# OCTOBER 1961 <br> Practical 2. <br> <br> Wh1:3M5SS 

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PUSH－PULL ULTRA LINEAR OUTPUT＂BUILT－IN＂TONE CONTROL PRE－AMP STAGES Two inpat sockets with associated controls allow mixing of＂mike＂and includes 5 valves，ECC83，FCCB3 ELSA．EL84．5Y3．High Quality seo－
tionally wound output transformer tionally wound output transformer operation，and reliable small con－ densers of curreat manufacture．IN－ DIVIDUAL CONTROLS FOR BASS AND TREBLEE＂L1ft＂and＂Cut．＂ lcs．Six nerative reedback loops． Hum level $50 \mathrm{D} . \mathrm{B}$ ．down．ONLY 23
 OUTPUT．Suitable for use with all ma OUTPUT．Sultable for use with all makes and types of pick－ups and mperophones．Com－ parable with the very best designs．For STANDARD or LONG PLATING IRECORD FOF IUSICAL LNSTRUMENTS guch as STIEING BASS，GUITARS，etc．，OUTPUT SOCKET With plug provides 300 v ． 30 mA and 6.3 v ． 1.5 a ．For supply of a RADIO FEEDDER UNIT．Size approx．12－9－7in．For A．C．mains $200-250$ v． 50 c．D．s．Output for 3 and 35 ohms speakers．Kit is complete to last nut．Chassis is fulty punched．Full （Or factory bullt $51 /$－extra）．
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COLLARO RC 475 SPEED MIXER AUTO－CHANGERS．Turnover studio Plck－up head．for 200 －250 $\mathbf{2}$ ．A．C．\＆ 7.19 .6 ． Carr，4／6．
THE SKYFOUR T．R．F．RECEIVER A design of a s－valve long and Medium wave 200－250 ．A．C．Mains receiver with selendum rectifier，High gain H．F，staze and low distortion detector．Valve line－up 6K7，SP61．6V6G．Selectivity and quality excellent．Simple to construct．Point－to－ Point wiring diagrams，instructions and parts list，1／9，maximum ballding costs e4．18．6．inc．attractive Wainut veneered
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GIJA MINIATURE 2－3 WATP GRAM AMPLIFIER．For use with any single or auto－change unit．Output for $2-3$ ohm speaker．For $200-250$ V．A．C．mains．Size $11 \neq 2 \nmid \times 2 \mathrm{fln}$ ．Controls：Vol and Tone with switch．Only E9／8．


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PILAMENT TIRANSFURMERE All with $200-250 \mathrm{v} .50 \mathrm{c} / \mathrm{s}$ ，prlmarles $6.3 \mathrm{\nabla}$ ． ．5 \％．5／9；6．3 ₹． 2 a，7／6；0－4－6．3 v． 2 a，7／9： v． $\mathfrak{a}$ ，7／11； 6.3 v． 3 a， $8 / 11 ; 6.3$ v， 6 a， 176； 12 \％． 1.6 a twice， $17 / 6$ ．
Midget Battery Pentode 66：1 tor 3S4，etc．
Smali Pentode， $5000 n$ tö3a
Sraall Pentode $7 / 8,000$ n to 30
Standard Pentode 5,000 n to 30
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$10,000 \Omega$ to $3 \Omega$
Push－Pul 8 watts．सL8i4，or 8 BV 8 to
Push－एull $10-12$ watts $6 \dot{V} 6$ or EL8 $\ddot{1}$ to
Push－Pull 10－12 watts to matich 6ví or EI 84 to 3－5－8 or 150
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Push－Pull 20 watts，＂sectionaliy wound．6L6．KTGR etc．，to 8 to $150 \ldots 49 / 9$

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Primaries 200－250 v． $50 \mathrm{c} / \mathrm{s}$ ． 250 v． $60 \mathrm{~mA}, 6.3$ v． 2 \＆ Both above stze 2 ． 8.3 V． 2 a． $\because 11 / 9$ Both above size $21 \leq 24 \times 2 t i n s$.

| $150 \mathrm{ma}, 7-10 \mathrm{H} 250$ ohms．． $11 / 9$ |  |  |
| :---: | :---: | :---: |
|  |  |  |
| 100 mA .10 H 200 ohms． |  | 8／9 |
| $80 \mathrm{~mA}, 10 \mathrm{H} 360$ ohms． | $\bullet$ | ． $5 / 9$ |
| $60 \mathrm{~mA}, 10 \mathrm{H} 400$ ohms． |  | 4／21 |

## CHARGER TRANSFORMERS

All with $200-230-250$ V 50 c／s Primaries： 0－9－15 v．14 8，11／日；0－9－15 v． 2 a，14／日；0－9－15

AUTG（Step up／Step down）THANG． $0-110 / 120-230 / 250$ \％ $50-80$ watts． $13 / 9$ ； 1－110／120－200／230／250 \％． 150 watts．27／9．

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At last a quality F.M. Tuner Kit at a price you can afford. Just look at these fine features, which are usually associated with equipment at twice the price.
$\star$ F.M. Tuning Head by famous maker. $\star$ Guaranteed Non-drift. \& Permeability Tuning. + Frequency coverage 88-100 $\mathrm{Mc} / \mathrm{s}$. $\star$ OABI Balanced Diode Output. * Two I.F. Stages and Discriminator. * Attractive maroon and gold dial ( $7 \times 3 \mathrm{in}$. glass). $\star$ Self powered, using a good quality mains transformer and valve rectifier. $\star$ Valves used ECC85, two EF80's, and EZ80 (rectifier). $\star$ Fully drilled chassis. $\star$ Everything supplied, down to the last nut and bolt. $\star$ Size of completed tuner $8 \times 6 \times 5 \frac{1}{2} \mathrm{in}$. $\star$ All parts sold separately.

$$
\{4.19 .6 \text { Plus } 816
$$

Circuit diagram and illustrations, $1 / 6$, post free.

OUTPUTSTAGE \& SPEAKER FOR F.M. TUNER UNIT
All parts, including speaker, ECL 82 valve, and simple instructions to make two. stage output unit for converting F.M. tuner into F.M. receiver. ONLY 45/., plus $4 / 6$ P. \& P.
E.M.I. 4-speed Player and P.U.
 Heavy 8sin. metal turntable. Low flutter performance $200 / 250 \mathrm{~V}$ shaded motor with tap at 80 V for amplifier valve filament if required. Turnover LP/78 head. Price $89 / 6$. Plus 416 P. \& P .

SUPER STEREO KIT MK. II A kit of ready-built units only requiring interconnection. Comprising two midget 3W amplifiers, push button switch, transformer, control unit (bass, treble and vol.), power pack, two speakers, indicator light, valves (ECL82, EZ80 range), and comprehensive instructions.

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\{3.19 .6 \text { Plus } 616
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F.M. TUNER HEAD


A permeability tuned tuner head by a famous maker, supplied without valve (ECC85) 1816 plus 1/9 P. \& P. Valve 816 extra.

## HARVERSON SURPLUS CO. LTD.

## Introducing HARVERSON'S 39/6

Monaural Amplifier Kit
In response to numerous requests from delighted purchasers of our "SUPER STEREO KIT" We have produced a "MONAURAL AMPLIFIER" on similar lines.

* A UCL 82 valve provides a triode amplifytng stage, and a pentode output stage ( 3 watts), enabling good amplincation and sparkling reproduotion to be combined with physical compactness (amplifier size, $7 \times 3 /$ $x$ 6in. high).
* Modern olrcuitry design. good qualtty O.P. transformer (to match to gow keep hum and distortion to a low level.
* The controls, volume on/off, and tone are complete with attractive cream and gold knobs.
* The amplifier has a built-in fully smoothed power supply, using a sood quality mains transformer (A.C. mains only) and metal rectifler.
* All you need is supplied including easy to follow instructions which guarantee good results for the beginner and expert. All components. leads. chassis. valve, knobs, ete. are firgt grade items by promiment manufacturers.
OUR PRICE
Plus 4/6 Post and Packing. $39 / 6$


5in. LOUDSPEAKER TO SUIT 14/6 EXTIKA
ALL PARTS SULD SEPARATHLY

## CHILD'S NURSERY LAMP

A child's nighe light of unusual design. Contemporary styled lampholder of robust construction finished in either red or yellow. Entirely safe (bulb socket shielded from" prying fingers"), complete with flex and a push-button switch. 200/250 volts A.C. only. The low-consumption bulb element is made in the shape of either flowers or angel fish, and when switched on glows in fluorescent colours (the fowers pink with green leaves, or tho fish green with purple weed). Made by a famous manufacturer and originally priced at 2916. Please state lompholder colour breference, and whether fish or flower element is required.
OUR BARGAIN PRICE ONLY plus 9d, post and pasking.


10/9

## SUPERHET CHASSIS-less Valves \& Cabinet

 Modern $A C / D C$ chassis with printed circuit and ferrite rod aerial. Although not completely built, the main components are mounted. L. \& M. wave coverage. 4 valves (UBF89, UCL83, UCH81, UY85). Everything supplled except valves and cabinet. With speaker and simple $\mathbf{~} 3.6 .6$ plus $3 / 6$ instructions.
## TRANSISTOR AMPLIFIER KIT

A complete kit of parts to build a compact 4-transistor ampllfier, with volume control and printed cct. board. Two GT3 driver transistors, transformer coupled. I watt output from matched pair GTI5. Supplied with output transformer and 2 tin. 3 ohm speaker. Ideal for
record player, etc.
$59 / 6 \quad$ plus ${ }^{4 / 6}$

## CONDENSER/RESISTOR PARCEL

50 mixed P.F. Condensars and 50 mixed Resisters. An assortment of useful values. All popular sizes-all new-a must for the servicoman and constructor
ONLY $10 /=$

## AT $\frac{1}{2}$ PRICE WHILE THEY LAST! GOLDRING MU-METAL CASED CARTRIDGES

## Sapphire styli. Brand new and boxed

 Our Price £2.15.0P \& P $1 / 6$ including lns.

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| POWER |  |  |  |  | $\begin{aligned} & \text { GET102... } \\ & \text { XA103 } \\ & \text { PXA101 } \\ & \text { PXA102 } \end{aligned}$ | $\cdots$ | ... | 716816 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| OC36 | ... | ... |  | 10'- |  |  |  |  |
| OC44 |  |  |  | 91. |  | ... |  | 916 |
| OC45 |  | ... |  | 81 |  | ... | ... | 916 |
| OC71 |  |  |  | 51. | AMERICAN |  |  |  |
| OC75 | ... | ... |  | 616 |  |  |  |  |  |  |  |
| OC76 |  | ... |  | 616 | ${ }^{2 N} \mathbf{2 N} 1488{ }^{\circ}$ | ... |  | $6 / 6$ 616 |
| OC78 |  | ... |  | 616 | ${ }_{2} \mathbf{\$ 7 1 2}$. | $\ldots$ | ... | 716 |
| OC780 |  |  |  | 616 |  |  |  | 76 |
| GETIS | ... | $\ldots$ |  | 91 | DIODE |  |  |  |
| GETI5 |  |  |  | 1616 | OABI |  |  |  |

Please add 6d. postage for each transistor.

## TRANSISTOR SPEAKER

Weston Electric $3 \Omega$ speaker. Slze $2 \frac{1}{2} \times \nmid \frac{1}{}$ in. deep. $12 / 6$ p.p. I\%

## THE HARVERSON COMPLETE F.M.|V.H.F. RECEIVER KIT $£ 6.19 .6$

AT LAST-A COMPLETE F.M. RECEIVER IN KIT FORM: Specially designed with the home constructor in mind, this kit enables the construction of a completely self-contained V.H.F. receiver, at fraction of the normal cost of comparable equipment. This is basically a quality selfpowerad F.M. tuner plus 2 separate audio amplifier stages, and output transformer and speaker.

* F.M. Tuning Head by famous maker.
* Guaranteed Non-drif́c.
* Permeability Tuning.
* Frequency coverage $88-100$ Mc/s.
* OAaI Balanced Diode Ourpur.
* Two I.F. Stage and Discriminator.
* Self powered using a good quality mains transformer and valve rectifier.
* Valves used ECC85, two EF80's, ECL82 and EZ80 (rectifier).
* Fully drilled chassis.
* Good quallity speaker.
* Well designed output transformer.
* Attractive maroon and gold glass dial.
* Two ourput stages (using ECL82).
* Everything supplied, down to the last nut and bolt.
* Compact size.
* Ail parts sold separately.

OUR PRICE $\mathbf{5 6} \mathbf{1 9 . 6}$ Plus ${ }^{1 / 6}$


## 83 HIGH ST., MERTON, S.W. 19 <br> HErrywood 3985/6 „HARVERSON'S UNEQUALLED VALVE SERVICE $\star$

| OA2 | 1716 | 676 | 71. | 10D2 12- | 53W4 76 | DK |  | E50(E) |  |  |  |  |  | $\begin{aligned} & 201 \\ & 3 \mathrm{C} 80 \end{aligned}$ |  |  | $\begin{gathered} 916 . \\ 1716 \end{gathered}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| OB2 | 1716 | 6F11 | 1713 | IOFI 2616 | $3523 \quad 1016$ |  |  |  |  |  |  |  |  | 42 | 916 | H(1.5) | 616 |
| OZ4 | 51. | 6F12 | 416 | 10F9 11'6 | 35Z4GT 6\%- | DK92 | 91. |  |  |  |  |  |  |  |  | ) |  |
| IA5 | 6\% | 6F13 1 | $11 / 6$ | 10LD3 816 | 35Z5GT 91. | DK96 | 6 |  |  |  |  |  |  |  |  |  |  |
| IA7G | 12'. | 6F15 | $15 / 3$ | 10LDII | 43 10\% | DL33 | 916 |  |  |  |  |  |  |  |  |  | 716 |
| 1 C 5 | 1216 | 6F23 | 1016 | 1511 | $500510 \%$ | DL66 | 1716 |  |  |  |  |  |  |  |  |  | 寿 |
| D6 | 1016 | 6F32 | 1016 | $10 \mathrm{Pl} 3^{15 \%}$ | 50CD6G | DL68 | 15. |  | 06 |  |  |  |  |  |  |  | 16 |
| IG6 | 1716 | 6F33 | 716 | 10P14 1913 | 3616 | DL72 | 151. |  |  |  |  |  |  |  |  |  |  |
| IH5G | 1016 | 6G6 | 616 | 12A6 5\%- | 50L6GT 916 | DL92 |  |  |  |  |  |  |  |  |  |  |  |
| 1 L 4 | 316 | 6H6 | 3'- | 12AC6 15/3 | 53 KU 19111 | DL94 | 716 |  |  |  |  |  |  |  |  |  |  |
| ILD5 | 5. | 615 | 51. | 12AD6 17/3 | 77 8\% | DL96 | 816 |  |  |  |  |  |  |  |  |  |  |
| ILN5 | $5 /$. | 616 | 516 | 12AE6 13/11 | $78 \quad 616$ | DM | 716 |  |  |  |  |  |  |  |  |  |  |
| N5G | 1016 | 6J7G | 61. | $12 \mathrm{AH7} 81$. | $80 \quad 91$. | E80F | $20 \%$ | EF183 |  | W61 |  |  |  |  |  |  |  |
| \|R5 | 616 | 6J7GT | $10 / 6$ | 12AH8 1216 | 83 15\% | E83F | 37 | EFI84 |  |  |  |  |  |  |  |  | 6 |
| \$4 | 91. | 6K7G | 5. | 12AT6 716 | 85A2 25- | EA50 | 2 | 32 |  |  |  |  |  |  |  |  |  |
| 55 | 61. | 6K7GT | $6{ }^{1}$. | 12AT7 6\% | $150 \mathrm{~B} 2 \mathrm{15} \mathrm{\%}$ | EA76 |  | L32 |  |  |  |  |  |  |  |  | 816 |
| T4 | 316 | 6K8GT | 1016 | I2AU6 23/3 | 161 1016 | EABC80 |  | 33 |  |  |  |  |  |  |  |  | 716 |
| 105 | 61. | 6K8G | 616 | I2AU7 616 | 185 BT 33/2 | EAC91 |  |  |  |  | 6 |  |  |  | 216 |  |  |
| 2 P | 2616 | 6K25 19 | 19111 | 12AV6 12'8 | 3041016 | EAF42 |  |  |  |  |  |  | 451 |  | 1016 |  | 4/- |
| $2 \times 2$ | 416 | 6 LI | $23 / 3$ | $12 A \times 7 \quad 716$ | 3051016 | E834 |  |  |  |  | 16 |  | 716 | 55 | 91. | A70 | 41. |
| 3 A 4 | $6 \%$ | 6L6G | 81. | $12 \mathrm{BA6} 81$. | 807 7616 | EB41 |  |  | 17 |  | 23/3 |  | 2216 | UF86 | 711 | A73 | 41. |
| 3 A5 | 1016 | 6L6M | 916 | $12 \mathrm{BE6}$ 91.1 | 956 1617 | EB91 |  | 83 |  | 过 |  |  | 1416 | F89 |  | OA79 | 41. |
| 3B7 | 1216 | 6L7GT | 716 | 12BH7 $21 / 3$ | $1821 \quad 167$ | EBC3 | $23 / 3$ | 83 |  | 37 |  |  | 316 | L41 | 91. | OA81 | 41. |
| 3D6 | $5 \%$ | 6 L 18 | 13'- | 12E1 30\% | 4033L 126 | EBC33 |  |  |  |  |  |  | 121 | UL44 | 2616 | OA86 | 61. |
| 3Q4 | 716 | 6L19 | 2313 | 1215GT 416 | 5763 1216 | EBC41 |  |  |  |  |  |  | 316 | UL46 | 1416 | OA91 | 51. |
| 3Q5G | 916 | 6LD3 | 816 | 12J7GT 916 | 17193 | EBC8 |  | 91 | \% | 08 |  | SU25 | 2616 | UL84 | 816 | OA9 | 51. |
| 354 | 71. | 6LD20 15 | 15111 | $12 \mathrm{K5} 17111$ | $\begin{array}{ll}7475 & 716 \\ 9002 & 516\end{array}$ | EBF80 |  | 95 | 016 |  | 15\% | SU | 91. | M | 1713 | 210 | 25) |
| $3 \vee 4$ | 716 | 6N7 | 81 | 12K7GT 516 | $9002{ }^{2} 5$ | EBF8 | 1 |  | 6 |  |  | T4 | 91. | M34 | 17/3 | 1211 | 40\% |
| 5R4G | 1716 | 6P25 | 1216 | 12K8GT | AC/PEN 2313 | EBF89 |  |  | 251 |  |  | TDD4 | $12 / 6$ | M80 | 1513 | C16 | 541. |
| SU4G | 616 | 6P26 19 | 1911 | 12Q7GT | 23 | EBL2 | $23 / 3$ |  |  |  | 1311 |  | 2616 | URIC | 1817 | C19 | 541. |
| $5 \times 4$ | 101. | 6P28 | 2616 | 12SA7 816 | 7-pin 151. |  |  |  |  |  |  | 33 | $33 / 2$ | U6 | 19111 | C23 | 871. |
| 5 Y 3 | 616 | 6Q7G | 616 | $125 C 7816$ | AC2PEN | EC52 | 516 |  | 231 |  | 916 | 32 | 120 | U7 | 1617 | C26 | 44!. |
| $5 \mathrm{Z3}$ | 1216 | 6Q7GT | 11. | $12 \mathrm{SG7}$ |  | EC54 |  |  |  |  | $18 /$ | TP22 | $15 /$. | U8 | 2616 | C28 | 25\%. |
| 5Z4G | 91. | 6R7G | $10 \%$ | 12 SH 7816 |  |  |  | EM8 | 1016 |  | 116 | TP | 151. | U9 | 716 | 35 | 48\% |
| A7 | 1016 | 6SA7GT | T 816 | 12517816 | 33 |  |  |  | 13 |  | 81. | P2620 | 33/2 | YIN | $18 / 7$ | C44 | 26\% |
| 8 | 91. | 6SC7 | 716 | $125 K 7$ |  |  |  |  |  | CF82 | 1016 | TY86F | 1313 | UY21 | 1617 | 45 | 231- |
| $6 \mathrm{AC7}$ | 41. | 6SG7GT | T 81. | $125 Q 711$ | 7 |  |  |  |  | PCF84 | 1617 | U12/14 |  | UY4I | 716 | OC65 | $22^{16}$ |
| 6A | 516 | 6SH7GT | T 8\%- | 12 SR 7 |  |  |  |  |  | CF86 |  | U16 |  | Y85 | 17. | C66 | $25 \%$ |
| G7 | 716 | 6SJ7GT | $\mathrm{T}^{8 /-}$ | $12 Y 410$ | - | ECC35 | $23 / 3$ | YY8 |  | L82 |  | U18/20 |  | MP4G | - | C70 | 14/- |
| 6AK5 | 8 - | 6SK7GT | T | 14S7 271 |  |  | 61. | EY86 |  | CL83 |  | U19 |  | MMS4B | 15' | C71 | $14 \%$ |
| AL5 | 41 | 6SL7GT | T | 9AQ5 | 16 |  | 816 | Z35 |  | L84 |  | U22 |  | VP2 | $12 / 6$ | OC72 | 17. |
| 6AM6 | 416 | 6SN7GT | T | 9HI | 16 | 3 | 716 | EZ40 |  | L85 | 1617 | U24 | 29110 |  | 151. | OC73 | 201. |
| $6 \mathrm{AQ5}$ | 716 | 6SQ7GT | T | 20DI | 1216 | ECC84 | 91. | EZ41 | 1. | NA4 | $23 / 3$ | U25 | 1711 | VP2B | 1416 | OC75 | 151- |
| AT6 | 71. | 6SS7GT | T ${ }^{81}$ | 20F2 2616 | $\begin{array}{ll}\text { CBLI } & 2676 \\ \text { CBL31 } & 2313\end{array}$ | ECC84 | 816 | EZ80 | 71. | PENB4 | 2616 | U26 |  | VP4B | 23/3 | OC77 | $21 \%$ |
| Al | 10\% | 6U4GT | 1216 | OLI 2616 | $\begin{array}{ll}\text { CBL31 } & 23 / 3 \\ C \text { CH35 } & 23 / 3\end{array}$ | ECC88 | 181 | EZ81 | 71. |  |  | U31 |  | VPI3C |  | OC78 | 171. |
| $6 \mathrm{AV6}$ | $12 / 8$ | 6U5G | 716 | $\begin{array}{ll}\text { PPI } & 26 / 6 \\ \\ 2313\end{array}$ | $\begin{array}{rr}\text { CCH35 } & 23 / 3 \\ C K 506\end{array}$ | C91 | 516 | FC4 | $15 \%$ |  | 2616 | U33 | 2616 | VP23 |  | OC81 | $18 \%$ |
| $6 \mathrm{B8}$ | 51. | 6U7G | 816 | $23 / 3$ | $\begin{array}{ll}\text { CK506 } & 6 \% \\ C L 33 & 19 / 3\end{array}$ | ECF80 |  | FW4/50 | 00816 | PEN 25 | 416 | U35 |  | VP41 |  | OC170 | 351- |
| 6BA6 | 716 | 6V6G | 71 | 2616 | $\begin{array}{ll}\text { CL33 } & 193 \\ \text { CV63 } & 1016\end{array}$ |  |  | FW4/800 | 8/6 |  |  | U37 |  | VRI05 | $8 /$ | OC200 | 541. |
| 6BE6 | 61. | 6V6GTG | G 81- | 23/3 | $\begin{array}{ll}\text { CV63 } & 106 \\ \text { CYI } & 1817\end{array}$ | ECF86 | 1911 | GU50 | 2716 |  | 251. | U43 |  | VRI50 | 716 | OC203 | 58\% |
| 6BG6G | $23 / 3$ | $6 \times 4$ | \%- | 25A6G 1016 | $\begin{array}{ll}\text { CY1 } & 187 \\ \text { CY31 } & 11 \%\end{array}$ | EC86 | 2616 | GZ30 | 91. | PEN44 | 2616 | U45 |  | VT61A |  | TJ | 40\% |
| 6 BH 6 | 81. | $6 \times 5 \mathrm{GT}$ |  | 25L6GT 10\% | CY DI DI | 21 | 23/3 | GZ32 | $10 \%$ | PEN45 | 1916 | U50 | 616 | VT501 |  | TJ2 | $45 \%$ |
| 6 BJ 6 | ${ }^{61}$ | 6/30L2 | 1216 | 25Y5GG 916 | D15 1016 | ECH35 | 616 | GZ33 | 19111 | PEN45 |  | U52 |  | W76 | 51 | TJ3 | $50 \%$ |
| 6BQ7A | 23 | 7A7 | 1216 $21 / 3$ | $\begin{array}{ll}25 Z 4 G & 916 \\ 25 Z 5 & 916\end{array}$ | D63 $\quad 10 \%$ | -CH42 | 91. | GZ34 | 141. |  | 2616 | U54 | 19111 | W81M | 6 | TPI | 40\% |
| $6 \mathrm{6R7}$ | $23 / 3$ | 786 | $21 / 3$ 816 | 25256 | D77 4\% | ECH81 | 91. | GZ37 | 19111 | PEN46 | 716 | U76 |  | W 107 | 1817 | TP2 | $40 \%$ |
| 6B\$7 | 25 | 787 785 |  | 2750 19111 | DAC32 1016 | ECH83 | 311 | H63 | $12 / 6$ | PEN38 | 83 23/3 | U78 | 51. | W729 | 1911 | TSI | 101. |
| 6BW6 | 816 | $7 \mathrm{7C5}$ |  | 27507 711 | DAF91 6\% | ECL80 | 91. | HABC80 |  | PEN45 | 3DD | U107 | 1617 | $\times 24$ | $24 / 7$ | TS2 | 1216 |
| $68 W 7$ $68 \times 6$ | 61. | $7 C 6$ 747 |  | 28D7 30 Cl 8\% | DAF96 816 | ECL82 | $10 / 6$ |  | 1316 |  | 33/2 | U191 |  | X 4 | 5 | TS3 | 151- |
| ${ }_{68 \times 6}$ | 5\%. | H7 R7 |  | 30F5 6\% | DD41 1311 | ECL83 | 1913 | HL2 | 716 | PEN/D |  | U201 |  | $\times 61(C)$ | 1216 | TS4 | 241. |
| 6C4 | 516 | 7R7 |  |  | DET25 716 | ECL86 | 1617 | HL23 | 15/3 | 4020 | 33/2 | U251 |  | X63 |  | V30/10 | OP 2816 |
| $6 \mathrm{C5}$ | 616 | 7S77 | 816 | 30 Ll 8\% | DF33 1016 |  | 2313 | HL23DD | D 716 | 6 PL33 | 1913 | U281 | 1911 | X65 | 1216 | $\times \mathrm{AlO1}$ | 23/- |
| 6 | 1316 | 7 Y 4 | 716 | 30 LIS 1116 | DF66 151- | EF22 | 141. | HL4IDD |  | PL36 | 12'. | U282 | $22 \cdot 7$ | $\times 66$ | 1216 | XA102 |  |
|  | 91. | 8D2 | 316 | 30P4 12\% | DF91 316 | F36 | 41- |  | 1913 | PL38 | 2616 | 3301 | $23 / 3$ | X76M | $14 /$ | $\times$ X103 |  |
| CD6G | 3616 | 8D3 | 416 | 30 PI 2716 | DF96 816 | EF37A | $81 /$ | D |  |  |  |  |  |  | $23 / 3$ | $\times$ A104 |  |
| 6 CH 6 | 91. | 98W6 | $15 / 3$ | 30PLI 1016 | 6 DF97 91. | EF39 | 516 |  |  | L82 |  |  |  |  | 2313 |  |  |
| 6D6 | 616 | 9D2 |  | 30PLI3 1616 | DH63 616 | 6 EF40 | $15 \%$ | HN309 |  | PL83 |  |  |  |  | 616 |  |  |
| E5 | 1216 | 610 Cl | $3^{\prime \prime}$ | 35A5 $21 / 3$ | 3 DH76 51 | - EF41 | $9 \%$ | HV2 |  |  |  |  |  |  |  |  | 161. |
| F1 | 26 | 10 C 2 | 26 | 35L6GT 916 | 1 DH77 | - EF42 | $10 / 6$ | HVR2A |  | - PL820 |  |  |  |  |  |  |  |

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SPECIAL OFFER! ONE DOZEN 6K7G $£ 1$, plus 216 P. \& P.
BRAND NEW COSSOR 10 -inch TUBE, I08K OR 75K, 1816, plus 6/6 P. \& P.
Regunned Tubes Supplied-Any Type-Any Size. Write for List
OSCILLATOR COIL FOR ANY TAPE DECK, 516, plus 6d. P. \& P.



