformer with H.T. and L.T. secondaries. The H.T. winding is centre tapped to facilitate full-wave rectification, while the heaters of the two valves are wired in parallel and energised from the 6.3 V L.T. winding.

This kind of amplifier runs at about 260 V H.T. (from the rectifier). This gives about 240 V on the valve anode and 225 V on the screen grid with currents of 41 mA and 4.8 mA respectively. The total H.T. current, therefore, is in the order of 46 mA as measured in the cathode of V1. The A.C. voltages either side of the centre tap on the H.T. winding of the mains transformer are 235 V .

\section*{Push-Pull Stereo Circuit}

To illustrate the more complex push-pull circuit we show at Fig. 7 the circuit of the Decca SG188 stereo record reproducer. For any stereo system
two identical amplifier sections are required which are given as Channels \(A\) and \(B\) on the circuit.

Each channel has a voltage amplifier tone control stage, followed by two more voltage amplifiers, a phase splitter, two pentodes in pushpull and a pair of parallel-connected rectifiers to provide the necessary current for the two channels. For the following discussion Channel A will be considered, bearing in mind that the rectifiers and power circuits only are common to both channels.

The stereo pick-up gives two outputs, one which is fed to Channel A and the other which is fed to Channel B. The pick-up signal is fed direct to triode V1A via the equalising circuit C50 and R 50. This gives a rising response to the higher audio

The signal goes in at the top of R56 and comes out at the slider of VR2. It thus passes only lowfrequency signals to the volume control and the amount of low A.F. relative to high A.F. passed depends upon the setting of VR2.

\section*{Two Signals}

In that way, then, the volume control receives two signals, one by way of the treble high-pass filter and the other by way of the bass low-pass filter, and as each of these filters are adjustable the required overall frequency response can be accurately established. This type of tone control circuit is also extensively used


Fig. 6-The eircuit diagram of a simple single-stage A.F. amplifier, used in the Cossor, Model 559 Record Reproducer. in hi-fi amplifiers and control units.

The equalised and tone-controlled signal is developed across the volume control and the required level is tapped off at the slider and fed to the control grid of V2A. This is a fairly conventional A.F. amplifier but has facilities in its cathode circuit for the application of negative feedback. The stage is biased by the voltage dropped across R62 and R64 as series in the cathode circuit. R66 is the anode load from whence the amplified signal is fed to the grid of V3A via the coupling capacitor C60.

R65 is the grid leak for V3A and reflects the voltage dropped across R69 in terms of grid bias at the grid. Current negative feedback is applied to this stage, since R69 does not have a bypass capacitor.

V4A is the phase splitter valve. This is direct coupled to the anode of V3A and the splitter is biased because the voltage at
signals, since C 50 is 100 pF (having a high impedance to low A.F.) and R50 is 1 M. R 52 is simply the grid return for V1A.

The equalised signal is developed across the anode load R51 and fed through C52 to the tone control system. Thus from C52 we have a signal applied to the "treble" circuit (C53, VR1 and C54) and also a signal applied to the "bass" circuit (R56.VR2, C55, C56 and R57). Now when VR1 and VR2 are set to the centre of their ranges a signal of frequency characteristics almost equal to that at the output of C52 is fed to the volume control VR3 and there is no tone correction. There is attenuation, though, which is the reason why the circuit features three voltage amplifiers. At high A.F. C54 "looks" almost like a short-circuit, while C53 has a relatively low value of impedance. Thus, with VRI slider at C53 end of the control, maximum treble is fed to the volume control and this value of treble diminishes as the control is turned in the opposite direction.

The network comprising R56, VR2, R57, C55 and C56 is, in effect, an adjustable low-pass filter.
its cathode is V2 more positive than the voltage at its grid, thereby making the grid V2 negative with respect to its cathode.

\section*{Push-Pull Drive}

The phase splitter produces two signals, one at the anode, across R71, and the other at the cathode, across R70. As these resistors are accurately balanced the two signals are of equal amplitude, but owing to the phase inversion effect of the valve the signal at the anode swings positive when the signal at the cathode swings negative and vice versa. These signals represent the drive for the push-pull valves and are fed through C64 to the control grid of V3A and through C63 to the control grid of V4B.

The output pair are biased for class A conditions, meaning that there is no flow of grid current, and the signals are re-established as one complete waveform across the centre-tapped primary of the output transformer T1. They are here coupled to the low-impedance secondary winding, which is tapped to suit a range of loudspeaker impedances.


Fig. 7-The functions of all the components employed in this twin-channel, push-pull amplifier (Decca SG/88) ore given in the text.

\section*{Negative Feedback}

A further secondary winding on T 1 is employed for feeding back a fraction of the output signal to the cathode circuit of V2A as ncgative fecdback. This is done through the frequency-selective network R63 and C59, with R61 as the other arm of a potential divider. In effect the feedback signals are reflected, via the cathode, to the control grid circuit of V2A in counteracting phase to the signals originally applied from V1A. This results in a reduction in total signal applied (hence another reason for the three voltage amplifiers), but its asset. of course, is that it cancels harmonic and other distortions, including hum.

The output valves are biased for class A by R75 and R77 in their cathodes, with the grid return circuit occurring through the balanced grid leaks R73 and R74. R76 is a low-value grid stopper arranged to prevent parasitic oscillations in the output stage. The cathodes of the output valves are decoupled by the electrolytics C65 and C66. This, along with the negative feedback, gives the stage a good damping factor, which is an essential requirement for high-quality reproduction.
Anti-resonant devices comprising R79/C69 and R80/C66 are connected across the primary of the output transformer and the screen grids of the output valves are connected in parallel and fed through R78, with C67 providing decoupling.
Each voltage amplifier stage is individually decoupled on the H.T. line, which is necessary in the interests of low-frequency stability, particularly when two amplifiers are sharing a common power supply. V1A is decoupled by R58/C51, V2A by R67/C57 and V3A by R72/C61.

\section*{Power Supply}

The power supply used in this model is not isolated from the mains. It will be seen that an auto-transformer is used for feeding the anodes of the rectifiers V7 and V8 and this winding is connected to the mains supply via chassis. There is, however, a separate winding for the paraliel-
connected valve heaters and is centre tapped to chassis to reduce the pick-up of hum to the smallest possible level.
The valve anodes are connected by limiting resistors, necessary to avoid overloading of the rectifiers on surges, while the cathodes are connected in parallel, with C 87 serving as the reservoir capacitor.

\section*{Stereo Balance Control}

In twin-channel stereo systems a separate control labelled " balance " is often featured. This simply serves to balance the overall gain of the two channels. In Fig. 7 the balance control is VR7 and it is connected in the cathode circuits of the two first voltage amplifiers and, since the slider is connected to chassis. equal gains should occur with the control set to the centre of its range. When the control is adjusted so that the resistance in one cathode circuit is reduced then that valve increases slightly in gain. while its partner decreases slightly in gain and vice versa.

All the voltages to be expected in the various stages are marked on the circuit and. it will be obvious that the circuit of Channel B is identical to that of Channel A.

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\(\mathcal{J}\)HE theoretical circuit shown in Fig. 1 is very similar to the simple Geiger Head published with the author's Digital Counter in the February issue. The main difference lies in the choice of a completely different type of Geiger-Tube, the Mullard MX124/01. The actual tube is enclosed in a thinwalled glass envelope coaxially within a sealed-on test-tube for containing the liquid to be tested. Thus the liquid intimately surrounds the GeigerTube proper, which accounts for the very high sensitivity.

\section*{H.T. Voltages}

The MX124/01 has an unusually low operating voltage ( 400 to 500 ) compared to other tubes of this type. This is a distinct advantage for amateur circuitry. The arrangement of the H.T. feed in the circuit is somewhat unusual, a conventional 300 V positive supply in conjunction with an additional 100 V negative supply being used.

There are two good reasons why this arrangement has been adopted. Firstly, +300 and -100 are becoming standardised outputs for stabilised power supplies, and are thus also the main outputs of the "Experimenter's Power Pack" published recently in this magazine, which is admirably suited for operation of this unit.

Secondly, the EC92 cathode-follower headamplifier can be run off the same H.T. supply in this arrangement, as is evident from Fig. 1. The power supply requirements are seen to be identical to those of the Digital Counter, and the two units may be run simultancously off the "Experimenter's Power Pack ".
lt is, for reliable and accurately reproducable results, highly desirable to run this equipment off a stabilised power supply, though other ordinary simple power supplies could be tried. It will then probably be necessary to use separate power supplies for this head and for the Digital Counter.

It is absolutely essential that the total voltage applied to the tube never exceeds 450 V , as otherwise flashover and possible destruction of the tube can take place. Thus the positive H.T. must not exceed 350 V .

\section*{Threshold Voltage}

Mullard quotation for the Threshold Voltage for the MX124/01 is "maximum 400 V ". Individual samples vary and the tube in the author's prototype was found to have a threshold at 360 V . It is desirable to operate the tube at approx. 50 V above threshold which gives 410 V for the author's prototype.


The finished instrument.

When the unit is initially put into operation, the output should be connected to an oscilloscope, and the pulses observed as the positive stabilised H.T. is varied on the power pack. As the H.T. voltage is gradually reduced, the pulse amplitude will also decrease, until it vanishes at the threshold voltage.
The voltmeter reading should then be noted, and the H.T. increased by about 40 to 50 V . This assures the proper operating point having been set, and it should be checked in the same manner from time to time as the tube ages.

\section*{Pulse Amplitude}

Fig. 2 is self-explanatory as far as the theoretical details of the generation of the pulses are concerned. The treatment is, of course, simplified, as no account has been taken of chemical effects within the tube also leading to rapid extinction of each discharge.

Nevertheless, the capacity-effects sketched in Fig. 2 generally dominate and are sufficient to give a measure of control over the output pulse amplitude, by means of adjustment of Cl . The larger the capacitance of C 1 and Cstray, the greater is the charge-per-pulse passing through the tube, i.e. the greater the strain on the tube. It is thus desirable to keep both of these capacitances small.

Naturally, any capacitive loading of the tube increases the violence of the discharge on each pulse, and it may thus seem strange that a circuit is proposed which deliberately introduces such loading.

The advantage gained, however, is the production of a substantial pulse giving secure operation of simple counter circuits aimed to avoid all snags and critical effects in the input stages, and this advantage is considerable for amateur purposes.

