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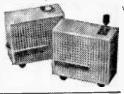
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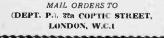
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| 0 mA. 1 | 0 H 200 | ohms | | | 8 | \$19 |
| mA, 10 | | | | | 5 | 5/9 |
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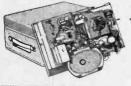
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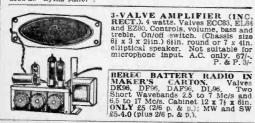
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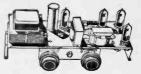


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This chassis is an ideal partner for the radiogram cabinet appearing on this page

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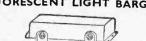


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- Tuning condensers for items 2 and 4, 10/6. 22.
- 23. Printed circuit for items 1 and 6/6.
- Printed circuit for items 2 and 4, 7/6. 24.
- 25. 2%in, speaker, 3 ohm, 19/6; 80 ohm. 19/6. 26. 3in. speaker, 3 ohm, 18/6; 80 ohm.
- 18/6. 27.
- Sin. speaker, 3 ohm. 18/6: 35 ohm Hi flux, 19/6: 35 ohm Super Hi flux, 22/6. 28.
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- 29. Battery connectors. la pair; miniature. 1/- pair. large, 1/-



Circuit comprises 2 HF transistors reflexed to equal 4 stages. Permanent germanium diode and high gain AF output stage, fitted with miniature speaker, proper tuning condenser, yourne control and in case with handles as illustrated (less monogram), completely portable. No aerial or earth required. Pocket 4 uses 3 transistors and 1 diode, price 42/6, plus 2/6 post and insurance. Pocket 5 uses 4 transistors and 1 diode and has feedback control, price 55/, plus 2/6 post and insurance. Prices are for medium wave models, long or medium versions 8/6 extra.

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approximately—or aerai attachment—several inclusify operation inclusify determined only 3/6. Circuit employs six transistors and two diodes, it incorporates all latest refinements, and oscillator I.F. Transformers are pre-aligned so no instruments are necessary. Anyone who can solder competently can make this set. The instructions are fully comprehensive with plenty of illustrations. Service is available in the unlikely event of your getting into difficulties. All components fully guaranteed.

Price of all components and cabinet to make set as illustrated £9.19.6. Post and insurance 5/-. Battery 3/6 extra.

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December, 1961



ractical Wireless

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VOL. XXXVII No. 658 DECEMBER, 1961

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HALEAN MALLEN

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THE P.W. 'CITIZEN'

WO months ago, in our October issue, we presented a Blueprint, free with every copy, designed to introduce the newcomer to radio construction to the simplest of receivers, which we hoped would provide an adequate amount of knowledge from which he could proceed to more ambitious projects. Many such newcomers, spurred on by success with the 'Tutor' (the October Blueprint), rose from the status of "beginner" by building the 'Mini-Amp', the subject of the November Blueprint.

This month, the experienced constructor and student alike can build a transistorised radio-the Blueprint accompanying this issue (and its related article) provide the details necessary to build the 'Citizen', a superhet tuner. The 'Citizen' comprises a frequency-changer and an I.F. amplifier, both of which are assembled by mounting components on to group-boards, in a similar fashion to that adopted for the construction of the 'Tutor' and 'Mini-Amp'.

The 'Citizen' may be used with any suitable amplifier to make a complete receiver, but if the reader decides to make use of the 'Mini-Amp', he will be able to choose an advance design for a cabinet far removed from the conventional 'box' form, which is necessarily employed in much commercial and home-constructed equipment because of the size and shape of the electronic units used. The group-board units which we have described place few or no restrictions before the constructor when the shape of the finished instrument is considered, and for those readers, then, who feel that with this receiver they could with advantage adopt an unusual styling for the case, we are giving in the next issue details of a cabinet, which although unorthodox in design, is extremely attractive in appearance. It will incorporate a 4-speed battery-operated record-player and a large loudspeaker for high undistorted output from all records-LP's and EP's up to 12in. in diameter. The complete unit forms a useful radiogram which works from its own internal aerial and batteries and may be operated anywhere independently of the domestic mains supply.

OUR OUERY SERVICE

NCE again we must remind our readers of the rules of our Free Query Service. The followings points should be carefully noted:

- (i) We cannot undertake to answer technical queries over the telephone
- (ii) All queries must be accompanied by the query coupon from the current issue
- (iii) If a postal reply is required a stamped and addressed envelope must be enclosed with the query.

We must also point out that we cannot design circuits to readers' specific requirements. Nevertheless we shall continue to help readers as far as possible but it should be remembered that all information necessary for answering the query should be sent to us.

Our next issue dated January, will be published on December 7th.

Round the World of Wireless

POTENTIAL AND CURRENT NEWS

Broadcast Receiving Licences

THE following statement shows the approximate number of Broadcast Receiving Licences in force at the end of August, 1961, in respect of wireless receiving stations situated within the various Postal Regions of England, Wales, Scotland and Northern Ireland. The numbers include Licences issued to blind persons without payment.

| Region London | | ••• | Totai 685.880 644.886 470,722 503,292 434.920 383,880 222,597 |
|-------------------------------------|----|-----|--|
| Total England and Wales Scotland | •• | ··- | 3.346.177 371,317 116.461 3.833.955 |

Speaking Clock for Sudan

ALAWIA EI Fatih El Bedawi, a typist in the Sudanese Embassy, recently went to Tin Pan Alley in London for a recording task which will take her fourteen days. Alawia, who has been a broadcaster in Khartoum, was chosen by her Government to record her voice for a speaking clock which is being installed on four Sudanese telephone exchanges by Associated Electrical Industries Limited.

The system will come into service on 17th November. It will enable telephone users in the Khartoum and Omdurman areas to find out the correct time in Arabic or English, whichever language they choose.

The installation, which has been designed by AEI Telecommunications Division, uses a tape recording system synchronised by a crystal controlled master clock which ensures accuracy equal to a variation of less than a second a month. This accuracy can be maintained completely independently of power failures because the equipment runs on the exchange battery supply.

Photomultiplier Tube Symposium at EMI House

MORE than 100 delegates from government and university research laboratories and industrial establishments throughout the United Kingdom and abroad

The Marconi navigation unit type 6402 with two of the sealed modules opened for maintenance. Each module may be reassembled and sealed with only four screws, and filled with dry nitrogen to give the added protection of a dry, inert atmosphere.

came to the Symposium of Photomultiplier Tube Applications, held at EMI House from 13th to 15th September.

Aims of the Symposium were to exchange information on the application of photomultiplier tubes in a wide variety of scientific and industrial fields and to encourage discussion on the ways in which improvements can be made and new fields opened.

Percy Allaway, Managing Director of EMI Electronics Ltd., welcomed delegates to the Symposium and Jack Sharpe, of EMI Valve Division, in his capacity as Chairman, opened the proceedings by giving a general introduction to photomultiplier tubes.

Mr. K. Rippon and Dr. M. A. Ford discussed the use of photomultiplier tubes in emission spectrometers and spectrophotometers. The growing importance of the vacuum ultra-violet in the former field was stressed, whilst it became evident that the spectrophotometer requires tubes with as wide spectral range as pos-An extremely elegant sible. application of spectrophotometer techniques for the measurement of the visual pigments in the living human eye was presented by Dr. W. A. Rushton, F.R.S., of the Physiological Laboratory Cambridge. Two applications of

photomultiplier tubes in colour television were described. Mr. Oxenham of Sylvania Thorn dealt with the Zebra colour television display system, while Mr. Hacking of the BBC considered the problems of the colour film scanner.

In a discussion of the nucleonic field, Mr. R. B. Owen of A.E.R.E. Harwell gave a general survey in which he pointed out the importance of photoelectron utilisation and the time characteristics of multiplier tubes.

Lectures were given in the first floor theatre and the ground floor reception room was available as an overflow room where delegates were able to hold discussions in a more relaxed atmosphere. Closed-circuit television linked these two rooms and a sound relay system included a talk-back link so that questions could be put to the speaker from the lower floor.

Four New Transmitters

THE BBC has placed an order with Marconi's Wireless Telegraph Co Ltd. for four 250kW short-wave transmitters. The new transmitters form part of a re-equipment programme for BBC's External Services transmitting stations; two will be installed at the BBC's Daventry station and two at the station at Rampisham, Dorset. The transmitters are being specially developed and will meet the specified requirements of the BBC. They will operate on any of the broadcasting bands in the frequency range 3.95-26.1 Mc/s.

The transmitters are of the single-channel type arranged for manual wavechanging, which can be carried out in under five minutes. The final modulator and final R.F. stages each use two BY.1144 vapour-cooled valves in push-pull, giving a carrier output of 250kW. Valves in the penultimate stages are also vapour-cooled, the smaller valves being air-cooled. The vapourcooled valves will be made by the English Electric Valve Co. Ltd. In the vapour-cooling system, which saves both plant and space, the heat from the valves produces steam in the water jackets sur-rounding them. This is led to a condenser, which converts it to water for return to the water jackets.

The vapour-cooling technique is already in use in the two newly installed 10kW short-wave transmitters at the BBC's Rampisham station and will be used in the four 100kW short-wave transmitters on order for the Daventry station.

Special precautions have been taken to minimise the possibility of spurious radiation from the 250kW transmitters causing interference in other bands, particularly the television bands. The R.F. stages are completely enclosed in screening boxes and harmonic filters are fitted in the output transmission lines.

It is expected that these four new transmitters will be brought into service during 1964.

Radio Hobbies Exhibition

MR. HENRY LOOMIS, Director of Voice of America, is to open the 1961 International Radio Hobbies Exhibition on 22nd November.

Mr. Loomis was educated at Harvard University and the University of California and obtained the degree of Bachelor of Science. After being a Lieutenant Commander (Overseas) in the U.S. Navy between 1940 and 1945 he became assistant to the President of Massachusetts Institute of Technology, and from 1950 to 1958 he held U.S. Government appointments, durDirector of Broadcasting Service of the U.S. Information Agency -Voice of America.

1961 Exhibition The is sponsored by the Radio Society of Great Britain and exhibitors will include the Army, Navy and Royal Air Force, each of which have their own radio groups throughout the world.

Exhibits will include new communications receivers from home and overseas; transistor components and kits of parts for build-it-yourself receivers, transmitters and television sets. Aerial equipment will be a feature for short and VHF wavelengths.

Many radio, television, recording, hi-fi and amateur groups will show their latest equipment. A Silver trophy will again be presented at the Opening Ceremony-for the most outstanding home-constructed piece of radio equipment.

The G.P.O. Research Branch will be exhibiting for the first time.

New VHF Sound Broadcasting Station for the Channel Islands

THE new BBC VHF sound broadcasting station for the Channel Islands was brought into service on 16th October. It is located on the same site as the

ing which he was appointed as BBC's television station at Les Platons, Jersey, and is one of the twenty-one new VHF stations so far approved for extending the coverage of the VHF sound service in the United Kingdom.

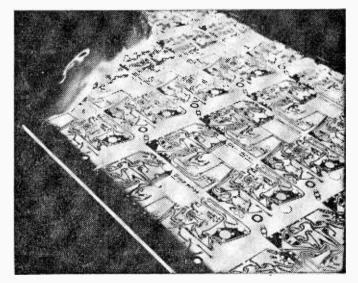
Starting on 9th October daily test transmissions from the new station were broadcast throughout normal programme hours.

Les Platons receives its programmes from the mainland by radio from the BBC's VHF stations at North Hessary Tor or Rowridge and transmits the West of England Home Service on 97.1Mc/s, the Light Programme on 91.1Mc/s, and the Third Programme with Network Three on 94.45Mc/s. The transmissions are horizontally polarised, which means that listeners' receiving aerials should be mounted horizontally.

Control Equipment for Russia

AN order for eighteen control for centres, valued at about £70,000, has been obtained by Motor and Control Gear Division of Associated Electrical Industries Ltd. from Constructors John Brown Ltd.

The equipment will be used to control the electric motors in two projected Russian detergent plants, one at Volgadonsk and the other at Shebekino.



Even with modern electronic devices, visual inspection remains necessary in many instances; above, printed circuit panels are shown under scrutiny at the Boreham Wood factory of Printed Circuits Limited.

a portable GRAMOPHONE AMPLIFIER

BUILDING THIS UNIT WILL PROVIDE A WORTHWHILE MEANS OF USING UP SOME OLD COMPONENTS WHICH WILL BE FOUND IN EVERY "SPARES BOX"

By V. E. Holley

HIS small amplifier costs very little to build —in fact, many constructors will probably be able to find most of the parts in the spares box. Nevertheless, it has quite a rewarding performance and a gain which is adequate for most types of pick-up, radio feeder unit, etc.

Circuit

The very simple circuit is shown in Fig. 1. The input signal is applied to a volume control, VR1 and thence via the tone control network VR2/C1, to the grid of a resistance coupled pentode voltage amplifier, 6J7. The resistor R3 is the anode load and the screen is fed from a potential divider across the H.T. supply. Normally, the screen of a resistance-coupled pentode must be decoupled by a fairly large capacitance, but if the impedance from screen to cathode can be made reasonably

low, as it is in this case, little is lost by omitting the decoupling. The cathode of the valve is tapped on to the potential divider at a lower point which is selected so that the current in the potential divider together with the cathode current of the valve, produce the correct bias across the parallel-connected resistors R4 and R5. These in turn are selected so that their relative values in series cause the desired amount of negative voltage feedback from the output transformer secondary to be injected at the cathode of V1. It will be noted that V1 operates with both current and voltage feedback so that its input impedance is high and only a small capacitance is needed in the tone control network.

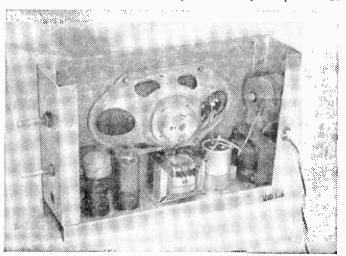
Output Stage

The signal from V1 is transferred via C2 to the grid of V2, which is an output tetrode, 6V6. R6 is the grid resistor and R7 provides cathode bias. It will be seen that R7 is not bypassed so that V2 also operates with negative current feedback. This is undesirable as a rule, because it has the effect of increasing the apparent anode resistance of the valve so that its less desirable qualities are accentuated. In this case, however, this effect is counteracted by the negative voltage feedback and the net result is a reduction in the apparent anode resistance and an improvement in the linearity of the amplifier.

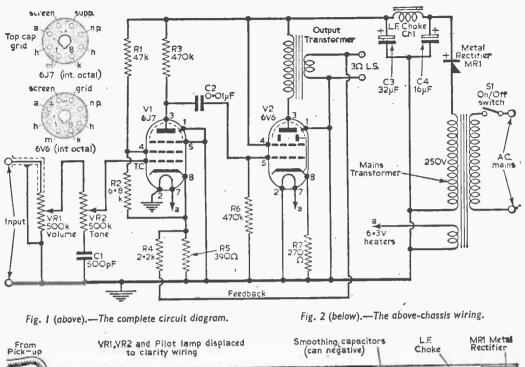
The output transformer in the anode circuit should have a ratio of about 40:1 to match a 3 Ω speaker to the optimum load for the valve which is 5,000 Ω . Only an inexpensive transformer is required as its deficiencies will be largely made good by negative feedback.

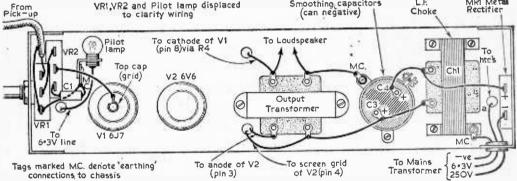
Power Supply

A double-wound mains transformer is used, thus providing complete isolation of the amplifier from the mains. It should have a 250V half-wave secondary capable of supplying 50mA and a $6\cdot3V$ 1A winding for the valve heaters and indicator lamp: the latter should not consume more than $0\cdot25A$ if the heater current is to be kept down to 1A. Any type of half-wave metal rectifier can be used so long as it can pass 50mA at 250V. Smoothing is provided by the electrolytic capacitors C3



A rear view of the amplifier.





and C4 in conjunction with the choke Ch1 and, as the hum is very well taken care of by negative feedback, it is not necessary that the choke should have a large inductance.

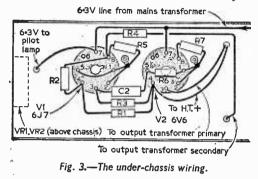
Construction

There is nothing critical about the lay-out and the amplifier can be constructed in any form suitable for the purpose for which it is to be used. The prototype was built to fit into a commercial record player cabinet of conventional shape, having a vertical section to the left of the turntable measuring about 12in. \times 9in. \times 3in. and this form will be described.

The speaker is mounted on a piece of plywood or hardboard 11 in. \times 6³/₄ in. and the amplifier chassis which is 2⁴/₂ in. wide is secured to the hardboard by 4B.A. bolts, two at each side and two at the bottom. The arrangement will be clear from the illustration. The chassis is of 18-gauge aluminium sheet to the measurements given in Fig. 4. The mains transformer is mounted separately in the player cabinet underneath the motor board, remote from the pick-up, and its output is taken to the chassis at a point adjacent to MR1 by a 3-core cable—H.T., L.T. and common negative. The transformer can thus be of any reasonable shape and size and there will be no interaction between it and other components. The switch S1 is fitted to the cabinet adjacent to the point of entry of the mains lead.

Components and Wiring

All the components are standard and there is plenty of room for them in the chassis—in fact, there is considerable scope for miniaturisation to suit smaller cabinets. Of the resistors, R1 and R7 should be 1W and the remainder $\frac{1}{2}W$ or $\frac{1}{4}W$. The capacitors should be 350VW. If valves other than the specified types are used, they should have the same general characteristics or some alteration may be required in the feedback loop. In the illustration, V1 is shown with the top cap screened but this is not really necessary. Wiring diagrams are given in Figs. 2 and 3. Tinned copper wire of 22s.w.g. is suitable for all the wiring and lengths of more than an inch or so should be covered with sleeving.