## MOTOR SNIP

Minlature motor 24 in . long $x$ ling diametar, laminated poles and armature, separate winding cor reversing. Operates off $30-30 \mathrm{v}$. stepdown transformer through
 Stepdown transformer, Original cost at least $\mathrm{S}_{3}$ each. Snip price for one month only 8/6, plus 1/6 postace

## INFRA-RED HEATERS

12in. Hl-fidelity loudspeaker. High sux, permanent magnet type with handle up to 12 wet famous maker. Price $32 / 6$ new by post aud Insurance.

Hi-Fi Snip
Infinite Wall Baffle

## N1cely <br> Veneered <br> and ${ }^{1}$ dol. lished. Cor- <br> ner fitting <br> (attaches to <br> pleture rail). <br> floorspace. <br> Gives really <br> fantastic <br> sults with only <br> speaker fitted for tweeter. Oniy <br> owh. carrlage andinsurance $3 / 6$. <br> Smallest Possible 2-gang



With built-In trimmers, polystyrene cased. size only $1 \times 1 \times 7 / 161 n$. price match, 21/. P.P. input osciliator to put transformers ia/B and P.P. Out gram iree with any of above.

Building A Scope?


31 n . oscllloscope tube.
 for 750 watt alement ( 3 microns). Price tor 750 watt alement and Instructions 15/6, plus $2 / 6$
post and insurance

## CHARGING SWITCHBOARDS



Type A. 550 w. 18 v --contatns thice reverse surrent relays. one volumeter rated 25 v. f.s.d, one main rated 15 amps in amps. i.s.d., one secondary ammeter 20) amps. $1 . d$. varlable resistor and two varlable resistor, one 11 ohm Complete in metal case afi ohm variable resistors. Price \&2.15.0, carriage and ins. 15 . aft. 81n. apdrox. Type B. 1280 w. 50 v 0.12 amps .
varlable resistor and four 1 ohm - contains one 14 ohm one main ammeter rated at 40 amm variable reststors, dary meters rated at 20 amps . sod and ine seconrated at 50 volts, and two reverse one voltmeter Complete in metal case-siro approxi curt relays. 2 2t. 8in. Price e4.15.0, carriake 15/-
Conntectiny lieads ior these swiuchboards, with Nifam pluks 30/- each.

## FLUORESCENT LIGHT BARGAIN

made type 3 Fm . American heater, electrostatic defle v. 0.8 amp . heater. electrostatic deflection, brand now and guaranteed with circuit diagram of scope. $15 /-$ each, plus $1 / 6$
post and insurance.

## Transistor Set Cabinet



Very modern cream cabinet, slze of $x$ $3 \times 1$ in. with chrome handle, tuning knob and scale. Price 7/6, plus 1/6 postage and packlng.


Kit of Parts comprisins: choke. two tamp holders, starter holder and starter, to watt, 19/6: 60 watt, 23/6.
Plus 2/- post and insurance.

## THIS MONTH'S SNIP

A fully-built, tested and ready to work pocket radio using six semiconductors and tuning over the long and medium wave bands. An excellent performer and a real bargain at 65/15/post free.
Seven days approval. Send for one today. If you are not $100 \%$ pleased then return it within seven days and your money will be refunded.


Por Tranalstor Circults or Dear Ald Very IIghtwelght and easy to wear, cord almost invisible, good quality production of music and voice, complete with minjature plug and socket ready to use-correct impedance OK or red spot and similar translstors Crystal and Magnetic, $8 / \%$. Post and Insurance $1 /$ -

## Morganite Potentiometers


$50 \mathrm{~K}, 100 \mathrm{~K}, 250 \mathrm{~K}, 1 \mathrm{meg}, 2 \mathrm{meg}$
Gang tyine $3 /-$ each-values avallable: $5 \mathrm{~K}+5 \mathrm{~K}, 100 \mathrm{~K} \pm 100 \mathrm{~K}$, i meg. $\pm$


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A pocket alze meter but with a big scale and a 20,000 ohms per volt D.C., therefore an ideal vision servicino -robustly made and complet with leads and prods 20 ranges as follows:
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8. Miniature slide switelı double pole change over. 2/6.
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| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| TUBOLAR |  | TUBUL |  | CAN T |  |  |
| 1／350V | $21-$ | 50／350V | 5／8 | 16／45V |  | － |
| $2 / 350 \mathrm{~V}$ | 2／3 | 100／25V | 3／－ | 32／350V |  | 4）－ |
| $4 / 450 \mathrm{~V}$ | $2 / 3$ | 250／25V | 8i－ | 100／270V |  | 5／8 |
| $8 / 450 \mathrm{~V}$ |  | 500／12V | 3 － | $2,500 / 3 \mathrm{~V}$ |  | $4 i-$ |
| $8 / 500 \mathrm{~V}$ | $2 / 8$ | $8+8 / 450 \mathrm{~V}$ | $3 / 6$ | 5，000／6 V |  | 5 5－ |
| 18／450V | 3／－ | $8+8 / 500 \mathrm{~V}$ | 51－ | $32+32 / 38$ |  | 5／－ |
| 18／800V |  | $8+16 / 450 \mathrm{~V}$ | $3 / 9$ | $32+32 / 45$ |  |  |
| $32 / 450 \mathrm{~V}$ | $3 / 9$ | $8+16 / 500 \mathrm{~V}$ | 5／6 | $32+32+3$ | 32／3 | \％／－ |
| 25／25V |  | $16+16 / 450 \mathrm{~V}$ | $4 / 3$ | $50+50 /$ |  |  |
| 50／25 $\overline{\text { V }}$ | 2／－ | $16+16 / 500 \mathrm{~V}$ | 6）－ | $64+120$ |  |  |
| $50 / 50 \mathrm{~V}$ | 2／－ | $32+32 / 350 \mathrm{~V}$ | 4／8 | $100+20$ | 275 | 12／6 |

## C．R．T．BOOSTER TRANSFORMERS

For Cathode Ray Tubes having heater Tubes with falling emission，fuli instructions supplied．
Type A．Optional $25 \%$ and $50 \%$ Boost． Mains input 6.3 V or 10.8 V or 13.3 V ．
Main liput．
12／6
TYPEAz．High quality，low capacity． $10 / 15 \mathrm{pF}$ ．Optlonal boost $25 \% .50 \% .75 \%$ ． Mains input．

16／6
Type B．Mains Input．Low capacity． Multi output 2，4，6．3， 10 and $13 V$ ， Boost $25 \%$ and $50 \%$ ．This transformer

## $\int_{\text {MAX }}$

CHASSIS
CUTTER
The cutter conslsts of three parts：a die．
a punch and an Allen screw．

 Multiratio，push－pull，7／6．Ditto， 10 w；15／8．Minl पLA，5／－： 10 甘， $85 \mathrm{~mA}, 10 / 8 ; 10$ H， $150 \mathrm{~mA}, 141$

MAINS TRANSFORMERS $200 / 250$ v．A．C． STANDARD， $250-0-250,80 \mathrm{mLA}, 6.3 \mathrm{v} .3 .5 \mathrm{c}$ ． tapped 4 v． 4 a．Keotisier 6．3 $\mathbf{\nabla}$ ． 1 日． 5 v． Ma．or 4 v．${ }^{2}$ a．ditto， $350-0-350$

MINITURE $200 \mathrm{v} .20 \mathrm{~mA}, 5.3 \mathrm{v} .1 \mathrm{a}$. MIDGET， $2: 20$ จ． $45 \mathrm{~mA}, 6.3$ マ． 2 a． |  |
| :--- | :--- | :--- |
| $15 / 6$ | STD

 Ditto，tapped sec． $2,4,6.3$ v．，it amp． $8 / 8$ Ditto，sec． $6.3 \nabla .3$ amp．
$3,4,5,6,8$ g 10,12 LOW VOLTAGE． $2 a$ ， $3,4,5,6,8,9,10,12,15,18,24,30$ v． Ditto， 500 ซ． $110-240 \mathrm{v}_{0} 150$ w．．．22／6

## TELEVISION REPLACEMENT

## Line Output Transformers

from 45／－each，New Stock
and other timebase components
Most makes available
S．A．E．with all enquirles．
FOLL WAVE BRIOGE SELENIUM RECTIFIER：
 CHARGER TRANSFORMERS．Tapped input 2001
250 v ．for charging at 2,6 or 250 v．for charging at 2,6 or $12 \nabla_{\text {．}} 11$ amps．， $15 / 6$ ． 2 amps．， $17 / 6$ ；${ }^{4}$ amps．， $22 / 8$ ．CIIrcuit included．
4 AMP CAR BATTERY CHARGER meter Leads，Fuse Case，etc．，for $\overline{6}$ v．or $12 v_{0}, 69 / 6$ ．

## BOOKS

40 CircuitsforGiermanium Diodes $3 /$－ ＂W．W＂Radio Valve Data， $6 /-$ ． Hikh Fidelity speaker Enclosures， $5 /$ Valve and TV Tube Equivalents， $9 / 6$ ． TV Fault Finding，5／＝：
Quality Amplifiers，4／6．
Radio Valve Guide．Books 1，2， 3 or 4，5／－each．
Transistor Superhet Receivers，7／8．

CRYSTAL MIKE INSERT by Acos $8 / 6$
Prectsion engineered．
ACOS CRESTAL
ACOS CRYSTAL MKE
DE
SUE
LOUDSPEAKER P．M． 3 OKM．Sin．Role，17／6； Sin．Plessey，19／8．7in．$x$ 4in．Plesseg，18／न； $6 \frac{1 i n}{}$ Rola，18／6． $10 \times 6 \mathrm{in} . \mathrm{m}^{27 / 6 . ~ 10 i n . ~ R o l a, ~} 30 / \%$ 4 in Tweeter， $25 / \ldots 12 \mathrm{in}$ ．R．A．， $30 /=14 \times 8 \mathrm{in}, 45 \%$ STENTORLAN EF1012． 10 in ． 3 to is ohms， 10 w．， 85／－．


CRYSTAL DIODE G．E．C．，2／－．GEX34，4／－．
HIGH RESISTANCE PHONES． 4,000 ohms， $15 /-\mathrm{pr}$ ． MIKE TRANSF， $50: 1,3 / 9$ ea．； $100: 1$ ，Potted， $10 / 6$. SWITCH CLEANER，Fluid squirt spout， $4 / 3$ tin． TWIN GANG TUNING CONDENSERS． 365 pF miniature lin．$x$ lin．$x$ linin．， $10 /-.500 \mathrm{pF}$ standard with trimmers，9／－；midget，7／8；with trimmers， $8 /-$ INGLE， $50 \mathrm{pF}, 2 / 6 ; 76 \mathrm{pF}, 100 \mathrm{pF}, 160 \mathrm{pF}, 5 / 6$. solid dielectric $100,300,500 \mathrm{pF}, 3 / \mathrm{B}$ ．
CONDENSERS．New stock． 0.001 mfd .7 kV T．C．C．，5／6；Ditto， 20 kV ．，9／6： $0.1 \mathrm{mfd} ., 7 \mathrm{kV} ., 9 / 6$ ． Tubular 500 v． 0.001 to 0.05 mfd ， $9 \mathrm{~d} .0 .0 .1,1 / \mathrm{m}$ ； $0.25,1 / 6 ; 0.5 / 500$ v．，1／9；0．1／350 v．，8d．；0．01／2，000 v． CERAMIC CONDS． 500 v．， 2,000 volte， $3 / 6$ ．
CERAMIC CONDS． $500 \mathrm{v}^{2}, 0.3 \mathrm{pF}$ to 0.01 mid ．， 8 d ． SILVER MICA CONDENSERS． $10 \% 5 \mathrm{pF}$ to 500 pF ， $1 /-; 600 \mathrm{pF}$ to $3,000 \mathrm{pF}, 1 / 3$ ．Close tolerance． $( \pm 1 \mathrm{pF})$
$815 \mathrm{pF}, 5 \mathrm{pF}$ to $47 \mathrm{pF}, 1 / 6$ ．Ditto $1 \%$
1000
pF $815 \mathrm{pF}, 1 / 9 ; 1,000 \mathrm{pF}$ to $5,000 \mathrm{pF}, 2 /-$ ．
$465 \mathrm{ke} / \mathrm{s}$ SIGNAL GENERATOR． Total cost 15／－：Uses B．F．O．Unit SIZE $24 \times 41$ ready made．POCKET required fix lin．Slight modifications Battery $7 / 6$ extra $69 \mathrm{~V}+1 \ddagger \mathrm{~V}$ ．Detalls S．A．E．

Wavchange Switches． 2 p．2－way 3 p．2－way，short spindle，2／6： 6 p．4－way ${ }^{2}$ water，long spindle，6／6： 2 p．6－way， 4 p．2－way， 4 p． 3 －way，long spindle， $3 / 6 \%$
3 p． 4 －way， 1 p．2－way，long spindle， $3 / 6 ; 1$ Wavechange＂MAKITS＂．Wafers avall－ abla： 1 p． 12 wafer． 2 p． 6 wafer， 3 p .4 wafer 42 p． 3 water；${ }^{6}$ p．$_{2} 2$ wafer． 1 wafer， $8 / 6$ waters in $014,3 / 8$ water， $16 / \%$ additiona
Toggle Switches，
d．p．d．t．， $4 /-$ ．， $2 /-$ ；d．D．，
3／6； d．p．d．t．，4／－

JASON FM TUNER COIL SET， 29／－H．F．coil，aerial coil，osclilator coll，two i．f．transformers $10.7 \mathrm{Mc} / \mathrm{s}$ ， detector transformer $\begin{aligned} & \text { gid heater choke．} \\ & \text { Circuit }\end{aligned}$ 6AM6，2／6．Complete Jason FMT Kit．Jason chassis with calibrated dial， components and 4 valves，$£ 6.5 .0$ ．

Valveholiders．Pax．int．oct．，4d．EA50， 6d．B1 1 A ，CRT， $1 / 3$ ．Eng．and Amer． 4 ， 5， 6 ，and 7 pin． $1 /-$ MOULDED Mazda and Int．oct．；6d．；B7G，B8A．B8G，BGA，8d． B7G with can，1／6．B9A with can， $1 / 9$. B7G．B9A cans． $1 /-$ each．int．oct．， $1 /$ ． B7G．B9A cans． $1 /$－each．

THE ORIGINAL radio component
Our written guarantee with every purchase．
Bus 133 or 68 pass door S．R．Station Selhurst．


Neon Malns Tester Screwdriver, 5/-. Solder Radiosrade, 4d. yd., thb 5/=. $11 \mathrm{~b} \%$
Black Crackle Paint. Air drying. 8/- tin.

## HIGII GAIN TV PRE-AMPLIFIERS

 BAND I B.B.C.Tunable chanaels 1 to 5 . Gain 18db. ECC84 valve. Kit price 29/8 or $49 / 6$ with Dower pack. Detatls 6d. (PCCB4 valves if preferred.)
BAND 111 I.T.A.-Same prices.
Tunable channels 8 to 13 . Gain 17 dB .
Paxolin Panels, $10 \times$ 8in.. 1/6.
Miniature Contaet Cooled Hectifers. 250 V 50 mA . 716 ; 250 V 60 mA . $8 / 6 ; 250 \mathrm{~V}$ $85 \mathrm{~mA}, 9 / 6: 200 \mathrm{~mA}$. $21 \%$; 300 mA . $27 / 6$.
Selenlum Rect. 300 V 85mA. $7 / 6$.
Colls. Wearite "P" type. 3/- each. Osmor Midget " $Q$ " type. adj. dust core. from 4/- each. All ranges.
Teletron D.W.R. L. and Med. T.R.F. with reaction, 3/6.
Ferrite Rod Aerials. M.W., 8/8: M. and L. 12/6.

Osmor Ferrtte Rod Aerlals, L. and M. for transistor circuits. 10/- each.
Ferrite Rods, ${ }^{18} \times \ln$., 2/6.
H.F. Chokes, $2 / 8$.
T.R.F. Collg, A/HF, 7/- palr; HAX, 3/-, DRRL, 4/-.

Aluminium Chassis. 18 s.w.g. Plain, undrilled, 4 sides. riveted corners. lattice fixing holes, $2 i 1 n$. sides. $7 \times 41 n$. . 1atice $4 / 67 \mathrm{n} .15 / 9 ; 11 \times 710.0 / 9 ; 13 \times 91 \mathrm{n}$. $18 \times 16 \times \operatorname{in} .1816$
Aluminjumirantlis. $18 \mathrm{~s} . \mathrm{w} . g . .12 \times 121 \mathrm{n}$. 4/6; $14 \times 91 \mathrm{n} . .4 /-; 12 \times 81 \mathrm{n}$., $3 /-; 10 \times 71 \mathrm{n}$. 2/3.

## AUTOCHANGER ACCESSORIES Suitable player cablnets (exoept <br> Amplifier playër cabinets $\ddot{\text { éncent }}$ 4H.F.) <br> 2-valve amplifierand $6 \dot{3} 1 \mathrm{n}$. speaker $78 / 6$ 3-valve amplifier and 6iln, speaker $951-$ Wired and lested ready for use with above.

QUALITY 2-STAGE HI-FI AMP. LIFIER. A.C, only. 200-250V. Valves ECL82 and Ez80. 3 watt quality output. Mullard tone circuits, bass boost, treble and volume controls. separate engraved Perspex iront-panel with de lure finisb. Heavy duty output transformer 3 ohm. Shrouded mains transformer. Stove enamened chas 18.10 .0 C1rcuit supplled.

Wirewound Ext. Speaker Control, 100. $3 /=$
ALADDIN FORMETS and coree, ty. 8d.; 11n., 10 d .
0.3 in. FORMERS 5937 or 8 and cans TV1
 or $2 . \frac{1 i n .}{} \mathrm{sq}$
with cores.
SLOW MOTION DRIVES, EpIcyelic ratio 6-1. 2,3.
SOLON IRON, 25 W .200 V or 230 V . $24 /-$ MAINS DROPPER. $3 x$ Hin. With adjustable sliders. 0.3A, 1.000 ohras. 4/3 0.2A. 7,000 ohms, $4 / 3$.

LINE CORD. $0.3 \mathrm{~A} ~ 60$ ohms per foot, LINE CORD. 0.3A 100 ohms per foot. 2 -way. 1 -per foot: 0.2A 100 ohms per fo

MIKE TRANS. 50-1, 3/8; 100:1. potted. 10/6 P.V.C. Conn. Wire, 8 colours, single or stranded, 2d. yd. Sleeving. 1.2 mm . 2d. stranded, 2d. yd. Sleevi,
4 mm . 3d.; 8mm. 5d. yd.
Speaker Fret. Gold cloth. $17 \times 251$.. 5/-;
 2sin. wide. $5 /-$ ft. Samples. $S$.
panded Metail. Gold, $12 \times 12 i n . .6 / 4$


## PRINTED CIRCUIT BATTERY PORTABLE KIT

Medium and long wave. Fowerful $7 \times 4 \mathrm{in}$. bigh Flux Speaker. T.C.C. Printed Circuit and condensers. Components of linest qually clearly identifled with aspembly instructions. Osmor Ferrite Aerial Coils Kexine covered attache case cabinet. Size $12 i n$. x 8 in. $x$ in. Batteries used BI'36 (L5SI2) and AD35 (L3040) 10/: extra, Instructions 9d. (free with kit) Mains Unit ready made for above 39/6. Bold separately, Details free.

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ARIEENTE TRANSISTOR
TRANSFOIRMERS
Type D3035. 7.3 CT: Push Pull to 3 ohms or Type D3034. 1.75: 1 CT. Push Pull Driver for OC72, etc. $1 \times 1 \times$ tin.. $8 / 6$.
Type D3058, 11.5:1 Output to 3 ohms for OC72. etc., $1 \times 2 \times 1$ in., $8 / 6$. Type D167. 18.2:1 Output to 3 ohms for
 Type D239, 4.5:1 Driver 2ransiormer.
 : $x+x$ in.. $10 \%$.

## ARDENTE TRANEISTOR <br> VOLUME CONTROLS

Type VC1545. 5K with switch, dia. 0.8in. 8/Type VC1760. 5 K with ${ }^{\text {switch, dia, } 0.71 \mathrm{~m}_{\text {. }}, 10 / 6 ~}$

## WEYRAD

COIIS AND THANSFORMERS FOR A z-WAVE TRANSISTOR SUPERR-
AND FERRITE ROD AERIAL Long and Medium Wave Aerlal-RA2W. On fin. rod. $7 / 161 \mathrm{n}$. diameter. 208p tuning. $12 / 6$.
Oscillator Coll P50/1AC. Medium wave.
For 176pF tuning, 5/4.

1st and 2nd 1.F. Transformers-P50/200. 770 kc/s, $11 / 161 \mathrm{n}$. diameter by tin. high. | $5 / 7$. |
| :--- |
| 3 rd |

3rd 1.F. Transformer-P50/3CC. to feed diode detecior, 6/-
Driver Transformer-LFDT2. $1 \mathrm{~S} / 16 \mathrm{x}$ f $x$ 111n. $9 / 6$.
Printed Circuit-PCA1. Size $24 \times 84 n-$ Roady drilled and printed with com. ponent positions, $9 / 6$.
minn., These com makers and performance transistor makers and periormance Constructor's Booklet 2/-.
NEW MUIIAKI TRANSISTOKS
Audio OC71 6/- R.F. OC44 10/6 Sub-miniature EJectrolybies (15V). Sub-miniature $5 \mu \mathrm{~F} .8 \mu \mathrm{~F}, 25 \mu \mathrm{~F}, 50 \mu \mathrm{~F}$, $100 \mu \mathrm{~F}, 2 / 6$.
 and L.W. Kadio Kit. 32/8. or deaf aid earplece, $12 / 6$.
"FW"FHOADFARER
AM/FM RAD10 KIT
Transistorised throughout. Advanced deslen. operated from internal batteries or direct from mains. AM sections all on prin audio Ampliter Tiner, FM Tuner. Audio Amplifer. Mains Supply Unit
Attractive Plastic Cabinet Ferrite fod Aerlal for AM. Telescopic Aerial for FM. Order now. Pownsistor kit. All parts. printed circuit and cabinet. Osmor designed kit. £8.15.0.