\section*{Tube Life}

The price paid for this advantage is a shortening of tube life, to the region of at least 100 million counts, instead of the almost infinite life achievable in more critical specialised circuits. While such a life would be too short for high counting-rate professional laboratory use, it is still more than ample for the amateur uses intended in this article.

One will be operating at counting rates around 100 per minute for the purposes envisaged, so that even with the minimum life of \(100,000,000\) counts, at least 15,000 operating hours are certain. Probably much more.
The prototype shows that, after completing more thinn 2,000 operating hours under these conditions, changes of tube characteristics are at the most a fraction of \(1 \%\) of those of a brand new tube.

\section*{Slow Counting Rates}

The adverse effects on dead-time and plateauslope are of little importance at the slow counting rates intended, though probably seriously limiting the suitability of this circuit for work at normal laboratory counting rates of some hundred or more per second. The plateau-constancy over long periods of usage under the conditions specified has proved itself in practice. and the use of stabilised power supplies adequately removes errors of counting due to plateau-slope for the present purposes.

The actual values of C1 and Cstray do not affect the output pulse amplitude as much as the ratio of their values. The total pulse-voltage generated is necessarily equal to the difference between operating point and threshold, which we deliberately set at about 40 to 50 V .

This pulse voltage is seen in Fig. 2 to appear across C1 and Cstray in series, the two capacitances thus forming a voltage-divider. Only the portion appearing across Cstray is passed on to the cathode follower V2, and hence to the output. If a reasonably large part of the total pulse voltage is to appear at the output, therefore C 1 must at


Fig. 1-The circuit of the head.
least be equal to, or somewhat larger than Cstray.
This is the reason for including an actual physical component for C 1 , part of which is made up by the inherent stray anode capacitances of the tube and wiring, and the rest by a physical component in the form of a pair of twisted insulated wires.

It is desirable to set conditions such that, finally, C1 (total) and Cstray are approximately equal. This condition is realised when the pulse output voltage from the unit is about half of the threshold-excess, i.e., some 20 to 25 V peak. The output pulses should be observed on an oscilloscope in comparison with A.C. sinewave voltages of known amplitude, using the same Y -amplifier gain in all cases.

The length of twist of the insulated wires forming C 1 is altered, until the output pulses are observed to have 20 to 25 V amplitude. It need hardly be said that the operating point must previously have been set 40 to 50 V above threshold, as described above.

\section*{The Cathode Follower}

This stage is fully conventional. C3 blocks the negative 100 V D.C., allowing only the positive pulses to pass. and be reproduced accurately at the same amplitude and form at the output. R4
(Continued on page 729)

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\section*{THE "TINYMITE"}

\section*{(Continued from page 726)}
and \(C 2\) give heavy decoupling for the stage. C4 and R 7 remove any D.C. component from the output otherwise resulting from the cathode circuit of V 2 .

The purpose of V2 is not voltage amplification as the output voltage of the geiger tube is ample for the digital counter, etc. The purpose is, rather, to reduce the impedance, allowing transmission of the output signal on reasonably long lengths of coaxial cable without loss. This function certainly amounts to \(a\) form of power-amplification, however.

\section*{Gieger-Tube Screening}

The manufacturers specify operation of the tube in a 2 in . thick all round lead container, which can weigh anything up to half a hundredweight! Whilst this is certainly essential for efficient industrial use, it is by no means necessary for amateur use, provided the factors concerned are understood and taken into account. At any rate, it is clear why the bare tube alone must be removable in an industrial arrangement, and mercury-cup connectors used: the whole unit with lead casing would be far too heavy and cumbersome to move about!

The advantages of the heavy lead casing are principally twofold, neither of which is essential for the amateur. Firstly, and most important, the tube is thereby screened from ambient levels of X-rays or other radiation from other experiments and equipment operating on the premises nearby, which have nothing to do with. but would scriously interfere with, the experiment running with the tubc in question. This danger of interference is not likely to arise under amateur conditions, provided such sources as luminous watches the clocks are kept away from a running experiment.

Secondly, the lead casing would absorb a large portion of the "Cosmic" background radiation coming from outer space, etc. This reduces the "background-count per minute" to be subtracted from a count made with a liquid sample, i.e. it improves the "signal-to-noise ratio", giving better resolution and shorter required counting times for a given desired accuracy.

This may be important for industrial concerns where time is money, but is unimportant for amateur usage. The saving in expense, and convenience in construction, achieved by onlitting a lead screen outweighs all other considerations for the amateur.

\section*{Important Points}

When operating the tube without a lead screen, the following two points must be watched care-fully:-
(a) The unit is vulnerable to interference from external radioactive sources of sufficient intensity. Such sources must be removed to a distance of at least three yards, or kept fixed in position during an experiment, their effects being included in the subsequently subtracted " background count" made without the test-liquid in the tube. In particular, do not move the hands about near the unit during a count whilst wearing a wristwatch with luminous figures.
(b) The background count will be higher with the tube completely empty than when filled with pure non-active distilled water. This is due to the water acting as a weak screen, absorbing some of the low-energy components of the cosmic radiation.

Thus the "background-count" should always be made with the tube filled with pure distilled water, because the water-content of the subsequently counter test liquid will give the same reduction of cosmic background. Failure to observe this procedure can cause quite serious errors.

In the author's prototype, the background-count was found to be 40.4 per minute with the tube completely empty, but only 38.3 per minute with the tube full of distilled water. The count with a certain sample filled into the tube was 47.2 per minute, representing a correct signal of 8.9 per minute due to the sample.

Had the empty-tube background count been used in error, the sample-signal would apparently have been only 6.8 counts per minute, an error of well over \(20 \%\) !

When using a lead screen the weaker cosmicradiation components are absorbed anyway, so that then there will be no difference in background counts for an empty tube or one filled with distilled water.


Fig. 2-Production of pulses and effect of Cl : (a) output pulses; (b) threshold voltages; (c) equivalent circuit of the geiger tube.

\section*{Photoolectric Effect}

Geiger-Tubes of the type here specified are often sensitive to light, giving an appreciable countingrate in response to illumination. This effect was found to be immeasurably small for normal wavelengths of light in the author's prototype. A back-ground-count of 40.4 per minute was obtained with the empty tube, whether completely dark or whether strongly illuminated with a couple of 25 W bulbs Sin. away.

The accuracy limits of this experiment were about plus-or-minus one count per minute. Thus error due to normal room illumination, if present at all, is likely to be less than \(2 \%\). Nevertheless, it is desirable to keep the tube dark, for safety. The arrangement adopted satisfies this condition, in that most of the tube length is inside the body of the wooden case.

The rest is covered by the black P.V.C.-Tape, to within about tin. of the spout, which is covered by a cap, also desirable to reduce evaporation of the sample liquids. Any suitable opaque material of suitable shape and size can be used for the cap, preferably insulating and loosely fitting. Do not use a cork of any sort, as this could press down on and break the delicate inner construction of the tube.

\section*{Care of the Geiger-Tube}

Counting times of more than three hours maximum should seldom if ever be required with the sensitivity achieved by this head. Samples prepared as already discussed in the "Digital Counter" article, and with the further remarks below, normally require counting times of only 30 to 60 minutes for sufficient accuracy. Thus samples need never be left very long in the tube.
Prolonged presence of samples in the tube can cause diffusion through the thin glass of the inner unit, raising the background count permanently.
Thus all samples should be poured out immediately after conclusion of a count, and the tube willed out thoroughly at least three times with clean or distilled water.
Never use tarry, greasy or sticky liquids which could soil the tube permanently or render cleansing extremely difficult. Although dilute acids do no damage avoid using caustic alkalis and do not insert warm or hot liquids into the tube.

\section*{Preparation of Samples}

Procedure outlined in the "Digital Counter" article should be observed. Whilst it is still necessary to concentrate rainfall and other water samples, lower concentration factors can be used than with the simple Geiger-Head described in the "Digital Counter" article.
The simple Geiger-Head, furthermore, gives really quick definite signals only with those rainfall samples representing the verge of real contamination. With present levels of radioactivity in rainfall, long careful overnight counts are required for reasonable quantitative measurements but with the unit described in this article, definite strong and reliable signals are very easily and very quickly produced even with rainfall of present levels of activity.


\section*{Quantitative Data}

Serious experimenters, and particularly schools and clubs, will be interested in doing quantitative work with this apparatus, to determine not only relative values of radioactivity in liquid samples but also absolute values in terms of equivalent weight of radium per unit volume of the liquid.

The author has had available standard solutions of uranium and thorium, as well as possessing a high-voltage Geiger-Tube of similar type supplied with extensive calibration charts from the manufacturers. Using this apparatus as comparison standard, the prototype MX124/01 has been carefully calibrated. The results of this work, here given in full, may reasonably be supposed to be applicable to any sample of the M \(\times 124 / 01\) tube used under the conditions specified in this article.

\section*{The Curle}

The unit used for measuring absolute values of the radioactivity of substance is the Curie. A quantity of substance having the same effective activity as one gram of radium is said to have an activity of one Curie. This unit is extremely large, so that convenient practical units are the microCurie ( \(\mu \mathrm{C}\) ) and the pico-Curie ( pC ) representing a millionth part, and a millionth of a millionth part, of a Curie, respectively.
One millogram or ordinary thorium has an activity of about 100 pC . This was found to give, when effectively contained in the (exactly) 8 c.c. of liquid needed to fill the MX124/01. an increase of counting rate of about 10 per minute with the head described in this article.

Similarly. one milligram of ordinary uranium has an activity of about 350 pC . and was found to give an increase of counting rate of about 35 per minute when present in the \(8 \mathrm{c} . \mathrm{c}\). contents of the MX124/01.
The sensitivity to this type of radioactive substance is thus about one count per minute per 10 pe present in the contents. These substances. i.e. heayy elements, emit principally alpha-rays (helium nuclei) and gamma-rays (exceedingly short wavelength wireless waves), the tube responding principally to the latter.
(To be continued)

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Pri. 200/250 v , sec. \(2,000-0-2,000 \mathrm{~F}\). 500 mA . tapped \(1.500 \mathrm{\nabla}\). New. boxed, \(\mathbf{2 6 . 1 0 . 0}\). Carrlage \(15 /-\).