Operation

When construction is complete, a check should be made with a meter between C4 and chassis to see that there are no shorts in the H.T. wiring. The power can then be switched on and the H.T. voltage checked. If there is instability it will be due to incorrect connection of the voltage feedback circuit and will disappear if the connections to the output transformer primary are reversed. The input arrangements to V1 may, of course, be modified to suit the signal source as desired; the performance will not be affected except insofar as the response may be modified by alterations to the tone control network.

| | | COMPONE | | | | | | |
|-----------|----------------------------|--------------|--------------|--|--|--|--|--|
| Resistors | | | | | | | | |
| RI | 47k IW | | 390 Ω ½W | | | | | |
| R2 | 6.8k 12W | R6 | 470k 1W | | | | | |
| R3 | 470k 1W | | 270 Q ÎW | | | | | |
| | 2.2k, 1W | | 270 22 777 | | | | | |
| | | apacitors (3 | 150VW) | | | | | |
| CI | 0.0005 μF | | 0.01 µF | | | | | |
| C3 | | rolytic 350\ | | | | | | |
| C4 | | rolytic 350 | | | | | | |
| •• | iv protect | Choke | | | | | | |
| Ahor | It 10H 50m | | | | | | | |
| 1000 | | Valves | | | | | | |
| VI | 6 17 | | | | | | | |
| V2 | 6 j7, octai 6V6,octai b | base bor si | milar | | | | | |
| 72 | ovo,octai b | ase j | | | | | | |
| | | Rectifie | r | | | | | |
| Meto | alcontact | cooled (o | r with fins) | | | | | |
| | | Transform | ers | | | | | |
| Mair | 1 s —250 7 50 | mA, half w | ave; 6.3V 1A | | | | | |
| Outț | out—About | 40:1 for 3Ω | speaker | | | | | |
| | | Indicator Id | 1mp | | | | | |
| 6-3V | 0-15A | | | | | | | |
| Singi | e pole on/o | ff switch | | | | | | |
| 250V | IA | | | | | | | |
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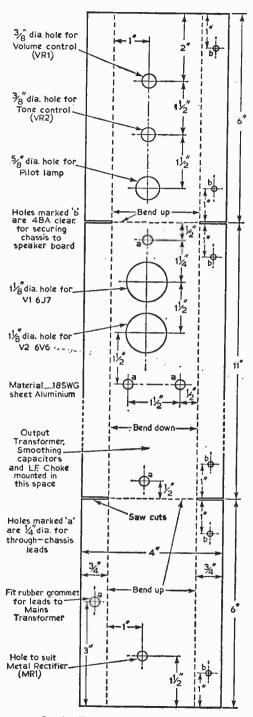


Fig. 4 .- The chassis drilling details.

An Improved Valve-Voltmeter

A FEW MODIFICATIONS TO AN INSTRUMENT DESCRIBED IN P.W. MARCH 1961, WILL PROVIDE THE CONSTRUCTOR WITH AN EXTREMELY RELIABLE UNIT.

By M. L. Michaelis

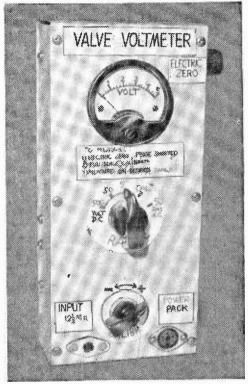
General Description

This circuit is specifically based on the circuit principle already introduced by Mr. J. B. Dance on pages 996 to 998 of the March 1961 issue of *Practical Wireless*. Thus it uses the same form of cathode-coupled balanced D.C. Amplifier as the basic circuit. Upon experimenting with Mr. Dance's circuit, the author devised a number of modifications, which led to the production of this article. This does not mean that any fundamental criticism is intended against the former circuit; on the contrary. Mr Dance's circuit as such is perfectly sound, and was found to function very well when his instructions were exactly followed. This present article is merely intended to present some additions and further ideas.

New Circuit Features

The basic circuit is already taken to be understood from the previous article. If readers do not have the relevant issue of *Practical Wireless* to hand, then that need not disturb practical issues, as completely new theoretical circuit and clear wiring-diagrams are provided here. It is intended to discuss here only the circuit modifications made, and to explain the reasons for them, and then to give such other practical information as is considered necessary to build the present circuit.

The main new feature here is the built-in calibrator circuit. This provides, from the A.C. heater supply, a D.C. reference-voltage of exactly 5V. When the unit has been connected to any available power supply, the range-switch is first set to the "adjust calibration" position, and built-in meter-shunt VR2 (see Fig. 1) is turned until exactly full-scale deflection results. ("Electrical Balance" (Zero) must of course have been set previously with VR1.) In this way the meter sensitivity is automatically adjusted to suit the H.T. voltage which happens to be used, and the calibration holds on the measuring ranges for any H T. voltage supply for operating the unit, as long as it lies between about 250 and 350V. With the circuit of Mr. Dance, the calibration held only



The complete unit.

for one particular H.T. voltage supply, so that his unit needed to be calibrated for use with one particular H.T. supply.

Zener Diode

The calibrator uses a normal meter-rectifier bridge in half-wave connection for rectifying a sample of the heater voltage. C4 acts as smoothing, and the zener diode (D2) with R12 stabilises the D.C. to exactly 5V. A zener diode is a semiconductor-diode much resembling a transistor in appearance, and has the following properties: if its anode is made positive to its cathode, then it conducts exactly as any other diode. If its anode is made negative to its cathode, then at first it does not conduct, again the same as any other diode, but if this negative voltage exceeds a certain value called the zener voltage, then the diode

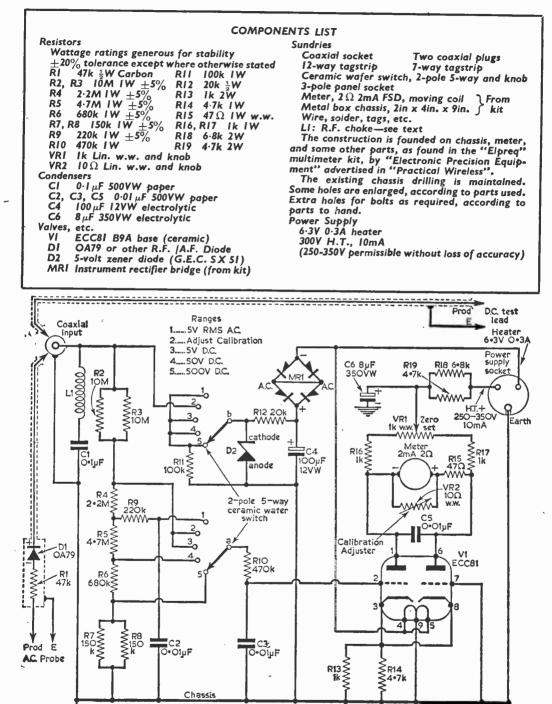


Fig. 1.—The circuit of the instrument.

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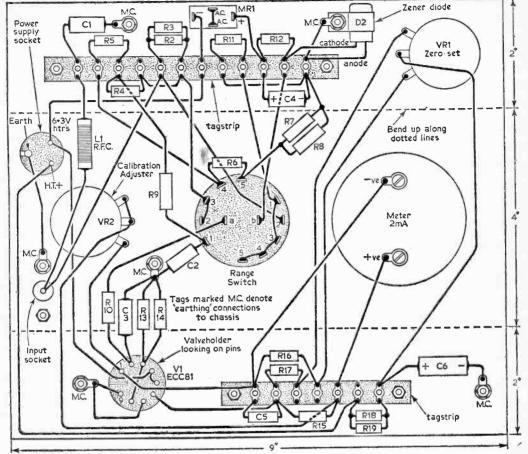


Fig. 2.- The complete wiring diagram-the sides are shown bent flat to clarify the wiring.

suddenly conducts again. Thus, in the circuit here described the zener diode D2, which has a zener voltage of 5, always draws just that amount of current through R12 to keep its cathode at exactly 5V positive to chassis (R12 may be altered in value to bring the cathode voltage of D2 to exactly 5. R12 should not be made less than 2.7k.)

The second major modification to the original circuit is a drastic change in the circuit-values connected with the anode circuits, to make the whole circuit of lower impedance. This is to suit it to a cheaper and less sensitive meter than the one specified by Mr. Dance, whilst nevertheless maintaining the original high input impedance with consequent high overall-sensitivity. The main reason for this modification is that the whole circuit was designed to be built using chassis and many parts of a Multimeter Kit advertised in this magazine. The author has purchased several of these kits, and after building one up as originally intended, experimented by modifying the others to various other circuits. The present instrument is one of the results.

The kits almost always used moving-coil meters of basic sensitivity 2mA FSD, and about 2Ω internal resistance, and the present circuit values were adapted for this type of meter. The lk potentiometer in the kit, originally intended for "ohms zero", serves here as VRI for the elec-trical-zeroing. The meter-rectifier bridge in the The meter-rectifier bridge in the trical-zeroing. The meter-rectifier bridge in the kit serves as the calibrator-rectifier, and is connected as half-wave rectifier, by shorting the A.C. connections to each other, and using only the D.C. connections as shown in the circuit diagram. The chassis is used as it is. The holes originally for the two test leads are to take the input coaxial socket and the miniature 3-pole power-supply VR2 is fitted through the existing hole socket. originally intended for the multimeter voltage/ current selector, and the range switch maintains its original position. The switch in the kit is rejected to the spares box, and a high-insulation ceramic-wafer switch is here used for the range switch. VR1 maintains its original position. Apart from a few simple holes for mounting-bolts of tagstrips, earthing tags and the valveholder, virtually no alteration is required to the chassis supplied with the multimeter kit.

Scale

Driving the 2mA FSD meter to full-scale under the circuit conditions existing here represents just about the limit of linear drive which V1, an ECC81, will accept. The meter should be fitted with a linear scale calibrated 0 to 5, and then, in the finished circuit, R14, R15 and R18 are carefully adjusted to give best linearity over the whole scale by comparing readings given with this instrument with those given by another ordinary meter, with various voltages used as test. The author's instrument, after careful trimming, gives 10% accuracy on all ranges, under all H.T. supply voltages between 250V and 350V. Thus it seems hardly worthwhile using resistors of

greater accuracy than the 5% ones specified in the parts list. Use of a 1mA FSD meter, if available, would probably increase the accuracy limits sufficiently to warrant 1% tolerance resistors for R2 to R9. If a 1mA meter is used, then R4 to R8 inclusive should be halved in ohms value. VR2 should be chosen to equal about five times the meter resistance, and R15 should be approximately 50Ω, less the meter resistance. But it should be emphasised that the purpose of this instrument is not increase of accuracy, but rather a large decrease of loading imposed on the circuits being measured, so that voltages even on high-impedance resistors chains can be accurately measured without falsification. An accuracy of 10% is the normal tolerance of amateur multimeters anyway.

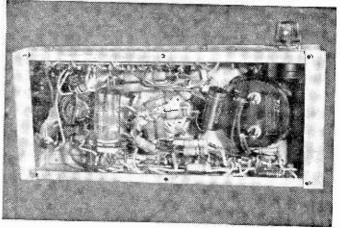
It should be pointed out that the method of calibration and adjustment with variable shunt and built-in reference voltage used also compensates for change of valve characteristics with age, an added advantage over the original circuit.

an added advantage over the original circuit. Finally, L1 makes C1 inoperative at R.F., so that the same A.C. Probe is usable for A.F. and R.F. Choose L1 so that the resonant frequency of L1 and C1 lies between the highest A.F. frequency and lowest R.F. frequency required to be measured. About 200μ H is suitable.

Operation of VR I

As stated, VR1 is used to obtain electrical zero and, normally, zero should be found when VR1 is at the centre of its rotation. However, if VR1 is seriously displaced from the centre of its rotation on the more sensitive ranges, before zero can be found, then the grid (pin 7) may be connected via a resistor of between 1 and 10M to chassis instead of direct to chassis. Alternatively, another wafer on S1—S1c—might be used to switch a suitable resistor from pin 7 of V1 to chassis individually on each range.

Such modifications are not essential, for accuracy is not seriously disturbed even if VR1 is far



A rear view of the voltmeter.

from the centre of its rotation for balance to be obtained.

Circuit Adjustments

By far the most critical component for influencing the linearity of response, i.e. equal increase of deflection for increase of input voltage being measured, is the cathode resistance combination R13 and R14. The constructor is advised to start with all component values as specified, and if this does not give satisfactory linearity right away, then R14 should be replaced by various other values within about 2.5k and 10k. A fine correction can be made with R15. The value of the combination R18 and R19 largely affects the range of H.T. supply voltages within which satisfactory operation is possible.

Power Supply

Any available power supply of 250 to 350V H.T. and 63V A.C. at 03A is suitable. The H.T. consumption is about 10mA. One side of the heater supply and H.T. negative may be commoned in the power supply used.

The small 3-pin socket for power-supply connection used by the author consists of one of the fittings now often used for connections on taperecorders, and a 3-core cable is attached to the fitting plug, with colour-coded wander-plugs fitted at the other end of the cable.

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699

Checking TEST Instruments

By G. A. W. Partridge

THIS UNIT WILL ENABLE THE CONSTRUCTOR TO MAKE QUICK, SPOT CHECKS ON HIS TEST EOUIPMENT

HE balanced voltage system is regarded as one of the most accurate methods of checking the readings of ordinary test instruments. Its operation is simple and the apparatus is quite easily constructed.

However, it will be appreciated that this home-made equipment Millimetre scale cannot compare with the high grade apparatus on the market, but it will indicate any erratic Large terminal behaviour of an instrument which may have become unreliable.

Operation

A slide wire is stretched between two terminals mounted on a board (Fig. 1). A scale marked in millimetres is placed close to the slide wire which is connected to the circuit shown in Fig. 2. The battery is connected to the slide wire and the switch is thrown

to the left thus bringing into circuit the Standard Cell S.C. which has an EMF of 1.0183V. The slide wire is quickly touched with the test prod along its length until a point is found where no current is indicated on the milliam-meter. The position of this point is noted by measurement in millimetres. The test prod must not be left in contact with the slide wire for more than a second at a time to avoid drawing current from the Standard Cell.

As soon as the null point on the slide wire has been found, the switch is thrown to the right, and the null point again found and noted on the millimetre scale. The reading of the voltmeter which is under test is also noted. The correct voltage is calculated from:-Correct Voltage=

Standard Cell Voltage x Slide wire reading with Voltmeter in circuit

Slide wire reading with Standard Cell in circuit.

This voltage, which is very accurate, is compared with that indicated on the voltmeter and any discrepancy noted. The same procedure can be carried out over the entire voltmeter range. After a little practice readings can be very quickly taken and worked out.

Additional Ranges

The instrument as it stands will test up to about 2V, so other apparatus will have to be added in order to test voltmeters with higher ranges. Fig. 3 shows how this is achieved.

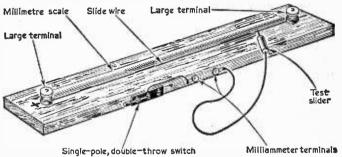


Fig. 1.—The basic slide wire potentiometer.

A number of accurate resistors are connected in series, and the voltmeter under test is connected to the appropriate voltage tap. The potentiometer measures the small voltage which appears across

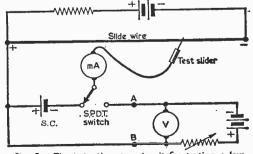


Fig. 2 .- The potentiometer circuit for testing a low range voltmeter.

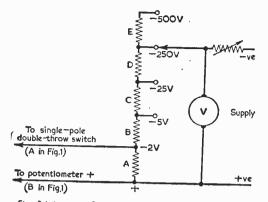
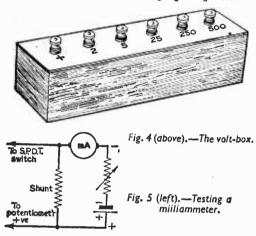


Fig. 3 (above) .- Circuit for testing high-range meters.



resistor A which is proportional to the voltage across the voltmeter. The tests are carried out in the same way but the voltage on the potentiometer is multiplied by the appropriate ratio. For example, the voltage across A will be 2 when 250V is applied to the 250V tap. Therefore 250=125 which is the ratio in this case. 2

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The ratios for the taps are:----
Tap 5 = 2.5
Tap 25=12.5
Tap 250=125
Tap 500=250
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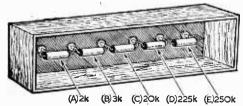


Fig. 6.-Rear view of the volt-box showing the resistors in position.

The measurement of current is also carried out with resistors. Fig. 5 illustrates the method. Assume that the milliammeter is scaled to 100mA. The 100mA shunt is connected as shown and gives 2V when 100mA is flowing through it. The ratio in this case will be 50. For example if the voltage measured is 1.35 then the current flowing through the milliameter is $1.35 \times 50 = 67.5 \text{mA}$.

The slide wire is made from resistance wire of about 2Ω per yard. This is not critical, but the higher the resistance the higher the voltage that can be measured. It is just over a meter in length and is stretched tightly between two terminals one meter apart on a wooden base 4ft. x 4in. x in. The meter rule or tape is held in position by in screws or tacks.

The switch which is of the single-pole-doublethrow type is mounted on the side at the centre of the board. Two terminals are placed 2in. apart and about 6in. away from the switch as shown in Fig. 1. The nearest terminal is connected by a small length of bell wire to the centre of the switch. The test prod is connected to the other terminal by 3ft of light flex.

Fig. 4 shows the general idea of the volt-box. A row of terminals are mounted on the box which



Fig. 7.—A current shunt.

is made from stiff cardboard. Fig. 6 illustrates the internal connections.

When ordering the resistors state that they are for measurement so that the supply firm will provide more accurate resistors than those used for ordinary radio work. They may cost a little more but for accurate tests they are essential. Five W resistors are required, and the values are:-A=2000 Ω ; B=3000 Ω ; C=20.000 Ω ; D=225,000 Ω ;

E=250,000Ω.

The shunts, or current measuring resistors, are each mounted separately on wooden bases with terminals as shown in Fig. 7 with the current range marked clearly on them. The 10mA shunt is 200 Ω ; the 100mA shunt is 20 Ω ; the 500mA shunt is 4Ω .

These resistors are obtainable along with the Weston Standard Cell (small type) from the Doran Instrument Co., Stroud, Glos.

There are a few points that must be borne in mind while operating this test set. First, all connections must be as tight as possible. Second, the test prod must not be in contact with the slide wire for more than a second at a time. Third, the Standard Cell must be kept in a cool place. Fourth, not more than 1A must pass through the slide wire. Use two large $1 \frac{1}{2} V$ dry cells with a 1 Ω 1W resistance in series. Finally, give the slide wire about two minutes to warm up before starting work, and tighten it if necessary.

PRACTICAL WIRELESS





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PRACTICAL WIRELESS

702

R.F.

LF.

and A.F. Signal Generator

HIS unit requires very few parts, and runs from a 224V, B112 or similar miniature layer H.T. battery, with a 14V cell for the filament. It produces a modulated radio frequency signal, which can be used to test or align R.F. and I.F. stages in a receiver, or to calibrate home constructed sets. An audio output is also available, and this is suitable for stage-by-stage tests of A.F. amplifiers, or the audio circuits of receivers.

It is possible to calibrate the generator tuning dial by means of a receiver, as will be explained. Despite its simplicity, the generator will be found to be very useful for aligning, trimming, and testing TRF and superhet receivers of mains, battery, and transistor type.