## BRITAIN'S MOST COMPREHENSIVE

 PRACTICAL COURSE IN RADIO • ELECTRONICS TELEVISION:

# Practical Wireless 


YOL. XXXYII No. 656 OCTOBER, 1961


## The "Tutor" Blueprint

WITH each copy of this issue of Practical Wireless, we are giving away another blueprint: the "P.W. Tutor", as it is called, has been designed for absolute beginners to radio construction, those who are, perhaps, new readers of this magazine, or those who have for some time wished to know more of the basic principles from which many of the more advanced designs appearing in these pages obtain their origin. This blueprint then does not only constitute details of simple radio receivers which anyone can build, confident that successful sets will result from their efforts, but it has also been designed by our experts-leaders in the field of technical journalism-to provide also a foundation of the principles of radio reception and receiver construction. This surely is the only way to begin a satisfactory association with this hobby-from a sound knowledge of the absolute fundamentals.
The article relating to the "Tutor", on pages 504 to 509 , shows, by easy stages, how four simple radio receivers may be built by anyone who is prepared to follow the step-by-step instructions, learn the meaning of the various circuit symbols (page 508), and spend a few minutes reading and practising the "Hints on Soldering" given on page 509 .

The components used in all the sets are inexpensive and readily obtainable and most of them are mounted on a group-board which greatly simplifies the construction.

The first receiver is a crystal set. This type of circuit has Jong been recognised as the ideal introductory circuit for the newcomer to the ranks of the amateur radio enthusiasts. It is for this reason that we feel justified in describing, in detail, the construction of a simple crystal set as the starting point for the beginner.

Three other sets follow this first receiver, each being progressively more advanced than the one before, and incorporating long and medium waveband coverage, transistor amplifying stages, as well as regeneration to improve volume and selectivity. The construction of a simple cabinet is also described which will be suitable for any of the four sets, and will give the final receiver a professional appearance.
Many of the more experienced readers of Practical Wireless may feel that in publishing this blueprint for the beginner, we have neglected our responsibility to those who have already established themselves as radio enthusiasts. We can but hope that any such readers will be patient, for this blueprint is the first of three; the other two are to be published in the November and December issues. The November blueprint will be of a transistorised amplifier, using the group-board method of construction, which will be capable of operating a loudspeaker from a battery record player or radio tuner. The December blueprint will give details of a superhet receiver, again built on a group-board, and designed to operate with the amplifier of the November issue, to form a complete radio set which the experienced constructor and the beginner alike will find to be a useful domestic receiver with an excellent performance.

Our next issue, dated November, will be published on October 6th.

## Hound the Worlal of Wireless

## POTENTIAL AND CURRENT NEWS

## Broadcast Receiving Licences

THE following statement shows the approximate number of Broadcast Receiving Licences in force at the end of June, 1961, in respect of wireless receiving stations situated within the various Postal Regions of England, Wales, Scotland and Northern Ireland. The numbers include Licences issued to blind persons without payment.

| Region |  |
| :---: | :---: |
| Home Counties* | 6888,047 |
| Midiand |  |
| North Eastern | 508.102 |
| North Western | 437,436 |
| Wales and Border Countles* | 387.442 225973 |
| Total England and wales |  |
| $\xrightarrow{\text { Scotland }}$ Northern Ireland |  |
|  |  |
| Grand Total |  |

## International Trade Fair

'THIS year's Pacific International Trade Fair is to be held in Lima, Peru, during October.
The British pavilion will be of modern design and will be one of the main attractions for visitors. The Board of Trade and the British delegation, in designing the pavilion, have ensured that British products will be exhibited, to best advantage. Exhibitors' and general trade 16 mm films will be shown to visitors -in a fully equipped cinema, with projection equipment from the RCA Great range.

## President Nkrumah Visits New Broadcasting Station

PRESIDENT Nkrumah recently visited the new external broadcasting station at Tema, near Accra, Ghana, which is being constructed by Marconi's Wireless Telegraph Co. Ltd. This station will give Ghana a modern high-power short-wave broadcasting system.

Under the contract Marconi's have designed and erected the transmitting station buildings and supplied and installed four 100 kW high frequency radio transmitters. Marconi's will also supply technical staff for the supervision and maintenance of the station


The transmitter hall and partially completed tower of a new broadcasting station at Temo, Ghana, which is being constructed by Marconi's Wireless and Telegraph Co. Ltd.
(Picture by courtesy of "Radio Review and TV Times", Ghana.)
for a period for four years and train personnel of the Ghana Broadcasting System.

## New BBC VHF Sound Broadcasting Station

'THE BBC's new VHF sound broadcasting station on the site of the Air Ministry radio station on the cliffs some 400 ft above Dover, was brought into service on 8 th August.

The Home Service is transmitted on $94.4 \mathrm{Mc} / \mathrm{s}$, the Light Programme on $90.0 \mathrm{Mc} / \mathrm{s}$, and the Third Programme with Network Three on $92.4 \mathrm{Mc} / \mathrm{s}$, each with a mean effective radiated power of 3.5 kW . A large number of listeners in South-East Kent, including Deal, Ramsgate, Broadstairs and Margate, Dover and Folkestone, are now able to receive greatly improved BBC sound broadcasting services.
The new station is of the translator type and will operate unattended. It will receive its programmes from the Wrotham VHF sound station by radio and make a direct frequency change on each without demodulation.

## Weather Ship Improvements

1 OLLOWING the completion
of an Air Ministry contract for the supply and installation of new radio communication and
automatic direction finding equipment, and the modernisation of the radar on two ocean weather ships the Marconi Company has been awarded a similar contract for a third ship. The Marconi equipment at present being installed includes four 1 kW independent sideband transmitters, eight receivers. a medium frequency direction finder and a VHF automatic direction finder and displays.

## Ionising Radiations in Industry

A SAFETY code for workers exposed to ionising radiations in industry is laid down in the Ionising Radiations (Sealed Sources) Regulations, 1961, made by the Minister of Labour, Mr. Joh.l Hare, and presented to Parliament on 3rd August.
The regulations impose requirements for safeguarding the health and safety of persons employed in factories and other places to which the Factories Acts apply, who may be exposed to ionising radiations from sealed radio-active substance, and from certain machines, such as X-Ray apparatus. They require the restriction of the exposure of workers to such radiations, the adequate shielding of sources of ionising radiations and instructions for workers likely to be
exposed to them, about the hazards involved and the precautions to be taken.

Maximum permissible doses of radiation are laid down, and the regulations include requirements for the medical supervision of workers, and for the wearing of film badges to measure personal doses received.

## Vaive Manufacturers' Interests Merge

ON the 1st August this year, Thorn-AEI Radio Valves and Tubes Ltd. began trading.

It was announced on 16th June that Associated Electrical IndusIndustries Ltd., were to merge their respective interests in the manufacture and sale of cathode ray tubes and radio valves. The productive capacities of both companies in this field have been pooled and include factories at Sunderland, Harlow, Rochester and Footscray.
AEI and TEI are both represented on the board and have equal shareholdings. TEI is responsible for management.

From ist August all AEI's interests in radio valves and cathode ray tubes for the entertainment industry were transferred to Thorn-AEI Radio Valves and Tubes Ltd., but AEI is continuing to manufacture valves and cathode ray tubes for industrial purposes.

## Radio Equipment for New Air craft

THE "Sixty Series " of airborne radio equipments and navigation aids, made by Marconi's, has been specified by British European Airways for use in their fleet of de Havilland Tridents.

The principal design aim in the
"Sixty Series" has been for greatly improved reliability through new concepts of mechanical and circuit design. The units are transistorised, are very small and light and have an extremely low power consumption.
The equipment will include VHF communication equipment, VHF navigation and approach guidance equipment, automatic direction finder or radio compass and an aircraft selective calling system.

The "Sixty Series" has also been specified by BOAC for their fleet of Vickers VC 10's.

## The Centre of Sound

$I^{N}$N June this year, the Centre of Sound was opened in London and established as the national headquarters of the British Recording Club. The Centre also aims at promoting the growth of the audio industry in this country and on the ground floor is housed a permanent exhibition of audio equipment. This exhibition is open to the public every day except Sunday, from 9.30 a.m. to 11.00 p.m.

Also for the benefit of the general public there is an Information Bureau on the ground floor which will give advice on all audio problems. It is staffed by a team of experts and is open every day from 9.30 a.m. to $5.30 \mathrm{p} . \mathrm{m}$. For the benefit of evening visitors a skeleton staff is employed from 5.30 p.m. to $11.00 \mathrm{p} . \mathrm{m}$.

Full club members of the Centre of Sound automatically become members of the British Recording Club. Facilities for members include a small theatre with a bar, a cinema, a library, a restaurant and television lounges.

The Centre of Sound is in Archer Street, Piccadilly, London W1.

## Engineering Division Appointments

TYHE BBC recently announced the appointment of Mr. J. A. G. Mitichell as Scottish engit neer. He succeeds the late Mr. F. W. Endicott and becomes responsible for the engineering services of the BBC's sound and television studios and outside broadcast units in Scotland.

## Audio Avenue at the Radio Show

A $N$ extensive display tracing the history of sound recording from 1888 to 1961 was a feature of the Audio Avenue at the Radio Show this year. Occupying some 500 sq. ft. this feature, " Milestones in Recording", was presented in conjunction with the E.M.I. group of companies.

Among the many vintage instruments featured in this display was one of the earliest weight-driven acoustic recording machines, an Edison phonograph and the microphones used exclusively by the Royal Family from 1924 to 1945 . The modern era of recording was represented by the latest type of studio tape recorders, stereo mixer consoles and other high-fidelity equipment.


The Centre of Sound; headquarters of the British Recording Club.

# Remote Control Unit <br> THIS INSTRUMENT WAS DESIGNED TO OPERATE AN AUTOMATIC MECHANISM OVER A SHORT RANGE <br> By V. E. Holley <br>  

$\subset$HIS apparatus was designed so that the door of a garage could be made to open automatically on receipt of a command signal from the driver of an approaching vehicle. It is, of course, suitable for any other control service where only a short range is required. While the mechanical part of the installation is rather outside the scope of these pazzs, it must be said briefly in explanation that the controlled door is of the roller shutter type which, when the retaining bolt is withdrawn, rises
under the influence of springs incorporated in the roller. The bolt is in fact the armature of a solenoid which the apparatus here described is designed to energise. It requires a current of 0.25 A at around 240 V D.C.

## Commond Signal

The more obvious methods of control by photoelectric circuits, contact pads laid in the approach road, etc., suffer from the defect that they can be operated by unauthorised persons. They were there-
fore rejected in favour of the following arrange-


Fig. I.-The circuit of the instrument.


Fig. 2.-The drilling dimensions of the aluminium chassis.
ment which depends upon a secret signal given by the driver of the car. Referring to Fig. 1, the tuned circuit L1/C1, is carried on a bracket beneath the car aad the buzzer and switch or bellpush in some convenient operating position inside. The second tumed circuit L2/C2 is buried several inches below the surface of the approach road in such a position that the car must pass over it to enter the garage. Operation of the buzzer energises L1 at its resonant fr-quency and the signal is transferred inductively to L2; the two coils may in fact be regarded as the two windings of an R.F. transformer with a step-up ratio of $1: 2$. With the circuit shown, sufficient signal transference is obtained with the coils three or four feet apart and, as the service operating distance is less than 18 in., there is sufficient sensitivity in hand. It is n t necessary that L1 should pass exactly over L2; satisfactory operation is obtainable with a divergence of up to 18 in . either side.

## Signal Amplification

The signal induced in L 2 is taken by underground cable into the garage and presented to the grid of the valve V1. This is a high-gain pentode, 6AC7, arranged as an R.F. amplifier. An inductive load in the anode circuit would no doubt increase the gain considerably but the 10 k resistor R 2 is adequate provided the screen and cathode resistors are efficiently bypassed. The amplified signal is transferred via C5 to the diode, D1, where it is rectified and the resultant voltage is applied to the grid of the valve V2. Any other high-gain R.F, pentode can be used for V1, the values of the associated components being adjusted as necessary.

## Output Stage

The function of V2 is to operate the relay and both valve and relay must be selected for compati-

## COMPONENTS LIST

Resistors $\frac{1}{2}$ W (unless otherwise stated)

| $R 1$ | 68 k | $R 4$ | 470 k |
| :--- | :--- | :--- | :--- |
| $R 2$ | 10 k | $R 5$ | 2.2 k |
| R3 | $180 \Omega$ | $R 6$ | $1 k_{s}, ~$ |

Capacitors 350VW (unless otherwise stated)

| $C 1$ | $0.002 \mu F$ | $C 4$ | $0.1 \mu F$ |
| :--- | :--- | :--- | :--- |
| $C 2$ | $600 p F$ | $C 5$ | $0.005 \mu F, 1000 \mathrm{VW}$ |
| $C 3$ | $0.1 \mu F$ | $C 6$ | $0.1 \mu F$ |

C3 $0.1 \mu \mathrm{~F} \quad$ C6 $\quad 0.1 \mu \mathrm{~F}$
C7 32 $\mu \mathrm{F}$ (electrolytic)
C8 $8 \mu \mathrm{~F}$ (electrolytic)
C9 $8 \mu \mathrm{~F}$ (electrolytic)
Clo $8 \mu \mathrm{~F}$ (electrolytic)
Valves
VI 6AC7 (octal base)
V2 6SL7 (octal base)

## Diode

GEX34
Relay
See text
Rectifiers
MRI RM4, $250 \mathrm{~V}, 300 \mathrm{~mA}$
MR2 Contact-cooled, 250V, 20 mA (minimum)

## Mains Transformer

$250 \mathrm{~V}, 20 \mathrm{~mA}$, half-wave;
6.3 V, IA

## Fuses

| FI | 100 mA |
| :--- | :--- | :--- | :--- | :--- |
| F3 | IA |

Sockets
Two (dissimilar) for external circuits
Buzzer and bell push
Any type
bility. The relay in the original equipment is of a simple type which is obtainable for a few shillings; the energising coil has a D.C. resistance of 4 k and the operating current is 3 mA . This fits in well with a high- $\mu$ triode valve and the prototype uses one half of a double triode, 6SL7. In the quiescent condition, the valve is biased by the resistor RS so that the anode current is 2 mA . Diode D1 is connected so that the arrival of a signal produces a positive voltage on the grid of the valve which
(Note that R7 is used to feed H.T. to the spare, or unused, half of the 6SL7 to prevent cathode poisoning.)

## Power Supply

The H.T. requirement is about 15 mA at $250-$ 300 V , while the heaters and indicator lamp need a little under 1 A at 6.3 V . This is supplied by a miniature mains transformer of the type used in television converters. The 250 V half-wave secondary feeds a contact-cooled rectifier and smoothing is provided' by R6 in conjunction with the $8 \mu \mathrm{~F}$ capacitors C9 and C10. No mains switch is included as it is convenient to control the supply to the prototype from the mains outlet to which it is connected.

## Controlled Circuit

The direct current for operating the door control mechanism is produced by the rectifier MR1 and its associated reservoir capacitor, C7. The supply is taken direct from the mains and the relay contacts are included in the A.C. portion of the circuit. The connection to the mains should be made as in Fig. 1 so that, in the quiescent condition, line voltage is present in the controlled circuit only as far as the relay contact. The three fuses are a necessary precaution since the equipment will be switched on for long periods unattended and they should not be omitted. In the prototype, F2 and F3 are at the mains connection and F1 is on the chassis.


Fig. 3.-The underchassis wiring diagram.

## Construction

The unit may be constructed in any desired form. A chassis about 9 in . $x 3 \frac{1}{2}$ in. $x ~ 1 \frac{1}{2}$ in. of 18 s.w.g. sheet aluminium is convenient with the drilling dimensions given in Fig. 2. A point-topoint wiring diagram with the wiring and components opened out for clarity, is given in Fig. 3.

## Coils

The coils L1 and L2 are wound with enamelled copper wire of 30 s.w.g. on identical formers made from three layers of $\frac{1}{8}$ in. plywood glued together as a "sandwich". The centre layer is 6 in . $x$ 6in. and the outers $6 \frac{1}{2}$ in. $x 6 \frac{1}{2}$ in. so as to form a slot $\frac{1}{4}$ in. deep all round in which the winding can be laid; the corners of the centre layer should be rounded off. The ends of the windings are brought through holes in the cheeks and soldered to two small wood screws which serve also to anchor the tuning capacitor. The details are shown in Fig. 4. Fifty turns are required for L1 and 100 for L2, giving a step-up ratio of $1: 2$.

When the construction is complete and the unit is operating satisfactorily, the coils should be thoroughly dried out and immersed in molten pitch or bitumastic p...nt to make them impervious to moisture. If pitch is used it should be heated very slowly to a temperature at which it is just sufficiently viscous to coat the coils thoroughly and the immersion should not be prolonged unduly. Waxed paper capacitors do not take kindly to this treatment and ceramics should be used for Cl and C2. The bracket for securing L1 beneath the car should of course be fitted before immersion.

## Other Components

The relay must suit the valve as already mentioned and the contacts must be capable of carrying the current of the controlled circuit. Nothing is required of the buzzer except that it should buzz heathily and any type will do; the prototype uses an electric door bell with the gong removed. The diode should be suitable for low radio frequency operation and a GEX34 performs very well. The resistors may be half watt except R6 (1 watt) and the capacitors $350 \mathrm{~V} . \mathrm{V}$ except CS for which a

1000 VW component is advisable because breakdown or leakage here would cause the relay to operate. Sockets are required for connection of the signal circuit. L2/C2, and the circuit to be controlled. They should be dissimilar to avoid accidental wrong connection.

## Testing

The completed unit should be set up on the bench with the coils L1 and L2 facing each other and about 3 ft apart. If consistent and reliable operation is obtained at this range, it can be assumed that the equipment will be satisfactory in service. A range of 5 ft was obtained with the prototype by tuning L2 accurately to the signal and capacitors of values between 500 pF and


Fig. 4.-The constructional details of the former for LI.

1000 pF can be tried across the coil for optimum results if maximum range is required.

A 9 V grid bias battery is suitable for operating the buzzer, or power can be taken from the car battery. The orignal equipment is designed for operation from a 12 V car system but satisfactory operation will be obtained from a 6 V systerr provided that the buzzer does not require too much current.

## MULTIRANGE INSTRUMENT PROTECTION DEVICE

By J. B. Ayer

The protection system described here approaches the ideal; it consists of a relay ( 6 V to 28 V D.C.), two switch banks ("break before make" types), a lamp ( 6 V to 28 V D.C.), and a D.C. supply.

One switch bank is ganged with the range selector switch of the instrument and the other ganged with the function selector switch.

The protection system provides the following facilities.
(i) The instrument will be switched on only if the range selector switch is on the top range position initially.
(ii) It will disconnect the instrument instantaneously if the function selector switch is operated without previously setting the range selector switch on top range.


Note: $x$ is position of Range Selector Switch on top range
Fig. 1.-The circuit of the unit. Relay contact (a) is wired in series with the meter leads.

# TROUBLE in the LOCAL OSCILLATOR 

# RECOGNISING AND CURING SOME FAULTS TO BE FOUND IN SUPERHET RECEIVERS 

By G. J. King

$\ell$N a superheterodyne receiver the local oscillator section of the frequency changer stage often gives trouble and results either in complete failure of the receiver, lack of sensitivity or apparent misalignment. In effect, the local oscillator is the heart of a superhet receiver. If the frequency is incorrect or the heterodyne signal voltage too high or too low, then the performance is impaired.

## Operation

In spite of its importance, the local oscillator is probably the section of the receiver which is most taken for granted. Should the oscillator fail to produce a heterodyne signal of any kind, the receiver will not tune signals since the operation of a superhet depends on the mixing of a locally generated signal with the incoming signal to produce an intermediate-frequency signal in the anode circuit of the mixer section of the frequency changer valve, this being subsequently amplified to the required degree before being applied to the detector stage.
The difference between the frequency of the incoming signal and that of the local oscillator gives the intermediate frequency, a common value nowadays being $470 \mathrm{kc} / \mathrm{s}$. The oscillator frequency may be $470 \mathrm{kc} / \mathrm{s}$ (or whatever the $1 . \mathrm{F}$. is) above or below the incoming signal frequency, depending on the design of the receiver or, sometimes, on the waveband to which the receiver is adjusted.

## I.F. Pick-up

It is clear that if the local oscillator fails, no I.F. signal will be produced. Nevertheless, the receiver may not be totally dead. The recelver will not tune stations, of course, but it may pick up odd morse signals or even a Continental station. The reason for this is that the I.F. stages are still operative and sensitive and if any stgnal appears on the aerial at a frequency within the I.F. passband, and if the signal is strong enough. it may well break through the first stages of the receiver and undergo amplification in the I.F.
channel, where it will be detected in the normal way and give a signal from the loudspeaker.
If the tuning is operated, the station will occur over the entire tuning range, though it may be slightly stronger when the tuning is set to one extreme end of its range. This is because at one end of the range the first tuned circuits are brought closer to the intermediate-frequency and the attenuation which they offer at the I.F. is progressively reduced. If the receiver features an I.F. trap in the aerial circuit, then this may afford sufficient attenuation to prevent such I.F. pick-up.

What usually happens, however, is that when a receiver fails the experimenter or service technician endeavours to locate the faulty section by removing the aerial lead from the aerial socket and applying it to various internal points around the frequency changer stage. If the local oscillator is responsible for the failure, when the aerial lead is connected to the signal grid of the mixer or to an associated lead or component (point $A$ in Fig. 1), I.F. pick-up may occur loud and clear. This is because the signal (or signals) in the range of the I.F. is applied direct to the I.F. amplifier stage, which then acts as a fixed-tuned TRF section.

## Partial Failure

In some cases the oscillator may not fail com pletely over the whole of the tuning range, but may suddenly burst into life at certain critical points on the dial, while at other points the symptoms already described may occur. This is typical local oscillator trouble, but which may occur only on some bands and not on others.

Low sensitivity of the receiver, if not due to any other cause, may be the result of low heterodyne voltage. This would point either to coil trouble or to alteration in value of an associated oscillator component. Sometimes in old sets, the oscillator coil or colls lose their "goodness "their Q -value probably diminishes-and this results either in intermittent operation or complete failure.

On the other hand, if the oscillator is operating too strongly, as may be caused by a feed resistor decreasing in value, the sensitivity may in some cases also be reduced. In addition, harmonics of the oscillator fundamental frequency may be generated. and these may well cause spurious I.F. signals which could possibly cause disconcerting
whistles and interference on certain signals tuned in the normal way.

In order to obtain the best results, the local oscillator must produce a signal voltage within a certain range, usually between 5 and 15 V . and for any given signal level there is a heterodyne voltage which provides optimum conversion conductance in the frequency changer valve. Fortunately this optimum value is not highly critical, and deviations to either side of the optimum will not normally impair the operation of the frequency changer by any marked degree. However, if the oscillator voltage deviates considerably from the optimum value, then poor results are bound to occur.
the tuning gang for the oscillator is usuatly of smaller capacitance (and size) than those sections used for tuning the aerial and R.F. circuits.
The signal output or attenuator of the signal generator should be adjusted to give reception comparable to that obtained with the oscillator of the receiver, and then the signal strength should be increased and decreased so that the effect of too much and too little oscillator voliage may be noted

Too little voltage will mostly cause a hiss on reception as well as decreasing the sensitivity, while too much voltage will cause whistles and if further increased will also cause a fall-off in sensitivity, as already described.


Fig. I.-The local oscillotor or frequency changer stoge of a superhet receiver.

## Worthwhile Exercise

The effects of changes in oscillator voltage can easily be observed by the experimenter and service technician by first tuning the receiver to a medium power transmission. making the local oscillator inactive and then injecting into the mixer section a signal of correct frequency from a signal generator-unmodulated, of course!

The correct frequency for the signal generator can be found first by tuning it to a frequency equal to the incoming signal frequency minus the I.F. and if this does not bring back the station, then tuning it to a frequency equal to the incoming signal frequency plus the I.F. In sets where the local oscillator is above the signal frequency,

This exercise is well worth while for it may be practised as a test procecture when a receiver is in for repair with a suspect local oscillator. This will quickly prove whether or not the oscillator is responsible for lack of signals.
It is best to inject the generator signal at the grit oit the oscillator valve after first breaking the connection between the escillator coupling capacitor and the oscillator coils or switch. The oscillator coupling capacitor is Cl in Fig. 1 and the point of injection is shown at B.