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For 1 ifin. dia. panel hole.
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\section*{STABILISED POWER UNITS}

THE latest versions (Mk. III) of the Lexor stabilised power units models LT.12-05 and LT.24-05, are now available.

New features of the Mk. III include a much reduced longitudinal noise factor and an improved overload and short-circuit protection. The two models available have output voltage ranges of \(5 \cdot 5-14 \mathrm{~V}\) or \(18-28 \mathrm{~V}\). The output voltage of either instrument is continuously variable and may be adjusted either by a panel knob or a pre-set control. Both instruments will deliver output currents up to 0.5 A continuously at all voltage settings.
The units are mounted in steel instruments cabinets 8 in . x 5 in . \(\times 5 \frac{3}{} \mathrm{in}\). finished in grey hammer stove enamel with contrasting blue panels. The price of the new Mk. Ill units is \(£ 257 \mathrm{~s}\). and they are made by Lexor Electronics Limited. 25-31 Allestey Old Road. Coventry, Warwickshire.


The new Multicore solder dispenser.


POCKET SIGNAL GENERATOR
FOR engineers, radio and TV servicemen who require a small and convenient form of input for testing or fault finding, Electronic Machine Control Ltd., have produced the "Pensource" range of pocket signal sources.
These instruments are made available in several ranges and give an output of approximately \(\frac{1}{2} \mathrm{~V}\).

Basically each "Pensource" is a transistorised oscillator built into a robust chromium plated case. The supply to the oscillator is provided by a \(1 \frac{1}{2} \mathrm{~V}\) penlight cell and under normal conditions of use, should last approximately four to six months.
The "Pensource" costs \(£ 410\) s. and a leatherette case is also available at an extra cost of 10 s . 6 d . The makers are Electronic Machine Control Lid., Mayday Road, Thornton Heath, Surrey.


One of the new Lexor stobilised power units.

\section*{NEW SOLDER PACK}

NEW from Multicore Solders Limited is a solder dispenser especially suitable for use by the amateur constructor. It is. in fact. an extruded aluminium tube, the top being tapered to a delivery hole through which the solder is drawn as required. This arrangement prevents the solder tangling and the flat base of the dispenser allows it to be stood firmly on the work bench, leaving the user complete freedom of both hands whilst working.

The contents of the new pack is a 16 ft length of 18 s.w.g. Ersin Multicore Savbit alloy and its price is 2 s . 6 d . complete. The manufacturers are Muliicore Solders Lid., Maylands Avenue, Hemel Hempstead, Hertfordshire.


One of the new switches from Carr Fastener こo. Ltd.

\section*{MINIATURE SOLDERING IRONS}

RECENTLY A.N.T.E.X. Ltd, have added to their range of Precision soldering irons. Amongst the new additions is the model E240, a lightweight instrument operating from \(230-240 \mathrm{~V}\) mains and with a power consumption of 20 W .

The novel design of these irons makes them easy to handle and attractive. Interchangeable bits are available to fit this model as well as a wirestripper attachment. The price of the complete iron is 35 s . and the makers are A.N.T.E.X. Ltd., Grosvenor House, Croydon, Surrey.

\section*{MULTIRANGE METER}

THE model 88B multimeter from Taylor Electrical Instruments Ltd., is similar in operation to their popular model 88 A , but is somewhat reduced in size. It is available in

\section*{NEW SLIDE SWITCHES}

JUST incorporated with the range of components produced for the electronics industry by Carr Fastener Co. Ltd., are two new slide switches. These are identical in specification but differ slightly in their mounting facilities. Both switches are of the double-pole, double-throw type, and can be used for radio wavechange, instrument or any relatively low voltage switching application.

Constructionally, the switches differ only in their steel shell, one having vertical fixing lugs and the other having two 0.125 in . diameter holes at 1.125 in. centres and alternative side-fixing lugs. Carr Fastener Co. Ltd., Stapleford, Noltingham.


The model E. 240 soldering iron is made by A.N.T.E.X. Limited.


This new multimeter is monufactured by Taylor Electrical Instruments Lid.
either a bakelite or wooden case.
The sensitivity of the instrument is \(20.000 \Omega / \mathrm{V}\), and other features include a mirror scale, an overload protection device and a reverse polarity facility.

Among the ranges included in the instrument are, resistance ranges up \(1050 \mathrm{M} \Omega\) and decibel ranges. The instrument will also measure capacitance and inductance but a model 388 adapter is required.

Another accessory which is available is a high voltage probe for measurements up to 25 kV .

The two batteries used in the meter are located in a separate compartment. The types used are Ever-Ready U. 2 and B. 121.

The makers of this new multimeter are Taylor Electrical Instruments Lid., Montrose Avenue, Slough, Buckinghamshire.

\section*{THE TRANSISTOR CLOCK}

ONE intriguing result of research in radio engin-eering-the transistor principle-has now been applied to clock-making. The Kundo (Crown Manufacturing Co. Ltd.) transistor clock, on display at the recent Watch and Jewellery Trade Fair, has an operating mechanism of unusual simplicity. A magnet attachment to its pendulum dips into a coil at each oscillation, producing, by induction, a voltage pulse which, fed into the transistor, triggers the flow of current from the battery to the drive coil. A driving impulse is thus imparted to the pendulum.

Needing no maintenance, this extraordinary timepiece runs continuously for no less a period than three years!

呞 and 15 whm \(\begin{gathered}\text { olm } \\ \text { ont }\end{gathered}\) put. A really first-class Amplitie Giving H-Fi quality at a reasonable cost. Mullard's latest circult. Valve line up: E1PBS, EL84. EZ81. Extra HT and l'I available tor
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\(100 / 25 \mathrm{~V}\) & \(2 /-\) & \(80+50 / 350 \mathrm{~V}\)
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814.00V & \(2 / 8\) & \(80+50 / 350\) \\
& \(2 / 20+2001\)
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\section*{Transistor Components}

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\section*{THE B.I.E.T. IS THE LEADING ORGANISATION OF ITS KIND IN THE WORLD}

\title{
A Simple 3-Valver \\ By T. M. Bush
}

\(\mathcal{J}\)HIS unpretentious little receiver can be built very cheaply. Considering the extreme simplicity of the circuit, it has a very good performance and with careful manipulation of the controls, the single tuned circuit will enable all the more powerful transmissions to be received clear of interference.

\section*{Circuit}

The EF91 is a high slope miniature valve which is available ex-equipment very cheaply indeed. Three of them are used in this receiver. The first is arranged as a pentode R.F. amplifier but it will be noticed from Fig. 1 that there is no tuned circuit associated with it. The high slope of the valve, however, goes a long way towards repairing this omission and quite a worthwhile gain is achieved. Because the EF91 does not have variable-mu characteristics it was necessary to achieve some method of gain control other than by variation of bias, and the problem was solved very satisfactorily and simply by feeding the signal from the aerial to the slider of a 1 M potentiometer in the grid circuit.

The second valve, connected as a triode, is used as a conventional leaky grid detector, regeneration
being applied through the variable capacitor VCl to sharpen the tuning and increase the sensitivity. Because the R.F. stage isolates the aerial from the tuned circuit the tuning is not affected by aerial loading and if by chance, as will sometimes happen, too much reaction is applied, the resultant oscillations will not be radiated to the annoyance of the neighbours. Resistor R5 and capacitors C2 and C3 remove the R.F. component from the output and the audio signal is passed via the capacitor C4 to V3, the output valve. This is another EF91, again triode connected. The optimum load could not be discovered but this is not of much importance with the triode connection and an output transformer having a ratio of \(50: 1\) was found very satisfactory for a \(3 \Omega\) loudspeaker.

\section*{Power Supply}

A miniature double-wound mains transformer of the instrument type, having an output of 20 mA at 250 V and 1 A at 6.3 V supplies the power in conjunction with a contact-cooled metal rectifier. Smoothing is provided by the resistor R8, and the associated electrolytic capacitors C5 and C6. A


Fig. I-The circuit.


Fig. 2-The drilling dimensions of the chassis.
pilot or dial light, if fitted, should be 6.3 V 0.04 A , so as not to exceed the rating of the transformer winding. A separate on/off switch was fitted in the prototype but there is no reason why mains switching should not be incorporated with VR1. The power consumption from 240 V A.C. mains is less than 20 W .
connections around V2 and the coil are kept to a reasonable length. Tinned copper wire of 22s.w.g. covered with sleeving is recommended for all the wiring, details of which are given in Fig. 3. The loudspeaker is connected direct to the secondary terminals of the output transformer on top of the chassis. It is good practice to connect one of these

\section*{Modifications}

It will be noticed that the bias resistors of V1 and V3 are not bypassed. Consequently, if greater gain is required, capacitors may be fitted across them as shown in dotted outline in Fig. 1: A further increase in gain can be obtained by reducing the value of R2 to \(150 \Omega\) but this will increase the current through the value and is permissible only if the mains transformer can accept the extra load. The total H.T. current in the prototype was exactly 20 mA .

\section*{Construction}

The prototype was constructed on a chassis of \(18 \mathrm{~s} . \mathrm{w} . \mathrm{g}\). aluminium sheet measuring 8 in . \(\times 4 \mathrm{in}\). \(\times 1 \frac{1}{2} \mathrm{in}\)., details of which are given in Fig. 2. This gives plenty of room for standard size components with the exception of the reaction capacitor, VC1, where a miniature must be used in order that it may be accommodated within the depth of \(1 \frac{1}{2}\) in.; alternatively, the chassis could be made deeper. Construction may proceed in any convenient order. Thie layout and the arrangement of the wiring and components is not at all critical so long as the


The receiver nearing completion.
terminals to chassis and a solder tag should be fitted for the purpose on one of the transformer holding-down bolts.

\section*{Components}

Resistors may be \(\frac{1}{2} \mathrm{~W}\) or \(\frac{1}{3} \mathrm{~W}\). except R 8 which should be 1 W . The capacitors have to withstand (Continued on page 741)

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Fig. 3-The complete wiring diagram.