Circuit

The circuit is shown in Fig. 1, and component values are so arranged that the R.F. oscillations are interrupted at audio frequency by grid blocking. The A.F. output socket provides an audio tone which is used for testing speakers, and A.F. amplifier stages. The R.F. output socket gives modulated R.F. at the frequency to which the generator is tuned. A single switch selects either of the two tuning ranges, and has an "off" position. A separate filament switch could be used, and a 2-pole, 2-way switch would then suffice for range selection. THIS BATTERY-OPERATED UNIT WILL BE FOUND INVALUABLE IN CALIBRATION, ALIGNMENT, ETC.

By F. G. Rayer

The two coils used were arranged to cover about 1,600kc/s to 500kc/s (about 190-600m) and 500kc/s to 170kc/s (about 600-1,800m). This includes 465kc/s, for I.F. alignment, in addition to all the usual medium-wave band, and most of the usual long-wave band. Harmonics are available up to 30Mc/s.

The M.W. coil was a standard air-cored type, with the addition of a dust core. For L.W., a standard-cored L.W. coil was found suitable, with the core almost unscrewed. The coils should be of the type which have reaction windings.

Valves other than the 1S4, may be used, 3S4, DL92, and similar types being satisfactory. The holder must, of course, be wired to suit.

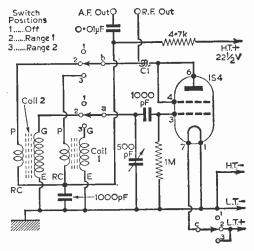


Fig. 1.—The circuit of the instrument.

The cabinet is a 6in. x 7in. x 2in. "universal chassis" with extra 6in. x 7in. back plate. An extra 7in. x 2in. runner forms the chassis.

The panel layout is shown in Fig. 2. The sockets of the twin strip project through clearance holes. The chassis should be bolted to the panel, but the generator should not be installed in its cabinet until finished.

Fig. 3 will act as a guide to marking out the tuning scales. The exact position of markings will depend on the tuning condenser, coils, and other

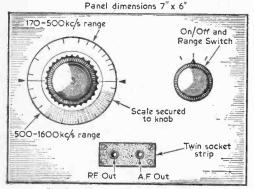


Fig. 2.- The layout of the front panel.

factors, and can be obtained as described later. The scale is cemented to the tuning knob, and rotates with the knob, readings being taken off at the panel markings shown in Fig. 2.

Generator Wiring

Fig. 4 shows connections and components, the underside of the valveholder being included so that pins may be seen. The tuning condenser should be of the full 500pF capacity, for the coverage mentioned, and its frame is in contact with the aluminium panel.

An L-shaped clip is cut from scrap metal, and drilled so that the switch secures it to the panel. The arms of the clip are bent to hold the $1\frac{1}{2}V$ filament cell, and $22\frac{1}{2}V$ H.T. battery, as in Fig. 4. Current consumption is small, and to avoid crackling, owing to poor contact, the battery leads are soldered directly to the batteries. This should only be done after completing other wiring.

The switch has three positions. One is for "off" and no circuit is completed, the unused contacts being ignored or cut off. With the switch in its next position the filament circuit is on, and the first tuning coil is connected. G2 and P2 indicate Grid and Plate (reaction) tags of coil 2. In the final switch position, coil 1 is in circuit, G1 and P1 indicating Grid and Plate tags of this coil. The filament is also switched on, as before. The coils can be fixed on brackets, or bolted to the chassis.

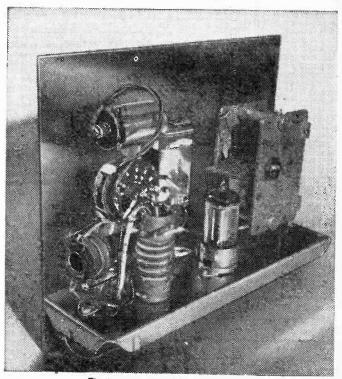
Points marked M.C. are connected to the chassis in the usual way. Condenser C1 is formed by winding three or four turns of insulated wire round the insulated covering of the lead from valve to switch, as shown. Check connections against Fig. 4 before inserting the valve and installing the batteries.

Use as Audio Generator

For this application, the tuning calibration is of no importance. With the generator switched on, a strong audio tone should be heard in 'phones wired from the A.F. output socket to chassis. The note will vary according to the range selected, and the position of the tuning control. If this audio tone is heard, this indicates that

If this audio tone is heard, this indicates that the generator is also producing its radio frequency signal. If no tone is heard, connections to the reaction windings on the coils may be reversed. Figs. 1 and 4 show usual connections, as indicated by most coil manufacturers. "G" denotes Grid, "P" indicates Plate (reaction) and "R.C." is for Reaction Condenser, with "E" showing the Earth or metal chassis connection.

To make stage-by-stage tests of audio circuits, take an insulated test prod connection from the A.F. output socket of the generator. Apply the prod to A.F. circuit points one by one, working



The instrument with its case removed.

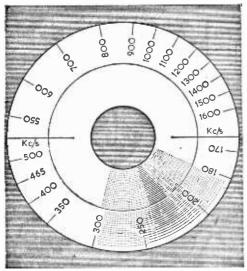
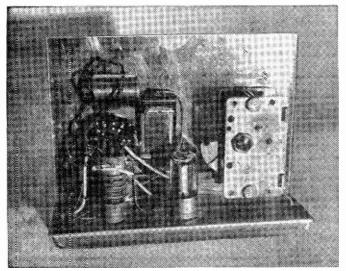


Fig. 3.—The markings of the frequency scale.

backwards from the speaker. Volume should increase, as each extra stage is introduced. When the point at which a fault arises is passed, reproduction of the audio tone will cease. If the audio tone is not heard at the very beginning of these tests, with the prod applied to the output valve anode, then the speaker itself, or its output transformer must be suspected. But note that



A rear view of the Signal Generator.

volume at this point will be small, as there will be no additional amplification.

In most cases no return connection need be made to the generator. But when volume is very small (as when testing a speaker and transformer) the generator cabinet may be wired to the receiver chassis. Take usual precautions with mains equipment, especially A.C./D.C. sets with a "live" chassis.

If tests are made systematically, working backwards through the receiver or amplifier, the source of a fault may be localised to a single component, if this is in a coupling circuit. Otherwise, the fault will be localised to one stage. The valve, and associated resistors, etc., in that stage should then be examined, substituted, or tested with a meter, according to the facilities available.

I.F. Circuit Testing

Point by point tests of intermediate frequency stages are made by plugging the test lead into the R.F. output socket of the generator. Apply the prod to the final I.F. stage anode, and tune the generator until its note is heard on the receiver.

The prod may then be transferred point by point, until the frequency changer anode is reached. If a defect is present in an I.F. transformer winding, or elsewhere, reproduction will cease when this point is passed.

To align I.F. stages, the generator tuning scale must be calibrated. The generator is then tuned to the correct frequency, and the I.F. transformers are adjusted for maximum output.

In all cases where R.F. and I.F. stages are being checked, keep the receiver audio volume control near maximum, and reduce coupling to the generator, if necessary, to obtain a tone of moderate strength in the speaker. Critical adjustments can then be most easily made. If a strong signal is injected to early stages, and the receiver volume control is near minimum, the receiver

AVC action will make adjustment difficult. It will often be sufficient merely to place the generator test prod near the appropriate lead of the transformer or coil.

Generator Calibration

If an accurately calibrated receiver is available, place the generator output lead near the aerial socket of the receiver. Tune the receiver to various frequencies, adjust the generator tuning to the same frequency, and mark the dial accordingly. Initially adjust the coil cores to give about the wavebands mentioned.

If a calibrated generator can be borrowed, adjust this to various frequencies, tune the receiver to the same frequency, then tune the 1-valve generator to the same frequency, and mark its dial.

Extremely accurate calibration is possible from a 100kc/s crystal marker. Tune the receiver to the 200kc/s harmonic, adjust the generator to this, and mark its dial.

Then repeat at 100kc/s intervals, marking the generator scale each time.

If none of these means is available, the 1.500m Light Programme will furnish a 200kc/s marker signal. To use this, tune the receiver to 200kc/

(e.g. the Light Programme transmitter). Tune the generator to this frequency, and mark its scale. Leave the generator tuning untouched, and tune the receiver until the generator harmonic on 400kc/s is heard. Leave the receiver tuning untouched, and tune the receiver until the generator harmonic on 400kc/s is heard. Leave the receiver tuning untouched and tune the generator to 400kc/s, and mark its dial. Return the receiver to 200kc/s, readjust the generator to this frequency, then tune the receiver to 600kc/s (ignoring the 400kc/s harmonic already used). Then leave the receiving tuning, and adjust the generator to 600kc/s, and mark its scale. Proceed in this way until the whole of both bands has been calibrated at 200kc/s intervals.

A list of BBC transmitters will give their frequencies, and these furnish additional check points. Tune in the required station, adjust the generator to this frequency, and mark its dial.

A 465kc/s calibration point for the generator can be obtained by placing the output lead near the I.F. stage of a receiver using this frequency, and tuning the generator for maximum response from the receiver.

Harmonics

As the correct use of harmonics can be extremely useful, both for calibrating the generator and for other purposes, it should be noted that these arise at multiples of the frequency to which the generator is tuned. For example, if it is tuned to 200kc/s, its note will be heard at 200kc/s (fundamental), 400kc/s, 600kc/s, 800kc/s, and so on, each harmonic being a little weaker than the previous one.

Similarly, if the generator is tuned to 400kc/s, it will be heard at 400kc/s, 800kc/s, 1,200kc/s, and so on, but not at 200kc/s. That is, its harmonics are always *multiples* of the frequency to which it is tuned.

With an average receiver, the harmonics of 200kc/s can be heard at 200kc/s intervals, right up to 1,600kc/s. With a sensitive receiver, the harmonics may be heard up to 4Mc/s. As the initial setting of the generator can be extremely accurate (e.g. from the 200kc/s Light Programme) the check points thus obtained are very useful indeed for calibrating home-constructed receivers, or similar purposes.

If the generator is tuned to 1,500kc/s, its harmonics can be heard up to 30Mc/s, with a sensitive receiver. With the generator tuned to 1,000kc/s, harmonics may be heard up to about 25Mc/s. These will, of course, be at 1,000kc/s, or 1Mc/s, intervals, and will be extremely useful for calibrating a home-built short-wave set, or for similar purposes.

A simple TRF receiver, with reaction, is very satisfactory for helping to calibrate the generator. With reaction sufficiently advanced,

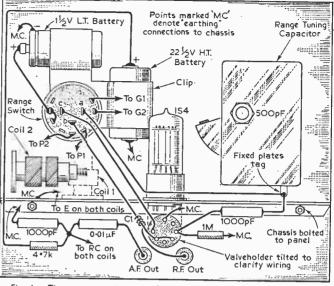


Fig. 4.—The component layout and wiring diagram of the complete unit.

the exact tuning point can easily be found. An ordinary superhet is suitable, especially if it has a tuning meter or magic eye. In this case, the meter or eye will show the correct tuning point. If there is no meter or eye, turn the receiver volume control to maximum, and reduce volume by providing very loose coupling, as already explained.

When adjusting the generator to the same frequency as a radio station, reduce the volume of both signals, disconnecting the receiver aerial if necessary. With a little care, a standard of calibration sufficiently accurate for normal purposes can be achieved.

Aligning R.F. Stages

To adjust aerial or R.F. circuits, inject a signal of about 1,400kc/s at the aerial terminal, tune to this on the receiver, and adjust the M.W. trimmers for best results. Then inject 600 or 700kc/s, tune to this on the receiver, and adjust M.W. coil cores for best sensitivity. Repeat a few times.

If the receiver has a calibrated tuning dial, adjust trimmers and cores for best accuracy of reading, as well as best results. For a homeconstructed receiver with uncalibrated dial, adjust for the expected waveband coverage (say 200-550m on M.W.). The dial can be calibrated at desired points, from the generator.

Treat each band separately. In simple dual-range receivers with only one pair of trimmers, these are usually adjusted for best M.W. reception.



A

COMPLETING THE ALIGNMENT

By D. R. Bowman

(Continued from page 592 of the November issue)

N last month's issue, the first three parts of the alignment procedure were completed.

4-Switch the signal generator to controlled output. Plug in coaxial lead. Bring it to the board and clip the outer braiding to chassis. Connect coaxial cable core (inner) to the base winding of Tr3 via a 25pF capacitor. Leaving ratio detector core (secondary) alone, re-align for maximum output in the loudspeaker.

5-Transfer the signal generator input to the base of Tr2 (C11). Complete alignment of T2 and T3 as before.

6-Screw in the core of the ratio detector transformer until it overlaps both primary and secondary windings. Adjust the core of the primary for maximum output. Very carefully screw the core of the secondary in towards the primary, keeping adjustment of the primary by slowly withdrawing the primary core. This is a two-handed operation, aimed at varying the coupling between primary and secondary by the adjustment of the coupling core. Continue until maximum output is heard in the loudspeaker. Then, reverse the direction of travel of the coupling core and rotate 11 turns, adjusting the primary core to maintain resonance. This gives more-than-critical coupling (about 1.5 critical) with little reduction in sound output; the decrease should be just noticeable, not a pro-

Transistorised VHF Superhet

nounced drop off in volume. If 11 turns reversed travel causes a considerable drop in sound, less movement of the core is needed; a reduction of 2dB is ideally required and this may be judged

by ear to a sufficient degree of accuracy. 7—Insert a third core in the ratio detector secondary winding. Rotate this to see if a minimum output point can be found. If not, use a brass slug instead of a dust core. Rotate the tuning element, whether iron dust or brass, for a minimum output between positions of high output. This point will be quite sharp and will be characterised by a change of "quality" of the output tone as the minimum output point is traversed.

8-Set the signal generator to 90Mc/s and connect the coaxial lead to the aerial socket. Set C7, C13 to approximately half setting and C12 to half capacitance. Rotate the core of L1 until a signal is heard; if a signal is heard in two positions of the core, the setting which gives least inductance is correct.

9-Set the signal generator to 86Mc/s. Rotate C7, C13 until the signal is heard. This should occur at nearly maximum capacitance; if not, adjust L1.

10-Set the generator to 100Mc/s. Adjust C12 to hear the signal, and the core of T1 for maximum output.

11-Set to 89Mc/s and locate the signal with tuning capacitor C7, C13. Rotate the core of T1 for maximum output.

12-Reset to 100Mc/s and adjust C12 for maximum output.

13-Repeat the adjustments 11-12 until no further improvement results.

(Continued on page 712)



A Recording Problem

In the details which I gave in the October issue of a tone problem connected with a tape recorder, many readers wrote with suggestions as to the cause of the trouble, and some very ingenious suggestions were made by some. However, several readers made the same suggestion and it would appear that this is, in fact, the real answer, and it concerns not the material from which the tape is made, nor its manner of storage, but the method of use. A Mr. Berry of Burton-on-Trent says he suffered from this trouble and after experimenting with different types of tape over a period of time without satisfactory results, he turned his attention to the deck, and located the fault in the playback head. A small adjustment of the arm holding the pressure pad was the remedy, and since doing this he has had no further trouble.

Electronic Games

Some experimenters find a great deal of entertainment in the adaptation of standard electronic techniques to the requirements of equipment and apparatus which is not normally used in the electronic fields. Recently I saw a most ingenious electronic version of noughts and crosses-not the simple electric method which was seen at a Radio Show some time ago. This was truly electronic and made use of a computer network, and I was not really surprised when this was followed shortly afterwards by a modification to enable the game of "Nim" to be played. In this, as most of my readers know, a number of matches are laid out and the object is to make your opponent take the last match. This electronic version guarantees success, without worry, and according to the design cannot be beaten. I wonder how many other well-known parlour games have been adapted in this way. No doubt those who are engaged in designing and building computers for industrial purposes often think of other uses for them, a fact which is bound to come up when development work is being carried out. This is an interesting field for experiment by those readers who can follow simple computer design, and, as usual, we shall always be pleased to see the results of a reader's handiwork, and if interesting enough. to publish them. I am sure there must be some very interesting developments possible, even in such games as poker or bridge.

world. You will probably remember that the U.S.A. proposed that a rocket could fire an immense quantity of these strips into space, where they will form a fairly substantial metal layer from which signals could be bounced, but astronomers are complaining that this would make telescopic viewing even more difficult than it now is, whilst radio telescopic investigators complain that it will give false readings. I believe that the idea has been temporarily shelved, but I wonder if any-unknown effects are likely to result from the various atomic explosions which are made from time to time. Will not the radiations which result remain for all time in space, and perhaps gradually form up to make a complete screen round our earth, thus preventing scientific observations of a certain kind, and perhaps even eventually preventing satisfactory control of space craft designed for the moon and other planets. I often wonder if it is possible for the men engaged in this work to calculate the possible effects over a period of time or whether they are not more interested in the present, as they will not be here later to feel the results of some of these activities. It would be reassuring if the powers concerned could let us have from time to time information on this aspect, as well as letting us know that a certain type of explosion has taken place.

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PRACTICAL WIRELESS

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December, 1961

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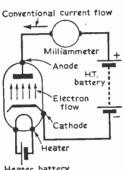
PRACTICAL WIRELESS

Understandi WER THE DIODE VALVE Supplies AND THE HALF-WAVE **RECTIFIER CIRCUIT**

N order to understand how power supplies work, it is first necessary to understand fully how the diode valve works, since all power supplies are concerned with diodes of one form or another. The power supply circuits used in radio engineering generally use A.C. mains as the power source.

The function of the power unit

The function of the power unit is to provide smooth D.C. voltages as required by valves and devices. This other article will only deal with the more important circuits and not with heater supplies, as similar circuits are used for low voltage supplies and H.T. supplies.



The Diode

When any material is sufficiently, heated electrons (which have a negative charge) are thrown off. When electrons are emitted from a heated cathode they

Heater battery

Fig. 1 .--- The current flow through a diode valve.

collect around the cathode. Since the cathode loses electrons it perforce becomes positive. This tends to attract the electrons back. Electrons, then, are continually being emitted from the cathode only to fall back. If a positive charge is placed

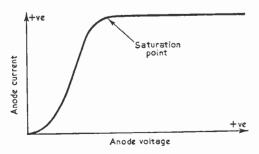


Fig. 2.- The anode voltage to current characteristic of a diode.

By A. Foord

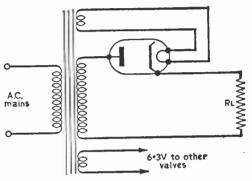
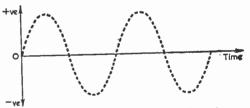


Fig. 3. (above) .--- A half-wave rectifier circuit.