## Checking Oscillator Voltage

One of the best ways of checking quickly whether an oscillator is working is by breaking
the connection from the anode feed resistor (R1 in Fig. 1) to the H.T. line. inserting a milliammeter in circuit, as shown, making a note of the current reading and then purposely making the oscillator inactive. One way to do this is to put a shortcircuit across the oscillator tuning capacitor section of the gang or, preferably, to swamp the oscillator tuner circuit by a large value capacitor. This latter method is shown in Fig. 1 by the $0 \cdot 1 \mu \mathrm{~F}$ capacitor Cs. A change in oscillator anode current should be observed; if it is not, then one can be almost certain that the oscillator was not working before the short or swamp was applied.

The oscillator current may fall or rise, depending on the characteristics of the oscillator circuit. The main factor to observe, however, is a change in current, and this should be very marked when a healthy oscillator is temporarily put out of action.

## Voltage Method

Another method is to put a voltmeter across the oscillator anode load resistor, R1, as shown. This will avoid having to break the oscillator feed circuit, but the voltmeter should be of the high resistance type to prevent the normal circuit conditions from being appreciably disturbed. When this method is adopted the change in current will be reflected as a change in voltage across the load resistor.

It should be noted that the oscillator voltage rarely remains constant over a waveband as the tuning capacitor is swung from one end of its travel to the other There may also be a difference in voltage between wavebands. In an endeavour to keep the heterodyne voltage reasonably constant, the design engineer may find it necessary to damp the feedback on one band relative to the other bands. This is often achieved by switching a resistor in the oscillator circuit of the band requiring damping, this action being accommodated by a separate switch section on the wavechange switch.
The primary elements of the oscillator circuit given in Fig. 1 are Cl the oscillator grid coupling capacitor; R2 the oscillator grid resistor; R1 the oscillator anode load resistor; C3 the oscillator anode coupling capacitor; C2 the oscillator tuning section of the gang; L3 the L.W. oscillator coil; L4 the M.W. oscillator coil; S3 and S4 (which are ganged to S1 and S2): C4 the L.W. padding capacitor. C5 the M.W. padding capacitor; TC3 the L.W. oscillator trimmer, and TC4 the M.W. oscillator trımmer.

The components most likely to break down and cause oscillator failure are C1, C3 and R1. For weak oscillation, or oscillation which cuts off at certain points on the band. Cl should be checked by substitution, for this may have gone high in value. R1 should also be checked if necessary. Across C3 and the padding capacitors. C4 and C5 an appreciable R.F. voltage exists and this sometimes causes one or more of these components to go intermittent or noisy.

A noisy component in the oscillator circuit will give rise to background crackles which may be weak but progressively build up to quite a loud moise, and may then suddenly go weak again.

Should this occur on only one waveband, the associated padding capacitor should be an immediate suspect Poor insulation on the associated oscillator coil is another frequent cause of this symptom. Should the trouble be present on all wavebands, $\mathrm{C} 3, \mathrm{C} 1$ or R 1 are likely suspects and each should be checked by substitution in turn.

It should be noted that similar crackling effects sometimes originate in the l.F. amplifier stages owing to a noisy capacitor across one of the l.F. transformer windings. To prove this, the oscillator should be made inactive temporarily as already described, and if the crackling ceases, then the oscillator section is almost certainly to blame.

## Frequency Change

If one of the padding capacitors alters in value, not only will the oscillator voltage change from optımum, but the frequency of oscillation will also change. The local programme will no longer tune in at the correct point on the dial. but if the frequency change is not too great, will occur at a point somewhere on the dial, depending upon the extent of capacitance change. For example. if the trouble occurred on. the L.W. band of the receiver in Fig. 1, the fault would either be in L3 or in C4. Coils which contain dust-iron cores in their formers should also be checked to ensure that the cores have not shifted.

The valve itself should not be overlooked, of course, and if there is any doubt a substitution test will prove the matter conclusively. The triode section of the valve in this circuit works as the local oscillator, while the hexode section constitutes the mixer, the valve as a whole being known as a frequency changer.

## Thermal Tests on Transistor Miniatures

INTERMITTENT performance on transistor portables in the form of increasing distortion with time, cessation of local oscillator and cone warping of speaker, can often be due to heat action. This accounts for trouble on a hot beach. and fade-outs in the hot dash pockets of motor vehicles. The thermal lag between exposure to heat and the slow heating of the components can cause the radio to work in the car, but to remain dead for an hour or so after the removal from the hot surroundings. This is due to a period of time elapsing while the circuit cools down againalthough the case exterior seems cool enough. Tests made in normal air temperatures fail to show the fault condition.

To avoid the favourite dodge of using a hot hair dryer (450W), it has been found that gentle heat radiated from the bench lamp ( 75 W ) on an exposed printed circuit of a transistor portable, the lamp being placed within 3-6in. of the open back of the radio, brings on the fault after a short period without the risk of overheating.

## ABOUT

L<br>CURING ELECTRICAL AND MECHANICAL FAULTS<br>By P. J. Good

0U D

Loudspeaker faults can be divided into two primary classes, mechanical and electrical. An electrical fault usually causes either complete failure or intermittent operation, while a mechanical fault can produce a diversity of symptoms. Some of which may not immediately be associated with the loudspeaker, but may be put down to distortion in the A.F. stages of the receiver.

## Electrical Faults

Electrical faults are few, as a modern loudspeaker simply comprises a coil of wire, called the speech coil, which is arranged to move in a magnetic field. The output transformer is sometimes included on the loudspeaker chassis, and for this reason the transformer will be considered as part of the loudspeaker in this article. It should be noted, however, that the output transformer may not, in fact, be on the loudspeaker itself, but on the chassis of the receiver.

The transformer serves to match the impedance of the speech coil to the output valve, and thus has two windings; a low resistance winding which is connected across the loudspeaker's speech coil, and a high resistance winding which is connected to the anode circuit of the output valve. The transformer has a step-down ratio from the output valve to the speech coil, and this ratio is computed in relation to the impedances of the anode circuit and the speech coil.

In Fig. 1 is given the basic loudspeaker circuit, and it is fairly obvious that there are four main possibilities of failure. These are a break in the speech coil winding. a break on one of the windings of the transformer, a disconnected or broken wire in the loudspeaker circuit and, possibly less obvious, shorting turns in the output transformer.

## Complete Fallure

The first hint that the loudspeaker may be responsible for the failure of a receiver is complete absence of the residual mains hum which is normally detected on any receiver by holding an ear close to the loudspeaker. In this event, the speaker should be unplugged from the transformer
and the speech coil connected across a 1.5 V battery in series with a resistor of about $100 \Omega$. The resulting 15 mA of current in the speech coil should produce quite loud clicks and crackles as the battery connection is scraped (see Fig. 2). If this happens. then the speaker can safely be said to be electrically sound. The resistor is included to limit the current, for without it, a relatively high current can flow in low resistance speech coils and damage the winding on low-power units.


Fig. I.-A trpical output stage of a receiver, showing the loudspeaker circuit.

If th: speaker remains dead, then there is a break somewhere in the speech coil circuit. Very flexible wire is used to connect the speaker terminals to the speech coil and a break sometimes occurs at one of the terminations, which can usually be mended by skilful soldering. If these wires are in order, a check should be made of the soldered connections or small wire tags in the centre of the cone which anchor the ends of the speech coil. Although these wires are held by cement, they can be traced to the soldered blobs


Fig. 2 (left).-A method of checking loudspeakers.
Fig. 3 (right).-Here, on extension speaker is used and an on/off switch is incorporated in the circuit.
with a pin or pointed tweezers. If the break is located, the wire should be freed from the cement, cleaned of enamel, resoldered and finally recemented in position to avoid vibration. If there is no break at these points, the trouble lies in the
speech coil winding and, apart from replacing the cone and speech coil assembly complete, there is little that can usually be done.

If the test given in Fig. 2 produced crackles, the wires connecting the loudspeaker unit to the secondary of the output transformer should be checked for continuity. On some sets a switch is incorporated in the speech coil circuit to switch on and off the internal speaker if an extension speaker is connected, as shown in Fig. 3. The switch may simply be a plug and socket arrangement or something more elaborate, but in either case it should be checked for continuity.

## Output Transformer Test

There are two methods of checking the output transformer complete with speaker. One is to connect a voltmeter between the anode of the output valve and the chassis of the set, after first checking that H.T. voltage is in fact present on the H.T. line, as shown in Fig. 1. If the primary of the transformer is in order, a voltage slightly lower than the H.T. line voltage will be registered at the anode of the valve (assuming that the anode circuit is taking current). If the speaker circuit is normal, slight crackles should be heard from the


Fig. 4.-A method of determining the turns ratio of an output transformer.
loudspeaker as the voltmeter test probe is scraped on the anode tag. An alternative method is to disconnect the primary of the transformer from the valve anode and H.T. line and connect the winding across a 1.5 V battery. If all is in order, crackles should again be heard from the loudspeaker as the battery connection is scraped.

## Transformer Turns Ratio

The turns ratio of the output transformer is governed by the "optimum load" of the output valve and the impedance of the speech coil, both in ohms. Optimum load values are given in valve data booklets and the speech coil impedance is sometimes marked on the loudspeaker chassis. It should be noted that the impedance is generally taken at $1,000 \mathrm{c} / \mathrm{s}$, and is, therefore, slightly higher numerically than the D.C. risistance of the speech coil. As a rough guide, the impedance is a little over twice the D.C. resistance value.

The turns ratio is equal to the square root of the optimum load divided by the speech coil impedance which, put in mathematical terms is:-

$$
\mathrm{Tr}=\sqrt{ }(\mathrm{Lo} / \mathrm{Zs})
$$

where Tr is the turns ratio, Lo the optimum load and Zs the speech coil impedance. The expression may be altered to find Lo or Zs.

For example,

$$
\begin{aligned}
& \mathrm{Lo}=\mathrm{Tr}^{2} \times \mathrm{Xs}, \\
& \text { and } \\
& \mathrm{Zs}=\mathrm{Lo} / \mathrm{T}_{\mathrm{F}}^{2}
\end{aligned}
$$

Thus, given any two factors, the third or unknown can always be found.

If, for instance, the optimum load were $2,000 \Omega$ and the speech coil impedance $5 \Omega$, then 5 divided by 2,000 is 400 , and the square-root of 400 is 20 . The required transformer in that case would have a turns ratio of $20: 1$, which is a fairly common value.

The same reasoning applies to any loudspeaker matching problem. Some transformers have tapped primaries or secondaries or both to enable the best match to be obtained from any optimum load to any speech coil impedance. Tapped transformers of a similar nature are also available to match a low impedance loudspeaker into a low impedance source. For example, a matching transformer would be required to match, say, a $15 \Omega$ loudspeaker to a $3 \Omega$ extension loudspeaker socket on a radio or radiogram, or vice versa.

## Checking the Turns Ratio

An approximate idea of the turns ratio of an output transformer can be obtained by applying low voltage A.C. across the secondary winding (low resistance winding) and measuring the voltage appearing across the primary winding, as shown in Fig. 4. About 2V A.C. should be used, and this can be obtained from a step-down mains transformer. It should be measured as accurately as possible on an A.C. voltmeter, as also should the voltage across the primary winding. The ratio of the two voltages is approximately equal to the turns ratio of the transformer. For example, if 2 V were applied and 60 V appeared across the primary winding, then the turns ratio would be $60: 2$, or $30: 1$.

## Shorting Turns

An output transformer with shorting turns may not cause total failure of the set or amplifier, but will most certainly cause low volume and distortion, with loss of bass frequencies. By using the set-up shown in Fig. 4, shorting turns will give an obviously low output voltage and the transformer will quickly heat up.

## Mechanical Faults

Mechanical faults rarely cause total failure of the set, but they produce noises, such as buzzes, rattles and distorted reproduction. A distinct buzz may be caused by the speech coil being out of centre and touching the magnet pole pieces, or by a damaged or broken centring device, a split or tear in the cone, loose turns of wire on the speech coil, loose mounting bolts, holding the loudspeaker in the cabinet, vibrating connecting leads, etc.
Such faults can usually be located by operating the set with the loudspeaker in its normal position and touching the various parts of the loudspeaker in an endeavour to pin-point the source of the noise. If the speech coil is out of centre, lightly pressing a finger at a certain point on the cone will often either clear the effect or, at least modify 'it.
Eventually, it will be necessary to remove the loudspeaker from the cabinet in order to effect a
(Continued on page 502)

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## A Recording Problem

I have not yet got round to owning one of the modern tape recorders-mainly because I feel that 1 have no need for one. I have a very good record reproducing installation and this fills all my requirements so far as "mechanical" music is concerned. But I recently heard of a recording problem which seems to be rather mysterious, and perhaps one of my readers may be able to offer a suitable suggestion as to the cause and, perhaps the cure. An enthusiast had a recorder of wellknown make and one day purchased a used spool of tape, but successfully made a recording of his own over the existing recording. When played back this was perfectly satisfactory (it included many of his own remarks and he was able to recognise his voice perfectly). The record was put away with others, but next time he played it, his voice had dropped several tones. The speed was correct but his voice was definitely much lower, although the speed was correct, and he wonders whether the molecular structure of the tape deposit could have altered in some way to produce this variation in reproduction. If so, of course, then tape will require special care if it is saved, as it may give a false impression when played at a later date. I suggest that there must have been some magnetic material near the tape where it was stored, and that he was lucky that the recording was not completely erased. Has anyone any other opinions?

## Revenge !

I recently commented on the increasing outdoor use of transistor portables and, apart from many letters agreeing with my dislike of this form of abuse, and the many boroughs and districts which have so far enforced a ban on their use, one reader has suggested a neat form of counterattack." I am afraid the Post Office would not look kindly on his suggestion, but 1 feel that this is something which needs thinking about. He suggests the use of a low power R.F. oscillator, switched on when the offending receiver is audible. If the oscillator were tuned to the same frequency, the R.F. would tend to swamp the AVC and reduce the output. Failing that, modulation of the R.F. at $1 \mathrm{kc} / \mathrm{s}$ would effectively jam the receiver. Two transistors would do the job, tuned over the medium waveband or operating at $465 \mathrm{kc} / \mathrm{s} \pm 10 \mathrm{kc} / \mathrm{s}$ to cause I.F. break-through. The range required, the reader says, would be about 20 ft . He adds, in rather a sarcastic vein. "Keep clear of G.P.O. detector vans." I would be interested to know whether such a device would be contrary to the Post Office regulations, and if not, what steps could be taken by anyone with an offending portable who might be annoyed at the "inter* ference "?


## HEAT SINKS, I.F. TRANSFORMERS AND COILS

By D. R. Bowman

(Continued from page 397 of the September issue)

Mthoroug解 sary in the audio section of the receiver. However, layout is not at all critical and no difficulty should be experienced with instability.

## Negative Feedback

With the transformers specified, leakage inductance is low enough for quite a large amount of negative feedback to be applied if desired. Here however, a moderate amount only is used, approximately 6 dB .

## Overall Gain

Moderate amounts of gain per stage have been designed for, in the interests of stability, except in the R.F. stage where the maximum feasible has been required. The R.F. stage gives about 15 dB , the frequency changer 10 dB , the I.F. stages 25 dB
each, and the audio amplifier about 70 dB . The total is thus 170 dB , from which has to be deducted approximately 8 dB per stage (as far as the detector) as transformer insertion loss, and about 20 dB for loss in the detector stage. This, with 6 dB negative feedback in the audio section, gives a total of approximately 112 dB overall gain.

## Power Supplies

A 9 V supply is required. The DT9 is a convenient battery, and wilt last a reasonable timeabout a month or six weeks if the receiver is used


Fig. 2.-The construction of the clips for the output transistors-these clips are used to fasten the transistors to their heat sinks (which are described in the text).

## COIL WINDING DATA

All formers are bakelite 0.27 in. diameter Screening cans. required for transformers T2, T3, T4 and T5 are $\frac{17}{32}$ in. $\times \frac{17}{32}$ in. $\times 2 \frac{3}{8}$ in. All dust cores are VHF (purple-coded) type
LI $3 \frac{3}{4}$ turns $18 \mathrm{~s} . \mathrm{w} \cdot \mathrm{g}$. bare, spaced 0.3 in . outside length. Unscreened; one core required
TI Primary-6 turns I8s.w.g. bare, spaced 0.6 in . outside length

Secondary- $1 \frac{1}{2}$ turns PVC-covered connecting wire interleaved each side of last (H.T.) end of primary; one core is required
All the following coils are wound in the same direction. The primary and secondary would thus form a winding of continuous direction but for the interruption at the "middle"
T2 Primary-28 turns 285.w.g. enamelled, close-wound
Secondary- 12 turns 24s.w.g. enamelled, close-wound
Spacing: $\frac{1}{4} \mathrm{in}$. between winding ends
(Note: The secondary is topped 3 turns from the earth end of the winding; this tapping is the base connection to V3.) Two cores are required
T3) Primary- 12 turns 24s.w.g. enamelled,
T4 close-wound, topped 3 turns from "inner" end
Secondary-12 turns 24s.w.g. enamelled, close-wound, tapped 9 turns from "inner" end of winding
Spacing 0.4 in. between ends of winding
Two cores are required for each transformer
T5 Primary-28 turns 28s.w.g. enamelled, close-wound, tapped 7 turns from "outer" end
Secondary-8+8 turns 24s.w.g., closewound, biflar; Spacing 0.3 in . between ends of winding
Tertiary - $9 \frac{1}{2}$ turns 28s.w.g. enamelled, close-wound, wound over 10 turns of primary nearest the top. I turn Sellotape as insulation
Three cores are required
for about 4 hours daily. The receiver gives good output even when the battery voltage has dropped to 6 , and continues to provide a useful signal, at


Fig. 3.-The discriminator transformer windings (T5 in the circuit). The method of winding the bifilar secondary has been shown by using thick and thin lines to represent the two halves, but, of course, the same gauge of wire is used for both.
much reduced output quality, down to a battery voltage of 4 . The oscillator section continues to operate down to 2.6 V with the particular transistor used, though, of course, overall receiver gain at this voltage is negligible.

## Heat Sinks

Before fixing, the driver and output transistor heat sinks should be prepared as follows. Three pieces of sheet aluminium, $16 \mathrm{~s} . \mathrm{w} . \mathrm{g}$, measuring 3 in . $x 2 \frac{1}{2}$ in. are sawn out of a flat sheet. Snipping with tin-snips causes curvatures which must be avoided. A $\frac{1}{4} i n$. flange is turned over on one short side. Then a flat is filed, very lightly, on the middle of the sheet. It is most important to see that this flat is really accurate. A $\frac{1}{8} \mathrm{in}$. hole is now drilled in the flat portion and burrs carefully removed. Three pieces of $22 \mathrm{~s} . \mathrm{w} . \mathrm{g}$. aluminium, $\frac{3}{4} \mathrm{in}$. $\mathrm{x} 1 \frac{1}{\mathrm{i}} \mathrm{in}$. are sawn out of a flat sheet and bent round over the shank of a $\frac{6}{82} \mathrm{in}$. drill. The final curvature has to be $\frac{3}{16}$ in. to accommodate the OC81 transistors, and the natural springiness of soft aluminium sheet, with a very little force, will enable the transistors to be inserted firmly and closed into these cooling clips. Fig. 2 shows the arrangement. The assembly should be inspected against a strong light to ensure that no gaps occur between the transistors and the cooling clip. If small gaps appear, silicone grease-a smear only-may be used to assist dissipation of heat, but gaps should be avoided even if it means making six clips to get three good ones. Before assembly, the tuning condenser should be inspected. If the bearings carry an appreciable amount of grease it should be wiped away, and if at all slack the bearings should be tightened up. This precaution is mentioned here because in the prototype receiver some considerable trouble was found in obtaining electrical contact of the required effectiveness; the capacitor tuned very noisily through stations. This instability was removed partly by tightening up, partly by soldering to a side pillar of the capacitor an additional phosphor-bronze leaf-spring contact which was arranged to press heavily on the spindle


Fig. 4.- The connections of the windings of the discriminator transformer-the numbers refer to the coil base connections given in Fig. 6 overleaf.
between R.F. and F.C. sections. This spring was connected to chassis through a short length of copper braid. The capacitor had seen previous service, and it is not expected that a new component would cause trouble.

## The R.F. and F.C. Stages (see table, page 493)

1 The coils for R.F. collector and oscillator are wound on 0.3 in . bakelite formers, and the direction of winding is immaterial. The wire is $18 \mathrm{~s} . \mathrm{w.g}$. bare and, preferably silver-plated, for the collector and oscillator coils; these coils are first wound on


Fig. 5.-The mounting lugs of the tronsformers are cut as shown to enable them to be passed over the fixing bolts (see text).
Fig. 6.-The 1.F. transformer windings and the numbering of the base connections.

## LIST OF COMPONENTS

Capacitors and resistors are as shown in the circuit diagram.
All resistors are of $\frac{1}{4} W$ rating and of 10 per cent tolerance, except as shown below:

R38 5 per cent
R37 5 per cent
R39 $3 \times 10 \Omega 10$ per cent, in paraliel
Volume =ontrol: 10k with D.P.D.T. switch, log or semi-log
-Capacitors: All 180pF capacitors are 5 per cent - silver-mica types

C5, C10 are type N750K (Erie)
Capacitors C2, C3, C4, C8, Cll, C14, C15, C19, C20, C21, C23, C25, C28, C29, C31, C40 are of the ceramic miniature type (Erie)
CCI and CC2 are $10 \mathrm{PF} \pm 10$ per cent silver. mica
C37, C39, C43 are $8 \mu$ F electrolytic 6VW sub-miniature types
C38, C45 are Plessey type CE 7037
C42 is Plessey type CE205
C46 is $0.25 \mu \mathrm{~F}$ tubular (TCC)
C4I, C44 are TCC type CEIOODE
The tuning capactor is jackson Bros. type C808
( (catalogue number 5103)
Transformers (Gilson):
Driver transformer: type WO. 1806
Output transformer: type WO.929/6v ( $3 \Omega$ )
Speaker: 7in. x 4in. elliptical, $3 \Omega$
Bottery: DT9 or equivalent
a din. drill shank and then slipped, with some force, on to the former. The F.C. emitter winding, of 22s.w.g. copper wire, in thin sleeving (or PVCcovered "connecting wire) is added between the "earthy" turns of the R.F. collector winding. The spacing is adjusted to the specified value, and then the whole windings are covered with contact adhesive (clear) and allowed to dry thoroughly. The properties of this adhesive have not been measured but appear to be not markedly inferior to polystyrene cement, and the job is much more reliable than when polystyrene cement is used with thick wire.

## The I.F. and Discriminator Transformers

(see Figs. 3, 4, 5, 6 and 7).
The I.F. transformers could be constructed in the normal way, and for mounting, the lugs of the


Fig. 7.-The connections of the I.F. transformer windings.
can slipped through slots in the printed circuit board ready for bolting down. However, cutting neat slots in the laminated board is not a simple matter, and in the prototype the following method of canning the I.F. transformers was adopted.

When the transformers have been wound, all cement is thoroughly dry and all exposed metallic surfaces are covered with Sellotape, the sin. 6B.A. bolts are screwed through the fixing holes from the "inside" and are tightened up. The can is then slipped over the assembly. The lugs are then snipped through so that, on bending over, the halves can be worked round the 6B.A. bolts and flattened against the underside of the bakelite former. A brass washer is placed over the bentover lugs and then a brass nut is screwed down firmly. Nearly tin. of bolt will stand proud for insertion through holes in the laminated board, and when these in turn are screwed down, with washer and nut, against the copper surface of the printed circuit board a good electrical earth to the can is achieved.
(To be continued)

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# An Earthed Grid R.F. Amplifier 

By E. A. Parker

TMOSPHERICS and other interference generated outside the reiver limit its useful sensitivity on the communications bands below about $20 \mathrm{Mc} / \mathrm{s}$, but at higher frequencies they are much less intense and interference (except that generated by motor car ignition systems, of course) is virtually non-existent. At these high frequencies, then, receiver noise is very important, and the noise level of the receiver and the associated aerial will set the level below which signols will be inaudible. Since noise generated in the earlier stages of a receiver will undergo far more amplification than that generated in the later stages, any effort made to reduce receiver noise must be concentrated on the first R.F. stage, and to a progressively lesser degree on any subsequent R.F. or frequency changing stages.

In the case of an average communications receiver using one R.F. stage, the addition of a low noise pre-amplifier will give a most marked improvement in the signal-to-noise ratio. The existing R.F. stage has now been moved one stage away from the aerial, and the noise which it generates receives less amplification than before for a given signal output at the speaker or 'phones. The writer modified his R208 receiver in this way, using the grounded grid triode unit to be described. It was also found that the replacements of the original octal based R.F. valve - an EF39 - with an EF50 or the more recent EF91 or EF80 miniature valves again improved the performance of the set. Octal-based valves are unsuitable for use above $40-50 \mathrm{Mc} / \mathrm{s}$ owing to their inherent noise and the fact that their gain tends to fall off fairly rapidly above this frequency range.

## Valves

Triode valves are much less noisy than pentodes or tetrodes, but they cannot be used in normal amplifying circuits at radio frequencies owing to thẹir high anode-grid capacitance, which permits positive feedback at R.F. and so causes instability and oscillation. In the early days of wireless, this problem was overcome by introducing a further electrode-a grid was placed between the control grid and anode and maintained at earth potential with respect to the R.F. signal. This shielded the input to the valve from the output and prevented


Fig. I. -The effective circuit of on earthed grid triode.
positive feedback. Thus was born the tetrode valve, but, the extra electrode increased the inherent noise of the valve. However, methods were found where by the triode could be used as an amplifier at R.F. The most important of these was to earth the grid and apply the R.F. signal between cathode and earth. The amplified signal was in effect taken from anode and earth, as indicated in Fig. 1.