\section*{COMPONENTS LIST}

Resistors (all \(\frac{1}{2}\) W, carbon unless otherwise stated):
\begin{tabular}{lrl} 
R1 4.7 k & R5 27 k \\
R2 \(390 \Omega\) & R6 0.47 M \\
R3 1.2 M & R7 \(150 \Omega\) \\
R4 270 k & R8 1 k IW \\
VRI 1 M carbon potentiometer
\end{tabular}

\section*{Valves:}
\(\left.\begin{array}{l}\text { V1 } \\ \text { V2 } \\ \text { V3 }\end{array}\right\}\) EF91, B7G base
Coil:
Iron dust core, dual range, medium and long
wave bands, with reaction winding. (Repanco)
Capacitors:
Cl 470pF ceramic or mica
C2 270 pF ceramic or mica
C3 47pF ceramic or mica
C4 270pF ceramic or mica
C5 \(0.01 \mu F\) paper 350 V
C6 \(32 \mu \mathrm{~F}\) electrolytic, 350 V
C7 \(16 \mu \mathrm{~F}\) electrolytic, 350 V
VCI 300 pF solid dielectric variable
VC2 500 pF air dielectric variable

\section*{Transformers:}

T1 Output-about 50:1
T2 Mains-Tapped primary. Secondaries: H.T.: 250 V 20 mA half wave. L.T. 6.3V IA

Rectifier:
Contact-cooled 250 V 20 mA
(Continued from page 738)
the full H.T. voltage from the rectifier when first switching on and must therefore be 350 V working. Any kind of tuning capacitor, air-spaced or otherwise can be used for VC2 or one-half of a twogang component can be used as in the prototype. The coil L1, may be any iron-dust-cored dual wave type with a reaction winding but it is convenient if it is designed to plug into a B9A or B7G valve base. For tuning, a 3 in . diameter engraved knob is fitted direct to the tuning capacitor but there is no reason why a slow motion drive should not be fitted if desired.

\section*{Testing and Operation}

When the wiring has been completed, a test should be made with a meter between C6 and chassis to see that there are no short-circuits in the H.T. wiring. If all is well, power can be applied and transmissions should then be received. Two or three feet of wire as a throw-out aerial will usually be enough, though in poor reception conditions. some more efficient arrangement may be necessary. An earth is not essential, but will reduce mains-borne interference.

It will probably be found that with VR1 at maximum, some programmes will be receivable at adequate volume with VC1 set at minimum, but will suffer from interference from adjacent stations. In this case, the procedure is to reduce the volume by means of VR1 and bring it back to the desired level by the application of reaction, at the same time adjusting VC2 for the best results.

\title{
MIDGET MAINS PORTABLE
}

\author{
By V E HOLLEY
}

\(フ\)HIS handy little receiver was first built with one R.F. stage followed by a diode detector and in this form it gave good service in the north west London area. When later it was required for use in a less favourable location, a second R.F. stage was added to increase the sensitivity.

\section*{R.F. Amplifier}

The signal is supplied by a ferrite rod aerial (L1, L2 in Fig. 1) and two R.F. pentodes, EF91, are used to amplify it to a suitable detection level.

The full gain of the two stages is not required and indeed, could not be used with stability, so the gain is reduced by resistance loading in both anode circuits and by omitting by-pass capacitors from the cathodes. If greater gain is required, one or both of these capacitors may be inserted in the manner of C 4 , which is shown dotted in Fig. 1. Decoupling is provided in both anode circuits.
The inductance of the rod aerial is adjustable within fairly wide limits and the second tuned circuit, which is ganged to it, may therefore incorporate any dual range iron dust cored coil designed to cover the long and medium-wave bands with a 500 pF tuning capacitor.

It will be noted that there is no provision against overloading but as both valves operate with negative current feedback no trouble is likely to be encountered under normal conditions.

\section*{Selectivity}

The selectivity provided by the two tuned circuits is quite good and with the assistance of the directional properties of the aerial, the BBC programmes and some of the continentals can be received clear of interference in daylight and dark-
ness, in any reasonable reception area. Some further improvement might be obtained by applying reaction to L3 and L4; this was not tried.

\section*{Demodulation}

The signal at the anode of V2 is rectified by a germanium diode D1 (GEX34). After passing through the R.F. filter C10, R8, C11, audio frequencies appear across the volume control. VR1 together with a D.C. voltage negative to chassis, which is used for alignment purposes, as will be described.

\section*{A.F. and Output Stages}

A triode-pentode valve, ECL82, is used here in a conventional arrangement. Grid leak bias for the triode section avoids the need for a bias resistor and capacitor, but the pentode bias resistor must be bypassed in the normal manner in order to avoid negative current feedback which is, of course, undesirable in an output stage. The optimum load of the valve is \(5,600 \Omega\) and to match this to a \(3 \Omega\) loudspeaker, the output transformer must have a ratio of about 45:1.

If the D.C. resistance of the primary is more than about \(200 \Omega\), it is advisable to insert a resistor (R12) in the screen supply so that the voltage at the screen will not exceed that at the anode. The network R14, C15 serves to correct the response at the higher audio frequencies where valve and loudspeaker impedances rise considerably.

\section*{Power Supply}

The receiver requires an H.T. supply of about 60 mA at 210 V and a heater supply of something (Continued on page 745)


Fig. I-The circuit.


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This amplifier is made possible by the remarkable micro-alloy transistors it uses. These are available separately at the following prices:-
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Fig. 2-The chassis drilling details.

\section*{(Continued from page 742)}
under 2 A at 6.3 V . The use of a double wound mains transformer to supply this makes the chassis safe to handle at all times and considerably reduces mains-borne interference.

It is convenient to have a separate 6.3 V winding to supply the heater of V4 so that there is not a large potential difference between its heater and cathode, but if only one winding is available, it is quite in order to include V4 heater with the others. If this is done, the winding should be rated at not less than \(2 \cdot 5 \mathrm{~A}\) and it is most important to omit the connection between pins 4 and 7 of the rectifier. (See Fig. 1.)

Smoothing is provided by R16 in conjunction with the electrolytic capacitors C17 and C18, while R10 and C13 provide a little extra for the anode of V3a. The value of R16 may need adjustment in some cases to produce the correct H.T. line voltage. The mains switch is incorporated with VR1.

\section*{Construction}

The receiver is constructed on a chassis of 18 s.w.g. aluminium sheet. 9in. x 4 in . \(x\) 2in., details of which are given in Fig. 2. The layout is not critical. The grid circuit of V1 which includes the aerial, is the point where in-
stability is most easily introduced and care must be taken that it is not capacitively coupled to any of the later wiring. V1 and V2 must be screened.

The trimmers TC1 and TC2 are mounted on top of the tuning capacitor, and if in this position they can " see" each other, a small screen should be erected between them. The pilot light is also


The complete receiver, less its cabinet


Fig. 3.-The underchassis wiring diagram.
mounted on top of the gang and to achieve a symmetrical appearance in the finished receiver, should be positioned so that its height above the
tuning spindle is equal to the distance between that spindle and the spindle of VRI below.
(To be continued)

\section*{LIST OF COMPONENTS}

\section*{Resistors}


\section*{Capacitors:}

Cl \(0 \cdot 1 \mu \mathrm{~F}\) paper 350 V
C2 470 pF ceramic or mica
C3 \(\quad 0 \cdot 1 \mu \mathrm{~F}\) ceramic or mica
C4 \(\quad 0.1 \mu \mathrm{~F}\) ceramic or mica
C5 470 pF ceramic or mica
\(\begin{array}{ll}\text { C6 } & 220 \mathrm{pF} \text { ceramic or mica } \\ \text { C7 } & 220 \mathrm{pF} \text { ceramic or mica }\end{array}\)
C8 \(0.01 \mu \mathrm{~F}\) paper 350 V
C9 \(8 \mu \mathrm{~F}\) electrolytic 350 V
\(\mathrm{ClO} \quad 0.01 \mu \mathrm{~F}\) paper 350 V
Cll \(5,000 \mathrm{pF}\) paper 350 V
\(\mathrm{Cl} 250 \mu \mathrm{~F}\) electrolytic 25 V
\(\mathrm{Cl} 3 \quad 16 \mu \mathrm{~F}\) electrolytic 350 V
Cl4 \(16 \mu \mathrm{~F}\) electrolytic 350 V
\(\left.\begin{array}{ll}\text { VCI } & 500 \mathrm{pF} \\ \text { VC2 } & 500 \mathrm{pF}\end{array}\right\}\) twin-gang air variable tuner
TCl 100 pF trimmer
TC2 100 pF trimmer

\section*{Valves:}
\(\begin{array}{llll}\text { V1 } & \text { EF91 } & \text { V3 } & \text { ECL82 } \\ \text { V2 } & \text { EF91 } & \text { V4 } & 6 \times 4\end{array}\)
Diode:
GEX34 or similar
Pilot lamp:
LPI 6.3V 0.3A
Transformers:
TI Output 45:1
T2 Mains Tapped Primary. Secondaries: 250-0-250V 60.70 mA ; 6.3 V 2 A ; 6.3 V IA

\section*{Loudspeaker:}

LS \(3 \Omega ; 7 \times 4 \mathrm{in}\). elliptical
Switches:
SI 2-pole, 3-way
S2 D.P.S.T. (see VRI)
Coils:
L1, L2 Ferrite rod aerial, type FRA. 2
L3, L4 Miniature dual range, iron dust cored
Miscellaneous:
Three B7G valveholders, one B9A valveholder. Screening cans for V1 and V2. Material for chassis.

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\section*{THE BERKELEY}
(Continued from page 695) method is applicable when using "Croid" joinery glue which does enable a slight adjustment to be made before setting. lmpact adhesives are extremely powerful, but a great deal of accuracy is then needed when placing the sections together.

\section*{Loudspeaker Apertures}

Cut out the two loudspeaker apertures in the front panel and drill the holes for the fixing screws. For the main unit, drill four \(5 / 16 \mathrm{in}\). diameter holes equally spaced on a 13 in . diameter. The positions of the H.F. tweeter fixing screws are indicated on the Blueprint and a No. 10 drill (2BA clearance) should be used here. All screw holes should be countersunk on the outer surface of the panel, and enlarged on the inner surface to accommodate a box spanner; the locking nut must be flush with the panel surface, or slightly recessed, when the screw is locked in position as indicated in the inset on Fig. 1.