Fig. 4. (below) .- The voltage input to a half-wave rectifier.



on the anode by means of a battery, then electrons are attracted to the anode, and flow through the battery back to the cathode. It will thus be noted that electrons flow in the opposite direction to conventional current. This is due to the fact that the first scientists investigating electrical phenomena chose their direction of current flow before electron flow was discovered. It will thus be seen that when the anode is positive, conventional current flows from anode to cathode, as shown in Fig. 1; but when the anode is negative no current flows. Therefore, the higher the anode voltage the greater the current. This is only true until all the electrons emitted by the cathode reach the anode. when this occurs no more current flows, and the "saturation point" is said to have been reached. If anode voltage is plotted against anode current as in Fig. 2, it will be seen that the curve is not linear. In other words the internal resistance of the diode varies with the current.

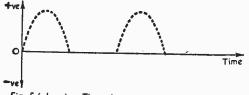
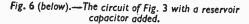


Fig. 5 (above).—The voltage output from a half-wave rectifier.



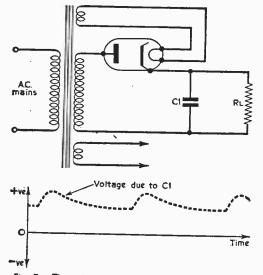


Fig. 7.—The voltage output from a circuit, such as that of Fig. 6.

The half-wave Rectifier Circuit

The complete circuit for half wave rectification is shown in Fig. 3. Basically it consists of a diode rectifier in series with a load resistance RL. The purpose of the mains transformer is to enable the A.C. voltage applied to the rectifier to be made a suitable value, and also to provide L.T. supplies for the rectifier and the heaters of other valves. Another advantage of the transformer is that it enables the chassis to be isolated from the mains, so that the chassis can safely be earthed. The input to the rectifier is of course a sine wave, a shown in Fig. 4. Since the diode conducts only when its cathode is negative to its anode, then the output voltage would be as given in Fig. 5. This is obviously a long way from a smooth D.C. voltage. The average value of the wave in Fig. 5 will be very much less than the average of Fig. 4, resulting in a low efficiency as well as a high ripple.

If however a reservoir capacitor CI is added to the circuit, as shown in Fig. 6, then the output is raised. Very simply, the capacitor is charged to the full peak voltage of the supply by each alternate half wave of the output, and then slowly discharges itself during the interval to the next half wave. The output voltage is then as shown in

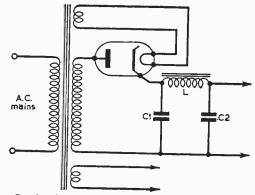


Fig. 8.—A half-wave rectifier circuit, with reservoir and smoothing capacitors and an inductor.

Fig. 7. Although this gives a much higher output voltage, there is still a fair amount of ripple left. To help reduce this to a reasonable value, the smoothing components L and C2 are added, as shown in Fig. 8. The D.C. voltage passes through L and over C2 unchanged but the A.C. component will divide itself between L and C2 according to the reactance of L and C2 and the frequency concerned (50c/s for normal mains). If the reactance of L were 15 times the reactance of C2, then the ripple would be reduced in the same ratio. From the A.C. point of view for every 15mV (say) developed across L, then only 1mV would be developed across C2, thus out of 16mV fed into the filter network only 1mV appears on the output.

(To be continued)

A Transistorised VHF Superhet

(Continued from page 707)

Final Inspection

Finally, a check should be made, using the aerial signal, to ensure that the correct band is being covered. If desired, final adjustments to T1 and C12 can be carried out on the Home and Light programmes. The receiver is very sensitive, so if this is done, one must ensure that the same stations are being received each time tuning is changed. The last adjustment is the ratio detector secondary core; this may need $\frac{1}{2}$ turn or so one way or the other, using a programme source of signal, to ensure that the minimum-noise tuning point is that giving best audible quality, and that when no modulation is being transmitted, equal noise each side of the tuning-point is obtained. The adjustment is fairly critical; so care will be needed.

For maximum sensitivity, the voltage across C37 should be used to indicate alignment rather than the volume of sound in the speaker. This method of alignment is more accurate and will result in some loss of bandwidth. Voltages measured will be much less than those obtained with a valveoperated receiver; a strong signal at the aerial may only give $\frac{1}{2}$ V or so, and weaker signals only 100mV or so, while good reception is obtained when only a very small voltage is measured across C37. The presence of only small voltages should therefore cause no dismay. PRACTICAL WIRELESS

Improving the All-band TRF

ADDING AN R.F. STAGE

By J. L. Wain

T was decided to rebuild the Beginner's T.R.F., described by F. G. Rayer in the March and April 1959 issue, making a few improvements and adding an R.F. stage. The final result was most satisfactory with extremely good sensitivity, selectivity, volume and tone. The first valve acts as the R.F. amplifier. A 2-pole 5-way switch enables the aerials to be tuned or untuned. VRI controls R.F. gain. The signal is fed via an R.F. transformer (detector coil) to the second valve, which acts as detector (as before). An EF39 valve was used as V1.

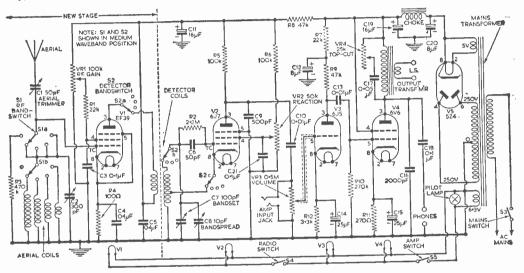


Fig. 1.—The complete circuit diagram of the improved receiver.

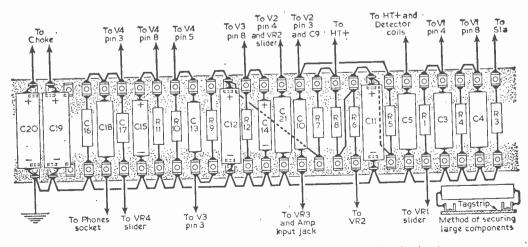


Fig. 2.- The wiring of the components on the large group-board under the chassis.

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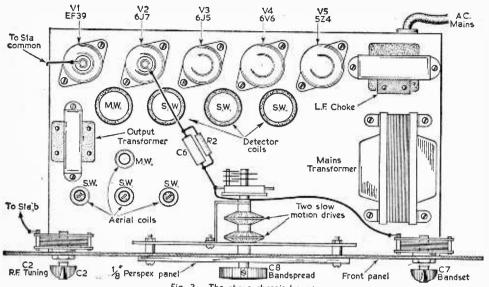


Fig. 3.—The above-chassis layout.

To make the circuit really comprehensive, two switches are included in the heater line, so that the power pack or the amplifier can be used alone. One switch, connected into the heater line between 6J5 and 6J7, is to cut out the tuner and the other connected between 6V6 and 5Z4 is to cut out the amplifier. A screened lead is taken from the volume control to a jack socket to provide an amplifier input.

Plug-in coils, did not appeal, so a 4-way 3-pole wavechange switch was used instead, with the H.T. and earth connected direct to the coils.

Chassis and Front Panel

The receiver is assembled on a chassis 7in. x 13in. x $2\frac{1}{2}$ in., and an aluminium front panel 16in. x 9 in. An aperture is cut in the front panel, with the aid of a fret saw and a half-round file, to allow a slow-motion tuning assembly to be fitted. The rest of the holes can be marked out from Fig. 4.

The extra stage can be added without alteration

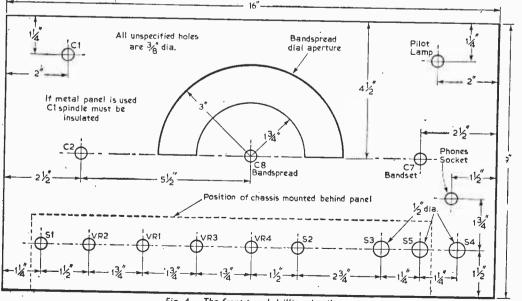


Fig. 4.—The front panel drilling details.

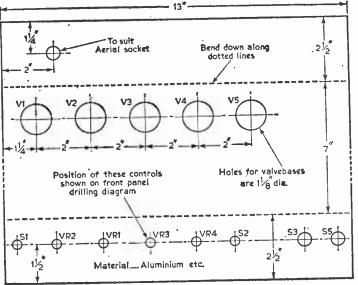


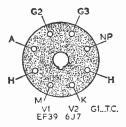
Fig. 5 .--- The chassis drilling details.

Aerial

to the original circuit (with the exception of the detector coils), but it is suggested that the receiver is stripped down and the construction started afresh.

Group Board

It was decided that practically all the components should be mounted on a group board, so a large 36-way group board was obtained. The components are arranged as shown in Fig. 2, and the group board is then fixed with the aid of 4B.A. bolts and lock-nuts to the underside of the chassis, and the remainder of the wiring can then be completed. It will be necessary to bend the wires of some of the larger capacitors, in such a way that they may be attached to the outer tags on the group board. It will be noted that C9 from the anode of 6J7 to earth is not included on the group board with the other components, because this was one of the flat mica type of



(To be continued) Power Pack Output Bandspread . Bandset DF Socket Trimmer Tuning . lot Phone Inpu Volume Cut Bandswitch DE Mains Amp. Radio Socket Bandswitch Reaction Gain Fig. 6 .- The front panel controls.

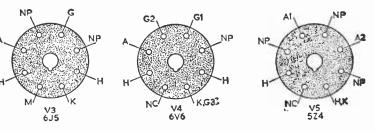


Fig. 7 .- The valve base connections.

condensers. A screened lead should be used for the connection from the slider of the volume control to the grid of 6J5.

Slow-motion Drive

The bandspread condenser C8 is fitted with a slow-motion drive so that stations can easily be logged. Two 5:1 drivers were purchased and connected together to give a ratio of 25:1. These drivers are made to fit directly on to the condenser spindle, but have a projecting lug which must be held by a bracket, or a long bolt and lock-nuts, or the drive will not function. A piece of aluminium about $1\frac{1}{2}$ in. x $2\frac{1}{2}$ in. is bent at right angles 1/2 in. from the bottom, to make a bracket for the bandspread condenser. The lugs of the two drives are also anchored to this bracket by the method explained above.

Practical Wireless

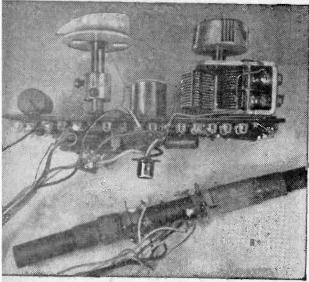


The P.W. 'Citizen' is the third blueprint design in our progressive series and has been especially designed for successful construction by those who, first began building radio sets with 'Tutor' in the October issue.

Preparing the Group Board

Refer to the Blueprint. Notice the numbering of the tags; as in the Mini-Amp, it is a good idea to stick paper strips on to the group board so that there is no confusion when wiring up by the numbers (see Fig. 2 on the "Mini-Amp" Blueprint). The numbering shown is when the strip is viewed with the soldering tags on top. Tags 17 and 35 are carefully removed by drilling partly through (on the rivet side of the board) with a $r_{\rm s}$ in. drill. The tags are removed so that the undamaged holes in the paxolin may take two small bolts which will eventually hold the tuning capacitor on to the board (see Figs 6 and 7). The spacing of the holes is already correct. The hole "D" in Fig. 3 is now enlarged to take

The hole "D" in Fig. 3 is now enlarged to take the $\frac{1}{2}$ in boss of the wave-change switch (S1), and two more holes are drilled each side of holes F and G as shown in Fig. 3. The position of these is important and therefore a *full-size template is* given in Fig. 15 (above). Two more holes are drilled near to tags 10 and 28. The oscillator coil should now be tried for a fit (the fixing tags go through the two outside holes). Do not attempt to force it into position for it may be damaged. If the fit is satisfactory, mount the oscillator coil from the rivet side of the group board and solder the fixing tags to tags 10 and 28 (see Fig. 4), making



The frequency changer unit

sure that pin 1 (near the red spot on the base-Fig. 8) lies near tag 10 and not tag 27.

Fixing the Tuning Capacitor and Wave-change Switch

The wave-change switch is mounted with the switch on the tag side of the board and the spindle on the rivet side. It is arranged so that the connections are in a similar position to those in Fig. 4 and the nut is then tightened up using a non-slip washer beneath it. It may be necessary to flatten out tags 4 to 8 and 22 to 26 as shown in Fig. 3, tag 8 being soldered directly, or wired, to the casing of the switch assembly (see Fig. 4).

The variable capacitor should now be examined carefully. It must have a metal screen between the two ganged sections and be fitted with small trimming condensers on the back (Cla and C2a-Fig. 7). The smaller section is C2 and the larger section is C1. Although three fixing holes are provided at the front of this condenser, these are not used. Two small threaded holes will be found on the back of the condenser and these are used for mounting. Bolts are fitted with solder tags and passed through holes 17 and 37 (Fig. 4) from the tag side of the strip. Two Ts in. thick washers are fitted on the rivet side of the strip and the bolts are then screwed into the holes on the condenser—the washers, in fact, space the condenser away from the board (see Fig. 7). Be careful that the bolts are not too long or they will badly damage the stators of the condensers. The mounted condenser will appear as in Fig. 7. Note

that both the oscillator coil and tuning condenser must be firmly fixed for good stability in operation.

Wiring in the Resistors and Fixed Condensers

Wire in R3 between tag 14 and tag 1 of the oscillator coil, using as little heat as possible, but making a good joint. Make sure that tag 1 is in the position shown in Fig. 4.

Wire R2 from tag 2 to tag 20, join 20 to 21 and connect R1 from 21 to 3 (Fig. 4). Wire C7 between tags 36 and 33 making the connections as short as possible. Fix C5, again with the leads as short as possible, between tag C of S16 and tag 29. Attach C3 between tags A and B of S16. Attach C6 across R3; i.e. from tag 14 to pin 1 on the oscillator coil. The condenser C4 is then soldered on the other side of the board to rivets 2 and 20 as shown in Fig. 6.

Wire tag 28 to coil pin 4, and tag 9 to coil pin 6. Join tag 33 to tag 29 with covered wire and then tag 29 to coil pin 3. Solder one of the soldering tags under the tuning condenser fixing bolts to tag 18 (see Fig. 4). Connect tag A of S16 to tag 8.

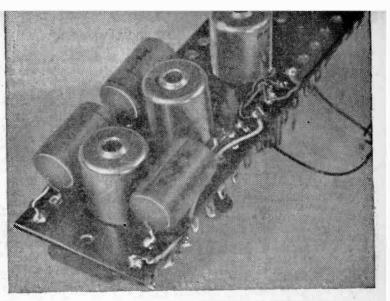
Above-chassis Wiring

Connect a red wire between tags 2, 8, 10, 14 and 18 as in Fig. 6. This is what



By J. Bisset

THE THIRD OF OUR PROGRESSIVE SERIES OF BLUEPRINT DESIGNS



The I.F. amplifler

would normally be called "Earth" or "Chassis", and is in this unit, battery positive.

Refer to Figs. 6 and 16 and note the wire connecting tag 11 and the stator of C1, the shape of this lead is quite important to prevent unwanted feedback.

Refer to Fig. 7 and connect a short lead from tag 36 to the stator of the oscillator tuning section C1.

Adding the Transistor

Check the wiring carefully. Put sleeving on the leads of the transistor (TR1) and then quickly solder them as follows (using a heat shunt as on page 509 of the October issue):—the base (centre lead) to tag A of Sla as shown in Fig 5; the collector (nearest the white spot lead) to coil pin 5 and the emitter (remaining lead) to coil pin 2. Position the transistor cenveniently but without bending the leads nearer than $\frac{1}{3}$ in. to the bottom flange.

Adding the Aerial

The aerial is made up of three parts (see Fig. 17). The long and medium wave coils are separate and may be slid along the ferrite rod to obtain optimum results. Two types are available (both under the part number RAW2). The type having thin leads from the actual coils connected to a circular tag strip in the middle is not the best for this design as the movement of the coils along the strip is restricted—the type having tag rings on each coil is to be preferred.

The coils are provided with coloured tags. If you have a meter, check that there is a connection between the sets of colours:—blue and yellow; black and yellow; white and green; white and red. (If not, the coil unit is faulty.) Connect leads up about 8in. long to the coil tags using the same coloured wires as the tag colours if possible, make sure that in soldering to the coil tags, the thin wires of the coils themselves are not detached.

Now test, the ends of the coloured leads as detailed above.

The leads should be held together in places with Sellotape or insulating tape, but should not be twisted together. The ends are connected to the group board unit as follows (see Fig. 5):—red to

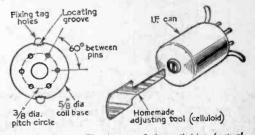


Fig. 15 (left).—The layout of the coil pins (actual size).

Fig. 18 (right).—A simple trimming tool for the oscillator and I.F. coils; the total must be made as shown so that the shank will fit inside the cores of the colls.

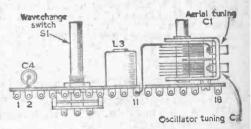


Fig. 16.—The position of the wire from C1 to tag 11 in the frequency changer section; this wire must be arranged exactly as shown to avoid the lower section of the variable capacitor gang (C2). tag C of S1a; yellow to tag B of S1b; green to tag B of S1a; black to tag 8; white to tag 21; and blue to tag 11. In addition a white lead about 4in. long between the white tags on both coils is required and connect a similar piece of yellow wire between the yellow tags (see Fig. 17).

THE I.F. AMPLIFIER

Preparation of the Group Board

No chassis is required, but some preparation of the board is necessary. Refer to Fig. 9. Note that the board has 12 holes down the centre. Holes C, F and J are used in the mounting of the transformers, but six other holes have to be drilled before these can be fitted.

Figs. 9, 14 (on the Blueprint) and 15 show that five holes are required to take the pins of each I.F. transformer and two more to take the tags for fixing. Do not force the transformers home; they are fragile, miniature, components and the tags must not be bent in any way.

Mounting the Transformers

These should be tested on receipt to make sure there is no connection between the outer case and Wires are now soldered to connect the following tags together: 23 to 24, 24 to 5.

Other Wiring

Refer to Fig. 12. A red wire is carefully soldered to the rivets 13, 11, 8, 6 and 3. It is bared only as necessary and care must be taken not to allow any spare or stray strands to short to another tag. A black wire is similarly soldered to tags 12, 9, 4 and 2. A white wire joins 1 to 10. Check these carefully.

Now solder in position the condensers C9, C10 and C11. Make sure the leads cannot touch any other tags but those intended; C10 is between 3 and 5, C9 between 26 and 27 and C11 between 22 and 21.

Fitting the Transistors and I.F. Transformer Leads

The transformer IFT2 is not wired as recommended by the makers but this will be mentioned later.

pin 5 of IFT3 is wired to tag 21; pin 5 of IFT2 is wired to tag 24; pin 5 of IFT1 is wired to tag 28; pin 2 of IFT3 is wired to tag 4; pin 3 of IFT2 is wired to tag 9; pin 3 of IFT1 is wired to tag 12.