The cathode impedance should have a value of about $150 \Omega$ at D.C. and the voltage drop across it provides bias for the valve. At R.F., the cathode impedance is conveniently provided by an R.F. choke, and a glance at Fig. 2 will indicate that in the actual unit, a choke and resistor are used in series. The anode impedance may be an R.F. choke or a tuned circuit.

## Screening

The earthed grid mode of operation thus provides shielding of output from input in the form of an earthed grid, and the arrangement functions-well with remarkably high signal-to-noise ratio. Valves designed for earthed grid operation differ from normal triodes in that care is taken to ensure that the grid extends along the whole length of the cathode, thereby totally screening it from the anode. Examples of such valves are types CV66, EC91 and 6C4. Any of these valves will work well in the circuit of Fig. 2-the circuit used by the writer. To lessen the effects of lead inductance, the grid is brought out to four pins each of which is then separately earthed; the anode is brought out to two pins for the same reason. (The inductance of inductors in parallel is less than the smallest.)

Yet another advantage of the addition of this unit was the fact that the aerial damping was removed from the first tuned circuit of the receiver, enabling the associated trimmers to be peaked sharply. This in itself resulted in an increase in gain. In addition, the input impedance of the circuit was low and matching the aerial to the receiver no longer presented any problems. Matching was far from critical. It will be noted that the circuit is aperiodic-untuned or non-
resonant-which has the advantage that no extra gang is demanded on the main tuning capacitor.

## Constructional Details

Turn again to Fig. 2; the radio frequency choke in the aerial circuit is best made by winding in one layer a length of fine wire [about $40 \mathrm{~s} . w . \mathrm{g}$.] (equal in length to one third of the wavelength of the lowest frequency to be received) on to a glass or ceramic former, so that the length of the solenoid is about twice its diameter. However, the writer had several radio frequency chokes of miscellaneous design in his junk box, and these


Fig. 2.-The circuit diagram of the unit.


Fig. 3. -The layout of the R.F. preomplifier.
were found to function equally as well as that specified above. The value of the resistor in series with this choke should be adjusted so that the D.C. resistance of the combination is 1502 approximately - the value required will be found to lie between 100 and $150 \Omega$. The chokes in the heater leads are not very critical and it was found that 40 turns of $26 \mathrm{~s} . \mathrm{w} . \mathrm{g}$. w-o. in a $\frac{1}{2}$ in. diameter paxolin former was all that was required for satisfactory operation between 10 and $60 \mathrm{Mc} / \mathrm{s}$. It has been found that this circuit will function readily at all frequencies up to $400 \mathrm{Mc} / \mathrm{s}$; and the inductance and consequently the number of turns required on the choke decreases with increasing frequency. At frequencies above $100 \mathrm{Mc} / \mathrm{s}$, however, ceramic or glass forners are essential. The chokes and capacitor in the heater

## COMPONENTS LIST

Earthed grid triode valve, e.g. CV66 or EC91
Ceramic valveho!der to suit
Resistors (see text)
100-150 $\frac{1}{2} \mathrm{~W}$; $4.7 \mathrm{k}, 3 \mathrm{~W}$ w.w.; 4.7k, $\frac{1}{2} \mathrm{~W}$

## Capacitors

50 pF , two $0.002 \mu \mathrm{~F}$, mica.
Single layer R.F. choke, or 40s.w.g. wire to wind and former
Two heater chokes, 26s.w.g. wire to wind and formers
circuit form a filter which eliminates mains-borns noise. and the chokes tend to isolate the heater and cathode from carth at radio frequencies. (The heater-cathode capacitance may be great enough to bypass to carth the signal applied to the cathode in the absence of the chokes.)

## Anode Load

A point of interest is that the anode impedance $(R)$ was derived from a $3 W$ wire-wound resistor of D.C. resistance 4.7 K -the D.C. resistance of $R$ limited the anode voltage of the triode to within safe bounds, and the inductance of the component presented an additional impedance to R.F. signals which increased with frequency. This tended to offset the effects of stray capacitance elsewhere in the receiver, and sensitivity at all frequencies was much greater than expected.

Fig. 3 indicates the arrangement of components used by the writer. The unit was built on a subchassis made from aluminium and measuring 2 in . x $3 \frac{1}{2}$ in. $x 1 \frac{1}{2}$ in. Although the layout was not found to be very critical (a welcome point at high frequencies), all leads should be kept as short as possible. Most components can be wired directly to the valveholder. The chassis should first be drilled to take the valveholder (ceranic)- a $1 \frac{1}{5}$ in. hole if a CV66 type valve is used (B9G base)-which should then be bolted in position. The tinplate screen should be soldered firmly to the valveholder as shown in Fig. 3, and the various components may then be mounted. "Tin" boxes provide a convenient source of tinplate-which is very easily soldered. Any paint should be removed for appearance's sake.
When the unit has been completed it should preferably be bolted securely inside the communications receiver as near as possible to the first tuned circuit. In many receivers it will be possible to mount it so that the anode pin of the earthed grid triode lies fairly close to the top of the first gang on the main tuning capacitor. The output lead may then be kept very short.
The unit consumes very little power, and may be run without trouble from the existing power stupplies of most communications receivers.

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# A Compact Power Supply <br> A 

 PROBLEM which frequently confronts the constructor is the provision of power supplies to equipment which has been built up on a chassis which "happened to be handy "-all too often, after a series of modifications and improvements there is insufficient space left for the rectifier and associated smoothing components. The rather neat assembly described here was evolved to meet just such an emergency which arose when a battery receiver had to be converted to mains operation, and the idea is offered in the hope that it will help other constructors who may come up against the same difficulty.
## Layout

The unit requires only a single $\frac{1}{8} \mathrm{in}$. hole for fixing to the chassis, and the space taken up at chassis level is no more than the diameter of the metal rectifier-say one square inch at the most. The smoothing components are carried some inches above the chassis where there is usually some spare space and where risks of overheating are reduced.

The diagrams are almost self-explanatory; the main feature of the design is the familiar Westing-house-type air-cooled metal rectifier, obtainable from surplus dealers for a few shillings. The screwed rod which forms the "backbone" of the rectifier is used to carry a Terry spring tool-clip, which in turn holds a metal-cased twin electrolytic smoothing condenser of suitable capacity and rating: the case of the condenser, forming the negative pole, is effectively earthed through the metal rod, the other end of which is passed through the fixing hole in the chassis and secured by a nut. (In the illustration at the top of the page the capacitor employed had a polythene coveringhence the earthing wire which is visible, running to a solder-tag just under the Terry clip.)

## Construction

Soldered to the red or positive terminal of the rectifier is a suitable dropper resistor, chosen according to the current demands of the equipment; a useful value for general purposes is a wire-wound $2,000210 \mathrm{~W}$ resistor, with a ceramic former and having substantial lugs. One of the "positive" wire leads from the condenser is also connected to this terminal of the rectifier, and the other end of the resistor goes to the second positive tag of the condenser, the thick wire lead giving adequate mechanical strength. This is point B (see Fig. 2), the output lead, and the unit is now ready to be connected up.

The simple circuit is shown in Fig. 1. A small eliminator-type transformer, having a single H.T. winding. is employed, thus isolating the chassis from mains and increasing safety.

This power pack can be made up in a few minutes, usually from odd components which can be found in the spares-box, and one or two kept ready-built will be found invaluable when power supplies are wanted in a hurry during experiments.

# CALCulating $\pi \cdot$ NETWORKS 

# DETERMINING COMPONENT VALUES FOR THESE COUPLING CIRCUITS 

$\mathcal{T}$

By G3OGR HE common use of a $\pi$-network is to couple a transmitter to the line feeding the aerial. In these circumstances, the network is nearly always required to provide an impedance transformation from a fairly high impedance to a much lower impedance. When it cannot do this satisfactorily, various difficulties in tuning and loading arise and it is hoped that means of arriving at suitable values may be useful, together with ways of overcoming the troubles which can arise when values are not suitable.

With circuits of reliable design, difficulties of this nature may not be encountered, unless an attempt is made to operate outside the conditions originally intended (c.g., with a very high impedance aerial). But, with converted or home-built equipment, or the pressing into scrvice of unsuitable components which may be to hand, trouble may be experienced.
A typical $\pi$-network is shown in Fig. 1. The amplifie! will probably be working Class C , which means it is provided with bias beyond cut-off, and anode current flows for only about $120^{\circ}$ to $150^{\circ}$ of the excitation. In these circumstances, the anode voltage can be expected to reach about twice the H.T. voltage. If a 600 V supply were used, the isolating condenser should thus be rated at 1200 V or higher. A 2 kVW or 3 kVW condenser would serve. If anode modulation drives the anode voltage from zero to 1200 V , the isolating condenser should be for at least twice this figure- 2400 V . A 4 kVW or 5 kVW condenser would probably be used. As the capacity is not large, a component of adequate rating can easily be fitted. The choke is usually 1 mH or larger, and needs to withstand the R.F. voltage developed. A receiver type choke is only suitable for low power.
The $\pi$-network consists of C1, L1 and C2. For a low output impedance, C 2 is large. The anode or plate load R1 for the Class C amplifier can be found by dividing the plate resistance by 2 . The plate resistance can be taken as $\mathrm{E} / \mathrm{I}$. If the valve is loaded to 100 mA at 600 V , this is $600 / 0 \cdot 1=6,000 \Omega$. One half of this is 3,000 ?.

It would be usual to employ a minimum $Q$ of about 12 , for such purposes. The capacitive reactance Xc of Cl is given by:

$$
\mathrm{Xc}=\frac{\text { Plate }}{\mathrm{load}}=250 \Omega .
$$

Assume the circuit is to be used for $3.6 \mathrm{Mc} / \mathrm{s}$. The capacitor reactance $X c=1 / 2 \pi \mathrm{fC}$. From the above, $Q$ may be expressed as R1/Xc. The coil reactance may be expressed by:

## $\mathrm{Q} \cdot \mathrm{RI}+\left(\mathrm{RI} . \mathrm{R}_{2} / \mathrm{Xc}_{2}\right.$ <br> $\mathrm{Q}^{2}+1$

Approximate values are suitable, because both C 1 and C 2 will be variable, for tuning and load adjustment. This gives approximately 170 pF for $\mathrm{C} 1,12 \cdot 5 \mu \mathrm{H}$ for L 1 , and $1,000 \mathrm{pF}$ for C 2 , where R2 is to be about $70 \Omega$.


Fig. I (above).-A typical $\pi$-network output circuit.
Fig. 2 (below). -The values of components determined
for a typical circuit.


## Practical Circuit

These values are inserted in Fig. 2. A 2 -gang 500 pF condenser is used for C2, with sections in parallel. If an output impedance higher than about $70 \Omega$ is to be matched, C2 has to be reduced in value. This is readily carried out by adjusting it as necessary. If a very high impedance is wanted, it may be found that Cl is too small, or L 1 too low, for resonance.
A symptom of this fault is that C 1 is nearly closed, while C 2 is still at too high a capacity. As

C 2 is opened further, C 1 has to be closed, and reaches maximum capacity, with loading stil: insufficient. This indicates that the network was not designed to operate into so high an impedance, on that frequency. If so, one solution is to use an impedance matching circuit in such a way as to allow the $\pi$-network to operate into a lower impedance. This is preferable when the $\pi$-network is already correctly arranged. But if it has been made on an experimental basis, it may merely indicate that the condenser actually in the Cl position is too small, or the coil inductance is too low.


Fig. 3.-A $\pi$-network output circuit for 2 -band operation.
When obtaining an output of very low impedance, it will be seen that C2 requires to be larger, if Cl and $\mathrm{L1}$ remain unchanged. An indication of this type of fault arises when it is impossible to load up correctly into a low impedance circuit, even with C2 fully closed. The solution is to increase the value of C2 (e.g., employ a 3 -gang condenser with all sections in parallel) or wire additional fixed capacity across it.
In Fig. 2, C1 is the approximate total capacity. The valve capacity, etc., will be in parallel with this, but can be neglected in the example given, because Cl is variable, and can be opened slightly to secure resonance.

## Coil Windings

When an approximately suitable inductance has been found, a satisfactory number of turns may be calculated, so that the network coil L 1 can be wound. A formula suitable for this purpose is:

$$
N=\frac{5 L}{n a^{2}}\left\{1+\sqrt{ }\left[1+\frac{0.36 n^{2} a^{5}}{L}\right]\right\}
$$

where " $a$ " is the radius of coil in inches, " $n$ " is the number of turns per inch, " $L$ " is the required inductance in $\mu \mathrm{H}$, and the result ( N ) is the number of turns. A typical coil could thus have 30 turns on a $\frac{1}{2}$ in. diameter former $2 \frac{1}{2}$ in. long, for the $3.5 \mathrm{Mc} / \mathrm{s}$ to $3.8 \mathrm{Mc} / \mathrm{s}$ band.

It will be apparent that other values of Cl and L1 could give resonance, but that these values would not also provide the correct impedance match or Q . The fact that Cl and C 2 are adjustable allows the network to perform effectively over the band required.
For 2-band operation, it is usual to tap a coil, so that a lower inductance is available for one
band. This can be arranged by fitting a switch. If additional capacity is required to obtain a sufficiently low impedance output on the lower frequency band, a 2 -way switch may be used to introduce this as well, as in Fig. 3.

The 170 pF condenser used for C 1 can readily be adjusted to the value shown in Fig. 2. For $7 \mathrm{Mc} / \mathrm{s}$, all values will be approximately one half those given for $3.6 \mathrm{Mc} / \mathrm{s}$. Resonance will thus be obtained with Cl at approximately 100 pF (including circuit capacity) and C2 at 500 pF . For lower


Fig. 4.-Two methods of impedance matching.
impedance transformation (e.g., higher impedance output) C1 will be increased, and C2 reduced. For higher impedance transformation (e.g., lower impedance output) C 1 will be reduced in value, and C 2 increased. It will thus be possible to load into low-impedance circuits with the $2 \times 500 \mathrm{pF}$ capacity at C2, and the extra fixed condenser, switched in for the lower frequency band, is not required on the $7 \mathrm{Mc} / \mathrm{s}$ band.

## Impedance Matching

When the $\pi$-network is correctly built, but it is impossible to load up the transmitter correctly, the impedance being fed is outside the range for which the network was designed. A frequent example of this arises with a high impedance aerial, such as an end-fed half-wave type. In these circumstances, no adjustment of Cl and C 2 will give adequate loading. In addition, the voltage across C2 may become too high, and the spacing of the condenser used here is not intended for the high voltage swing in a circuit of high impedance. If so, both the inability to load sufficiently, and the


Fig. 5a.-Values for reactance of Cl and LI for a $Q$ of approximately 12


Fig. 5b.-Volues for outputs in the region of $50 \Omega$
flash-over, may be avoided by an impedance matching circuit such as those in Fig, 4.

The L -section circuit allows the transmitter condenser C 2 to be adjusted for a low impedance output, while C1 in Fig. 4 is of small capacity and wide spacing, for the high impedance aerial. $\mathbf{C l}$ may easily be chosen by using a component of similar spacing and capacity to Cl in Fig. 3 .

The parallel tuner produces a similar result, but in this case the coil is parallel tuned by a condenser of about 150 pF to 200 pF , and with adequate spacing. The coil can resemble that in the transmitter. Only a few turns are required for the link, and loading can be adjusted by modifying the link
coupling, and the tapping of the aerial on the coil, as well as by adjusting the r-network output condenser.

In the case of a commercially made transmitter which cannot be loaded into an end-fed aerial, one of the circuits in Fig. 4 will provide a solution. The parallel tuned circuit may also be used to feed twin high impedance lines.

## Chart Values

To simplify working, the figures required may be taken from Fig. 5, which is for a Q of approximately 12. The load is found as already explained, for the anode voltage and anode current required.

It will be more convenient to express values directly in $\mathrm{Mc} / \mathrm{s}, \mu \mathrm{H}$, and pF , to simplify calculation. For example, if the frequency is expressed in $\mathrm{Mc} / \mathrm{s}$, inductance will automatically be obtained in $\mu \mathrm{H}$, which is more convenient than employing cycles per second and Henries.

With C2, the actual reactance required for a $50 \Omega$ output would be lower than for a $75 \Omega$ output, so that the condenser values would be greater for $50 \Omega$, than $75 \Omega$. However, except for the cases previously described, this can be accommodated by the adjustment of the condenser.

For a given load and frequency, lower reactances may be used for C1, L1 and C2, when a higher $Q$ is required. It would normally be satisfactory to take a $Q$ of 12 as near the lowest to be used. In some circuits it will be possible to plan the $\pi$-network for a $Q$ of 15 , or even 20 , but when the load R1 is fairly low, it will be found rather impracticable to provide the values of capacity needed, beeause they will become so large.

## ABOUT LOUDSPEAKERS

## (Continued from page 488)

permanent repair. If the fault is due to the speech coit being out of centre and the centring device has not shifted, the centring "spider" may have come loose from the cone or the speech coil former may have warped. A centring device which has cracked or parted from the cone can usually be repaired without difficulty, and repairs have been carried out successfully when the speech coil has actually broken away from the centre of the cone. The cone and speech coil assembly should be removed from the loudspeaker chassis and a cellulose cement should be applied between the coil former and the cone and allowed to set hard before reassembling. Loose turns on the speech coil can also be locked with a similar cement applied in a very thin layer.

If the speech coil former has warped, there is usually little that can be done, for even if the former is squeezed back to approximate its original shape, it very of ten warps again as soon as it warms up in the set. This trouble, in fact, often happens in small mains-type radio receivers, which become very hot inside and use a small loudspeaker. When the set is first switched on the reproduction may be normal, but after a warm-up period loudspeaker distortion becomes apparent, owing to warping of the speech coil. The only cure here is to replace the loudspeaker.

## Speaker Centring

To re-centre a loudspeaker, the retaining screw or screws of the centring device should be slackened. Pressure should then be applied to the cone as required and the retaining screw or screws tightened. The process may have to be repeated several times in order to achieve the best results. The speech coil must. of course, operate within the magnet gap without touching the pole pieces.

Gauges for pushing between the coil former and the magnet to hold the former in the correct position while tightening the centring screws are available, but if these are used care should be taken to avoid using too much pressure, otherwise the former may spring out of centre when the gauges are removed. One way of cheoking whether the speech coil is correctly contred is to apply about $2 V$ A.C. via a $100 \Omega$ current limiting resistor, to the speech coil terminals on the loudspeaker chassis. If all is well, the cone will vibrate freely without harshness or obvious fouling. The correct centring position can be established, if necessary, by adjusting the centring device with the loudspeaker connected to the A.C. supply, but the speech coil should not be allowed to rub on the pole pieces for any length of time, otherwise the coil winding may be damaged.

Metallic particles of a ferrous nature, or even rust, sometimes reduce the magnetic gap or stick to the pole pieces. These can be removed by pressing a piece of Plasticine or soft wax on the pole pieces and magnet assembly.

## HOW TO KEEP HADID EQUIPMENT

# f <br> 00 



# VENTILATING HOME-CONSTRUCTED INSTRUMENTS PRONE TO OVERHEATING 

By W. Cleland

Left.-Expanded aluminium was used in this oscilloscope for ventilation.

## Equillbrium

Usually electrical apparatus should be capable of continuous working. Laboratory equipment is sometimes kept switched on permanently to maintain steady conditions. This means that thermal equilibrum must be reached at a reasonable temperature. Cooling only begins to take effect as the temperature rises sufficiently above that of the surrounding air. Heat loss then increases rapidly until it balances heat production, and a steady temperature level above ambient is then maintained.


Fig. 1.-The curve " $A$ " represents the result of inodequate ventilation, curve " $B$ " with more ventilation.

Provision of ample ventilation not only ensures a lower ultimate temperature, it also considerably shortens the heating up period, and allows the heat to be distributed evenly in a shorter time. When numbers of valves are involved with an appreciable wattage dissipation in a confined space,
(Continued on page 534)

## Practical T U T

ITH each copy of this issue is included a Practical Wireless "Tutor" blueprint. This blueprint has been designed to give the complete beginner to radio construction a graded course to introduce him to the techniques and theory of wireless. The "Tutor" describes four simple receivers, each complete in itself, which can be built by the complete beginner with certainty of good results. The instructions fur building the first receiver are more detailed than those for the remaining three as the constructor will gain proficiency and will need less guidance as he works his way through the course. The main difficulty which the beginner will encounter is the art of soldering. A second difficulty will be in recognising circuit symbols. Both of these difficulties will. however, be overcome by a study of pages 508 and 509 where circuit symbols are given together with illustrations of the components concerned. Details of the soldering process are also given togcther with illustrations.

## The First Receiver

## The first receiver consists of a crystal set using

 the modern equivalent of the old "crystal and cat's whisker" of the early days of radio. The results from this set are very good, particularly if a good aerial and earth are used. The results obtained will encourage the constructor to build the second and subsequent receivers.
## Construction

The set is built on a wooden baseboard and this is the first part to be made. The baseboard is cut from inexpensive timber and is 7 in . long and about
${ }_{3} \frac{1}{8}$ in. wide-the nearest stock width of wood is quite suitable although it is better to err on the larger side. A hardhoard front panel is then cut
 the first set (see blueprint)-the other holes can be made at the same time if it is intended to build all four receivers. When the panel has been drilled, it is screwed to the front of the baseboard. A case can then be made as shown in Fig. 1 on page 507, but if the width of the timber of the baseboard differs from that given, then some dimensions will have to be altered. When the wood for the baseboard is bought, it should be possible to have it cut to the width given at little extra cost. The case is best made at this stage to avoid disturbing the wiring of the sets later.

The case may be given a coat of varnish or paint and the baseboard a coat of clear varnish before starting construction.

## Construction

First, the components concerned are mounted on the front panel: four terminals and the tuning condenser (C1). Then the coil must be made. The former for the coil is made from a $5 \frac{1}{2}$ in. length of cardboard tube about $1 \frac{\mathrm{in}}{}$. in diameter. Pierce a small hole (with a sewing needle) at a point $1 \downarrow$ in. from one end and pass the end of the 34s.w.g. DCC (double cotton covered) wire through it. The wire may be passed through another hole to anchor it securely as shown on the blueprint. Now wind on ten turns of the wire side by side in the direction shown on the blueprint. Now, double the wire back on itself for about 2 in . and twist the doubled-back portion together quite tightly so that does not come untwisted when it is pulled gently.


Making the Long Wave coil for the Stage 2 Receiver-iwo square: of cardboard are required together with a $\frac{1}{d} \mathrm{in}$. length cut from the cardboard tube used to make the Medium Wave coil, and a tube of Balsa Cement. The cardboard ring is glued to one of the cardboard squares and when the cement nos set, the excess cardboard is cut away to within a $\frac{1}{6}$. of the ring-see 2 . The remaining square of cardboard is then glued to the other side of the ring. These two pieces of cardboard eventually form the checks of the former. The corners of this square are bent (3) so that the 36 s.w.g. wire may be wound on to the fomer more easily. When winding the coil, pin holes are made in one cheek of the former and

the wire bassed through to anchor it. Balsa Cement may be applied where the wire passes through the cheek. When the coil has been completed, the remaining square of cardboard is cut to leave a circle of the some diameter as the first.

By R. E. F. Street

Wind on another ten turns and again double the wire back on itself for about 2 in . and twist it as before. Arrange the twisted portion so that it is in line with the first as indicated on the blueprint. Wind on another ten turns and make another twist. Carry on winding, ten turns at a time and twisting until 90 turns have been wound on altogether. Then, pierce another small hole at the "finishing" end of the winding, and wedge the wire in it, using a piece of wood-a sharpened match-stick is ideal. The wire does not pass through the hole, but is only anchored there. Cut the wire to leave about 6 in .

Balsa cement can now be used to fix the wire to the former securely. Spread it liberally around the twists of wirc and the two end wires of the coil. Allow the cement to dry and cut the wire at each twisted loop. Two ends will thus be formed at each twist. Unravel the cotton covering at each of these ends or remove it by scraping gently with a knife. Twist each pair of bare wires together and in such a way as to form a small "bunch" of copper wire at each twist or "tap". These taps can now be tinned with solder-apply the soldering iron to each in turn together with the solder and leave a small blob of solder at each tap.

The supports for the coil are next to be made.

Cut two pieces of hardboard $2 \frac{3}{8} \mathrm{in}$. long and as wide as the diameter of the cardboard tube. Place the tube at one end of each and mark a semicircle to be cut away so that the supports are circular at one end. One of the supports may now be cemented to the tube on which the coil is wound (so that the taps on the coil will be in the position shown on the blueprint) When the cement is dry, the other suppors may be glued in placethe two supports must, of course, be parallel.

The group-board may now be mounted and components C2 and D1 saldered in position. These are the only ones to be mounted on the group-board in this receiver. Note the position of the red, or positive, end of the diode D1. When soldering, remember not to overheat the compo-


The completed LW. coll.
nents, especially the diode. Leave the leads of the diode long-do not cut them at all-and conduct the heat away when soldering with a damp cloth or with pliers as shown on page 509.