The removable inspection panel on one side has a \(\frac{3}{4} \mathrm{in}\). rabbet all round. The top and bottom of the opening to take this panel will need a wood fillet glued and pinned on to make up a deficiency of \(\frac{1}{i n}\). The panel is held in place by a series of \(\frac{3}{4}\) in. x No. 8 csk. screws. Provided the edges of the cover fit the opening closely it should be necessary to insert a layer of felt only on the flat of the rabbet.

The base plinth is quite simply made from 1 in . \(x 2 \mathrm{in}\). batten, screwed and glued to the eabinet as shown (see section \(\mathrm{C} / \mathrm{C}\) on Blueprint), the corners being mitred and pinned. A few glue blocks on the inside can be applied.

Glue a thicknessing piece to the insides of the top and bottom front edges to give a \(\frac{3}{4} \mathrm{in}\). finish, which is afterwards veneering in conjunction with the top.

Clean up all the cabinet edges and fill in screw holes with plastic filler.

The top and bottom edges can now be veneered with the material sclected. The edges should be carried right round the cabinet and form a slight projection to mask the edges of the "Vinyl" or "Fablon" covering on the sides. Should this method be adopted a slight adjustment is required to the inspection cover, which will be half an inch less in length.

Paint the whole of the interior and front, which will be covered by loudspeaker fabric, with flat black undercoating. Unless the front is treated in this way the loudspeaker apertures will be discernible through the fabric.
Fit the loudspeaker screws and secure with nuts as indicated in the inset on Fig. 1. The screws should be countersunk type and \(1 \frac{3}{4} \mathrm{in}\). long. Use fin. diameter screws for the main unit, and 2BA screws for the tweeter.

Make up the beading as shown in section A/A and \(B / B\) on the Blueprint. The vertical lengths are rebated to cover the edges of the side members. but the horizontal length may be left solid.
Now stain and polish, if vencered. the top, edges and beads. The plinth looks well if ebonised.

All that remains now is to cover the sides with
"Fablon" or similar material, wrapping this round the front edges, and then to apply the loudspeaker fabric. This material is glued around the edges only, to a depth of 3 in . When it is set apply the beads and finish off the wooden surfaces with a final coat of polish.

A suitable loudspeaker covering is the synthetic material sold under the trade name of "Tygan", and is available in many patterns and shades. To obtain a taut surface, the "Tygan" should be shrunk by applying heat for a few seconds. This is most conveniently performed by holding an electric fire in front of the cabinet, about six inches away from the material. Watch carefully for signs of contraction, then immediately remove the fire.

Allow 24 hours for the glue to harden before carrying out this heat treatment.

\section*{THE LUXEMBOURG TUNER}
(Continued from page 717)
another set is available (a transistor portable is ideal) is to tune the second set exactly to Luxembourg and then to beat the signal generator into it until it is precisely the same.

Without altering the signal generator setting go right through the alignment procedure detailed above and the tuner will then be spot on tune to the "Station of the Stars". It is suggested that during the alignment it is advisable to put a shorting link between the junction of C2 and C3 and chassis in order to cut out the AVC, otherwise this can make exact adjustments rather difficult. Do not forget to remove this link afterwards otherwise the AVC will be ineffective.

\section*{Alignment without Signal Generator}

If you are having to tune up without a generator it will probably take a little longer as there must be a little trial and error adjustment to
start with. If a really good aerial is available then this can be connected first to pin 1 of V2 and T3 adjusted until Luxembourg is heard, do not worry if it is not full strength or if other stations are butting in. Now transfer the aerial to pin 1 of V1 and adjust T 2 and the station should emerge at full strength and with careful adjustment the unwanted stations can be eliminated.

Whichever method of alignment is used the final adjustment should always be made on the station itself with the tuner connected up to the actual aerial it is intended to use as this can have quite a marked effect on the tuning position of the two cores in T1.

Although the writer did not carry out experiments with other types of valve as more than enough signal was always available it is interesting to note that the EF91 valve which has considerably more gain has exactly the same base and connections and could possibly be substituted if desired although since this is not variable \(-\mu\) the AVC circuit would not be effective.


\section*{HI-FI FANATIC}

SIR,-I recently visited a home of an acquaintance of mine who has a fine collection of classical L.P. records and an elaborate hi-fi system, consisting of a separate amplifier, pre-amplifier, record player and loudspeakers. I'm not a great fan of the classics myself, but as he was so enthusiastic in explaining his equipment, I thought it only polite to ask to hear one of his records. This I did and it was obvious that he was delighted. He then told me to choose a record from his collection.

Simple enough, I thought, but it was at this point that I made my big mistake. In my enthusiasm to get the ordeal over with, I had taken both the inner and outer covers of the record off and was turning it over in my hands to choose the side I wanted, before my friend could stop me. The first I knew of my mistake was when my friend grabbed the record from me and started to inspect it closely for any marks or scratches. After a moment or so, it began to dawn on me what I thad done. In my innocence I had placed my fingers over the groove!

After many apologies from me and reprimands from my friend, he agreed to go on with the performance. Inside another 20 minutes he had finished making adjustments to the pick-up arm, the tone controls, the loudspeaker positions, cleaning the stylus etc, and then, and only then, could we hear the record.

I have heard about these record fanatics but I never before really believed that anyone could be so concerned about the welfare of something costing only 30 s. to \(£ 2\), and I count myself lucky to be able to listen to my cheap record player without worrying about how much dust is collecting under the stylus. - D. R. Davenport (Doncaster).

\section*{ELECTRONIC GAMES}

SIR,-You recently asked to hear from readers who have had experience of electronic games. I have designed such a game recently which is played to test a person's ability to recognise aircraft. The unit will be on show at the Schoolboy's Exhibition at Olympia on the Royal Air Force stand.

It consists of 18 transparencies of different aireraft and parts of aircraft which flash on individually for time periods varying from five to twenty seconds (this was achieved by using a modified P.W. circuit). On the control panel there are 18 buttons with 18 captions by the side of them, and a scoreboard registering the number of aircraft the player has recognised correctly.

The operator. gets a visual warning to tell him how long he has before the sequence begins.
The master timing circuit operates a uniselector having 25 circuits, out of which 18 are used for the selection of the transparencies. The other
seven are used to return the score to zero, to operate a warning as to the time left before the sequence starts and also to tell the player whether he is average, good or excellent at recognising aircraft.

In this unit, I used 59 relays, 58 of which were normal GPO type 3,000 and the other was a highspeed, dual coil type. Twenty-eight of the 58 ordinary relays were needed in order that the score could operate automatically. Eighteen were used for the transparencies, and the others used for a bell and several " anti-fiddle " circuits.-CPL. Edwards (R.A.F. Hendon).

\section*{RECEPTION ON THE CONTINENT}

SIR,-Early next year I am taking my holiday in
France and I was wondering what success I could expect of receiving British programmes on my car radio. This year, when I stayed at a hotel in France, I greatly missed hearing the Home and Light programmes, as the hotel's radio was always tuned to Continental stations. I wonder if any of your readers could tell me what the quality of reception would be.-A. A. Chilton (Cardiff).

\section*{R.I481 RECEIVER}

SIR,-I have recently been given an old R. 1481 receiver and would very much like to receive any details on the power supply and circuit of this set, from any reader who owns one.-C. Shingsley (Burgess Hill, Sussex).

\section*{CORRECTIONS}

THE TUDOR BATTERY SUPERHET. The 2-gang tuning capacitor VC1, VC2, should be Jackson type 02, not "type L'" as stated in the Components List on page 437 of the September issue.
THE STRAND AMPLIFIER. There is a wiring error on the Blueprint enclosed in the October issue. The heater wire of V2 (ECC83) as shown in Figs. 1a and 2 must be amended as follows: Connect together pins 4 and 5. Connect the \(6 \cdot 3 \mathrm{~V}\) supply to pin 4 (or 5 ) and to pin 9 .

Also note that in Fig. 2 pins 2 and 7 of V1 should be shown connected to the valveholder spigot, as described in the article on page 507. THE TROUBADOUR. Transistor types should read: Trl OC44; Tr2 OC45; Tr3 OC45, and not as given in Fig. 1 and in the Components List of the Blueprint (June 1962 issue).
THE P.W. SIGNAL GENERATOR. The following amendment should be made to the Components List on the Blueprint (October 1962 issue): L4 QHF8, L5 QHF9.

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 Club News \\ 
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\section*{REPORTS OF CURRENT ACTIVITIES}

\section*{AMATEUR RADIO SOCIETY OF CHESHAM AND DISTRICT}

Hon.Sec.: Capt. C. G. Stephenson, G3CL J/T, 21 Lynton Road, Chesham, Buckinghamshire.

At the moment, many of the society's members are spending their time improving their headquarters. However, morse and practical classes continue to be held each Tuesday, and on Fridays, RAE lectures are given.

CLIFTON AMATEUR RADIO SOCIETY
Hon. Sec.: C. Godsmark, G3IWL, 211 Manwood Road, London, S.E.4.
At the society's recent AGM, W. Martin was elected chairman, C. Godsmark secretary and N . Moore treasurer.

On October 5th, G3HWG gave a lecture on 'Oscilloscopes" and also demonstrated some of their uses.
DERBY AND DISTRICT AMATEUR RADIO SOCIETY
Hon. Sec.: F. C. Ward, G2CVV, 5 Uplands Avenue, Littleover, Derby.
A surplus sale was held on the first meeting in October and on 10th, "Technical Forum" was the topic for the evening.
On October 17th members enjoyed a film show and on November 3rd a number of members visited the R.S.G.B.'s exhibition in London.

\section*{DUDLEY AMATEUR RADIO CLUB}

Hon. Sec.: D, H. W. Pratt, G3MHS, 23 Kent Street, Upper Gornal, Dudley, Worcestershire.

The Annual General Meeting of this Club was held on October 12th. On 26th of the same month members attended a demonstration and talk by the Wolverhampton Model Radio Control Society.

\section*{LOTHIANS RADIO SOCIETY}

Hon. Sec.: G. Ritchie, c/o Cormie, 15 Rosslyn Terrace, Edinburgh 6.
"Monkey Glands for the HRO' was the title of the talk given on October Ilth by GM3PQU, who also gave a demonstration of TVI proofing. Visitors from the South Lanark, Fife and Falkirk groups who attended the meeting on October 25 th , were entertained with film show.
Future Events:
November 8th-"Some Aspects of Transistors" by Dr. C. Davidson.
November 22nd-A surplus sale.