The diode is now wired in between pin 1 of IFT3

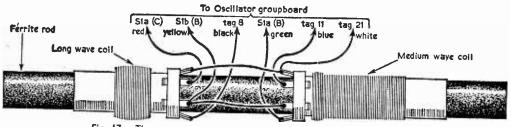


Fig. 17 .-- The connections to the coils on the ferrite rod aerial assembly.

any pin. They are mounted so that the blank holes fall over H, B and E and pin 3 in each case falls into J, C and F (see Fig. 9).

The transformers are fitted by pushing the pins through the holes and bending the fixing tags to reach the correct tags of the tag strip and then soldering them. The cans must be firmly fixed. A P50/3CC is fitted to tags 3 and 21, a P50/2CC to tags 8 and 26 and a P50/2CC to tags 13 and 30.

Readers may fit a numbered paper strip to the tag board to identify the tags as explained for the oscillator section. Check that no shorts occur between any tag and the can itself in every case, after fitting.

Fitting the Resistors

These are all fitted directly as shown in Fig. 10: R9 between tags 21 and 22; R8 between tags 6 and 24; R7 between tags 4 and 23; R6 between tags 26 and 27; R4 between tags 9 and 28; R5 between tags 10 and 28.

Fitting the Condensers

Condenser C12 is fitted between tags 1 and 19 ind C8 (bearing in mind the correct polarity) retween 28 and 11. and tag 1 with the red (or positive) end to the group board. Do not overheat this diode or it will be ruined.

Wire Tr3 as follows:—base (centre) lead, preferably sleeved, to pin 1 of IFT2 using as little heat as possible. The emitter lead is taken to tag 22 and the collector lead to pin 3 of IFT3. Fig. 11 should make this clear.

Tr2 is similarly attached, centre (base) lead duly sleeved to pin I of the first IFT1. The emitter lead is wired to tag 27 and the collector to pin 2 on IFT 2.

Supply

The supply may be taken from tag 27 on the "Mini-Amp" and no condenser or dropper resistors need be fitted. Thus, a red wire is taken from tag 13 to tag 2 on the "Mini-Amp" and a black wire from tag 2 to tag 27 on the "Mini-Amp".

Connecting the Unit to the Oscillator Stage

Although a separate 6V supply could be used, it is convenient to take the supply for the oscillator stage from the I.F. Section: a lead (red) is taken

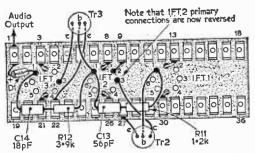


Fig. 19.—The wiring of the extra components necessary for neutralisation of the l.F. amplifier (see text).

from tag 2 of the oscillator to tag 13 of the I.F. amplifier and a black lead from tag 3 of the oscillator to tag 2 of the I.F. amplifier.

The oscillator output at 470kc/s is taken from tag 9 to pin 3 of IFT1 on the I.F. strip as shown in Figs. 5 and 11.

Volume Control

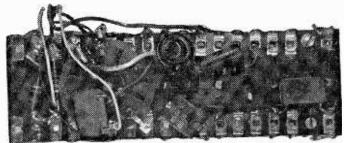
The output from the "Citizen" will be more than that from a crystal pick-up and when used with the "Mini-Amp" the simplest arrangement is to take tag 1 directly to the input of the "Mini-Amp" (centre tag of the amplifier volume control). This will mean Tr1 of the audio amplifier is being used unnecessarily on radio and more interconnection details will be given later, but this method of connection will enable the units to be lined up satisfactorily. Alternatively, for lining up, a pair of headphones can be used (between tags 1 and 3 on the LF, section).

The I.F. amplifier and the R.F. oscillator are now connected by three flexible leads. One lead is taken from tag 9 on the oscillator board to pin 3 of IFT1 on the I.F. amplifier. The other two leads go from tags 2 and 3 on the oscillator to tags 13 and 12 on the amplifier respectively.

The Alignment

Although it is always best to line up a superhet using a signal generator, it is not too difficult to carry out the alignment process using only signals received. Most constructors of the "Citizen" will not have access to a signal generator and therefore more details will be given of the method of alignment using received signals than that using a signal generator.

Before beginning the alignment, it is worthwhile



Rear view of the frequency changer unit.

to make another check of the wiring—in particular, make sure that the transistor connections are correct and that the wires for the battery connections are correct and will give the correct polarity. If the transistor or battery connections are incorrect, the errors in wiring will prove very costly when the unit is switched on for the first time.

When satisfied that the wiring is correct, switch on and at once there should be some sign that the unit is working. Of course, it will already be known that the "Mini-Amp" functions correctly, and if, when the "Citizen" is connected to the "Mini-amp", there is no sound from the loudspeaker, then it will be evident that there is a fault in the construction of the "Citizen".

The I.F. transformers in the "Citizen" are already aligned, and therefore it will probably be found that some stations are received right from the moment when the unit is first switched on.

For lining up the I.F. transformers, which is the first operation, a small trimming tool will be required—this can be fashioned from a small piece of celluloid or plastic as shown in Fig. 18. It must have the shape shown in the diagram and not a conventional screwdriver shape or it may damage the fragile cores of the I.F. transformers.

The coils on the ferrite rod should be positioned about one inch from each end of the rod, and then assuming that a station is being received, the rod can be turned so that the signal received from the station is weak—it will be found that when the rod points directly towards the station, the signal from it almost disappears—this is due to the directional effect of the ferrite aerial. The object of turning the aerial to the position of weakest reception is to reduce the effects of the AVC line of the set and thus prevent the effects of the adjustments from being masked.

When the position of weakest reception has been found, the volume control of the amplifier may be turned up to make the weak sound louder. The I.F. transformers may now be aligned.

Using the tool already made, turn the core of IFT3 for maximum loudness from the loudspeaker; repeat the procedure for IFT2 and then for IFT1—as the transformers are lined up, the signal will become progressively louder, and it may be necessary to re-orientate the aerial to reduce the signal. If the volume cannot be reduced sufficiently by repositioning the aerial, it is better to rotate the tuning capacitor to find a weaker signal than to reduce volume by adjusting the volume control. Finally, adjust the cores of each

transformer again until no further improvement, in volume, can be obtained.

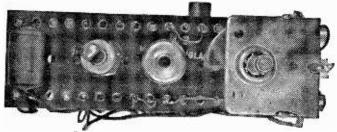
The I.F. transformers are now aligned and the settings of their cores should on no account be altered again—even as a last resort.

If a signal generator is available, the frequency of alignment is 470kc/s—use the full modulated output of the signal generator and couple it loosely to the I.F. amplifier, reducing the output as the transformers are brought into line. The alignment will be made easier if a large condenser— 0.1μ F to 0.5μ F is temporarily wired across C1.

R.F. Alignment

If a condenser has been used across C1, remove it and switch to medium waves (the anticlockwise position of S1, viewed from the rivet side of the board). When the tuning capacitor is rotated, stations should be received, the number depending upon the state of the circuit and the time of day. The alignment is carried out using two known stations—at night time, Radio Luxembourg and the Third Programme are suggested because these fall at the extremes of the tuning coverage. Other stations may be used, but one must be at the high frequency (short wavelength) end of the medium waveband and the other at the low frequency (long wavelength) end. Radio Luxembourg is specified above as it is broadcast on the highest frequency which it will be required to receive.

Turn the tuning condenser almost to minimum capacity—almost to its fully open position. Screw up the trimmers on the tuning condenser (C1a and C2a) tightly and then unscrew them about one turn. Now adjust the core of the oscillator coil until the station chosen at the high frequency end of the waveband is received. Then turn the tuning condenser to a position where the vanes



Front view of the frequency changer unit.

are about three-quarter closed—about 30° from being fully enmeshed. It is important to use a knob on the tuning condenser spindle for this operation so that the settings used for the two chosen stations can be found repeatedly. A makeshift cardboard dial could be fastened to the front of the tuning condenser so that pencil marks may be made corresponding to the stations. When the position has been decided for the

When the position has been decided for the Third Programme adjust the oscillator coil core (L3) until the signal is heard at the desired point. Return to the other station at the other end of the waveband and adjust the trimmer C2a until the station is at the desired point. Return to the Signal which will now be at a different position, but return the tuning condenser to the setting marked previously. Adjust the oscillator coil core to return the signal to the desired point. Return the tuning condenser to the setting and readjust the trimmer C2a until the signal is heard again. Repeat these adjustments until no further improvement is obtained and until both stations come in at the marked points. The oscillator alignment is then completed.

Next, turn the tuning condenser to the station at the high frequency end of the waveband. Adjust the trimmer C1a for best results. Set the tuning condenser to the station at the low frequency end of the waveband and adjust the position of the medium wave coil on the ferrite aerial for best results—the medium wave coil is the long, single layer coil, not the pile-wound coil. Repeat these two adjustments until no further improvement is obtained.

It should be noted that this latter part of the R.F. alignment should be carried out when the unit is housed in position in the case intended for it. Of course, the procedure may be carried out twice, once with the unit out of the case and finally with the unit in position to obtain optimum results. When the constructor is satisfied that the results are satisfactory, the medium wave coil may be sealed to the ferrite rod using Balsa cement or Durofix, taking care to keep the adhesive away from the wire of the actual coil.

The long wave alignment is simple and consists of tuning to the long wave Light Programme and adjusting the position of the long wave coil on the ferrite rod for loudest reception. This coil may also be sealed in position on the ferrite rod when results are satisfactory.

Neutralisation

Transistors, being similar to triode valves, have

appreciable self feedback which sometimes has to be neutralised. The I.F. amplifier described has been built in three prototypes and no troubles were experienced when IFT2 was wired as shown (Figs. 2 and 4).

Should any reader have trouble over "whisdes", this is a sign of poor alignment, or a badly wired oscillator section, or even that neutralisation is required. Fortunately the makers of the I.F. transformers have evolved an effective neutralisation system: connect a 1.2k resistor and a connect a

formers have evolved an effective neutralisation system: connect a 1²k resistor and a 56pF (1%) capacitor in series between pin 1 of IFT2 and pin 1 of IFT1 on the 1.F. amplifier. Connect also a 3-9k resistor and an 18pF (1%) capacitor in series between pin 1 of IFT2 and pin 1 of IFT3 (i.e. to the black end of the diode). Also, reverse the connections to pins 2 and 3 of IFT2 (see Figs. 11 and 19).

(To be continued)

Cable Contract

THE Republic of Indonesia has placed a contract with Associated Electrical Industries Ltd. for the supply of telephone cable. Since negotiations for this order began, cable manufacture within AEI has been rationalised and the cable will be manufactured by Telephone Cables Ltd., of Dagenham, an AEI subsidiary owned jointly with Enfield Cables Ltd.

The cables will be of the paper insulated underground and plastic insulated underground type and delivery will take place over a period of five years. The cable is being supplied to the Ministry of Land Transport, Posts, Tele-communications and Tourism.

FAULTS IN VHF/F.M. RECEIVERS 2-The I.F. Stages

By G. J. King

(Continued from page 607 of the November issue)

N Part 1 of this series we considered various faults that are likely to develop in the VHF tuner unit of an F.M.-only receiver or tuner or in the VHF tuner of a composite A.M./F.M. receiver. In the latter type of receiver, a VHF tuner fault is unlikely to affect the performance on A.M., so that while an A.M./F.M. set may function perfectly normally on the medium frequencies, it may be totally dead or exhibit a fault symptom only when switched to F.M. In this event, of course, the VHF tuner should first be investigated, but it should also be noted that similar trouble could occur owing to a fault developing in some other part of the set, as described in this article.

Switching Arrangements

In Fig. 8 is shown the two I.F. stages of a composite A.M./F.M. receiver. The heptode section of V2 functions as the first I.F. amplifier and when the receiver is switched to F.M., which is the position it is switched to in the circuit, the tuner I.F. signal is applied, via screened cable, to the heptode control grid through C22. The VHF tuner is made operative by a part of switch S4 which applies H.T.+2 to the tuner frequency changer, while another part of the same switch acts as local oscillator on A.M. It will also be noted that on F.M. a part of S2 short-circuits the A.M. AGC line.

These switches sometimes give trouble and can cause total failure or intermittent operation of A.M. or F.M. For example, it there is a poor connection in S4, H.T. may not get through to the VHF tuner The set would thus work perfectly on A.M. but not at all on F.M. Since H.T. is being switched, sparking occurs between the contacts and after a while this may produce an intermittent connection which would be likely to cause interference effects on F.M., possibly accompanied by tuning drift caused by variation of the H.T. voltage applied to the VHF frequency-changer valve.

Effect on A.M.

Trouble of a like nature may also result on A.M. due to high resistance switch contacts in the A.M. local oscillator circuit. This trouble rarely occurs in the ordinary wavechange switching, however, possibly because there is little or no H.T. current flowing through the switch contacts.

Various types of switch are used in A.M./F.M. receivers; some manufacturers favour the ordinary rotary type made up of several units on a common spindle. The switch units are positioned so

that they are as close as possible to the circuit which they are required to switch, and in this way the connecting leads can be kept as short as possible. This point should be remembered during the course of servicing. Another popular arrangement is the Plessey switch constructed of two long, narrow sections of low-loss insulating material. One section is fixed to the frame and the other is in the form of a slider which can move a limited distance along the fixed section, while the slider carries small metal contact strips which engage with the fixed contacts to provide the required switching arrangements.

Dual I.F. Transformers

In all composite receivers, the I.F. stages are coupled by two I.F. transformers connected in series. The primary winding of the F.M. I.F. transformer is always connected to the anode of the valve, while the secondary winding of the same transformer is connected to the grid of the following valve, as shown by IFT2 in Fig. 8. The A.M. I.F. transformer windings are then connected in series. The A.M. I.F. is usually 470kc/s, while the F.M.I.F. is 10.7Mc/s. This large difference in frequency allows this method of connection, since the impedance of the A.M. I.F. transformer is very low at 10.7Mc/s and it does not affect the F.M. I.F. coupling. Although there are separate transformers, when viewing the chassis, this may not appear to be so as only a single screening can is used to house both transformers.

Low Gain on A.M.

It sometimes happens that the sensitivity of the receiver falls off badly on A.M. while remaining fairly normal on F.M. Several cases of this symptom were caused by alteration in value of one of the fixed tuning capacitors across the windings of the A.M. I.F. transformers. These capacitors are usually installed inside the screening cans. Each core in the I.F. transformer should peak, but if this fails to happen with one core and it seems that the sensitivity could be improved by screwing the core farther into the former than is, in fact, possible, then the fixed capacitor across the associated winding will almost certainly have decreased in value.

Replacement should be made with components of identical type and value and the A.M. I.F. stages should afterwards be realigned, preferably with a signal generator and output meter, but failing that, by peaking the cores on the local station.

A.G.G. Troubles

In all composite receiver, AGC is applied in the normal manner on A.M. However, when the set is switched to F.M., the A.M. AGC line is usually shorted to chassis, and if there is F.M.

AGC then this is switched into circuit. F.M. AGC is not always used, and rarely used when the circuit features a phase discriminator detector. Where a ratio detector is used, an arrangement similar to that shown in Fig. 8 is used.

Here the F.M. AGC voltage is derived from across the ratio detector load resistor (to be dealt with in a subsequent article) and fed to the suppressor grid of the second I.F. valve, V3. In the event of a very strong signal, a high negative voltage will appear across the ratio detector load and this is used to reduce the gain of the I.F. stage accordingly.

This is a very simple circuit and rarely causes trouble. Nevertheless, should excessive fading and

attributable to failure or low emission of the triode section, even though the heptode section works normally as an 1.F. amplifier on F.M. A quick check for oscillator operation is to break the connection between the switch side of R9 and insert a D.C. milliammeter, with the negative terminal to the resistor. If the oscillator is working there will be a marked change of current when a short is applied across C26, the oscillator section of the tuning gang.

Noise on A.M.

Intermittent noise which varies in intensity has often been proved to be caused by a fault in the oscillator anode resistor R6. It is, in fact, possible

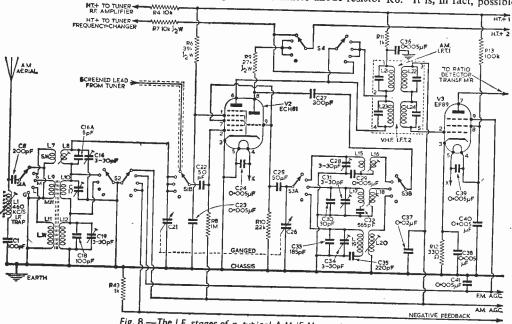


Fig. 8 .--- The I.F. stages of a typical A.M./F.M. receiver

distortion occur as the result of passing aircraft, for instance, the AGC feed from the ratio detector should be checked, as also should the associated components, such as C41 and switch S2. It has been known for poor insulation to develop on the switch, between two separate contacts, and allow an H.T. voltage to appear in the AGC circuit, thereby completely disturbing the normal operation. Similar trouble sometimes takes place on the printed wiring board, especially after a set has been in service for a number of years and excessive dust has been allowed to accumulate on the wiring.

A.M. Operation

"When a composite receiver is switched to A.M., the VHF tuner is no longer used, and the first I.F. amplifier (e.g., V2) is changed to a conventional A.M. frequency changer. The triode sec-tion is connected to H.T. and operates as the local oscillator.

Failure on A.M. but not on F.M. is often

to observe the effect on a milliammeter connected as described above by the current fluctuating in sympathy with the crackles and noise. This should lead immediately to replacement of the resistor. However, if this does not clear the trouble, and there is no sign of the noise on F.M., C25 and C27 should also be replaced.

As already intimated, noise may be generated in the oscillator switch, S4, and provided the contacts are not badly burned, the application of a good quality switch cleaner will solve the problem.

Printed Circuits

Most A.M./F.M. receivers use printed circuits which themselves sometimes introduce faults. When soldering parts into such a circuit, extreme caution should be observed to avoid overheating with the soldering iron. In the original type of printed circuit, undue heat results in the foil becoming loose from the board. This trouble may (Continued on page 729)

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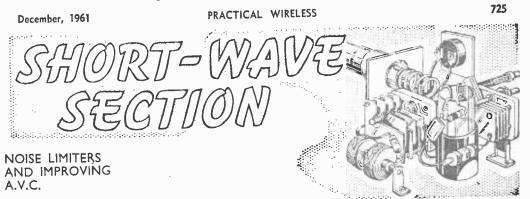
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NOISE limiter can be added to virtually any receiver circuit. Such a limiter is provided in some communications receivers, but is absent from some receivers of this kind. It is generally possible to add a limiter to commercially-made or ex-service receivers, though lack of space or other details may make this a little more difficult than with a home-constructed receiver.