Solder in the two wire links on the group-board which are shown on the blueprint. Connect the earth terminal to the moving plates connection of the variable condenser Cl ( M ) and take a wire from there to C2. Keep this wire near to the baseboard-the battery will be fixed over this wire in the three other stages. Connect the fixed plates of the condenser (F) to DI. Connect the headphone terminals to the tags indicated on the group-board. Two pieces of thin plasticcovered flex will now be required: one of these is connected to the aerial socket and the other to the fixed plates connection of the variable condenser.

Mount the coil-the end at which winding was begun should be on the left (viewed as shown on the blueprint). Connect the right hand end of the coil (6in. of wire was left) to the moving plates connection of the condenser. Connect the fiex lead from the aerial terminal to the third tap from the right on the coil, and the one from the fixed plates to the first tap from the left. The end wire of the coil is, of course, not used.

Connect the aerial and the headphones, rotate the variable condenser (C1) and at least one programme should be heard. If not, check the connections and if still no results can be obtained, connect the aerial to the same tap as the wire from the fixed plates to the condenser. The signal should now be heard. if a programme was


A variable condenser of the type used in all four 'Tutor' receivers. (The fixed plates connection is the lower of the two soldering tags.)


The Stage 4 Receiver.
obtained before the aerial tap was moved, then it will be noticed that although the signal is louder, it spreads over the full range of the condenser C1. The set is now not so selective-it does not tune so sharply-but it is more sensitive-the signal is louder.

Note that a good aerial and earth are essential for a crystal set of this type and poor results will of ten be due to insufficient signal reaching the set.
The tapping of the aerial on the coill can be altered to improve results and the best position will soon be found.

## The Stage 2 Receiver

Disconnect and remove the coil so that it is not damaged when the new parts are being added. Mount one of the Terry "clips," as shown to hold the battery. Cut off one "arm" from each of two Terry clips (to leave the holes for mounting). Each clip is then screwed to the baseboard to contact the two ends of the battery when it is in position. Use $\frac{1}{2}$ in. brass screws to mount the clips for ease of soldering later. Connect the left hand--positivebattery terminal to the earth socket, and the right hand-negative-battery terminal to one side of the on/off switch (S2). Connect the other side of $\mathbf{S} 2$ to the left hand headphone terminal. At the same time, remove the wire already there, shorten it and solder it to the tag marked $b$ on the group-board of the Stage 2 receiver. Join tag e to C2 as shown. Remove the wire linking the other headphone terminal to the group-board and connect this terminal to tag c .

Now make the Long Wave coil as shown in the illustrations (pages 504 and 505 ). 250 turns of the 36s.w.g. wire are needed. Note that both ends of the wire should be anchored through holes in the same cheek-the left hand one, and the direction of winding should be the same as for the M.W. coil, i.e. as shown on the blueprint.

Now join one of the inner tags of the wavechange switch S1 to the moving plates connection of the variable condenser C1.
Solder the transistor to tags e, b and c, with the emitter to tag e, base to $b$ and collector to $c$. Do not cut the wire short and use pliers or a piece of wet cloth to conduct away the heat when soldering the leads. The procedure is described and illustrated on page 509. Make sure that the transistor is soldered in the correct way round. A diagram is given on page 508. Great care should be taken where transistors are concerned or these expensive components will be ruined.

Remount the coil, and connect the M.W. winding as before, except that the right hand wire goes to an outer tag of $\$ 1$-corresponding to the inner tag used. To this outer tag is also connected the inner end (or starting end) of the L.W. coil-the other end goes to the inner tag in use on S1.
Replace the battery and switch on. Turn Cl with S1 in the M.W. position. The same stations as in the Stage 1 Receiver should be heard, but much louder and the aerial may be moved more to the right to reduce volume and improve selectivity. Several programmes should be audible, particularly at night.

Move S1 to the L.W. position and the Light Programme should be received. To improve results the tappings on the M.W. coil may be altered as required.

By now, even the complete beginner should have an idea of the meaning of the circuit diagrams and how they constitute a short way of describing receivers. It is a useful exercise to compare the circuit of the set just completed with its actual physical layout.

## The Stage 3 Receiver

Remove the battery and then disconnect and remove the coil. Mount components C4, R1, R2, C5, D2 as shown on the blueprint. Note the position of the red, or positive, end of D2. Wire in the associated links on the group-board and mount C3, the other variable condenser, on the front panel, moving S1 to the new fixing hole.

## Coil alterations

An $\frac{1}{8}$ in. to the right of where the M.W. coil finishes, pierce a small hole and anchor the end of the $34 \mathrm{~s} . \mathrm{w} . \mathrm{g}$. wire, leaving a 6 in . end. Wind on 30 turns in the same direction as the M.W. coil over a length of about $\frac{1}{4} \mathrm{in}$. Pierce another hole and anchor the wire and leave a 6in. end. Now remove 100 turns from the L.W. coil (leaving 150 as shown on the blueprint) and rewind 40 turns on top of the 150 turn coil as a separate coil. The ends of this coil are passed through the right hand cheek.

Solder in transistor Tr2-take great care not to damage it by incorrect connections or by excessive heat. Connect the wave-change switch to C 3
and C 1 as indicated, and also wire in the link shown (the one which joins two of the outside tags). Now remount the coil and connect it as shown. Note that if the windings have been made exactly as given on the blueprint, the letters on the diagrams can be used to assist wiring in of the coil.

Finally, insert the battery and switch on with SI in the M.W. position. Stations should be heard, and if C3 is rotated, should become louder until an oscillation is heard. Adjust C3 so that it is just short of the point at which oscillation begins and it should be found that selectivity is much greater than with the Stage 2 Receiver.

If it is found that closing C3 makes results worse, reverse the connections to the M.W. reaction coil. When results are satisfactory on M.W., try L.W. If reaction cannot be obtained, teverse the connections to the L.W. reaction coil. It should be noted once again that if the blueprint is followed exactly, the reaction will be obtained on both wavebands from the start.

## The Stage 4 Receiver

The Stage 4 Receiver is the circuit of the Stage 3 Receiver with an extra transistor amplifier added to increase volume.


## to help the beginner build the 'Tutor' <br> Fixed resistors.



Tuning condenserthe type used in the 'Tutor' is shown on page 506.


Crystal diode.

## CIRCUIT SYMBOLS

The four 'Tutar' recaivers described in this issue were designed especially for the absolute beginner to radio construction. It is therefore probable, that to some readers intending to build these sets, the circuits diagrams relating to them (on the Bluaprint) appear too complicated for them to comprehend. These circuits are, in fact, very simple and with the help of the diagrams, illustrations, and hints on soldering given in these two pages, even those with no previous knowledge of radio should be able to build any or all of the four sets satisfactorily.

The diagrams on this pase of the various circuit symbols, and the accompanying photographs of actual components, are, on the whole, self-explanatory. For instance, no one would mistake the symbol for a pair of headphones, but the sign for a tuning condenser (botzom left of this page) might prove confusing until it was pointed out that in circuit diagrams, a component crossed with an arrow usually means it is variable, e.g. variable resistors and condensers. The circuit symbol for a battery is given, without an illustration as it is felt that of all the components used in making these receivers, this, at least, is likely to be recognised by those unfamiliar with radio construction. Similarly, no photograph is given of a switch but the physical appearance of the two types used in the 'Tutor' may be seen from the Biueprint. The dimensions and construction of the tuning coil may be obtained from the article on the receivers and from the Blueprint.

0000
Tuning coil.

E...Emitter
B....Base
C.... Collector

Transistor

## ㅋ|l $\left.\right|^{ \pm}$

Battery.

It is essential in radio construction to be able to make good soldered joints. If poor joints are made, then the receiver or other apparatus may not work at all or may work for only a short period. The besinner may think that good soldering is difficult: it is not. Soldering consists of coating the parts to be joined with a thin layer of molten solder and allowing it to solidify over the oin.

THE TEMPERATURE OF THE IRON
The first essential is that the soldering iron should be at the correct tempera ture-if the iron is electric, then it will automatically be at the correct heat, but if it has to be heaced in the gas or in a fire, then it may easily be too hot or too cold. The correct heat is shown when the iron causes a green coloration to the flame of the source of heat.

The second essential is that the iron should be clean and tinned-if a new iron is bought, then before it is used for the first time, it should be heated to the correct temperature, cleaned with a file or sandpaper, and solder applied to the tid. This attion will give a coating of solder on the tip or bit of the iron. Note that this is the only time that solder is applied direct to the iron.

## THE CORRECT SOLDER

The third essential is that cored solder should always be used-preferably "Multicore Savbit" which contains a non-corrosive flux and also prevents erosion of the copper bit of the iron.
When soldering, heat the surfaces to be joined and apply the solder direct rather than carry it to the joint on the tip of the iron. This procedure is elearly illuscrated on the right. If the solder is not applied direct to the parts to be joined, then the flux which is included in the solder to make good joints easier serves no purpose and dry joints, which can be pulled apart easily, will result.

Transistors and diodes need very careful soldering if the heat of the operation is not to ruin them. The best method of conducting the heat away from transistors and diodes is shown in the illustration on the right. A pair of long-nosed pliers is used to hold the lead to be soldered and provided that the joint is made quickly, the pliers will conduct the heat away from the transistor. This procedure will also be found useful for other parts. Note that if the soldering tron is not sufficiently hot, it will take a long time to make joints, and the parts being soldered will become very hot.

(Above) Soldering a resistor to a tog-board, and (below) using pliers as a heat shunt when soldering transjstor leads.


## RESISTOR COLOUR CODE



2. Red
4. Yellow
7. Mauve

First Number-- Body
or
Band 1
Second Number-- $\left.\left.\begin{array}{l}\text { Tip } \\ \text { or } \\ \text { Band } 2\end{array}\right\} \begin{array}{l}\text { Mauve }=7 \\ \left.\text { Number of Noughts- }-\begin{array}{l}\text { Spot } \\ \text { or } \\ \text { Band } 3\end{array}\right\} \text { Orange }=3\end{array}\right\} 47,000 \Omega(47 \mathrm{k})$



Fig. 1.-The circuit of the meter.

## A Recording-Ievel Meter <br> By R. Dowling

## A USEFUL ADDITION TO ANY

7TAPE RECORDERS APE RECORDERS are at present enjoying an unprecendented popularity owing to their versatility and ease of use. This has made it possible to produce tape recorders at prices much below those of a few years ago. Despite the high sales, however, manufacturers have to make one or two economies in order to produce machines at the lowest possible price. For example, some decks have only one motor (with ingenious pulley switching to carry out the various functions); most decks have a combined record/playback head; and very few of the cheaper tape recorders have anything other than a simple "magic-eye" in order to estimate the optimum recording-level.

The purpose of this article is to describe a single-valve recording-level meter constructed in such a way that it makes an easy "add-on" unit to any tape recorder. It will be found that the mean recording-level may be determined with much greater accuracy than the average "magiceye ", resulting in a much improved signal-tonoise ratio on the recordings made.

## General Circuit Description

The circuit of the unit is quite straightforward, and is shown in Fig. 1. The valve used is a 12AX7 double-triode, one half of which is strapped as a diode. The audio signal from the tape recorder is fed to the cathode of V1a through an isolating capacitor ( $0.25 \mu \mathrm{~F}$ ) and the "set-level" potentiometer ( 25 k ). The rectified output of V1b is then fed to the grid of V1b. Between this point and earth is connected a CR combination ( $1 \mu \mathrm{~F}$ and 1 M ) giving a one-second time constant. This prevents the meter from trying to follow the audio signal peaks too closely, and accordingly gives a better measure of mean audio level. It should be noted, however, that if a milliammeter is used which is inherently rather sluggish, better results will be obtained with a rather smaller time constant (say, $0.5 \mu \mathrm{~F}$ and 1 M ).
The indicating milliammeter is connected in the cathode circuit of Vib. It should have a f.s.d. of


Fig. 2 (above).-The component layout: the 25 k potentiometer may be mounted on any small bracket. Fig. 3 (below).-A method of modifying the milliammeter scale; left, the original scale; right, the modified scole.


Coloured in Red
1 mA , and is shunted by the "set-zero" potentiometer ( 500 s 2 ww ).
The power supply required for the unit is only about 1 mA at 250 V and 0.3 A and 6.3 V . The tape recorder will itself usually be able to provide this light extra load with no difficulty. The whole unit may be built up on a small tag-board as suggested in Fig. 2.

## Calibrating the Meter

In the zero-signal condition, the meter will read full scale deflection: this is the reason why the milliammeter is shown mounted upside-down in Fig. 3. It is seen that the face of the meter is renumbered from 0 to 10, the portion from 7 to 10 being painted in red. A good plan is to unscrew the original meter dial and paint over the back with white paint. Then a new scale may be easily marked out, using ink-compasses and Indian ink.

The meter is set to the new zero by means of the set-zero potentiometer, and a signal (preferably a continuous tone) applied to the input of the tape recorder. The recording-level control on the machine is then slowly advanced in the normal way until the correct level is indicated on the "magic-eye". The set-level potentiometer is now adjusted until the needle of the meter reads about 7 , and thus the 7 to 10 portion in red will indicate over-modulation.
Finally, a word about the actual audio take-off point in the tape recorder. A satisfactory , point on most small machines is the "magic-eye" grid; in the unlikely event of the signal voltage level at this point being too low, one may alternatively take off a signal at the grid of the output valve.


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volly. D.C. Current: $0-50$ microamps. 0-2.5 m/a. o-250 m/a. Resistance: $0-6 \mathrm{k}$,
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## IHTERNATIONAL CORRESPONDENGE SCHOOLS



By E. V. King
(Continued from page 391 of the September issue)

$\mathcal{L}^{\prime}$AST month, Chassis No. 4 was constructed. This unit was the crystal check oscillator, and if the construction was completed and the multivibrator set on $10 \mathrm{kc} / \mathrm{s}$ as described, the unit should give marker, or check frequencies at intervals of $100 \mathrm{kc} / \mathrm{s}$ or $10 \mathrm{kc} / \mathrm{s}$ according to whether switch Sll is on or off. The complete circuit of Chassis No. 4 is given in Fig. 32a on this page so that the constructor will have a diagram of the unit as a whole if a fault should develop and repairs become necessary.


Fig. 32a. - The complete circuit of Chassis No. 4-the crystal check oscillator.

# THE P.W. SIGNAL GENERATOR 




Fig. 35. -The construction of the cobinet of the generator.
Figs. 33 and 34.-The circuit and construction of the dummy aerial unit.

## The Dummy Aerial

When an R.F. signal generator is connected to a receiver instead of the ordinary aerial, it is hest, though not absolutely essential, to connect it through a device which has approximately the same characteristics as the original aerial. This is particularly necessary when dealing with radio frequency amplifiers as in TRF receivers.

A special lead is therefore made which plugs in to the R.F. output socket of Chassis No. 2. It passes through a small can containing the (Continued on page 517)


Fig. 36. -The front panel of the completed signal generator.

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This A.C. Mains receiver is the latest model in the famous CLIPPER Series and combines really top performance with superb professional finish. It is the finest ALL BAND receiver at the price with a new high gain eircuit using ECC81 double triode, EL84 output, EZ80 full wave rectifier. Power output $3 \frac{1}{2}$ watts for $2 / 3 \mathrm{ohm}$ speaker. Covers $10-2000$ metres ( 5 coils). World-wide reception. Outstanding features include 3 planetary slow motion drives, separate electrical bandspread, air spaced low loss variables, satin silver dials, silver hammer front panel. Total building cost, including spaced low loss variables, satin silver dials, siver hammer front panel. Total building cost, including
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CODAR RADIO COMPANY, COLEBROOK ROAD, SOUTHWICK, SUSSEX
(continued from page 514) components of Fig. 33 and passes out to the receiver under test.

## Making the Dummy Aerial

Obtain a suitable "tin" can of $1 \frac{1}{4} \mathrm{in}$. diameter or more, and $2 \frac{1}{4} \mathrm{in}$. or more long. The lid may be clipped on or screwed on. The prototype uses a tin which contained Chinese Lacquer.

Refer to Figs. 33 and 34. Make L6 by winding $32 \mathrm{~s} . \mathrm{w} . \mathrm{g}$ enamelled copper wire on the $2 \frac{1}{4} \mathrm{in}$. former in a single layer for 100 turns. Apply cellulose cement and let it set. Fix the coil in the centre of the lid and remove any dust cores from the former. Fix one band of wire (about 26s.w.g) at each end by twisting and soldering and solder the ends of the coil to these "bands" (Fig. 34).

Drill two $\frac{1}{4} \mathrm{in}$. holes in the lid to take the two screened cables, and if necessary file away a little of the base of the coil former. Prepare the screened cable so that it can be fixed on the inside of the can by soldering the metal braiding to the can. Use rubber grommets to protect the cable where they pass through the can.

Connect the centre lead of one of the cables to the bottom of the coil, and attach crocodile clips to the ends of this lead as shown. The best method is to cut off the outer plastic covering for a few inches and twist the copper braiding into a "pigtail" and solder a length of single flex to it as shown. The joint can then be bound with insulating tape so that the lead does not break off with use.

The coaxial lead is taken through C30 to the top coil connection. Between the top and bottom of the coil attach R38, C31 and C32 as shown (Fig. 34). A single condenser of 400 pF may be used instead of C31 and C32. The other end of this second coaxial lead is taken to a plug for the R.F. socket. Be careful to connect this plug correctly. Check with a battery and bulb that the braiding and centre conductor are not shorting.

## Testing the Dummy Aerial

Connect the unit between the generator and any type of receiver. Switch on R.F. (modulated) for the correct waveband, and tune the receiver or generator until a note is heard. Even with com-

## COMPONENTS LIST FOR THE DUMMY AERIAL

Iyd of coaxial cabie; about Ift of single flex One coaxial plug (Belling-Lee)

## Two crocodile clips

$1 \frac{1}{4}$ in. $\times \frac{1}{4}$ in. diameter coil former (no cores are required)
A few yards of 32s.w.g. enamelled copper wire Three 220pF condensers-mica or ceramic
One resistor $-390 \Omega \frac{1}{2} W$
paratively simple receivers, the dial positions for certain "wavelengths" should still be about the same as when used with the normal aerial.

## Making the Cabinet

The three units are placed side by side with the power unit (Chassis No. 1) on the left and finishing with No. 4 (Crystal Check) on the right. The necessary wires are connected at the back, keeping to definite colours for the various connections in case servicing is required later. Verify that all the units still work as they did when tested separately. Note that all units must not be switched on at once or the mains transformer will be overloaded. When the crystal check unit is switched on, then the R.F. unit may also operate, but not the audio oscillator as well.

Four square-cut pieces of planed soft wood are purchased and assembled as shown in Fig. 35. Verify that the units will all fit in it and then cut out a piece of aluminium sheet from which to make the front panel. Another may be used, with ventilation holes for the back. Fix this aluminium sheet to the front of the case.

Place the four units inside the cabinet shell, and put a little Vaseline on the tip of each control spindle and switch. Offer the aluminium sheet

## COMPONENTS LIST FOR THE POWER OUTPUT METER

ImA moving coil meter-the prototype used a meter hoving a $2 \frac{1}{2}$ in scale, but a smaller type would be suitable. The internal resistance is immaterial
Four diodes-'surplus' types are sultable
R39 about 8.2 k -see text
R40 Any physically large, high-valued, resistor wound with one yard of 26s.w.g. Eureka wire (see Fig 38)
Two pole terminal block for flxing to the front panel of the completed generator
Nuts and bolts, soldering tags, Perspex etc.


Figs. 37 and 38. The circuit and construction of the power output meter.
carefully to the cabinet shell. The longest control knob will leave a Vaseline mark on the panel. This point is then drilled to take the spindle or switch concerned. The sheet is then offered up again with that spindle hole only cut. Another mark will then appear; this is then drilled out. The remaining holes are drilled in the same manner. A round file will be necessary and the actual switch holes must be sufficiently large so that the threaded portion of the switch may project right through the panel to receive a nut on the outside. This connects the panel (electrically) with the four chassis.
Remove the drilled panel.

## Screening

All of the inside of the cabinet is now screened with aluminium foil as is used for cooking purposes and obtainable from household stores. A few drawing pins will hold it in position. Bend it over so that when the panel is fixed, it will clamp the aluminium screen in place. Likewise the back will also clamp it and make the screen continuous.

The back may be of hardboard covered with aluminium foil, but be careful that it does not touch the terminal strips on each unit. Aluminium sheet ( $18 \mathrm{~s} . \mathrm{w} . \mathrm{g}$.) will also be suitable, and in either case ventilation holes will be necessary-four or five 1 in . holes along the bottom and top. For good screening, these will have to be covered with wire gauze as is obtainable, for petrol filters, from a garage.

## Marking the Panel

The units are placed in position and extra nuts are then put on to hold the units in place. The assembly is tested.
The panel now has to be marked in some way. First roughen the surface of the panel with sandpaper and then give it a coat of cellulose or lacquer. When the paint is dry, mark the panel. The following methods may be used:-

1. white paper, paste and Indian ink. Cover each piece with Sellotape.
2. white ink and cover the lettering with clear spirit varnish (not cellulose varnish) afterwards.
3. transfers obtainable from most radio shops. shops.
Control knobs of any type may be used, but the diagrams show types which are very suitable. The following Bulgin types are suggested:
Main R.F. Frequency, 1/K403
Main A.F. Frequency, 2/K402 (this has to be modified as explained later).
R.F. Output Control, 4/K400
A.F. Output Control, 4/K400.

All other controls use types 38 .
It must be stressed that large diameter knobs are essential for the two frequency controls.

## The Power Output Meter

It will be very useful to have a power output meter in the completed generator so that receivers may be tested and aligned without disturbing other members of the household. Various possibilities will occur to readers, but in this design a $3 \Omega$ dummy load is used with a meter fitted with a bridge rectifier working as a voltmeter. The meter is arranged to read directly up to 10 V , but it could be calibrated easily in Watts. "Wattage" is equal to the voltage multiplied by itself (i.e. squared) and divided by 3 . For instance, if the dummy load were connected to a receiver instead of its $3 \Omega$ loudspeaker and the reading was 6 V , the wattage or power would be ( $6 \times 6$ )/3-12W. Readers will note that the meter is not very sensitive, but this is purely in the interests of safety and R39 (Figs. 37 and 38) may be reduced. However, if the amplifier under test overloads the meter it will burn out, or the rectifiers will be ruined or both. The meter will not give a true power reading on a $15 \Omega$ loudspeaker, but will still be useful as an indicator when trimming receivers.

## Making the Output Meter Assembly

Refer to Fig. 38. A small sheet of Perspex or paxolin is drilled to take the meter terminals (e and f). Four other holes are also drilled at $a, b$, $c$ and $d$. Soldering tags are bolted at each of these four holes and the panel is then fixed to the meter as shown.
Take the output leads from a and d, make up the resistor R40 and solder it to a and d-if R40 burns out or is open-circuited in any way the meter will be ruined. Solder R39 ( $\frac{1}{2}$ W) from a to b.

Now, wire in the diodes: hold the wires in cold pliers when soldering so that the diodes are not heated. The red or positive ends must be wired as shown in Fig. 38. Tag e has a diode wired to $c$ and one to $b$, and $f$ has one wired to $c$ and one to $b$. Check that tag $e$ has two uncoloured ends connected to it and that $f$ has two red ends connected to it. If the meter used has the positive terminal on the right, reverse all the diodes and check the wiring against Fig. 37. Fix the unit to the front panel and wire the leads from $d$ and a through a grommet to the terminal block.
Next month the calibration of the R.F. and A.F. oscillators will be explained in detail so that the frequencies corresponding to various settings of the dial are known quite accurately.
(To be continued)

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| $O C 44$ | $11 \%$ | $O C 71$ | 616 | $0 C 76$ | $8 \%$ |
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| OC45 | $10 \%$ | $0 C 72$ | 81. | $0 C 78$ | 81 |
| OC70 | $6 / 6$ | $0 C 75$ | 81. | $0 C 81$ | $8 \%$ |

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69.12 .6
$E 1.9 .0$
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E12.10.0
K1. 7.6
65.5 .0
629.0 .0
42. 2. 2



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## SETS OF VALVES


(Continued from page 430 of the September issue)

A$S$ mentioned last month, the centre frequency of $10.7 \mathrm{Mc} / \mathrm{s}$ is set by moving a dust core in the former of L1. This method of setting the centre frequency ensures that the ratio of induc-tance-to-capacity in the oscillator tuned circuit is as high as possible-the only capacity in the oscillator tuned circuit consists of "strays" and


Discriminator response of an F.M. receiver.
that contributed by the valve. (1t is advantageous to have a high L/C ratio so that the variations in the capacity of the diode have maximum effect on the frequency of operation of the oscillator.)

The second half of $V 2$ functions as another cathode-follower and enables the output of the unit to be controlled by the variable control VR2.
Layout of the unit is not unduly critical, apart from that of the R.F. oscillator section where the aim should be to keep leads as short as possiblethe layout shown in Fig. 3 should be followed carefully.