\section*{MITCHAM AND DISTRICT RADIO SOCIETY}

Hon. Sec.: M. Pharaoh, G3LCH, I Madeira Road, Mitcham. A talk on R.F. heating and its uses was given by B. Ayrlwood at the meeting on October 5th and at the following meeting on 19th, VQ4EV presented a film show.
Future Event:
November 16th-"Why be Afraid of Transistors?" by G8TB.
MELTON MOWBRAY AMATEUR RADIO SOCIETY
Hon. Soc.: D. W. Lilet, G3FDF, 23 Melton Road, Asfordby Hill, Melton Mowbray, Leicestershire.

At the meeting on October 18th members listened to a recorded lecture on transmitter design and TVI by N. Shires.

NORTHERN HEIGHTS AMATEUR RADIO SOCIETY
Hon. Sec.: A. Bobinson, G3MDW, Candy Cabin, Ogden, Halifax, Yorkshire.

Members operated a station during this year's Scout Jamboree on the Air, under the call-sign G3MVH. On October 23rd, members travelled to Bradford to attend the film show given at St . George's Hall.

For the first meeting in November, G3FQH gave a lecture on single side band.

\section*{SHEFFIELD AMATEUR RADIO CLUB}

Hon. Sec.: D. R. A. Hill, 16 Tylney Road, Sheffield 2, Yorkshire.

The energy of many members at the moment is being expended on the task of furnishing the club's headquarters. The all-band transmitter and aerials also claim important places in the club's present programme.

In spite of all this work, many members are continuing to attend both the technical and general meetings and the novices \(f \| l a s s e s\) are carrying on successfully with morse classes held on alternate Wednesdays.

\section*{SLADE RADIO SOCIETY}

Hon. Sec.: C. N. Smart, 110 Woolmore Road, Erdington, Birmingham 23.

On October 19th, the club secretary gave a comprehensive lecture on a new transistorised D.F. receiver, and on 31st of that month members attended the Annual Dinner.

\section*{SPEN VALLEY AMATEUR RADIO SOCIETY}

Hon. Sec.: L. A. Metcalfe, IA Moorlands Road, Birkenshaw, Bradford, Yorkshire.

October proved to be a busy month for this society, starting with a talk called "Language of S.S.B." on 4th. A lecture called "Noise Problems' was given on 18th and later in the month members attended a film show.
The first meeting in November was devoted to "Tape Recor" ders".

\section*{STRATFORD-UPON-AVON AND DISTRICT AMATEUR RADIO CLUB}

Hon. Sec:: P. Robinson, G3MG J, 43 Loxley Road, Stratford-upon-Avon, Warwickshire.
To meet the May 1963 R.A.E., a series of lectures has been started dealing with radio theory.
The lectures for the two last meetings have been given by John Hewitt, G3MDU, and his subjects included alternating eulrent and voltage, alternating current with inductance, etc.
Future Event:
November 9 th-Coupled circuits, acceptors and rejector circuits, by M. Webb.

\section*{\(\star\)}

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\section*{ABSORPTION WATTMETER}
(Continued from page 719)
tiometer, but a reversing switch must be included and a reading obtained with the voltage applied to the wattmeter both "forward and reverse". The average of these is the "correct" meter reading. (This procedure takes account of differences in diode forward resistance.)

The voltage developed across 3 and \(15 \Omega\) resistors for the 5 and 20 W ranges have been calculated and are given in Table 1. The first step in the calibration process is to set the variable resistor controlling lincarity (VR5). Having adjusted VR5 for zero resistance, set the D.C. voltage applied to the wattmeter to 8.66 volts. Switch the wattmeter to measure 5 W at 1592 and adjust VR3 until the meter reads full scale. Then reduce the D.C. voltage to 7.75 volts and note wattmeter reading, and so on down column 5 of Table 1. When the linearity control is correctly adjusted, the results obtained should be similar to those given in Table 2. If the readings obtained are lower than these, set RV5 (linearity) to its mid-position and re-adjust RV3. Repeat the comparison of meter readings and applied voltage.
If the readings are still low then RV5 must be gither increased, whilst if the readings are high,解V5 must be reduced in value. This procedure may sound complex but in practice it takes but about 10 minutes.

When the linearity control has been set, the table of applied voltage against meter reading should be put to one side as this is required for absolute calibration of the meter. This may be

Table 2
\begin{tabular}{|c|c|}
\hline Voltage & Meter Reading \\
\hline 8.66 & 1 \\
7.75 & 0.81 \\
6.7 & 0.61 \\
5.5 & 0.40 \\
3.87 & 0.19 \\
2.74 & 0.09 \\
\hline & 0 \\
\hline
\end{tabular}
done by drawing a calibration curve or alternatively, the scale can be removed from the meter and re-calibrated by hand. This latter method is preferable, but can result in a very "messy" looking job if great care is not taken.

Table 3
\begin{tabular}{|c|c|c|c|}
\hline \multicolumn{4}{|c|}{\(7.5 \Omega\)} \\
\hline Voltage & Power & Voltage & Power \\
\hline 6.12 & 5 & 12.25 & 20 \\
5.5 & 4 & 10.95 & 16 \\
4.74 & 3 & 9.5 & 12 \\
3.87 & 2 & 7.75 & 8 \\
2.74 & 1 & 5.48 & 4 \\
1.94 & 0.5 & 3.87 & 2 \\
\hline
\end{tabular}
\begin{tabular}{|c|c|}
\hline \multicolumn{2}{|r|}{COMPONENTS LIST} \\
\hline \[
\begin{aligned}
& R 1 \\
& R \mid A \\
& R 2
\end{aligned}
\] & \[
\left.\begin{array}{l}
3 \Omega \\
47 \Omega \\
15 \Omega
\end{array}\right\} \text { See text for power rating }
\] \\
\hline \[
\begin{aligned}
& \text { R3 } \\
& \text { R4 } \\
& \text { R5 } \\
& \text { R6 }
\end{aligned}
\] & \[
\left.\begin{array}{l}
150 \Omega \\
330 \Omega \\
330 \Omega \\
820 \Omega
\end{array}\right\} 20 \%, \frac{1}{4} W \text { carbon }
\] \\
\hline VRI-4 & \(100 \Omega\) wire-wound potentiometers \\
\hline VR5 & \(250 \Omega\) wire-wound potentiometer \\
\hline \multicolumn{2}{|l|}{MRI-4 OA70 (Mullard)} \\
\hline MI & Meter, moving coil, \(0-1 \mathrm{~mA}\) f.s.d. \\
\hline SWI & Switch 3-pole, 2-way \\
\hline SW2 & Switch 4-pole, 2-way \\
\hline
\end{tabular}

The only job remaining now is to set the remaining range potentiometers as follows:

1 Set the meter to measure 5 W at \(3 \Omega\), apply a voltage of 3.87 volts and adjust RV1 for full scale deflection.
2 Sct the meter to measure 20 W at \(3 \Omega\), apply a voltage of 7.75 volts and adjust RV2 for full scale deflection.
3 Set the meter to measure 20W at \(15 \Omega\), apply a voltage of 17.32 volts and adjust RV4 for full scale deffection.
The lead to SW1A should now bc reconnected and the wattmeter is completed.

\section*{Additional Ranges}

If additional or alternative ranges are required it is quite simple to add or substitute these. In Table 3 are given voltages appropriate to 5 and 20 W ranges for \(7 \cdot 5 \Omega\) load.

FRIDAY, FEBRUARY Ist, 1963

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Sub Min. Solid Dilectric Size \(7^{* *}\) square \(x\) \(7 / 16^{\prime \prime}\) deep. Cap 192pF Aerial 78pF osc. TRIMMERS FITTED 1716 each.

\section*{J.B. DILEMIN CONDENSER}

Solid Dilectric available in 300 pF or 500 pF , 716 each.
Send for our Price Lists on Mini Amp Tutor, etc. etc.


COIL SET (OSC. and 3 I.F.s)
DRIVER TRANSFORMER.
Type PW/DT
OUTPUT TRANSFORMER.
Type PW/OT. \(\qquad\) 8/.
FERRITE ROD AERIAL.
Type PW/FR
816
2-GANG CAPACITOR. Type "OO"
VOLUME CONTROL, EGEN IOK. S/P/ SWITCH
SWITCH
TRANSISTOR Type Y.C. (set of
six) …................................-- \(\}\)
XTAL DIODE Type GD9.
SPEAKER
SPEAKER
431.

CASE complete with hande, front
grille, studs
22/5

CAPACITORS
\(25 \%\)
RESISTORS
1716
TRIMMERS TyPe MT 31/4A 1/3 - 318
PRINTED CIRCUIT BOARD - 14/6
COMPLETE DIAL ASSEMBLY (BOXED)
\(14 / 6\)
HARDWARE (Screws, Nuts,
Washers, Spacers, Battery Clips,
Aerial Cradle
519
\(\begin{array}{lll} & \text { Postage and Packing } & 2 / 6 \\ \text { INSTRUCTION HANDBOOK } & 2 / 6\end{array}\)

\section*{TRANSISTORS AND DIODES}

Transistors
\(0 \mathrm{OC35}\) 181.
\(\begin{array}{cc}O C 36 & 2116 \\ \text { OC44 } & 61\end{array}\)
\(\begin{array}{ll}O C 45 & 6 / 6 \\ O C 70 & 6 / 6\end{array}\)
\(\begin{array}{ll}\text { OC70 } & 6 / 6 \\ \text { OC71 } & 5 \%\end{array}\)
OC72 8\%
OC73 161.
\begin{tabular}{lr} 
OC75 & 81 \\
OC77 & 121 \\
OC78 & 81. \\
OC81 & 81. \\
OC84 & 816 \\
OC170 & 916 \\
OC171 & 1016 \\
OC201 & \(31 /\) \\
OC202 & 261.
\end{tabular}

A set of Transistors comprising 1 OC44, 2 OC45, 1 OC8ID, 2 OC8I, \(32 / 6\) set.
Set of Audio Transistors, I \(\times\) OC8I, \(2 \times 0 \mathrm{O} 8\) I, Driver Marched Pair, \(15 / 6\) ser

TERMS : Cash with Order or C.O.D. Postage and Packing Charges extra. Single valves \(9 \mathrm{~d} .\), Minimum Parcel Post charges \(2 \%\). Please include sufficient postage with your order. Minimum C.O.D. fees and postage 3/6. These Postal Rates apply to U.K. only. For full terms of businass see inside cover of catalogue. Personal shoppers \(9 \mathrm{a} . \mathrm{m}\). to \(5 \mathrm{p} . \mathrm{m}\). Mon. to Friday, Saturday 10 am . to I p.m.