Effects

Limiters of the type described here are included in the A.F. section of the receiver, and considerably reduce noise of the impulsive kind, originating in domestic equipment and switches, ignition systems,

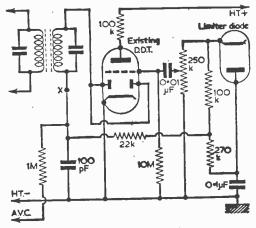


Fig. 1.--- A single diode noise limiter.

static discharges, and so on. These impulses are generally of higher amplitude than the average signal being heard, so the limiting device acts by cutting off signals above this level.

Such limiters are not intended to reduce noises such as general background hiss, or interference from other transmissions, or anything of that nature. But they can be very effective in helping clear the type of noise which causes loud, abrupt sounds in the speaker.

Many limiters introduce some comparatively slight audio distortion, or may cause some small reduction in amplification in the stage. For these reasons, a switch may be provided to short circuit the path through the limiter. The limiter is then switched in only when needed.

Self-Adjusting Limiters

It is convenient to have the limiter under the control of the AVC circuit, to obtain automatic adjustment to suit the strength of the signal received.

A circuit using a single diode, and providing limiting of positive peaks, is shown in Fig. 1. When the limiter is included at the time of building the receiver, it will be handy to use a diode

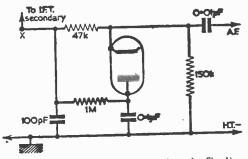


Fig. 2.—Another single diode limiter (see also Fig. 1).

from another stage, but there is no reason at all why a separate diode should not be employed. A suitable miniature diode for this and the other circuits is the 6AL5. If octal valves are preferred, a 6H6 is satisfactory. These valves are in fact double-diodes, but may be used as single diodes by joining the pair of cathodes, and the pair of anodes.

The limiter diode anode remains at about the AVC line voltage, and the valve has little effect on normal A.F. signals. A noise impulse is, however, able to drive the diode cathode negative with respect to the anode, so that the diode conducts. and the impulse is largely bypassed to earth.

A similar circuit, which can also be constructed as a separate unit, and added to an existing receiver, is shown in Fig. 2. The point "X" goes to the I.F. transformer secondary, as indicated by "X" in Fig. 1. The limiter stage can be constructed on a small chassis, or aluminium plate or bracket, and this can be mounted near the double diode triode stage of the receiver. Leads should be reasonably short, and clear of A.C. circuits, or should be screened, to avoid introducing hum.

Full-Wave Limiter

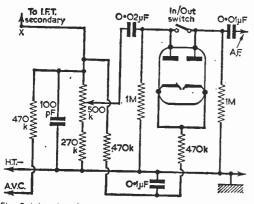
A very efficient limiter is shown in Fig. 3, and can use either of the valves mentioned. With the switch closed, the limiter is out of action.

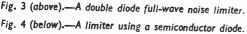
When the switch is open, the 500k potentiometer allows adjustment of the audio input, relative to the cathode voltage, which is derived from the AVC circuit, and this enables positive noise to be clipped at almost any required depth of modulation level. Clipping may be at well below 100% modulation level, with a corresponding reduction in noise. The remaining diode clips negative pulses.

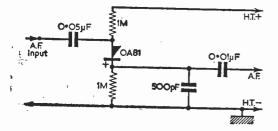
As neither half of the valve can conduct when its cathode is positive with respect to its anode, the circuit is very effective in limiting the depth of the audio signal which can pass. There is some loss of signal strength, but this is not very important with a receiver of usual kind having triode and pentode A.F. stages. (The triode will usually be part of the DDT state.)

This circuit may be set to clip at a pre-arranged level, or the potentiometer can be panel mounted. The in/out switch need not be immediately adjacent to the valve, and may thus be on the panel also.

A further limiter, using an 0A81 diode, is shown in Fig. 4. This may be included in an early part







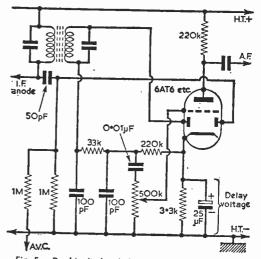


Fig. 5.—Double diode triode circuit with cathode bias.

of the A.F. circuit, for example between the diode detector and first audio stage.

In very small receivers, the limiter can be included before the output stage, especially if this operates headphones. There is no provision for following the signal strength level, in the way described for the self-adjusting limiters, but sudden bursts of noise will be reduced.

As all such random static noises generally are outside the control of the listener, it should not be overlooked that their effect can be much reduced by normal precautions. If they are mains-borne, a mains filter will be helpful. If they are picked up locally by the aerial, down-lead, or earth lead, it may be worthwhile changing the position of these, or using an anti-interference aerial. Static from some causes can be much reduced by employing a dipole or balanced type of aerial, instead of an end-connected aerial.

AVC Efficiency

Many receivers of fairly simple type do not have a very effective AVC system. It may allow overloading on local transmissions, or may be insufficient to counteract even moderate fading. If a signal strength or tuning meter is controlled from the AVC circu.; as is usually the case, this meter may fail to give any reading with weak signals.

A typical circuit providing detection and AVC is shown in Fig. 5. The triode section of the valve has cathode bias, and no AVC voltage is produced until the signal on the AVC diode exceeds the cathode voltage. This arrangement allows maximum gain to be obtained in the earlier stages, since no AVC is applied to weak signals. It also means that weak signals are not able to give a tuning meter reading.

A means of overcoming this is to return the cathode to chassis, as in Fig. 6. The AVC circuit is then able to operate at all signal levels. Bias for the audio amplifier is obtained by the flow of grid

(Continued on page 729)

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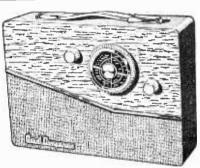
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(Continued from page 726)

current through the high value resistor, which should be 5.6M to 10M.

With this type of circuit, tuning meter indicaations will become possible at very low signal levels. A very similar effect, for comparative purposes, may be obtained by shorting the cathode bias resistor in Fig. 5, though the A.F. amplifier will then be less effective.

The increase in AVC action will bring about a general reduction in volume; since a larger AVC voltage is being obtained, this is unavoidable. With

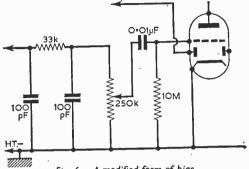


Fig. 6.—A modified form of bias.

very small receivers, the increase in AVC efficiency can still be worthwhile, if sufficient volume is obtained.

Controlled Stages

R.F. and I.F. stages frequently receive the screen grid supply through a single resistor, as in Fig. 7. This is a convenient and economical method, but does not allow best operation of the AVC circuit.

When AVC is applied, the cathode current falls, and there is a drop in current through the 33k resistor. This reduced current also reduces the voltage drop in the resistor, so that the screen grid voltage rises. In many cases this rise is considerable, and, to some extent, it off-sets the reduction in gain caused by the AVC circuit. If the screen is fed from a potential divider, as

If the screen is fed from a potential divider, as in Fig. 8, this effect is greatly reduced. Resistors R1 and R2 are so chosen as to maintain the voltage

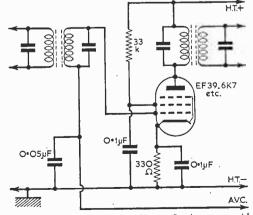
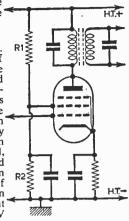


Fig. 7.---An I.F. stage with a dropper for the screen grid.

Fig. 8.—A modification to the circuit of Fig. 7 to increase the effects of the AVC.

at about the usual figure. The lower the value of these resistors, the more stable will the screen grid voltage become. Unfortunately, very low values are impossible because the bleeder current taken from the H.T. supply would be excessive. Even quite high values will, however, help to avoid so much fluctuation in voltage. A total value of about 50k will require an additional H.T. current of 5mA, with a 250V supply.



Calculation

The current through R2 can be found by dividing the required screen grid voltage by the resistance value; for example, it would be about 3mAwith 150V on the grid and 47k for R2. The current through R1 is the total of the screen grid current, and the current through R2. That is, 5mA, in this example, if the screen grid takes 2mA. The value of R1 is therefore such as to cause the required voltage drop at this current. If the H.T. line is 250V, then 100V must be dropped. So from V/I the value of R1 is 20k or 22k (the nearest preferred value). The bleeder current is V/(R1+R2), or 250/69k, or under 4mA.

FAULTS IN VHF/F.M. RECEIVERS

(Continued from page 722)

also be caused by the normal operating temperature in the set after several years' continuous use.

These troubles eventually result in a break in one of the printed wires. Unfortunately, the break may not be readily visible without the use of a magnifying glass and may also be of an internittent nature. In a grid circuit or in the detector, a wiring break may not cause total failure, but could result in curious hum effects which might not show up until the temperature inside the set rose and the disconnection occurred owing to flexing of the printed board.

Such faults can be difficult to locate, but the trouble can often be located by gently flexing the printed board, applying pressure to various sections until the fault condition can either be brought on, or corrected. One must be very careful, however, to ensure that a break is not unwittingly caused by rough handling during this process. When the fracture has been located, it may be repaired either by thoroughly cleaning the surface of the conductor and applying a blob of solder across the break, using the minimum amount of heat for the shortest possible time, or by replacing the whole length of the conductor with a wire between its two ends.

(To be continued)

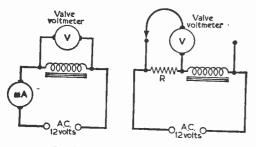
How to measure INDUCTANCES

CHECKING THE INDUCTANCE OF COILS SHOULD NOT BE By S. Jacob OVERLOOKED WHEN FAULT-FINDING

-APACITANCE and resistance can quite easily be determined by bridge methods or by using simple measuring instruments. However, inductance measurement is not quite so easy. There is some very complicated inductance testing gear on the market, but most of it is beyond the scope of most amateur needs. For this reason, coils are usually checked for continuity and for any possible earthing shorts and left at that. On the other hand, an inductance test will give a far more accurate indication of the condition of a coil, whether it is for A.F., I.F., or R.F. circuits. Shorted turns in R.F. coils and damaged cores

in A.F. chokes are revealed by inductance testing. Resistance and continuity tests are not likely to i show up these faults.

The casiest way to test A.F. coils is by the





ŧ

ammeter and voltmeter method shown in Fig 1. First of all the resistance of the choke is measured as accurately as possible, with an ohmmeter, or using the same circuit as Fig. 1, but with a D.C. voltage divided by the current in amperes. Now a suitable 50c/s supply is connected to

the circuit and the volt and milliammeter readings **calibrated** cathode ray oscilloscope, or any other **type** that does not draw current. If there is no A.C. milliammeter available, use the circuit in Fig. 2. Connect the valve voltmeter or its equivalent across R and determine the current in the circuit by dividing the voltage by the resistance of R. Now measure the voltage across the coil. Make sure that the supply is as steady as possible so that it remains the same for both tests.

Find the impedance of the coil by dividing the voltage measured across it by the current flowing. Now the inductance of the coil is calculated from:

$$L = \frac{\sqrt{(Z^2 - R^2)}}{314 \cdot 2}$$

where L is the Inductance in Henries; Z is the Impedance in Ohms; R is the Resistance (D.C.) in Ohms.

Let us take an example:

An A.F. choke is checked with an ohmmeter and found to have a resistance of 500Ω . Assuming there is no A.C. milliammeter available, the circuit in Fig. 2 is set up. A 200 Ω resistor is used as R. Let us assume that a 12V supply from a transformer is available. First measure the voltage across R. In this case it is, say, 3. Make a note of this and quickly check the voltage across the coil; perhaps it turns out to be 22. Now disconnect the apparatus and get down to calculations.

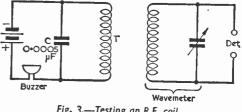


Fig. 3.—Testing an R.F. coil.

First, determine the current flowing through the circuit.

$$I = \frac{E}{R}$$
$$I = \frac{3}{200} \text{ amps}$$

This is from the 3V found across the 200Ω resistor R. Now find the impedance of the coil

$$Z = \frac{E}{I}$$

$$Z = 22 \div 3/200$$

$$Z = \frac{22}{I} \times \frac{200}{3}$$

$$Z = 1467\Omega$$

This is the impedance of the coil calculated from the voltage found across it which was 22, and the current flowing at the time was 3/200A. Now.

$$L = \frac{314 \cdot 2}{\sqrt{(Z^2 - R^2)}}$$

(Continued on page 737)

or



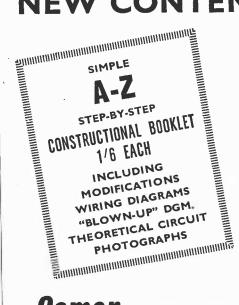
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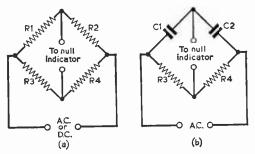


Fig. 1(a).—Basic Wheatstone bridge circuit. Fig. 1(b).—Basic de Sauty bridge circuit.

At balance $\frac{R1}{R2} = \frac{R3}{R4}$ for the Wheatstone bridge

and $\frac{C1}{C2} = \frac{R3}{R4}$ for the de Sauty bridge.

The bridge was energised by a small instrument transformer giving approximately 55V A.C. In the practical circuit (Fig. 2), R3 and R4 consist of a 10k w.w. potentiometer—the slider of which goes to the null indicator.

Standards

٦

The circuit, up to now, has become the form of Fig. 2. For the sake of clarity, it is still arranged in the familiar Wheatstone bridge manner. The standards Rx, Ry, Rz, Cx, Cy, Cz, should be as accurate as the constructor can afford. Rx, Ry, Rz are high stability 1per cent 4W components, with the exception of Rx which has a 1W rating.

| The values | are:—Rx | 100Ω |
|------------|---------|-------------|

| Ry | 10k | |
|----|-----|--|
| | | |

Rz 1M

Cx, Cy, Cz again are 1per cent tolerance. The values are:-

Cx 100pF Cy 10,000pF (0·01μF) Cz 1μF Cx and Cy should be best quality ceramic or mica components, with very low leakage. They are easily obtainable with a 1per cent tolerance. Cz, having a value of 1μ F, is rather difficult to obtain in anything except a $\pm 20per$ cent tolerance, which is useless for this purpose. Except by writing to the manufacturers for a special component (which is likely to be expensive), this component will be impossible to obtain. However this is easily overcome by obtaining a condenser of nominal capacitance 1μ F, but which is actually slightly below 1μ F in value, and padding it by putting a small capacitance in parallel with it to bring the value up to 1μ F exactly. A method of doing this will be described later.

The potentiometer used can be any value from 5k to 250k. For accuracy and long-term stability, it should be a wire-wound component—the larger its size, the better. In the prototype, a 3in. diameter component was used.

Bridge Supply

The A.C. supply for the bridge can be anything from 25V to 120V r.m.s. The prototype used 55V. The only point to be careful with in choosing a transformer is that on the low resistance range ($Rx=100\Omega$) the total resistance in the bridge will be in the order of 200 Ω and the current drawn from the transformer may overheat it. Provided that the measurements are made fairly rapidly, all should be well using a transformer rated at 500mA. The circuit is fused for protection.

The null indicator used in this instrument is the dual sensitivity EM34 magic eye. The constructor may use any "eye" though—EM80, 6U5, etc.

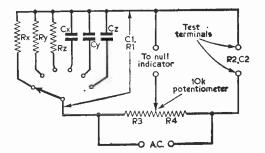


Fig. 2.—Practical combination of Figs. 1(a) and 1(b).

By M. A. Harris

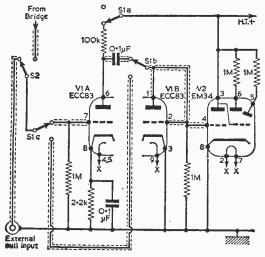


Fig. 3 .- The amplified null indicator.

-although the EM34 is the most sensitive. An amplifier is used in conjunction with the magic eye to provide the instrument with greater sensitivity. The amplifier (Fig. 3) is switched out to obtain an approximate balance point, and then switched in to obtain greater accuracy. This facility is provided so that rapid readings are easily obtained. If the amplifier were left permanently connected, the eye would be rather slow to open, especially on the capacitance ranges.

D.C. Restoration

From the amplifier, the signal is D.C.-restored so that only a negative voltage goes to the grid of the magic eye. In the prototype a double triode an ECC83—was used simply because it was to hand (Fig. 3). One triode was used as the voltage amplifier and the other half strapped as a diode to D.C.—restore the signal. If the constructor wishes, he may use any double triode or a single triode and a valve rectifier.

A switch was incorporated into the prototype to enable the magic eye and amplifier to be used to detect a null other than that from the bridge. The connection was brought out on to the front panel as a coaxial socket.

Screened lead is used where shown because the bridge uses 50c/s and hum could be picked up in the wiring and this would not enable the magic eye to indicate a sharp, definite null.

Power Supplies

Almost any sort of power supply can be used with this bridge, provided it gives 10mA at 250V and 0.5A at 6.3V. The instrument can be powered from another instrument that has enough power to spare. The prototype used a 250V half-wave winding and a 6.3V winding on a small replacement type of transformer. The rectifier used is an EZ80, so that a separate heater winding is not required. A full-wave winding could be used if the constructor wishes. Since the EZ80 has two anodes (in the prototype these were strapped together), it would serve quite well as a full-wave rectifier. Almost any rectifier could be used, however (a 6H6 or EB34 has been tried and found successful). A metal rectifier would also be suitable, since the rating need only be 10mA or so. An H.T. fuse was fitted.

The on/off switch is of the double-pole variety, thus isolating the equipment completely from the mains. A panel light is fitted—either the neon type wired (via a limiter resistor) across the bridge side of the switch, or an ordinary 6.3V bulb wired across the heater supply.

The circuit of the power supply is straightforward. The supply terminals were brought out to a three-pin miniature mains socket screwed on to the front panel. If the constructor does not wish to go to the expense of buying one of these, the mains lead can go through a hole in the back panel.

For the sake of clarity, the complete circuit diagram is given in Fig. 4, together with a list of parts (page 737). It is advisable to use screened (Continued on page 737)

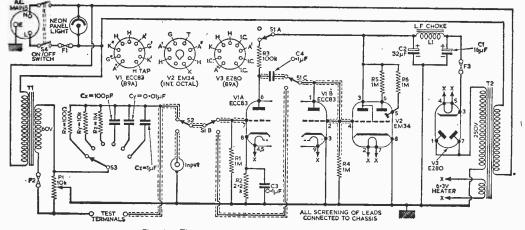


Fig. 4.- The complete circuit diagram of the bridge unit.

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|--|---|---|---|---|--|---|---|
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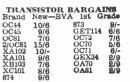
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1

1

-3

12.61

lead where shown on the diagram to prevent the pick-up of hum.