## Using the Unit

In use, the unit and the F.M. set to be aligned are switched on and allowed to reach their final operating temperature. A lead is connected from the X-deflecting plate of the oscilloscope to the input terminal provided. This lead can be of coaxial cable but at the oscilloscope end the outer sheath may be left unconnected; the earth connection will be made by way of the cable from the receiver to the oscilloscope. Coaxial cable will also be needed for the lead from the unit to the receiver. At the receiver end, the braiding of the coaxial cable is twisted together and soldered to a crocodile clip which is used to connect it to the chassis of the set under test. Another length of coaxial cable is needed for the input lead to the oscilloscope. One end is terminated with plugs suitable for the oscilloscope and the other end with a crocodile clip to form the chassis connection from the outer of the coaxial cable. At the receiver end, the inner of the cable is terminated


Fig. 4.-The above chassis view, showing the layout of components.
with a resistor of about $10 k$, to act as a stopper to prevent instability. This resistor should be soldered as near to the point where the inner leaves the outer as possible. In use the other end of the resistor is soldered to the desired point in the receiver. This lead is connected between earth on the scope and the Y-amplifier input-if one of these connections has to be long, be sure that it is the "earthy" one and keep as much of the inner wire screened as possible.

For the alignment, the oscillator valve of the set is removed or the oscillator is prevented from working-methods of doing this can be determined from the circuit diagram. The output from the unit is fed into the grid of the mixer-a stopper resistor may be required to avoid instability and may have a value of 33 to $470 \Omega$, the exact value being determined by experiment.

During alignment, it is an advantage if the output of the set can be heard. and this should be fed to an audio amplifier. The oscilloscope is switched to a low sweep speed- 10 to 20 per second-and the voltage at the grid of the limiter valve, of the receiver, fed to the Y -amplifier of the oscilloscope. The deviation control on the unit is set to maximum and a hum may be heard from the loudspeaker. If not, the setting of the dust core in L1 is altered until a hum is heard and a trace is obtained on the screen. When some evidence of the response is seen, the various controls on the unit and the oscilloscope may be altered for best results, bearing in mind that the input to the set should be kept as low as possible.

## Marker Signals

The shape of the trace may be altered to give the optimum characteristic by altering the cores on the I.F. transformers. If another signal generator is available, a signal may be injected in parallel with the main signal and this will give a

When the I.F. amplifier has been aligned satisfactorily, the output to the oscilloscope may be taken from the audio take-off point, but before the capacitor which feeds the audio to the output socket of the tuner or the A.F. stages of the receiver. This is essential if a distorted trace is not to result.
The deviation control should be set so that the response curve occupies the centre of the trace; in this way, the none-linearity of the frequencysw'ep circuit may be ignored for most purposes.
Of necessity, an outline only has been given of the method of using the unit and for a more detailed explanation, the reader is referred to the article by R. Brown in the September 1960 issue of Practical Television entitled "Using the Wobbulator", and to "Semi-conductor Diodes as Variable Capacitors" by R. B. Archer in the November 1960 issue of Practical Television.

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THE Airmec L.F. signal generator, type 252 is designed for the generation of pure and highly stable sinewave signals in the frequency ranges $30 \mathrm{c} / \mathrm{s}$ to $300 \mathrm{kc} / \mathrm{s}$.

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An output control provides smooth variation of output over the meter range; in conjunction with a step attenuator, it enables the output level to be

Right.-The EM87 valve; a new voltage level indicator for tape recorders. It is manufactured by Mullard Ltd.
set to any value from less than 1 mV to 15 V open circuit.

This signal generator is made by Airmec $L i m i t e d, \quad H i g h$ Wycombe, Buckinghamshire.
VOLTAGE LEVEL
INDICATOR
HE EM87 is a new Mullard voltage indicator valve primarily intended for use as a recording level indicator in tape recorders.

In many recorders the A.F. voltage appearing at the anode of the recording output stage is about 10 V , which is insufficient to close the display of currently available level indicators. The EM87 has a grid base of only 10 V and in addition it has a high sensitivity in the initial region of the control characteristic ( $\mathrm{Vg}=\mathrm{OV}$ ).

Over modulation of the tape is immediately apparent, since A.F.
 signals greater than 10 V in amplitude cause the luminous areas to overlap, giving a brighter centre postion to the display.

Maximum ratings are: anode


An L.F. signal generator made by Airmes Limited. voltage 200 V , anode dissipation 600 mW , cathode current 5 mA . and deflection electrode voltage 300 V . The heater draws a current of 300 mA at 6.3 V .

The EM87 has the same overall physical dimensions $\mathbf{( 7 2 . 8 m m}$ overall length, 22.2 mm diameter) and the same pin connections as the EM84. The fluorescent strip is 32.6 mm in length by 4 mm in width. This new valve is made by Mullard Limited, Mullard House, Torrington Place, London, W.C.1.

## 2-BAND POCKET PORTABLE RECEIVER

THE Ajax TR-220 de luxe portable receiver is now available in this country for $£ 1317 \mathrm{~s}$. 6 d ., which includes the battery ( 9 V ), leather carrying case and magnetic earpiece for personal listening. - This receiver covers the long and


The two new silicon diodes now available from Westinghouse Brake and Signal Co. Ltd.

## MEDIUM POWER SILICON DIODES

${ }^{\prime}$ TWO new ranges of high voltage. medium power silicon diodes are available trom Westinghouse Brake and Signal Co. Ltd. The SxBR8 is rated at 18 A and may be used at case temperatures up to $140^{\circ} \mathrm{C}$, whilst the SxBR25 is rated at 30 A and nay be used at similar case temperatures. Both ranges are available in voltage ratings of 100 to 1500 V peak, with ten intermediate voltages.

The diodes are hermetically sealed, using glass/ metal seals and the latest press seal techniques. Mounting is by means of a stud base which also serves as the anode connection. The cathode connection is made by means of ar insulated tlexible lead through the glass/metal seal. These diodes are manutactured by Westinghouse Brake and Signal Co, Lid., 82 York Way, King's Cross, London N.I.
medium wavebands and supplies a $2 \frac{1}{2}$ in. loudspeaker with a 200 mW output. The TR-220 is housed in a plastic case, measuring only $4 \frac{7}{8}$ in. $\times 2 \frac{7}{8} \mathrm{in} . x 1 \frac{1}{4} \mathrm{in}$.

Six transistors are employed in the circuit which uses a ferrite rod aerial. The Ajax TR-220 is distributed in this country by Acme Electric Co. (Finsbury) Lid,, 63 Great Eastern Street, London, E.C. 2.

## DOMESTIC RADIOS AT EARLS COURT

ACOMPLETE range of radio, television, record players, etc, were on show at the Pam stand at the Radio Show this year.
The model 222 portable transistor radio, which was shown, incorporates a printed circuit chassis and is presented in a cabinet of cream and royal blue. It costs 13 guineas.

Model TB. 77 is a fully transistorised table radio. It covers four wavebands and operates from an internal aerial. It is finished in a high gloss walnut veneer and costs28 guineas.
Two car radios were shown this year: one of them, the model CR.40, is operated from a 12 V D.C. supply. It covers two wavebands and will fit any make of car. It costs $18 \frac{1}{2}$ guineas.

A stereophonic radiogram (model RG.630) was also on show. This instrument includes a two waveband VHF receiver and a four-speed autochange for monaural or stereo record reproduction. The loudspeakers are fixed into swing doors for better stereo reproduction. This model, which costs 69 guineas, and the three other radios mentioned are all made by Pam Radio and Television Lid., 295 Regent Street, London, W.1.

(Above). -The Ajax portable receiver, distributed in this country by Acme Electric Co. (Finsbury) Ltd.
(Below).-A stereophonic radiogram by Pam Radio and Television Ltd.


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$\mathcal{T}$HE use of a tuned doublet for transmitting purposes is quite well known, but the efficiency of this type of aerial for receiving can be overlooked by short-wave listeners who have not yet used anything except the simplest form of aerial. An ordinary dipole with coaxial feeder has the advantage that no tuning is required, but such aerials only work effectively on frequencies which give a fairly accurate impedance match to the feeder. As a result they are usually cut for one band only, and not used on other bands. The tuned doublet requires a tuned circuit (which may be regarded as part of the system) but this is

Fig. I.-A doublet with two half-woves in phase.
easily arranged, and the aerial will work effectively over a very wide range of frequencies. A single aerial may thus be used for harmonically related bands, such as $80 \mathrm{~m}, 40 \mathrm{~m}, 20 \mathrm{~m}$ etc., and also for $49 \mathrm{~m}, 31 \mathrm{~m}, 25 \mathrm{~m}, 19 \mathrm{~m}$ and other short-wave broadcast bands. On all bands it is tuned to resonance, a coil and condenser being used for this purpose. This tuning can compensate for modifications in the length of the aerial top, or feeder, and so exact dimensions are not necessary for these items.


A balanced aerial can also give a considerable reduction in static and similar noise, compared with a single wire or end-fed or end-coupled aerial. This reduction in noise is somewhat similar to that achieved with a coaxial feeder.
Fig. 1 shows the approximate current distribution in an aerial wire which is three half-waves long at operating frequency. Section $A$ is one half-wave;
$B$ and $C$, each one quarter-wave, make up the centre half-wave, and D is the final half-wave. If the portions B and C are brought down to make a feeder, parts $A$ and $D$ will form the flat top, and this part of the aerial will consist of two halfwaves in phase.

When a station is received, the current flow in parts $B$ and $C$ will be in opposite directions, and thus provide a signal at the tuning coil connected

to the feeder ends X. A static impulse will, however, flow down $B$ and $C$ in the same direction, and thus cancel out at the tuning coil. This explains the reduction in static interference. Cancellation will not in fact be complete, owing to lack of exact balance, but will usually be worthwhile.
When the aerial is used on other frequencies; $A$ and $D$ will not be a half-wave each, but this has little effect on results. In the same way, the

Fig.' 2.-Practical construction of the aerial.
feeders $B$ and $C$ will no longer be a quarter-wave each, but this is unimportant because of the tuned circuit attached to the ends X . It is thus possible to use a wide range of lengths, for both the flat top, and the feeder. For the same reasons, one aerial will work over a wide range of frequencies.

## Doublet Construction

Fig. 2 shows how the doublet, with tuned feeder, can be made. Single 14s.w.g. copper wire is often used for aerials, but other types of aerial wire can be employed instead. Hard-drawn wire is satisfactory for the flat top, but soft-drawn or stranded wire will be more convenient for the feeder.

Each end of the flat top has one or two aerial insulators, and suspension cords or wires are taken to suitable supports. The leads forming the feeder are roughly 6 in . apart, and spacers can be obtained for this purpose, or made. The spacers will be needed at about 2 ft intervals: A pair of insulators in the flat top enables each feeder to be attached as shown. At this point the feeders should either be parallel, or fan out slightly. They should not run closer, as might be so if only one short insulator were used. If the top and feeders are not made with single lengths of uncut wire, joints should be soldered to avoid noises in the receiver.

The top of the aerial should be as high and in the clear as possible, and especially removed from local interference. Long distance results may easily be achieved with an indoor aerial, but when space is available outside, indoor erection is pointless, and reduces signal strength.

If the top of the aerial slopes, because the supports are of unequal height, this will modify the directional pattern. The latter also depends on the aerial length. However, the position of the aerial usually depends on the available supports, so there is little point in being too concerned about directional effects.

## Top and Feeder Lengths

When the system is operating as in Fig. 1, and the feeder is just short of an odd number of quarter-waves, parallel tuning is needed at the ends $\mathbf{X}$. When the feeder is just short of an even number of quarter-waves, series tuning is necessary. For all-band operation, it is thus necessary that the tuner condenser can be placed either in parallel, or series with, the coil.

It will be noted that parallel tuning can be used with anything up to one quarter-wave; that is, with very short feeders. Approximate quarterwave lengths for $160 \mathrm{~m}, 80 \mathrm{~m}, 40 \mathrm{~m}$ and 20 m are $132 \mathrm{ft}, 66 \mathrm{ft}, 33 \mathrm{ft}$ and 16 ft . Some typical top and feeder lengths, with the tuning to be expected, are given in Table I

| Top | Feeder | TABLE I Frequency | Tuning |
| :---: | :---: | :---: | :---: |
| 66 ft | 66 ft | 7 and $21 \mathrm{Mc} / \mathrm{s}$ | Series |
|  |  | 3.5, 44 and $28 \mathrm{M} / \mathrm{cs}$ | Parallel |
| $677 t$ | 42 ft | $3.5 \mathrm{Mc} / \mathrm{s}$ | Series |
|  |  | 7 and 28Mc/s | Parallel |
| 134 ft | 70ft | 3.5, 7, 14 and 28Mc/s | Parallal |

The top is the total overall length. Except when the aerial is very high, or a long way from the receiver or transmitter, the feeder will often be shorter than the examples.
A suitable aerial for reception can be an aerial with a 66 ft top (A and D each 33 ft ) and a feeder of any length. The type of open feeder described may, if desired, be replaced by $300 \Omega$ twin flat ribbon. This is slightly less efficient than the $600 \Omega$ open-wire line, but the losses are not particularly great if the feeder from flat top to receiver is not too long.

If it is desired to find out the particular top and feeder lengths for special bands, this can be found


Fig. 3.-Series tuning of the feeder.
Fig. 4.-Parallel tuning of the feeder.

directly in feet, for a half-wave, from:468
frequency in $\mathrm{Mc} / \mathrm{s}$
It will have been seen that the tuning varies from band to band. When the system of tuning for a band has been found, it should be noted down, so that it can be returned to at once, when necessary.

## Feeder Tuning

Circuits for this purpose are shown in Fig. 3. At "a" one variable condenser has been included in each feeder. In practice, one condenser is sufficient, if near the coil, and this can be included as at " $b$ ". In both "a" and " $b$ " a coupling loop is taken to the dipole input of the receiver. When the receiver has no dipole input, but only a single aerial terminal, the coupling loop is connected to aerial terminal and earth, as at "c".

For parallel tuning, the condenser is placed across the coil, as shown at "a" in Fig. 4. Either of the receiver coupling methods shown in Fig. 3 may be used.
When the aerial is used fo transmitting, it may be necessary to tap the feeders in an equal number of turns from each end, as at " $b$ " in Fig. 4, to secure proper loading. In some cases where the impedance is improved by this, tapping in the feeders can also give improved reception.
(Continued on page 533)

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(Continued from page 530)
With parallel tuning, the effect of taking an earth connection to a centre-tap on the coil can be tried, as this can further reduce static interference. A suitable tuning coil is shown in Fig. 5. If this is wound with 20 s.w.g. or similar wire on a ceramic former, it will do for both receiving and transmitting purposes. When the aerial is to be used for receiving only, the ribbed former is still convenient. as clips can easily be attached to the coil turns. There is, however, no need that the coil be of the dimensions given, provided it has a number of turns which allow it to be tuned to resonance on the bands required. Tinned copper wire will allow easy tapping, and tags or leads can be soldered on when the tapping points are found. Adjoining turns must not be shorted.

The loop consists of 2 or 3 turns of well insulated wire wound round the centre of the coil. The number of turns has to be a compromise for all bands, and more turns may well be used if the higher frequency bands are not of much interest.
For receiving purposes, almost any air-spaced tuning condenser will be satisfactory. A value of about 200 pF will generally be convenient. Smaller condensers may be used, but it will be necessary


Fig. 5.-Details of the tuning coil for the feeder.

Fig. 6.-Transposing the feeder to reduce the effects of interference.

to move tappings on the coil more frequently. A receiver type condenser will be suitable. For transmitting, a condenser with wide spacing may be required, except for low power.

If the feeder is taken to terminals equipped with short lengths of flex, and clips, this will allow easy adjustment. The condenser may also have flexible leads and clips, so that it can be placed in series or parallel with the coil, as required, and to permit changing the number of turns.

## Tuning Method

If the receiver has a signal strength meter, the tuning condenser is simply rotated to obtain best signal strength on the required band. The correct tuning point should show an improvement of several times in signal strength, but is not very critical as the circuit tunes flatly. If the condenser cannot be adjusted to give a definite peak in results, the number of turns in circuit may need adjusting. If results improve with the condenser fully open, too many turns are in use. On the other hand, if results are improved when the condenser is fully closed, more turns are required in circuit.

Once tapping points, method of tuning, and tuning condenser settings have been noted, they can he returned to easily.

When the receiver has no tuning meter or indicator, weak transmissions should be tuned in, and the aerial tuner adjusted for best results. Settings should then be noted, for future reference.

For transmitting purposes, the aerial can be tuned up roughly on the receiver, by noting the signal strength meter. The loop can be coupled by a short length of coaxial cable to the $\pi$-output of a transmitter, the coaxial sheath and one end of the loop being earthed as at " C " in Fig. 3. Meters may be included in one or both feeders, to show feeder current. Current will be fairly large for series tuning (low impedance), and fairly small with parallel tuning (high impedance).

## Transposed Line

When the aerial is used for receiving, the line may be transposed, as in Fig. 6, as a further aid to reducing interference. For reception in such circumstances, there is no need for the spacers to be so long, and the feeder leads can thus be closer together. The wires cross at each transposition block. The blocks may be cut from perspex or other insulating materials. To avoid contact between the leads where they cross, one lead can be each side of the block.

Local interference is less likely to cause trouble with a transposed feeder, because the interference strength will be more nearly equal in each wire, and will thus cancel out better at the ends of the feeder. The aerial may be used untuned by taking its feeders directly to a receiver dipole input, or by omitting the tuning condenser, so that the coil merely acts as a coupler.

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# Short-wave Listeners' Log 

IIOST Dx reception of amateur stations is usually on the 20 m and 15 m bands, these bands being from $14.00 \mathrm{Mc} / \mathrm{s}$ to $14.35 \mathrm{Mc} / \mathrm{s}$ and $21.00 \mathrm{Mc} / \mathrm{s}$ to $21.45 \mathrm{Mc} / \mathrm{s}$ respectively. Circumstances may make it difficult for some S.W. listeners to erect an extremely efficient or high aerial. Fortunately, however, a half-wave aerial for either the 20 m or 15 m band does not have to be particularly long. The actual lengths are 33 ft for the 20 m band, and 22 ft for the 15 m band. In very many cases it should be possible to erect an aerial of this length.
Tests with a simple dipole of this kind show that it can give excellent reception. Good results are obtainable even if the aerial is not at all high. A few listening periods with such an aerial, at a height of about 12 ft to 15 ft above ground, enabled many Amateur stations to be logged.

For a centre-fed dipole, the length of aerial wire mentioned is cut in half, a few inches extra being allowed to attach to the insulators. A low impedance feeder of any length is then taken from the centre. This feeder may be of $75 \Omega$ twin
flat lead, or of twin twisted flex, or may be a co-axial cable. In the case of the 15 m aerial, for example, the aerial itself would have two sections, each 11 ft long, with the feeder descending from the centre, so that the whole resembles the letter "T".

## Confined Spaces

If space is limited, it is in order to turn down vertically a few feet at each end, to accommodate the correct length. It is interesting to note, in this, that the HP9 station (Panama) was heard on two days at very good strength. As a transmitter was available, this station was called, and when describing his equipment he said that space was so limited that he was using a 20 m indoor dipole, with both ends turned down in the way explained.

1t is not necessary that the dipole top should be horizontal, so supports of unequal height may be used. The slope does, however, change the directive pattern. This is not usually of much importance, unless the best possible reception is wanted from one area, or unless experiments are to be made with directivity.

## How to Keep Radio Equipment Cool

## (Continued from page 503)

it may be difficult to make the heating-up period take less than an hour, and quite often the apparatus may be in use for a shorter time, so it is desirable that it should have a stable performance as independent of temperature changes as possible.

## Curve

The heating-up curve is easily plotted if an accurate mercury thermometer is inserted to measure the air temperature inside the case, an inch or two from the top. The thermometer can be inserted through a hole with a rubber grommet for protection. If it is of the total immersion type, the stem can be covered to avoid cooling of the projecting part of the thermometer. The thermometer must of course have a sufficient range, e.g., up to $240^{\circ} \mathrm{F}$, to ensure that it will read up to the maximum temperature reached without breaking. Over the first part of the curve, readings can be taken at intervals of five minutes. After half an hour, less frequent readings would suffice. All that is really important, however, is to check that a steady and not excessive temperature is reached in a reasonable time. If $140^{\circ} \mathrm{F}$ is exceeded, the test should be discontinued before any damage to components can occur, and the ventilation arrangements will require improvement.
This was well-illustrated by a small home-made oscilloscope contained in an aluminium case measuring $8 \frac{1}{\mathrm{~h}} \mathrm{in}$. $\times 7 \mathrm{in}$. x 9 in . The case had not been painted black, and this was an additional factor in retaining the heat, as unpainted alumin-
ium will not radiate heat so well. Reliance was placed on convection via 24 small louvres pressed in the sides. These provided apertures only tin. wide, and the total area of the openings was only 5 sq in. The louvres proved to be ornamental rather than efficient.

## 65W Dissipation

The oscilloscope contained seven valves and a cathơde ray tube, and there was a total dissipation of 65 W inside the cabinet. The heating-up curve (A) shows no sign of a steady temperature being reached even after two hours (see Fig. 1 on page 503). It was obvious that worked for long periods under these conditions, the oscilloscope would soon break down, and the only way to avoid this was to provide larger apertures. Experiments however were first made in separating the top and bottom of the case from the sides by $\frac{1}{2}$ in. spacers, but such a small gap had a quite negligible effect, and the original louvres had to be replaced by rectangular openings measuring $1 \frac{7}{8} \mathrm{in} . \mathrm{x} 1 \frac{1}{8} \mathrm{in}$., covered with expanded aluminium material of the type used for loudspeaker grilleswhich reduced the effective area of the openings by about $50 \%$ (see the illustration on page 503).

Six of these openings were made in each side, and two at the back of the case, giving a total estimated area of aperture of roughly 25 sq in ., or about five times the previous amount.
The ventilation now proved to be reasonably effective (Curve $\mathbf{B}$ ) and the final working temperature did not quite reach $130^{\circ} \mathrm{F}$ in a room temperature of $60^{\circ} \mathrm{F}$.


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$2 \frac{1}{2}$ in. square Rola C25 ....................26/10 2 $\frac{1}{2}$ in. square EMI ...18/6 4in. square Elac 5 in . round Plessey with O.P.T. ......1616 $6 \frac{1}{2}$ in. round Celestion ..................... 1716
8in. round Richard Allen ................ 1816 Oin. round Elac ...25112 in . round Plessey 2916 6in. x 4in. Plessey ... 1916 $7 \mathrm{in} . x 4 \mathrm{in}$. Plessey ... 1916 $8 \mathrm{in} . \times 4 \mathrm{in}$. Celestion and Richard Allen 19/11
IOin, x in . Celes=
tion and Plessey $21 / 6$

## LOUDSPEAKER

 CABINETSType suitable for an
8in. unit .........21/-
Type suitable for a
1Oin, unit ......... $25 / 6$
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$7 \times 4$ in. unit $\ldots . . .17 / 6$

## CRYSTAL

CALIBRATOR No. 10 Crystal controlled. Directly calibrated. Functions: Crystal, controlled oscillator providing fixed frequency signals of $500 \mathrm{kc} / \mathrm{s}$ and all harmonics of $500 \mathrm{kc} / \mathrm{s}$ up to $30 \mathrm{mc} / \mathrm{s}$ variable oscillator from $250 \mathrm{kc} / \mathrm{s}$ to $500 \mathrm{kc} / \mathrm{s}$ rom enabling all intermediate irequencies between 250 $\mathrm{ke} / \mathrm{s}$ to $500 \mathrm{k} / \mathrm{s}$ to be produced and modulated. Complete in carrying case/bag with all valves, leads and inwith all valves, leads and in-
struction book. $£ 4.10 .0$ ea.

## MICROPHONES

$\star$ Acos Mic., 3911. Crystal stick microphone for use as a hand, desk or floor stand unit. Listed at 3 gns. OUR PRICE 37/6. Table Stand 716 extra. Floor stand adaptor, $12^{\prime 6}$ extra.

* Acos Mic. 40, as supplied with modern tape recorders with a folding rest and 8 ft . lead. Listed at $£ 1.15$.0. OUR PRICE 1916.
* GBS Microphone, pencil stick type fitted with muting switch, 42'.
$\star$
T.S.L. Crystal "Stick" Microphone, Model MX3, for general purpose use, complete with table stand, 45\%.
$\star$ T.S.L. Moving Coil Mierophone, for high or low impedance. Brown and cream plastic case with a fold-in table rest, 6 ft . cable and a standard 3-way connecting Continental plug, £4.4.0.
$\star$ Acos Mic. 45, dual purpose, designed to fit into the hand, has built-in stand for desk use, die-cast case for a variety of applications from music to dictation, with lead, 25'-each.


## CAR RADIO KIT

Can be built absolutely complete for $£ 11.19 .6$. (Post 3/6).
$\star$ Small size. Will fit any car. $t 12$ volt Operation. $\star$ New Hybrid circuit. \& Transistor output. * New Type Brimar valves. tor output. $t, 12$ volt H.T. and L.T. $*$ T.C.C. © No Vibrator, 12 volt H.T. and L.T. \& T.C.C. R.F. scage. $t$ Medium and long waves. $\star$ Permeability tuning. $\star 7 \times 4 \mathrm{in}$. elliptical speaker.
Instruction Bookler giving full details, illustrations, dimensions, circuit diagram and shopping list, $2 / 6$.