A lst class Signal Generator covering \(200 \mathrm{Kc} / \mathrm{s}\) to \(200 \mathrm{Mc} / \mathrm{s}\) in 8 ranges．Radio broadcasts and I．F．，Amateur，VHF， Shipping，TV，etc．R．F．，I．F．，A．F．，modu： lated R．F．outputs．Easy to read and use with full details．Within \(2 \%\) accuracy． Size \(6 \frac{5}{⿳ 亠 丷 厂 彡} \times 4 \frac{5}{6} \times 2 \mathrm{in}\) ．
12 MONTHS＇GUARANTEE Leaflet on request

\section*{TAPE HEAD}

Miniature \(\frac{1}{2}\) Track
Record／Playback Head with Mounting Block． 850 ohm．

12／6，P．P．9d．

\section*{TAPE RECORDER MOTOR} Miniature Motor designed for Bat－ tery Recorders， \(4 \frac{1}{2}\) to 9 volts．Buite in governor， \(12 / 6\). P．P．II－．

\section*{＂TRANSFIVE＂ PORTABLE RADIO}


A simple to build 5－Transistor and Diode． Printed Circuit，Medium and Long Wave Portable．Features Sin．speaker，Car Portable． carded components．Building plans free on request．THE IDEAL PORTABLE Full after sales service and guarantee． （See Back Cover for other types．）

\section*{VERNIER DIAL}

New Miniature Slow Motion Vernier New 8 to I reduction．Marked \(0 / 100\) Ideal for all test equipment，14\％．
\(3 / 4 \mathrm{WATT} 4\) TRANSISTOR
AMPLIFIER

A printed circuit high gain amplifier size \(4 \times 2 \frac{7}{4} \times \frac{3}{3}\) in．using Mullard OC7I／OC8ID and \(2-0 \mathrm{C} 1\) Transistors．Ideal for Inter－ comm．，Record Player，Tuner Amplifier or any application requiring a quality and reliable amplifier．Suitable large magnet 5 －inch speaker， 15 ／．．

\section*{CATALOGUE}

New Edition Now Ready．Three times the size，full of compo－ nents and items．
Send \(1 /\)－stamp for your copy．
GUITAR CONTACT MICRO－ PHONE．High Impedance Guitar Contact Microphone with screened lead． Plugs into any valve amplifier．very sensitive．12／6．P．P．9d．

\section*{TEST LEAD KIT}

Complete set of test leads．Suitable for mosi instruments．Complete with pouch， 8／6．P．P．\({ }^{1 /-}\)－

\section*{POCKET RADIO BOOSTER}

Tubular unit，size \(9 \frac{1}{2} \times 3 \frac{1}{2} \mathrm{in}\) ．dia．，which plugs into earphone socket of any transistor radio．Performance increase is fantastic．Ideal for home or car． 52／6．P．P．｜／6．

\section*{PERSONAL EARPHONES ＊ 600 ohm． 1016 t Crystal \(\star 1,000 \mathrm{ohm} .1216\) 太 \(8 / 10\) ohm． 916} Fitted leads，Jack Plug and Socket．

\section*{SOLDERING IRON}

Antex miniature 15 watt \(220 / 250\) volt Iron．Easily removed \(\frac{3}{3}\) in．bic．Ideal for all miniature work，29／6．Spare bits，five sizes to \(\frac{1}{4} \mathrm{in} ., 3 \%\) each．
\begin{tabular}{llllr}
\hline CRYSTAL & ACOS 2 in. &.. & \(\ldots\) & 1016 \\
MIC． & ACOS \(1 \frac{1}{2} i n . .\). & \(\ldots\) & 716 \\
INSERTS & \(\frac{3}{4}\) in．sq．．．． &... & \(\ldots\) & 316 \\
\hline
\end{tabular}

TYPE 38，TRANSMITTER RECEIVER Complete with 5 valves．In new condi－ tion．These sets are sold without guarantee but are service－ 2216 P．P． able． 7.4 to \(9 \mathrm{Mc} / \mathrm{s}\) ．
Headphones \(7 / 6\) pair．Junction Box \(2 / 6\) Throat Mike 4／6．Aerial Rod \(2 / 6\).

\section*{TELEPHONE ADAPTOR}
t Ideal for recording or amplifying telephone conversations．Supplied with screened cable．Fitced rubber sucker， 14\％．

MARCONI 19 SET
CRYSTAL CONTROLLED CALIBRATOR
Crystal controlled osciliators giving either \(10 \mathrm{kc} / \mathrm{s}, 100 \mathrm{kc} / \mathrm{s}\) or \(1 \mathrm{Mc} / \mathrm{s}\) pips．Features neon modulator，supplied with spare valves and full handbook． 7916 P．P．

Ideal standard frequency check．
TRANSISTOR PORTABLE TAPE RECORDER


Fully Guaranteed
Supplied complete with microphone，tape， batteries and personal phone（for moni－ toring），and full instructions．New 4 transistor version with push－pull output， better quality，more attractive case，etc

The Above are FULLY ASSEMBLED TESTED and GUARANTEED．


A ready built miniature 250 mW push－pull amplifier incorporating input and output transformers， 4 transistors， 9 volt battery snap cord，speaker and column connec－ tion leads．Ideal for use with record players，intercoms，hearing aids，tape players，intercoms，
recorders，etc．Complete with full instruetions and circuit diagram．
\[
\text { PRICE } 52 / 6 \quad \text { P.P. } 116
\]

SUITABLE \(2 \frac{1}{2} \mathrm{in}\) ．SPEAKER 1616.

\section*{BATTERY RECORD}

PLAYER
6－7t volt Garrard turntable with crystal pick－up．Plays 45 r．p．m． Ideal for above amplifier．
\(55 /=\) P．P． 116
－Suitable cabinet for amplifier and player． 17／6．P．P．2／－．
LIGHTWEIGHT HEADPHONES

\(\star 2000\) OHMS \(12^{\prime 6}\)
＊ 4000 OHMS
1416
HIGH EFFICIENCY．

\section*{MINIATURE CLEAR FACED} Brand New PANEL METERS 0－50 microamp DC
．．．．．． 3916 0－50 microamp DC ．．．
 \(\begin{array}{llllll}0-1 \\ 0-1 & \text { milliamp } & D C & . . . & \ldots & \ldots . \\ 0-516 \\ 0-3 & \text { n } & \text { DC } & \ldots & \ldots & \ldots \\ 2716\end{array}\) \(0-300\) volts DC ＂S＂meter ImA
 ．．． ．．． \(27 / 6\)
 ．．．
．．． 4216

\section*{CRYSTAL MICROPHONES}

ACOS 39－1．Stick Microphone with screened cable and stand（list 5 gns．）， 3216．P．P． 116.
ACOS 40．Desk Microphone with screened cable and built－in stand（list \(50 \%\)－）， \(15 \%\) ．P．P． 116.
ACOS 45．Hand Microphone with sereened lead，very sensitive，25／－．P．P． \(1 / 6\). 100 C ．Stick Microphone with muting switch and screened cable，detachable desk stand，cord and neck，39／6．P．P．I／6． MC 24．Stick Mierophone with muting switch and cable，25／－．P．P． \(1 / 6\).
LAPEL．Miniature Mic．With clip．Ideal for recording， 151 ．．P．P．I／－．
BM 3．De Luxe Stick Mic．，with muting switch cable，neckcord and detachable stand．Complete 52／6．P．P． \(2^{1 /}\) ．
（IIlustrations of all types in our New Cata－ logue．I／－post free）．

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PREE TRANSIT INSURANCE, All Falven guaranteed or of fully ment or ex-equipment origin. Satisfaction or Money back Guarantea on Goods if returned un-
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Cart. \& Ins, 19/0
MOST mULLARD MAZDA, COSSOR. EMITRON, EMI-
SCOPE, BRIMAR PERRANTI TYPES PROCESSED IN OUR OWN PACTORY

RUN YOUR RADIO FROM MAINS BATTERY ELIMINATORS AND CHARGERS
1. For PP3 or equivalent 9 volt Pocket Radio Battery. 1816. P.P. 11-.
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2,000 ohms per volt AC/DC. Size \(5 \times 3 \frac{1}{2} \times 1 \frac{1}{1}\) in. \(751-\) Fully Guaranteed with test leads, battery and instructions.
0/10/50/250/500/1000 volts D.C., \(0 / 10 / 50 / 250 / 500 / 1000\) volts
\(0 / 500 \mu \mathrm{~A} / 10 / 250 \mathrm{~mA}, \mathrm{D} . \mathrm{C}\)
\(0 / 500 \mu \mathrm{~A} / 10 / 250 \mathrm{~mA}, \mathrm{D} . \mathrm{C} / 100 \mathrm{~K} / 1 \mathrm{Meg}\). 3 ranges resistance
Capacity and dB ranges.


MODEL
500

30,000
ohms
per volt
multi-
meter
£8.19.6

Fully
Guaranteed
8 Ranges D.C. volts to 1 kV . 7 Ranges A.C. volts to 1 kV . 5 Ranges D.C. current to 12 amps . 3 Range resistance to 60 meg . Short circuit, Buzz test. Output meter dB , etc., etc. Size \(6 \frac{1}{4} \times 4 \frac{1}{2} \times 2 \frac{1}{4} \mathrm{in}\). With Leads. Batteries and Instructions.


MODEL TP5S
A.C./D.C. voltageuptp 1,000 in 5 ranges. D.C. current
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to 500 mA .4 range resistance to 10 megs. Capacity dB scales, etc. scales,
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ohms/volt Fully Guaranteed
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With Test Leads, Battery and Instructions. Size \(5 \frac{1}{4} \times 3 \frac{1}{2} \times 1 \frac{3}{4} i n\).

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Limited Quantity of these Superb Multi-testers, new conditions and fully guaranteed.
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We stock the largest range in the Country of Transistors and Miniature Components for the home constructor. New Catalogue II.