COMPONENTS LIST

(bridge transformer) 200-250V primary, TI 40-120V secondary (mains transformer) 200-250V primary, 250V, 30mA, and 6·3V, IA secondaries **T2** Choke-almost any small smoothing choke 11 is adequate RI, R4, R5, R6 IM 1W R2 2.2k 1W R3 100k 1W C1, C2 16μF and 32μF, 350VW C3, C4 0·1μF 350VW Sla, b, c 3-pole 2-way switch **S2** Single pole, changeover switch 1-pole, 6-way switch **S**3 **S4** 2-pole, on/off switch Rx 100Ω I per cent H.S. IW 10k I per cent H.S. $\frac{1}{4}W$ IM I per cent H.S. $\frac{1}{4}W$ EZ80 (6V4) Ry Rż VI **V**2 ECC83 (12AX7) V3 EM34 100pF I per cent Сх Су 100,000pF I per cent Cz $I \mu F I$ per cent 2 insulated terminals, I coaxial socket, knobs, etc

Construction

A suggesterd layout will be given next month. The pointer of the bridge is made out of $\frac{1}{36}$ in. thick Perspex glued to the potentiometer knob. In the prototype, the Perspex was obtained from the protective screen of an old television set. A hairline was scratched down the centre, as shown, on both sides. This eliminates any parallax errors in reading off a value from the scale.

The chassis is 2in. deep and U-shaped, the front panel being of hardboard or plywood. An easy and economical way of mounting the magic eye is to bend a piece of metal at right angles, and on the longer side bolt two Terry clips. The inside of these clips is covered in felt or foam rubber. The magic eye slides into this. and it can then be bolted on to the front panel. The resistance and capacitance standards are soldered direct to the range switch. Do not fix Cz (1 μ F) permanently in place, as this will require padding.

The components R4, R5, R6 were soldered direct on to the magic eye holder. The other small components can be wired direct to the associated valve base.

Apart from these above considerations, construction should be relatively straightforward.

Calibration

As with any instrument, the accuracy is limited by (a) the standards employed;

(b) by calibration.

The standards employed for this are 1per cent high stability types, and one cannot do better than that.

The calibration can mean extensive use of expensive instruments, but the method to be described next month requires only the use of a protractor, a slide rule, and patience.

(To be continued)

How to measure inductances

(Continued from page 730) $\sqrt{(1467)^2 - (500)^2}$

$$L = \frac{314 \cdot 2}{314 \cdot 2}$$

$$L = \frac{\sqrt{2152089} - 250000}{314 \cdot 2}$$

$$L = \sqrt{1902089}$$

By using a set of square root table or a slide rule we find that 1902089 becomes 1379.

Now
$$\frac{1379}{314\cdot 2} = 4\cdot 3H.$$

R.F. Coils

R.F. and I.F. coils are tested by a completely different method. Fig. 3 shows the general idea.

High frequency is generated by means of the 0.0005μ F condenser C, the coil under test T and the buzzer B. A wave-meter is placed nearby, and it is connected to a detector which can be an oscilloscope or a simple crystal circuit with a pair of headphones.

The buzzer is turned on and the wave-meter is tuned to maximum signal strength. The wavelength in metres is used in

$$L = \left(\frac{W}{1884}\right)^2 \times 2000$$

L is the inductance in Microhenries.

W is the wave-length in metres.

For example, say the maximum signal were found at 540m. In that case:

$$L = \left(\frac{540}{1884}\right)^2 \times 2000$$

$$= (0.287)^2 \times 2000 = 0.082 \times 2000 = 164\mu H$$

This formula holds good provided C is 0.0005μ F. If it is desired to alter this value the formula:

$$L = \frac{W}{1884} \times \frac{1}{C}$$

has to be used (C is in μ F).

The apparatus for A.F. and R.F. coils are simple and so are the calculations, but a slide rule, or a set of square root tables will help considerably.



A SMALL PORTABLE SET EMPLOYING THREE TRANSISTORS

HE basic requirements to be fulfilled by this design were that it should be an easy circuit to construct and set up; it should be cheap, com-pact and give acceptable results from the local transmitter. It must be emphasised that this is by no means a long-range receiver (this being the province of the superhet circuit) and it is intended only for use in the primary service area of a transmitter.

Circuit

The R.F. section of the circuit is somewhat unusual, consisting of an R.F. transistor used as a reflexed R.F./A.F. amplifier with regeneration (reaction). The ferrite aerial is tuned by means of



By J. G. Ransome

that the collector current drawn by Tr2 is as near as possible to 10mA.

The values of the various components used in the circuit-with the exception of R4-are in no way critical, and the circuit should function per-

fectly well with components the values of which are within $\pm 20\%$ of those shown. If "surplus" types of transistor are used, it is suggested that a "white spot" type be used for Tr1, a "red spot" for Tr2, and a "green-yellow spot" type for Tr3. If a red spot type is used the bias on the base may require a little adjust the bias on the base may require a little adjustment, and this may be found by a trial and error substitution of R2.

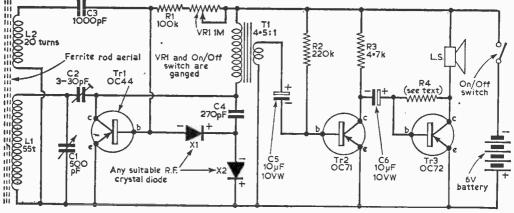


Fig. 1.—The circuit of the receiver.

C1. Regeneration is controlled by C2, which is pre-set for optimum performance, the final, fine adjustment being controlled by R2, which varies the bias on the base of Tr1. The R.F. stage feeds a voltage doubler type of detector in the base circuit of Tr1. T1 serves a triple purpose in this circuit; the primary acts as a collector load for Tr1 and also as an R.F. choke. The transformer then acts as a coupling unit for the detected A.F. and passes it on to the audio section (its proper function).

The A.F. section is a simple, very conventional R/C amplifier, the final output of which is delivered directly into a small, relatively high impedance loudspeaker, obviating the necessity for an output transformer. The bias of the output stage is controlled by R4, which also provides a little feedback. The value of R4 depends on the current drawn by the transistor, which can vary as much as $\pm 50\%$ in transistors of the same manufacture. The value of "R" is chosen so

Construction

The coil L1 consists of 55 turns of 28s.w.g. enamelled wire close wound on a $\frac{3}{8}$ in. diameter

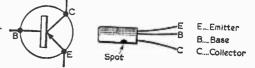


Fig. 2.—The connections of a transistor.

ferrite rod. The rod may be of any length, but it is recommended that the minimum length should be 2in. The coil should be insulated from the ferrite rod by first winding on a layer of Sello-tape, and then winding the coil on near the end of the rod. L2 consists of 20 turns of the same gauge wire wound over a paper sleeve so that (Continued on page 746)



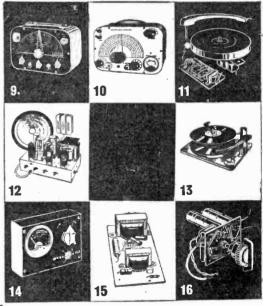
- 10. SIGNAL GENERATORS. Cash \$4,19,5 P. & P. 5/6. Coverage 120 kc/s to 84 Mo/s. Case 10 x 61 x 41n. Size of scale 61 x 31n. 2 valves and reothler. A.C. maine 320-250 v. Internal modulation of 400 c.p.s. to a depth of 30 per cent. modulated or unmodulated R.F. output continuously variable 100 millivations. C.W. and mod. switch variable A.F. output and moving coil output meter. Accuracy ± 2 per cent.
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A Dry-Battery Recharger

SERS of transistor receivers are not usually very worried about the cost of battery replacements. There is, however, one special disadvantage about dry batteries, namely the inescapable drop in voltage with use, which progressively limits the undistorted output available from the loudspeaker. While certain cells are made which exhibit the property of constant voltage during their life, these are not readily available "over the counter", and are also decidedly expensive.

Circuit

The simple circuit given here is designed to afford a "topping-up" for dry cells. It can be made up from "spares-box" components, because nothing is very critical. Fig. 1 is self-explanatory.

The transformer in the author's instrument is an old heater transformer, giving a voltage output of 13.3, with a tapping for 25% "boost"; it was previously bought as a cathode ray tube isolating transformer. As an alternative, an old audio output transformer might well be used, as long as a turns ratio between primary and secondary of about 20:1 can be chosen.

The rectifier may be any L.T. rectifier, capable of supplying up to 100mA; or two good selenium elements could be assembled from an old unit.

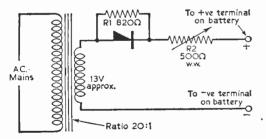


Fig. 1.-The circuit of the instrument.

D.C. Plus A.C.

The resistor in parallel with the rectifier requires some explanation. Experiments with pure D.C. indicate that with dry cells of the usual Leclanché type, uneven depositing of the zinc occurs, and re-charge results in loss of potential life, and considerable over-voltage after charge with rapid drop in service. The superimposition of A.C., and the fact that no reservoir or smoothing circuit is included, enables these difficulties to be avoided. The 500Ω variable resistor should be of the wire-wound type. It serves to adjust the charging current to the required value.

"TOPPING-UP" TRANSISTOR RECEIVER CELLS

By N. Mears

In first putting the unit into service, the charging current should be measured. Batteries of the DT9 size may be recharged overnight at at least 50mA, while smaller sizes should receive proportionately less. If the resistor R2 is provided with a pointer knob, the type of battery can be indicated on a scale and the control set accordingly when recharging.

Connections

Apart from the obvious precaution of ensuring that the battery is properly connected (best made certain by providing non-interchangeable terminal clips) there is little to worry about. It should be noted that it is not practicable to recharge a fully run-down battery, because the zinc will probably be on the point of perforation. However, if, following a few hours' use, a suitable topping-up charge is given, a Lew battery can be induced to give twice its normal life at least, and of course the voltage is maintained at a much better level in use. The writer uses two DTG batteries for alternate weeks, and after 24 weeks the original voltage of both is still found while the receiver is working. There seems little sign that either battery is nearing the end of its life, although, using the receiver four hours daily, the expected life of each would be about six weeks at the current delivered.

The circuit described above was designed for 9V transistor batteries. These are probably the most often used, but only a variation in series variable resistor is needed to take account of voltage up to 12 and down to 1.5.

The circuit is not at all suitable for running a transistor receiver direct, even if fitted with a reservoir capacitor and smoothing circuit.

Russian Delegation at Marconi's

M.R.S. A. MIKOYAN and three other members of the Soviet State Aircraft Committee delegation to Farnborough visited Marconi's Aeronautical Division at Basildon recently. The visit was arranged as a result of discussions at Farnborough last week with the Russian delegation, which included the aircraft designers Antonov and Ilyushin.

The delegation was hown round the Marconi airborne communications and navigational aids laboratories where they were particularly interested in the development of Doppler Navigators for civil aircraft and in the Sixty Series navigation and communication equipment. They were also shown a demonstration of closed circuit television equipment which is currently being used in airborne and airport applications.

Tracing Intermittent Faults

THE PROCEDURE TO USE WHEN NORMAL METHODS REMOVE THE FAULT TEMPORARILY

By "Serviceman"

By far the simplest fault to trace is that which causes complete failure of the set. The reason for this is that the fault condition is constant, and that complete failure must mean that there is an absolute and permanent breakdown somewhere in the circuit. The usual technique is to trace back from the speaker to the front of the set in an endeavour to locate the defective component or broken wire. A process of elimination would be used and it would not be very long before the fault were revealed.

Disappearance of Fault

When the fault is intermittent, however, the problem is often complicated since any slight disturbance to the circuit may clear the trouble temporarily and cause the set to work normally for a while. It may happen simply by connecting a voltmeter or even by scraping the aerial or earth wire on the socket. It is absolutely pointless to make ordinary tests on the now normal receiver, for all will be found to be in perfect order and it is not always possible to promote the fault condition again by circuit disturbance.

The usual exercise is to let the set continue playing out of the cabinet and in an accessible position in the hope that it will go off again so that a further attempt can be made to trace the origin of the trouble. Unless one is very lucky or uses special servicing techniques it may well need many attempts before the fault is eventually located.

There are other intermittent faults such as intermittent distortion, crackling and frying which are equally as complex to diagnose unless they are given special attention, but first let us investigate the intermittent failure fault.

Adjust and Listen

When it has been established that ordinary testing methods cannot be used because any slight disturbance to the circuit causes the set to burst into life, the set should be left running in its cabinet and with the back cover in position until it goes off again. When it goes off, quite a lot of information can be obtained without touching the inside of the set at all. First an ear should be held very close to the loudspeaker to detect the normal residual hum which should be present on all sets.

If hum is present, one can be sure that H.T. supply and L.T. circuits are in order; also the speaker and the output stage. If there is no hum, then the problem should not be very difficult to solve. The back cover should carefully be removed and the wires connecting the speaker to the output transformer should be moved about and slight tension applied to them to test the soldered joints at both the transformer and speaker tags. A dry joint on the speaker lead is a strong possibility at this stage.

Testing the Loudspeaker

If the trouble persists, it would be a good idea to connect a pair of headphones or another speaker across the existing speaker. If reception is now restored, the set's speaker has an intermittent fault which it may or may not be possible to repair.

Ouput valves sometimes go intermittent, which can be tested by tapping the valve sharply with

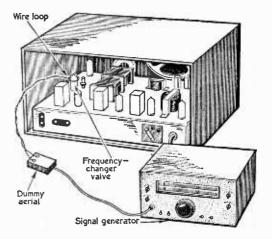


Fig. 1.—To prevent an intermittent fault from being corrected when test instruments are applied, a signal can be applied from a loop of wire slipped over the envelope of the valves, as shown.

the handle of a screwdriver. A series of loud crackles followed by normal reception would indicate that valve replacement would cure the trouble. Triode-pentodes, such as the ECL80 class, are particularly prone to this trouble towards the end of their life.

(Continued on page 745)



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(Continued from page 742)

Although it is unlikely for the H.T. supply to fail intermittently, a similar, though lighter tap on the rectifier may give some idea of a faulty valve. With early type 5V rectifiers, the filament had a habit of going open-circuit in an old valve when very hot. This would cause a gradual fade-away, however, and would rarely be corrected by circuit disturbance—such trouble can be seen by the filament being out and the valve cold.

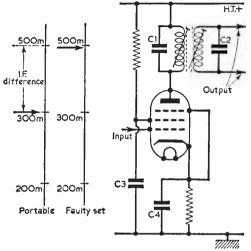


Fig. 2 (left).—The local oscillator of a suspect set can be checked by operating a portable receiver close to its frequency-changer. When the portable is tuned to a station or carrier, a whistle will be heard when the suspect set's oscillator is tuned to the same frequency. The two tuning points are caused by the l.F. difference in relation to the oscillator frequency. Fig. 3 (right).—Intermittent drop in volume is often caused by trouble in the l.F. capacitors C1 and C2. Instability and distortion should lead to a check of capacitors C3 and C4.

Intermittent faults have been known to occur in smoothing resistors from the rectifier cathode and, in some cases, in smoothing chokes. Generally speaking, when there is no residual hum, the intermittent fault is rarely affected by circuit disturbance, and normal fault tracing techniques can be adopted during the period that the fault is present.

Signal Circuits

Intermittent faults may occur on the signal alone; for example, a normal residual hum may be present and the set may exhibit the normal hiss which increases in volume as the volume control is turned up. This is almost the same effect as when the aerial is removed from a set which is working correctly, and is a symptom which is really sensitive to circuit disturbance.

If there is a distinct alteration in the level or the tone of the noise at the speaker when the volume control is turned, or if a slight crackling occurs when the control is rotated, then one can be reasonably sure that the whole of the A.F. section of the receiver is working correctly. At this stage, and with the volume control at maximum, it may pay to turn the wavechange switch through its various ranges. If there are definite "clicks" when the switch is turned from band to band, then there is little doubt that the I.F. stages are also in order.

Unfortunately, the fault at this time may clear, owing to the disturbance caused by operating the wavechange switch. Should this be the case, the back should be put on the cabinet and the set left running until it fails again.

I.F. Stage Check

The next time the set goes off a more scientific approach to the problem will be necessary. A loop of about twenty turns of 26s.w.g. insulated wire should be prepared of suitable diameter to slip easily over the valves. The ends should be twisted together for about a foot or so and connected to the terminals of a dummy aerial, as shown in Fig. 1. The dummy aerial should then be connected to the R.F. output terminals of a signal generator in the ordinary way.

Now, when the set goes off, the loop of wire should be slipped over the frequency-changer valve and the generator adjusted to full output at the set's I.F. If the set's I.F. stages are in order, the modulation of the generator signal will be heard from the speaker. In this way it is possible to establish what is right and what is wrong in a set without actually touching or disturbing the circuits. If there is no output here, the loop should be transferred to the I.F. amplifier valve. At this point, the signal output may only be very low and it is essential that the generator is on full output and the set's volume control turned full on. The generator will also need to be tuned accurately to I.F. peak.

I.F. peak. If there is output from the I.F. amplifier, but not from the frequency changer, the trouble would obviously be somewhere in the first stage. However, if there is also a strong output from the frequency changer, one can be almost certain that the local oscillator is at fault.

Local Oscillator Check

There is a good way of checking local oscillators without touching the suspect set if another radio or small portable is available. When the intermittent set is in one of its "good" conditions, the portable should be held as close as possible to the frequency-changer valve and tuned to a fairly strong station or carrier around 300m (mediumwave). The intermittent set should also be switched to the medium waveband and the tuning adjusted around the 500m mark until a beat note or whistle is heard on the station to which the portable is tuned.

The whistle, of course, is caused by the set's local oscillator beating with the portable's signal. The dial settings will not coincide on the two receivers, since the oscillator frequency is removed from the tuned frequency by the intermediatefrequency, but on most sets the oscillator works at a frequency equal to the tuned frequency plus the I.F. The difference between the two settings is thus the intermediate-frequency, as illustrated in Fig. 2.

When such a beat note has been established, it then remains to wait for the intermittent set to go off. If the beat note also disappears, the trouble is definitely caused by local oscillator failure.

This idea has been employed effectively to trace intermittent noise. The set would suddenly develop very loud "frying" and crackling noises, but as soon as a test prod was applied to obtain some idea of the cause of the trouble, the disturbance would nearly always clear. The local oscillator was suspected but there was no proof. The beat note set-up was arranged and the whistle was perfectly clear while the set was working correctly, but as soon as the crackle started from the set's own speaker, this was also heard from the portable superimposed on the whistle, thereby proving without doubt that the local oscillator was the culprit.

A valve change did not help, but the trouble was finally located to the capacitor coupling the local oscillator coil to the anode of the oscillator valve. Similar trouble has been located to the grid coupling capacitor in the oscillator circuit and, more often, to the anode feed resistor of the oscillator valve. In very old sets or in sets which have been subjected to damp, the local oscillator coils themselves are often to blame.