## SPECIAL OFFERS

 $12 \times 6$ in., $2^{\prime}-; \quad 12 \times 12 \mathrm{in}$. Set of Mullard Transistors, compris-
ing 1 OC44, 2 OC45, 1 OC8ID, $20 \mathrm{CB1}$
. $37 / 6$ set
Special Purchase, ex-Government 319 each

TELEFUNKEN, STEREO HIGH FIDELITY AMPLIFIER
Five watts total outpur ( $2 \frac{1}{2}$ watts each channel), size 12 in . wide $x 9 \mathrm{in}$. deep 2 in . high, weight 9 lbs . Hammered enamel finish in green/grey with gold trim, control and press buttons in cream with black, blue and red lettering. Provision made to feel the amplifier from radio, tape recorder, FM tuner, etc. Listed at \& 16.16.0.
Special Alpha Offer.
E12.12.0

## CATALOGUE

OUR 1962 CATALOGUE IS NOW AVAILABLE. PLEASE SEND I/IN STAMPS FOR YOUR COPY. TRADE CATALOGUE ALSO AVAILABLE. FOR WHICHPLEASE ATTACH YOUR BUSINESS LETTER HEADING.

[^2]
# THE WORD MAXI-Q OF DENCO (CLACTON) LIMITED IT IS ALSO A GUARANTEE OF WORKMANSHIP \& TECHNICAL PERFORMANCE 

OUR RANGE OF PRODUCTS IS SO GREAT THAT WE NOW HAVE TO REQUEST THE AMOUNT OFI/4d. FOR OUR GENERAL CATALOGUE AND TO SAVE YOU POSTAL ORDER POUNDAGE CHARGE WE REQUEST SEND 1/4d. IN STAMPS.


## MODULATED TEST OSCILLATOR MTO. I

$\star$ Provides a modulated signal suitable for t.F. alignment, also trimming and tracking R.F. sircuits.

* Frequency is continuously variable from $170-475 \mathrm{ke} / \mathrm{s}$ and $550-1,600 \mathrm{ke} / \mathrm{s}$.
* Suitable for the alignment of transistor receivers.
* Operates from a single 9-volt grid-bias battery (not supplied) which is housed within the unit.
* The case is manufactured from steel and is finished in silver hammer. The front panel is gloss black bearing white lettering. Dimensions are $5 \mathrm{I} / \dot{\mathrm{l}} \mathrm{in} . \times$ $4 \mathrm{l} / 16 \mathrm{in} . \times 3 \mathrm{in}$.
* Supplied with full operating instructions.


## PRICE E3/I716

PLEASE SEND S.A.E. WITH ALL ENQUIRIES

## DENCO (CLACTON) LTD.

(DEPT. P.W.)
357/9 OLDROAD, CLACTON-ON-SEA, ESSEX
STOP PRESS:
MULLARD "TWIN THREE-THREE" STEREO AMPLIFIER. Punched Aluminium Chassis and Hammered Gold printed Front Panel, 25/9d.


## REPORTS OF CURRENT ACTIVITIES

## amatedr radio mobile society

Hon. Sec.: G3FPK, 79 Murchison Road, London E. 10.
At the Longleat Mobile Rally many A.R.M.S. members were present to enjoy the many attractions of this event. held in this local beauty spot. There were five notable rallies during August; the Derby Mobile Rally and Hamfest, held as part of this Society's Gulden Jubilee Year celebrations; the Hetton Show and Mobile Rally, which included show iumping in its attractions; the Stamford Rally Fest; the Luton Mobile Rally and the South Manchester and Stockport Amateur Radio Rally, the main event of which, was a navigation and mobile contest.

Future Events:
September 10th-National Mobile Rally.
September 17th—Lincoln Hamfest and Mobile Rally.

## BLACKWOOD AMATEUR RADIO SOCIETY

Hon. Sec.: P. M. Fulton, GW3MMU, 36 Sunnybank Road, Blackwood, Monmouthshire. Wales.
For the past three months members have been helping to transform an old cottage into new headquarters for the society. Both inside and outside the cottage have been subjected to alterations and it is hoped that it will be officially opened quite soon. New members are still wanted urgently.

## BURSLEM AMATEUR RADIO CLUB

Hon. Sec.: W. Luscott, 36 Rothsay Avenue, Sneyd Green, Hanley, Stoke-on-Trent.
Meetings are held at Burslem Town Hall on the third Wednesday of each month and start at 7.30 p.m. A morse class is included at each meeting.

A series of lectures and demonstrations have been planned for the winter months-commencing in September. New members are always welcome.
DUDLEY AMATEUR RADIO CLUB
Hon. Sec.: D. H. W. Pratt, G3MHS, 23 Kent Street, Upper Gornal, Dudley, Worcestershire.
This newly formed club held its first general meeting on the 18th August. Until a headquarters can be found all meetings will be held at 23 Kent Street, Upper Gornal, Dudley, Worcestershire.
GUILDFORD AND DISTRICT RADIO SOCIETY
Hon. Sec.: J. R. Barker, 35 Banders Rise, Merrow, Guildford, Surrey.

The July meeting was designed to give younger members experience in setting up a portable station. On the 28th July, Ken Orford gave a talk on "Propagation-Past, Present and Future."

Future Event:
October 1st-A Car Treasure Hunt.

## LEEDS AMATEUR RADIO SOCIETY

Hon. Sec.: D. Dinsdale, 69 Spen Lane, Leeds 16, Yorkshire.
This society will soon begin a new programme of activities, starting on September 20th with an informal exhibition of members' equipment.

## Future Events:

September 27th-Demonstration of 4 m equipment.
October 4 th-Spares Sale.
MITCHAM AND DISTRICT RADIO SOCIETY
Hon. Sec.: M. Pharaoh, G3LCH 1 Madeira Road. Mitcham. G3NFA/P was at Hindhead during the 2-metre field day and made quite a good score. The number of contacts made by G3NFA (assisted by G3LSP and G3LCH) was 195 with severa! contacts with stations other than English. G3LAR, who was operating from the Norfold area during the contest, made about 72 contacts.
NEWBURY AND DISTRICT AMATEUR RADIO SOCIETY
Hon. Sec: G. T. Allen, G3JTK, 83 Huntsmoor Road, Tadley, Hampshire.
At the August meeting, members brought/items of test equipment etc., to the headquarters and explained their various uses. Future Events:
Feptember 29th-"On understanding radio"; a short talk by G3LLK.

October 1 st-The Southern Regional Meeting.
October 27th-Constructional Competition.

## NORTHERN HEIGHTS AMATEUR RADIO SOCIETY

Hon. Sec.: A. Robinson, G3MDW, Candy Cabin, Ogden, Halifax,
Yorkshire.
Recent activities have included a talk by G2SU on his " 50 Years of Radio," and a visit to a local television factory. The subject of the meeting on September 6th was Radio Astronomy. Future Event:
September 20th-An informal meeting.

## PETERBOROUGH RADIO SOCIETY

Hon. Sec.: D. Byrne, G3KPO, Jersey House, Eye, Peterborough.
A barbecue has been planned for September 10th at the Society's riverside site at Alwalton. Autumn and winter meetings will be held at the Peterborough Technical College at 7.15 p.m. on the first Friday in each month.

Future Events:
October 6th-"Aerials".
November 3rd-The Arinual General Meeting.
READING AMATEUR RADIO CLUB
Hon. Sec.: R. G. Nash, G3EJA, 9 Holybrook Road, Reading, Berkshire.
From August 25 th, Friday evenings have been taken up by slow morse classes given by G5XB or G6WO, starting at $70^{\circ}$ clock. On August 25th D. Keable discussed the method of aligning superhet receivers.

Future Event:
September 30 th-G5TP will demonstrate and discuss the G2DAF SSB transmitter.
SLADE RADIO SOCIETY
Hon. Sec.: C. N. Smart, 110 Woolmore Road, Erdington, Birmingham 23.
On August 25 th members visited an electrical control manufacturer's factory for a demonstration of automatic control equipment.

Thursday evening meetings include informal discussions, operation of the club transmitter, and instruction in morse. Slow morse transmissions are radiated each Monday evening from G3AYJ on $1.9 \mathrm{Mc} / \mathrm{s}$ from $8 \mathrm{p} . \mathrm{m}$. to $8.30 \mathrm{p} . \mathrm{m}$.

Future Events:
September 8th-Exhibition of members ${ }^{2}$ equipment.
September 16th-Annual dinner.
September 22nd-A lecture called "How far can radio waves be heard?"
WANSTEAD, WOODFORD AND DISTRICT RADIO CLUB
Hon. Sec.: J. R. Seaman, 67 Beattyville Gardens, Ilford, Essex.
During August the club held its field-day. Members operated on $1.8,14$ and $144 \mathrm{Mc} / \mathrm{s}$ for most of the time.
Members for the junior section is continuing to grow.

## COURSES OF INSTRUCTION

## BATTERSEA MEN'S INSTITUTE

Latchmere Road, Lavender Hilt, Battersea, London S.W.11. The radio course, in preparation for the City and Guilds Examination in May 1962. has been extended, and now takes place on Monday and Thursday evenings, from 7.30 to 9.30 p.m., at the Spencer Park School, Trinity Road, London S.W.11. The course covers the entire syllabus of the examination and no prior knowledge of radio is required.

There are also two classes-beginners and advanced-in general radio and television at the Battersea Institute.

Classes commence on the 25th September and the schools will be open for enrolment during the week 18th to 22nd September. Fees: one class $£ 10 \mathrm{~s}$. 0 d ., two classes $£ 12 \mathrm{~s}$. 6 d .

## ILFORD LITERARY INSTITUTE

High School for Girls, Cranbrook Road, Ilford.
Classes for the eight month RAE course will be held on Wednesdays at 7.15 to $9.15 \mathrm{p} . \mathrm{m}$. Classes of the six month morse course will be held on Mondays from 7.30 to 9.30 p.m.

Fees lor those living in the Essex County Council area are; 30 s . for the RAE course and 20 s . for the morse course.

Classes commence September 18th.
Those interested should apply to, Mr. C. H. L. Edwards, 28 Morgan Crescent, Theydon Bois, Epping, Essex.
STREATHAM AND TOOTING L.C.C. INSTITUTE
J. Caley, 6 Farnan Road, Streatham, London S.W. 16.

Radio and television classes at Dunraven, Penwortham and Hillcroft schools will be held on Mondays, Wednesdays and Fridays at 7.30 p.m.

For the benefit of new students instruction will be given on basic principles assisted by practical demonstration, and test equipment.

Classes commence on September 25th.
WEMBLEY EVENING INSTITUTE
99 Watford Road, Wembley, Middlesex.
Radio Amateur's Examination classes will be held on Mondays at the Wembley Evening Institute, Copland School, High Road, Wembley. Morse practice will be held from 7 to 8 p.m., and radio theory from 8 to 10 p.m. Persons wishing to enrol may do so from 11th September to 14th September, and classes start tho following week.

The Editor does not necessarily agree with the opinions expressed by his correspondents.


#### Abstract

Whilst we are always pleased to assist readers with their technical difficulties, we regret that we are unable to supply diagrams or provide instructions for modifying commercial or surplus equipment. We cannot supply alternative details for receivers described in these pages. WE CANNOT UNDEATAKE TTO ANSWER QUURRIES OVER THETELELE PHONE. If a postal reply is required a stamped and addressed envelope must be enclosed with the coupon from page dii of the cover.


## YOUNG ENTHUSIASTS

SIR,-I made my first radio (a crystal set) when I was $12 \frac{1}{2}$. Since then I have made a transistor set and a few one-valve receivers (some of the designs were taken from issues of P.W. dated 1930 to 1940). I also made a moise oscillator.

I would be pleased if anyone could supply information about a station received on Sunday, 23 rd July, at $10.15 \mathrm{p} . \mathrm{m}$. The transmissions were repeated alternately in English and Italian and as far as I could make out were as follows: "This is Rome Radio, Maritime Radio Telephone Service. This is a test transmission for receiver ..." I could not ascertain the wavelength but it was on the lower part of the S.W. band. - D. Hill (Edinburgh).

## LIGHT PROGRAMME AMPLIFIER

S IR.-I read with interest Mr. Joyce's letter in the August issue, concerning reception of the Light Programme on his amplifier without a tuner. This occurrence is common among audio amplifiers and is caused by rectification taking place in one of the circuits. Most probably the input wires to the amplifier form a tuned circuit which resonates at one of the Light Programme frequencies. Rectification in the amplifier is of ten caused by a grid bias resistor " going high", making the valve operate nearly at cut off, thereby producing anode bend rectification.

Mr. Joyce could, with advantage, connect a tuning capacitor across the input te minals to his amplifier, thus enabling another station to be runed in.-S. H. Nankivell (New Mills, Derbyshire).

## PHONETIC ALPHABET

SIR,-I thoroughly agree with Mr. P. A. Ellis's plea (August) for an official phonetic alphabet. The situation is made worse by those gentlemen who use geographical names in their transmissions, so that one is likely to hear something like: "Glasgow, Fife, Cardiff ".

The I.C.A.O. alphabet is not ideal, but if everyone used this there would at least be some uni-formity.-F. Dorman Byers (London, S.E.19).

## LIGHT PROGRAMME VOLUME

SIR,-I have noliced. while listening to the Light Programme on medium waves. that a marked increase in volume occurred immediately the television receiver was switched on in the next room. The two aerial systems are quite independent and
the mains supply for one is from a power point, while the other is connected to the lighting circuit.

The receiver is a conventional four-valve TRF. I wonder if any reader can explain this occurrence? -T. F. Wall (Preston).

## CORRESPONDENTS WANTED

$S^{I R},-I$ would very much like to correspond with anyone interested in Short-wave reception, transmitting and radio construction in zeneral. I will answer all letters received.-R. Chipperfield (4 Bayston Road, Stoke Newington, London N.16).

## TRANSISTOR RESULTS

SIR,-I have built a number of transistor receivers over the past year or so and have been very intrigued with the ferrite type of aerials. So far 1 have not seen a single article, either in your magazine or in any other, which gives characteristics or calculations for such an aerial. In examining some commercial sets I find that there are single rods, flat slabs and, in some cases. two or three rods bound together. I have experimented with these types of aerial and cannot find any basis upon which I could draw up my own data. Using the sane winding. placed upon slabs and doubled-up rods, the performance is distinctly different, and I was unable to find the optimum arrangement; single wires, Litz, silk and cotton covered, of all gauges seeming to give quite unrelated results. I do not own any reliable test apparatus, so 1 could not make quantitative measurements, but 1 should like to sce some definite data, preferably issued by one of the better firms, on this important aspect of the modern portable receiver.-G. HUTCHEON (Derby).

## TRANSMITTER LICENCES

$S^{I R},-$ Recent correspondence in your magazine about the possibility of a novice licence, brings to mind my own wish of a couple of years ago, when I was all for such a scheme. Now, however, after passing the RAE and the GPO morse test, I realise that such a licence would do more harm than good, particularly as it is evidently those pcople who do not have the necessary knowledge to pass the examinations who want low-power transmitter licences.
I do not consider it so difficult to learn what is required for the RAE and to learn the C.W. code. -C. R. Morley (Reigate).

## CORRECTION

Will readers please note that the advertisement for Messis. Stern Radio Ltd., in both issues dated August and Scptember, for the "special offer of tape " should have read 1.200 ft on 7 in . Spool 21/-. 1.800 ft on 7 in . Spool 32/6, and not vice-versa as printed.

## BUILD A BETTER RECORDER

 track models Here are professionally designed Kit 'A' (4TR) amplifiers mounted on printed circuit amp. for Monarboards complete with transformers deck. 9 gns. and valves for building with Collaro or BSR Decks. Everything included down to the last piece of measured wire. Available as separate amplifier or with cases, speakers and decks. When built you will possess an. instrument of high professional standard at truly popular prices.

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WITH A
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I55 HIGH ST., BRENTFORD, M'SEX.

## Become a Television expert this easy way

The Bennett College offers you a complete course

THE Bennett College offers you personal tuition in a course that's non-mathematical and particularly easy to follow. It contains clear diagrams which cover everything you want to know from beginning to end (and even includes the basic principles of sound radio if you wish).

The complete home-study course covers everything: Production of the signal, scanning and reproduction of picture from signals. Aerials, types and purpose. The cathode-ray tube. Time-base oscillators, and output circuits. Synchronisation. Video frequency amplifiers. The TV tuner, turret incremental, etc. Television test gear. Television faults.

For more details, please fill in the coupon below. Your studies cost very little and the book you need is included in the cost.


## IN THE HOME, IN THE CAR, BY THE SEA, IN FIELDS AFAR <br> THE CONTESSA <br> IS VOTED BEST OF ALL <br> A really remarkable <br> 2 BAND 6 TRANSISTOR SUPERHET KIT

(As displayed at the Radio Hobbies Exhibition)

The CONTESSA is the professional looking set with the professional performance.

Study these brilliant features which cannot be found in any other kit....

- Waveband Coverage of $530 \mathrm{k} / \mathrm{cs}$ to $1620 \mathrm{k} / \mathrm{cs}$ and $160 \mathrm{k} / \mathrm{cs}$ to $270 \mathrm{k} / \mathrm{cs}$.
- Assured reception of at least a dozen stations in daylight!
- Large clearly-calibrated station-named dial.

Internal high-gain Ferrox Aerial.
5.1 ratio slow motion tuning.

Fitted with the latest 12000 line high-fux loudspeaker.

- Power of 410 milliwatts from the single-ended push pull final stage.
- Specially designed aerial matching coil for use in a CAR.
- Only first grade fully guaranteed Mazda matched transistors and diodes are used. Double tuned IF transformers for maximum gain and knife-edged selectivity.
Fully drilled printed circuit panel marked with component numbers.
- The two colour case measures $10 \times 7 \frac{1}{2} \times 3 \frac{1}{2}$ in. and weighs approx. 4 lbs .
- Battery lasts 4 months with normal usage. Book supplied with detailed assembly instructions, diagrams and circuitry.
- Anyone can build this set-everything supplied just a soldering iron required.

> Inclusive price for all associated components,
> cabinet and battery, complete in every detail.
> Or our BUY AS YOU $3 / 6$ Regd. P.P. separately. Send for BUILD SCHEME any parts sold and parts list, $3 / 6$ post free.

## See and hear a working model at:RADIO CLEARANCE LTD. <br> 27 Tottenham Court Road, London W.I Telephone: Museum 9188

## RECEIVERS \& COMPONENTS

"HEATHKITS" can now be seen in London and purchased on easy terms. Free brochure. DIRECT TV REPIACEMENTS LTD., Dept. PW/7/9, 138 Lewhisham Way, S.E.14. Tideway 6666.

COMPONENTS, VALYES, Tubes. etc. Write or phone for free llst. ARION TELEVISTON, 4 Maxted Road Peckham, S.E. 15 (New X 7152).

SPEAKER REPAIRS. Cones/Ftelds fitted. Clock Coils wound. L. S. REPAIIRS, Pluckles, Ashford, Kent.

## "WEYRAD" TRANSISTOR RECEIVER

LONG a MEDIUM WAVE, P.P. ABLE TOTAL COST £8.5.6.
CONSTRUCTOR'G BOOKLET 2/CABINET TO SUIT 17/6.
TRANSISTOR AM FEEDER UNIT Size $4 t \times 3 \times 1 \mathrm{Hn}$. TOTAL COST OF COMPONENTS £4.10.0
CONSTRUCTOR'S BOOKLET, $1 / 9$.
Send S.A.E. for Shopplng Lists.
35 OHM ALLLAN SPEAKLRS, 2\%/1.
JACKSON " 00 " GANG (with Trim-
mers), 10/6.

## WESTHAM RADIO SUPPLIES Rear of 176 Abbotsbury Road WEYMOUTH, DORSET

KiTS BUILT, tested, supplled. S.A.E. details: - J.A.K. 6 Hooker Road Heartsease, Norwich. NFK NOR 25 .

SPEAKERS BRAND NEW 2in. 75 ohms 18/6, 3 in. 25 ohms 20/6, 5la. 35 ohms $22 / \%$ OC81D, OC81 mat pr 30/-, Diodes $1 /-$ min cap. $2 / 3$ each, RMS 10/6, SM5 11/6. TAPE: Stand: 5 in. $850 \mathrm{ft} 16 / 6$, 7in. $1.200 \mathrm{ft} 20 / \mathrm{F}$ 710 L.P. 1, 800ft 25/6. Postage pald by CHAPPLE RADIO, 107 Neasdea Lane, N.W. 10 .

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## CAPACITORS

$32 \mu F, 500$ v. $1 \frac{1}{2} \mathrm{in}$. diam., 4ivin. long, 3l-. $8 \mu \mathrm{~F}, 500 \mathrm{v}$. lin. diam., $4 \frac{1}{2} \mathrm{in}$. long, $1 / 9$.
WIRE ENDED PAPER CAPACITORS
$.1 \mu \mathrm{~F}, 400 \mathrm{v}$. Moulded, $\frac{3}{6} \times \frac{3}{4} \times$ l $\frac{3}{8}$ in., 4 for $2 \%$. $.02 \mu \mathrm{~F}, 800 \mathrm{y}$. Moulded, $\frac{7}{\theta^{2}} \times \frac{3}{4} \times 12$ in., 4 for $2^{\prime}$.
 T.C.C. Metalmite .1, .05, .02, .01, .005, .002, $.001 \mu \mathrm{~F}, 350$ v., 4 for 2 /3. 2250 pF , 2.5 kv , Moulded Mica, $1 \frac{1}{4} \times 1 \frac{1}{4} \times \frac{5}{10}$ in., I/ $^{2}$.

RELAYS. 300 ohm, D.P. c/o, $\frac{7}{8} \times 1 \frac{1}{2} \times 1 \frac{1}{8}$ in., 4 ?-. $5 k$ ohms, 3 wate, W.W. Colvern pots, $\frac{1}{2} \mathrm{in}$. shaft, $\mathrm{I}^{1 / 3}$.

## TRANSISTORS

Red Spot, 313, Yellow/Red Spot, 41., OC71, S'., OC72, 616.

Precision W.W. Pots. 3k ohm. $\pm$
 and wiper (with silver slip ring), 2/6. C.O.D. or cash with order. Orders below 5/= post 9d extra.

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17 and 15 in . Types $\qquad$ E6.10.0
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Electrostatic 90 degree and 110 degree tubes 10/. extra. Carr. paid.

17in. BBC and STV Receivers ... $\mathbf{E 1 9 . 0 . 0}$ COMPLETELY OVERHAULED AND FITTED WITH PROCESSED TUBE STV and BBC |Ain. Receivers ... $\quad \mathbf{6 2 . 1 0 . 0}$ COMPLETE WITH VALVES AND TUBE. CALLERS ONLY. CARRIAGE EXTRA. OPEN SATURDAY AFTERNOONS

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6in. Bia. (yes-six inch) Miliamelers $0 / 1$ fi. round Ernest Turner 78/- (3/6). 2thn. Dia. Voltmeters $0 / 500$ A. round Weston 1000 ohms per volt. $47 / 6(2 / 6)$. Sperlal Vaives $4 / 250 \mathrm{~A}$ £8.10.0: QY3/125 £6.10.0: 4212 £4. Simuson Model 443 Volt-ohmeters 2 in . meter in case es.10.0 ( $5 /-$ - . Metai Rectifiers 24 v .12 A 20\%-(3/6).
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Whde Band Aerial Amplifiers. ten separate outiets from one aerlal rack mounting \&9.10.0. (7/6) Pocket thatioactive Dosemeters, quartz fibre fountain pen type 25/- (1/-), reduction for quantities, 5 Foot P.O. Riteks 19in. Wide drilled and tapped
65\%-(10/-). Elliott of volt moving coll Goitmeters 2000 ohms ver volt, $24 i n$ coil deal as basic meter 25/- $(2 / 6)$. Alains filter deal as basic meter 25/-(2/6). Arains Fiter Units. laboratory precision type totally ohms SPD'T Relays 12/6(1/6). Metal Recuitiers $24 \times 12 A$ 20/-(3/6). AVo Getger Couners 24 e9.12A 20/-(3/6). AVN Getiger CombTransmitter Cahinets, 191n. Wide $£ 5(20 /-)$. P.O. Racks 191n. wide. 3ft. high 82 (10/-). Metal Rectifiers 12 v . 2 amp $5 /-(1 / 6)$. 20 Font Super Liehtweight Aluminium Tripod self supporting 1 in . dia. Masts, complete 7 lbs. welght $£ 10.10 .0$ (30/-).

> We lave large quantities of "hils and pieces" we cambot lisi-and invile your enquirles-we pan broliblbly fiply-sevpry one allswered.

Amounts in brackets are carriare England and Wales,
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NEW AND Surplus Valves, fully guaranteed. S.A.E. for List. A.so Reclaimed Valves, perfect 5/. maximum. Genuine bargains, valves bought.-LEWIS, 46 Woodford Avenue, Ilford. Essex.

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## SPECIAL NOTE

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