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 \(\times\) KA102 61. XA703 25\% XCI21 6\%. \(\times\) XAl03 4/- Power types XCI31 10\% \(\times\) XA104 4I XCl4I \(10 \%\) \(\begin{array}{ll}\text { XBIO2 } & 4!- \\ \times B 112 & 4 I_{-} \\ \times \text {Pairs }\end{array}\) \(\begin{array}{llllll}\text { XBIII } & 4 /- & 12 \mathrm{w} & 22 / 6 & \times C 171 & 10 \% \\ \times B 113 & 4 / 6 & 12\end{array}\) \(\begin{array}{llllll}\times B 113 & 416 \\ \times B 121 & 816 & \times C 156 & 2216 & \times C 163 & 71 . \\ \times 16\end{array}\) NPN types Pairs \(\times 5104 \quad 716\) \(\times 2701{ }^{2 \%} 50 \mathrm{w}\) 50\% XS101 10\% Many Others in Stock.
Complete range of over 400 Transistors and Diodes now available. Latest list on request with equivalents.
SPECIAL-Very Low Prices for Matched Sets from 2916 to \(32 / 6\).

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MORE TYPES-LOWER PRICES
GEIGER MULLER TUBES
Mullard Type \(M X I I 5,400\) volts. Gamma sensitive type. 2216. P.P. I/6.
OFFICE, WORKS or HOME USE

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INTERCOMM. SYSTEMS
* 2-transistor transformer coupled, two speakers in moulded cabinets. Features 2-way Buzzer system and talking. Supplied complete with cable 8916 and batteries.
P.P. I16
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P.P. \(2^{\prime /}\) batteries.

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Now stethoscope type stereo earphones with adjustable cubes. Fitted miniature jack plugs and leads. \(2 \times 8\) ohms impedance, 27/6.

\section*{STEREO AMPLIFIER}

4-Valve Amplifier with 2 watts output per channel to 30 ohms. Ready built, complete with Dials, Sockets and Knobs. Full tone, volume and balance controls. Crystal Input. 220/250 volt mains input.

Fully
7916
P.P. \(2^{f}=\)

Guaranteed
PRACTICAL TRANSISTOR
CIRCUITS 316 (Post Free)
Contains easy to follow plan of 40 all transistor units, including light operated switches, amplifiers, transmitters, receivers, test oscillators, signal tracers, hearing aids, radio control, etc. All parts available separately.

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Send IV. Stamp for New Triple Size Catalogue

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HOUSED IN ATTRACTIVE GOLD HAMMER FINISH PORTABLE CABINET. Battery operated, push-pull, 400 MW output. Low impedance microphone enables unit to be used up to 200 yards. Output on quality speaker.
* GUARANTEED for 12 MONTHS and \(100 \%\) SAFE.
\(\star\) MICROPHONE is placed within lOft. of baby; twin flex is taken to amplifier unit and placed in any room required. COMPLETELY BUILT 55.10 .0 \& TESTED. P.P. \(2^{\prime 6}\).
\(\star\) Used All Night, Every Night. Battery Life 3 to 4 months.
Also Telephone Amplifier (as previously advertised).
45.10.0 P.P. 216


\section*{MODEL PT34}


1,000 ohms per volt 4916 Fully
\(0 / 10 / 50 / 250 / 500 / 1000\) voles on A.C.
0/1/100 mA. O/500 mA D.C.
\(0 / 100 \mathrm{k}\) ohm resistance.
Complete with Leads, Battery and Instructions.


\section*{MODEL}

ITI-2 (200H)
20,000 ohms
per volt.
f5.5.0
Size \(4 \frac{1}{2} \times 3 t \times \frac{13}{18} \mathrm{in}\). With Test Leads, Battery and Instructions.
6 Ranges D.C. voltage to \(2 \frac{1}{2} \mathrm{kV}\).
5 Ranges A.C. voltage to 1 kV .
3 Ranges D.C. current to 250 mA .
Resistance to 6 meg .
Capacity and dB ranges.

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Famous Muitimeter, reconditioned and and fully guaranteed. Full A.C./D.C. voltage and current, resiscance, dB, power, ete. etc.


Supplied with Batteries, Leads and Instructions. (Normal price \(£ \mid 9.10 .0\) )
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LEATHER CASES FOR "AVO-7," 25/- extra.
ALL METERS FULLY
GUARANTEED for 6 MONTHS

\section*{Practical Wireless}

\section*{SERVICE}


AL OF these blueprints are drawn full-size and although the issues containing descriptions of these sets are now out of print, constructional datails are available free with each blueprint except for the PW Monophonic Electronic Organ and the PW Roadfarer.
The Index letters which precede the Blueprint Number indicate the periodical in which the description appeared. Thus PW refers to PRACTICAL WIRELESS; AW to Ampteur Wireless and WM to Wireless Magazine.
Send (preferably) a postal order to cover the cost of the Blueprint (stamps over 6d. unacceptable) to

PRACTICAL WIRELESS, Blueprint Dept., George Newnes, Ltd., Tower House, Southampton Street, London W.C.2.

\section*{SPECIAL NOTE}

THE following blueprints include some pre-war designs and are kept in circulation for those constructors who wish to make use of old components which they may have in their spares box. The majority of the components for these receivers are no longer stocked by retailers.
\begin{tabular}{lllr}
\multicolumn{2}{c}{ Title } & \multicolumn{2}{c}{ Number }
\end{tabular} Price

The PW 3-speed Autogram .. -
The PW Monophonic Electronic Organ

Title Number Price

\section*{CRYSTAL SETS}
\(\begin{array}{llll}\text { Junior Crystal Set . . . . } & \text { PW94 } & \text { 2/- } \\ \text { Dual-wave Crystal Diode } & \text {.. } & \text { PW95 } & 2 / 6\end{array}\)

\section*{STRAIGHT SETS \\ Battery Operated}

Modern One-valver .. . PW96 2/6
All-dry Three .. .. .. PW97
Modern Two-valver .. .. PW98

\section*{SUPERHETS}
A.C. Band-pass Three .. .. PW99 4/-
A.C. Coronct-4 .. .. .. PW100
A.C. D.C. Coronet .. .. PW101

The PW Pocket Superhet . .

\section*{MISCELLANEOUS}
(1n constructional details are available with this bheprime)
The PW Roadfarer
( Ao constructional cletails are available with this blueprint)

\section*{TELEVISION}

The PT Biad III converter

1/6
8-
-

\section*{PROVE IT YOURSELF! \\ SEE HOW EASY IT IS TO BUILD ONE OF OUR DESIGNS}

FULL DETAILS OF ANY MODEL ON REQUEST-WRITE NOW
THE

\section*{FABULOUS}

\section*{"CONTESSA"}

Mk. III
combined portable and car radio

6 WITH 600 mW MELLOWTONE OUTPUT on medium and long waves.
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ALE

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GUARANTEED THE VERY BEST
OBTAINABLE
* All parts sold separately

> TOTAL COST \(£ \mid 0.19 .6\) Р.P. \({ }^{16}\)

The New "CONTESSA" 6-Transistor Portable Superhet Radio features simple printed circuit construction and fully illustrated building instructions, with all parts clearly marked and identified. Fitted with 8 inch Ferrite Aerial, double IFT's and the latest in components and design. Full tuning of both Medium and Long Wave Bands with unbeatable, Selectivity and Sensitivity. Clearly marked station dial and room filling "MELLOWTONE" push-pull output are standard features. Performance is guaranteed to be better than any other design available to the home constructor whecher used at home, out and about, or in a car.

FULL AFTER SALES SERVICE AND GUARANTEE

NEW HUGE PURCHASE
REDUCES TOTAL COST
"CAPRI" POCKET-6
6-TRANSISTOR SUPERHET


Size only
\(4 \frac{1}{\frac{1}{2}} \times 2 \frac{1}{4} \times 1 \frac{1}{4}\) REALLY
POCKET
SIZE!
Themost compact 6 transistor and diode radio with speaker available to the home constructor. Features the latest in miniature components and circuitry. Supplied with Mullard transistors and two-tone moulded cabinets in red/white or blue/white with gold fictings. All components are supplied in packets and clearly identified. A printed circuit is used with fully illustrated building instructions. Push-pull output coupled with a sensitive and selective circuit make the "CAPRI" hard to beat. Fisted Earphone Record socker. Full tuning on medium waves with long wave Light

TOTAL
COST .19.6
P.P. 2/-
- Detailed Leaflet on Request After Sales Service and Guarantee 3-TRANSISTOR SUB-MINIATURE AMPLIFIER
New 3-transistor amplifier. 125 mW push-pull output to 35 ohm speaker. PP3 9 -volt operated.
* Size only \(1.9 \times 1 \times 1\) inches! Complete with circuit. \(45 /=\) P.P. Suitable \(2 \frac{1}{4} \mathrm{in}\). Speaker, 15

\section*{"QUINTET"}

MEDIUM AND LONG WAVE POCKET RADIO
PUSH-PULL SPEAKER OUTPUT

Red or Blue
with Gold
trim.
Total Cost
99/6 р.P. 2'-


A Five-Transistor and Diode 7-stage medium and long wave printed circuit loudspeaker radio. Features lst grade transistors and plainly marked printed circuit with carded components. Excellent results with full station separation guaranteed. Including Radio Luxembourg, Pushpull output up to 200 mW . Fitted 'Phone/ Record soçket and Car aerial socket. Full after sales service and guarantee.


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THREE PAGES of ITEMS

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Size only \(3 \times 2 \times \frac{3}{4}\) in.

Three
transistors
Two
diodes
A new printed elrcuir 5-stage personal pocket radio fully tunable on

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TOTAL \(59 / 6\)
COST
P.P. 116
- Building Instructions Free
"RANGER 3" A Three-Transistor Size \(4 \frac{3}{4} \times 3 \times 1 \frac{1}{4} i n\). Two-Diode Personal Radio for Medium Waves and Amateur top band and shipping. Quality output on personal phone. Fitted air spaced tuner, vol. control. No aerial or earth. Luxembourg guaranteed.
\(59 / 6\) P.P. Easy to follow illustrated 1i6 building plans Free on request.

We can supply most of the components specified on circuits published in this and other magazines and books. Let us quote for your circuit. Competitive Prices.```


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