Intermittent Drop in Volume

A common intermittent trouble is that the set is working perfectly normally when suddenly there is a marked decrease in volume. Again, if the circuit is disturbed, the fault may correct itself or the fault may be corrected (and sometimes brought on) by operating an electric light switch or electrical appliance somewhere else in the house.

This points conclusively to an R.F. or I.F. fault. The local oscillator is rarely to blame, but in the majority of cases, particularly if the trouble occurs on all wavebands, one of the fixed tuning capacitors across the I.F. transformer windings is responsible. Such components are forgotten since

TRANSISTOR TRF RECEIVER

(Continued from page 738)

the coil is free to move along the ferrite rod.

The actual physical layout of the components is not at all critical, and any convenient layout may be employed. As the layout will depend upon the size of the cabinet, and this in turn will determine the length of the ferrite rod employed for the aerial coil, no layout details will be given.

Operation

The setting up of the circuit is not very difficult if the following instructions are noted. Having checked the wiring for mistakes, connect the battery as shown, ensuring that the correct polarity is observed. Advance the potentiometer (VR1) to about half way when some sort of sound will be heard from the loudspeaker. With the aid of a milliammeter, adjust the collector current of Tr3 to 10mA by finding a suitable value for R4, either by trial and error, or by making R4 a variable resistor, and adjusting to the right current and then substituting a fixed resistor of equivalent value. The value of the resistor used need only be a near value—there is no real need for great accuracy. L2 should be moved as close as possible to L1 and the beehive trimmer C2 adjusted until the set starts to oscillate. By varying C1 it should be possible to tune in the local station. When this

they are usually housed in the transformer can, and one reaches the stage where pretty well every component in the set has either been checked or replaced.

This type of intermittent trouble is brought on by minute transient currents, as produced by any electrical disturbance, causing intermittent opencircuit (or correcting an open-circuit) in a capacitor carrying R.F. or I.F. such as C1 and C2 in Fig. 3. When such components are subjected to an ordinary capacitance test, the fault rarely shows, and it is only when R.F. or I.F. signals are present that they break down.

The best thing to do in a case like that is to replace all the I.F. transformer capacitors and be on the safe side. This of course should also lead to realignment of the I.F. transformers or, at least, to peaking of the iron-dust cores on a signal.

Effect of Temperature

Temperature has a great effect on intermittent faults, and while a set may exhibit intermittent symptoms when in the cabinet with the back cover on, when the chassis is removed it may work for days without trouble. In this event, the chassis should be worked up to a high temperature by covering it with a cloth or blanket (taking care not to forget about it, though). This should quickly bring on a fault that is sensitive to temperature.

An ordinary domestic hair dryer can be used to advantage to concentrate local heat on a particular circuit section. To localise the heat even more, a soldering iron is useful as it can be held very close to a suspect component. Intermittent instability and distortion are other faults caused by intermittent decoupling capacitors, such as C3 or C4 in Fig. 3, and a soldering iron has been used successfully by the author on many occasions to promote a fault symptom of this kind.

has been done the trimmer C2 should be backed off until oscillation just ceases. By varying the position of L2 with respect to L1 and by suitably adjusting C2 the position of maximum sensitivity may be found. L2 is then sealed in position with sealing-wax or Sellotape.

It will be found that the sensitivity control will have an effect on regeneration, and this will be found useful in areas where there are two transmitters—one being a little more powerful than the other.

| COMPONENTS LIST | | | | | | |
|--|--|--|--|--|--|--|
| Resistors | | | | | | |
| RI 100k 1/W R3 4.7k 1/W | | | | | | |
| R2 220k 1/2 R4 see text | | | | | | |
| VRI IM (with switch) | | | | | | |
| Condensers | | | | | | |
| Cl 500pF variable | | | | | | |
| C2 4-30pF beehive trimmer | | | | | | |
| C3 0·001 μF (1,000 pF) | | | | | | |
| C4 270pF | | | | | | |
| $C5 I0\mu$ F I0VW | | | | | | |
| $C6 I0 \mu F I0 W$ | | | | | | |
| TI type interstage transformer: 4-5 : I (Forti- | | | | | | |
| phone 55 or similar) | | | | | | |
| XI, X2 crystal diodes (any type suitable for R.F.) | | | | | | |
| Loudspeaker: C.M.S. 50 (T.S.L.) | | | | | | |
| Ferrite rod, wire for coil, etc. | | | | | | |
| | | | | | | |



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December, 1961



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The Editor does not necessarily agree with the opinions expressed by his correspondents

Whilst we are always pleased to assist readers with their technical difficulties, we regret that we are unable to supply diagrams or provide instructions for modifying commerical or surplus equipment. We cannot supply alternative details for receivers described in these pages. WE CANNOT UNDERTAKE TO ANSWER QUERIES OVER THE TELE-PHONE. If a postal reply is required a stamped and addressed envelope must be enclosed with the coupon from page iii of cover.

B.B.C. TELEVISION RECEPTION

SIR,—I have seen one or two letters recently about listeners picking up television on wavelengths far removed from the actual transmission, and I would like to offer a suggestion. I have experienced a similar fault, and in some cases it has been direct radiation from a badly adjusted receiver, but in most cases I have investigated it was mains borne. Why the signal should get into the mains I cannot say, unless the mains wiring acts as some sort of aerial, but the fitting of one of the special suppressed plugs into the mains outlet will generally prevent the trouble. Naturally, any aerial which a listener uses should be erected well clear of any television aerial.—F. BAILEY (Willesden).

VINTAGE MODELS

SIR,-How I agree with Mr. Newman (July issue) O concerning the reproduction from an old receiver. I do really think that if anyone could recover one of these old sets from a loft or some other place where it has for long been deposited, and get it going again at correct voltages, etc., one would be agreeably surprised at the per-formance. After all, we rely now mainly on higher efficiency valves for the performance which we obtain, whilst in the older days circuity was, in my opinion, of much more effect. We had very large coils with a minimum capacity across them, and I feel sure that the response from these efficiently tuned circuits was capable of much wider frequency bands than we get in modern apparatus. Has not F.M. been forced upon us because owing to the modern valves and circuits which they call for cut-off resulted at both ends of the scale? I would very much like to hear one of these old sets cleaned up and put to work on a modern transmission.—J. MANSELL (Warwick).

ADDING COMMUNICATION FEATURES

SIR,—The receiver series under the above title has been most interesting, but I do not think that the addition of the arrangement described will provide a reader with a real communications set. I have used two or three American communications receivers and I feel that much of their efficiency is due to the coils and associated circuitry. I have not seen any English sets with the same types of coils, ceramic formers, silvered wire and reliable switching. Is it that the conditions in America are so poor that the receivers have been developed to make the most of those conditions and as a result are more efficient than those developed in this country?—E. R. Le PAGE (S.E.15).

AMATEUR TRANSMITTING LICENCES

SIR,-Considerable interest has been expressed $\overset{\mbox{\scriptsize O}}{}$ during recent years by readers on the possibility of the provision of a low power transmitting permit, other than the current Radio Amateur's Transmitting Licence. Whilst it would not appear likely that any form of Novice Licence will be permitted, which frankly could lead to a lot of misguided tinkering with obsolete ex-government transmitters on our already overcrowded L.F. amateur frequency bands, there would appear to be a case for the consideration of a Citizen's Radio Permit similar to that in current operation in the U.S.A. For the benefit of readers who have not previously encountered mention of Citizen's Band Radio, it operates basically as follows; initially in 1949, class A and B Citizen's Radio Licences were originally issued by the FCC for the use of frequencies at UHF, but this did not become popular for the average man in the street for his two-way radio, house to car, fishing boat to shore camp, across town office to home, etc., mainly due to the cost of VHF equipment and very restricted line of site transmission range. Powever, in 1958 the class D Citizen's Radio Service was inaugurated whereby any American citizen over the age of 18 years could obtain a licence upon application, free of charge, without any form of test, simply by filling in the appropriate form and making postal application to the FCC providing the station is to be used for any legitimate purpose, i.e., private, social, or business communication with other similar stations. Transmissions to take place in the authorised frequency band 26,965kc/s to 27,255 kc/s on any of 23 specified crystal controlled channels spaced 10kc/s apart. (VFO operation not permitted.) Ground wave working only is allowed; attempts to work DX are illegal, as also are CQ calls.

FCC regulations govern the design of equipment, most of which takes the form of low cost transceivers, crystal controlled, maximum legal power input 5W, A.M. phone only, frequency tolerance of 0.005%. The simplest of these consist of single channel crystal controlled TX with super-regenerative receiver section, ranging to the more elaborate multi-channel switched tuned TX with double super crystal controlled receiver. Both mobile and home based stations equipment being available. Kits of parts with pre-wired frequency determining sections being also available for the boys who brew their own rigs. Typical operatinranges are reported as follows: Mobile-to-mobile 7-10 miles in city, 12 miles in country;

Base-to-mobile 10-15 miles in city, 17 miles in country;

Base-to-base 20 miles in city, 25-30 miles in country.

Very little TVI is encountered due to the low power used, the inclusion of L.P. and H.P. filters taking care of the odd cases.

With regard to a possible service of this nature on our side of the Atlantic the first consideration would probably be which part of the already loaded frequency spectrum to use. The writer would venture to suggest a 300kc/s slice at the H.F. end of the present ten metre amateur band as being suitable and least likely to cause anyone inconvenience, at least it would be more interesting to listen to than the present deadly silence which prevails.—R. ELLIS G3BKM (Huddersfield).

TRANSISTOR NOMENCLATURE

SIR,—As the number of types and makers of transistors grows, are we to be eventually landed with the same bewildering array of cryptic nomenclature as now exists with valves, whereby none but those who are actively connected with their use can readily identify a particular item by means of the figures and letters intended for that purpose. It would seem that in the past the position has been greatly aggravated through the selfish interests of individual manufacturers each producing items bearing identical functional characteristics but with physical differences rendering them not directly replaceable with each other. In the name of sanity, why must this be so? Of American origin a 6J5 is a 6J5, no matter who makes it. Any distinctive merits must surely be judged by the consumers in the end.—P. ASHDOWN (Lancs.).

Personal Phone for Transistor Receivers

A SIMPLE MODIFICATION THAT CAN BE MADE TO MOST TRANSISTOR SETS

KECEIVERS such as the PRACTICAL WIRELESS Pocket Super het, and other transistor sets, may be used to operate a personal earpiece, for individual listening. There are circumstances when this is an added convenience, and it avoids disturbing others. Ample volume is available with-

Ample volume is available without using the output stage, so the earpiece can be operated from the driver stage. This is most easily arranged by fitting a miniature twin socket, and wiring it in parallel with the driver transformer primary. That is, from battery negative line to driver collector, as shown in Fig. 1.

If preferred, it is in order to use ordinary medium impedance headphones, but when the maximum portability is required, a miniature personal earpiece will be more

personal earpiece will be more suitable. It is essential that the correct type of earpiece, of reliable manufacture, and in proper order, should be employed. If not, volume may be poor, or reproduction may be distorted. A medium impedance unit will be satisfactory, and this can be expected to have a D.C. resistance of approximately 250Ω . The driver will work best into a moderately high impedance, and low impedance units are unsuitable.

The output stage may be rendered inoperative by switching out the battery negative supply to these transistors, as in Fig. 1. A miniature on-off By S. Burrows

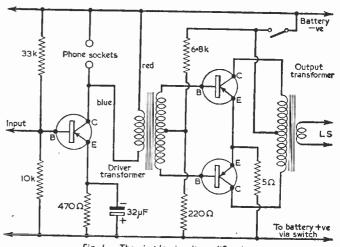


Fig. 1.—The simple circuit modification.

switch can be made from an Ardente S1100 wafer, if desired, or a screw-down type of switch can be made by soldering a 6B.A. nut to a small bracket, and running a short 6B.A. bolt through this. An alternative is to arrange that the earpiece plug opens fixed contacts when inserted in its socket.

Miniature plu \circ s and flexible cord may be obtained for the personal phone. Should any difficulty arise in obtaining these items, they may be obtained from Home Radio (Mitcham) Ltd.



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Club News m m III

BARNSLEY AND DISTRICT AMATEUR RADIO CLUB Hon. Sec.: P. Carbutt, G2AFY, 19 Warner Road, Pogmoor, Barnsley, Yorkshire. At the Annual General Meeting held in September, the following officers were elected; G. Wigglesworth—President, H. Eyre— Vice-president, P. Carbutt—Secretary, P. Bell—Treasurer and A. Balmforth—Chairman. Meetings are held on the second and fourth Evideum of a the meeting

Meetings are held on the second and fourth Fridays of each month, BRADFORD RADIO SOCIETY

Hon. Sec.: M. T. Powell, G3NNO, 28 Gledhow Avenue, Roundhay, Leeds 8.

Koundnay, Leeds 8. On September 12th the first meeting of the new session was held, and a talk on "4 metre mobile" was given by D. Millard. Meetings commence at 7.30 p.m. Slow morse classes, if pre-viously arranged, are held before meetings. On October 10th members took part in "Quiz Night", devised by G3EKE. A film show at St. George's Hall was given on October 24th.

In response to several requests the above Society will be holding In response to several requests the above Society will be notifing special Junior Section meetings from 7 to 7.45 p.m. before the meetings which are held at Cambridge House. The purpose of these Junior meetings will be to promote the interest of Radio and Electronics as a hobby by giving short lectures, demonstrations and individual help to our younger members. It is hoped that by providing these additional facilities to our young members, some of the boys will become so interested that they will wish to carry their studies further and eventually fill posts in the Radio and Electronics field.

Future Event November 15th-"Modern Methods of Communication" by F M Price

BRIDLINGTON AND DISTRICT RADIO SOCIETY Hon. Sec.: J. H. Jones, G3GBH, Flat 2, 18 Vernon Road, Bridlington.

The winter programme is now complete and new members or visitors are always welcome at meetings which are held on Wednes-day evenings, starting 7.30 p.m., at the The Royal Naval Cadets H.Q., "T.S. Contest", Applegarth Lane, Bridlington.The classes for the R.A.E. next May, are held each Tuesdayevenings at 7.30 p.m. Morse classes are also being held.The solution to hold a mobile rally and hamfest on SundayJune 24th, 1962, at the Spa Royal Hall, Bridlington.The winter programme is now complete and new members or

June 24th, 1962, at the spa Royal Hair, briding only BURSLEM AMATEUR RADIO CLUB Hon. Sec.: W. Luscott, 36 Rothsay Avenue, Sneyd Green, Hanley, Stoke-on-Trent. The society meets at Burslam Town Hall at 7.45 p.m., on the third Wednesday of each month. An interesting programme is arranged for each meeting, and new members are always welcome. A fifteen minute morse session is included in each meeting.

DERBY AND DISTRICT AMATEUR RADIO SOCIETY Hon. Sec.: F. C. Ward, G2CVV, 5 Uplands Avenue, Little-over, Derby.

Recent activity has included the Fifty Years of Wireless Exhibi-tion, a Mobile Rally and Hamfest, and the Festival of Youth Exhibi-tion. A Hitchcock gave a talk on "Direction Finding equipment" on October 18th and a surplus sale was held on November 1st.

Future Event: November 11th-RSGB Top Band contest.

GUILDFORD AND DISTRICT RADIO SOCIETY Hon. Sec.: J. R. Barker, G3PDX, 35 Banders Rise, Merrow, Guildford. 🌡

On October 1st, members took part in a Car Rally, organised by the society, who will put the proceeds towards the club contest transmitter

On 19th September, Benis Walker, (G3OLM) gave an interesting talk on SSB. A talk about some simple electronic units was given for members on October 12th.

Future Events:

November 9th—A talk on 2-metres. November 24th—A film show.

MORTHERN HEIGHTS AMATEUR RADIO SOCIETY Hon. Sec.: A. Robinson, G3MDW, Candy Cabin, Ogden, Halifax, Yorkshire.

At the meeting held on September 6th, members heard a lecture on Radio Astronomy given by Mr. Dougherty. On November 1st. Mr. Falkus gave a talk on Hi-Fi. Future Events:

November 15th—An informat evening. November 29th—G3OGV will give a talk about converters for 2 and 4 metres.

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REPORTS OF CURRENT ACTIVITIES

PETERBOROUGH AND DISTRICT AMATEUR RADIO SOCIETY Hon. Sec.: D. Byrne, G3KPO, Jersey House, Eye, Peter-

borough. The barbecue organised by members of the society, at Alwalton,

provedia great success. On November 3rd, the Annual General Meeting of the Society

was held. Future Event:

December Ist-Christmas Party.

PLYMOUTH RADIO CLUB

Hon. Sec.: R. Hooper, 2 Chestnut Road, Peverell, Plymouth. Business meetings are held on the first Wednesday of each month at the Guild of Social Service building and all meetings on

Tuesdays are held at the clubroom.

Future Evends:

November 14th—Sale of surplus equipment. December 6th—Judging for the "Ernie Hillyard" trophy.

TORBAY AMATEUR RADIO SOCIETY Hon. Sec.: G. Western, G3NQD, 118 Salisbury Avenue,

Barton, Torquay. After the formal business of the September meeting had been finished, members enjoyed two films.

tinished, members enjoyed two limits. It was announced at this meeting that two members of this society were placed first and second in the British section of the 1960 Scandinavian Activity Contest. The two members being, first G3IHJ, and second G3GM. Meetings are held at the Y.M.C.A., Castle Road, Torquay, on the

second Saturday of each month.

WANSTEAD AND WOODFORD RADIO SOCIETY Hon. Sec.: K. Smith, 82 Granville Road, Walthamstow, London E.I7.

London E.17. The junior section of the society have been particularly active recently, and have recently held a Camp and Field Day. A series of lectures on basic radio knowledge is in progress, and four members are entering this year's Autumn R.A.E. Meetings of the junior section are held on Tuesdays at 7.30 p.m., and the senior section meets on Wednesdays at 8.00 p.m.

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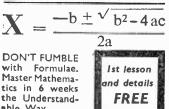
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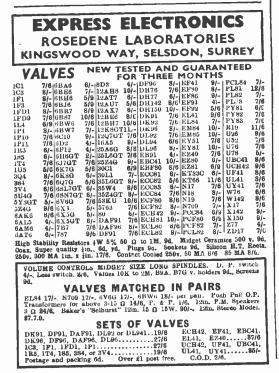


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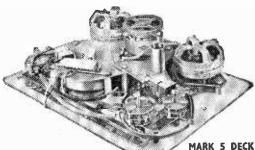
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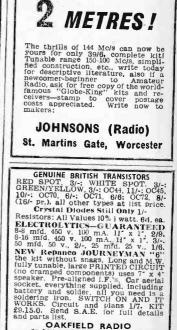
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December, 1961

