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## COMPUTERIEED

## GRAPHIC

## CARAVAN PSU ELIECTRONIC DOORBIELL



```
BAKERS DOZEN PARCELS
All the parcels listed below are brand new component.
M,
    513 amp ring main unction boxes
    513 amp ring main spur boxes
    2513 mmp fuses for ring mains
    voltage (aing
    3 flush el
    reolace 1 or 2 way switches
    5infles line switches
    in flex line swliches with neon
    280 watt brass cased elements
    2 mains transformers with 6v 1a secondarles
    mains transtormers with 12v 1/2, sec ondaries
    5octal bases for relays or valves
    l}\begin{array}{l}{12\mathrm{ glass red switches }}\\{40CP}\\{70\mathrm{ photo transistor}}
    4 OCP 70 photo transistors
    25 assorred gemanium iransistors OC45 etc
    2 ulvra sonic transmitters and
    2 2 15000 míd computer grade electrollics
    2 light dependent resistors similar ORP12
    5 diff micro switches
    2 mains interference suppressors
    l
250 various screws and self tappers
    1 of each wafer switches - 6p 2 wav: 4p 3 wav: 2p 6 way:
    1p 12 way
    $ tape deck counters
    6 digit counter mains valtag
    1BOAC in flight stereo unit (second hand)
    Nicad battery chargers
    2 kev switch with k
    2 aerosol cans of ICI Dry Lubricant
    96 x 1 metre lengths colourcoded connecting wires
    4 battery operated model motors
    2 solid diaelecrric 2 gang tuning conden
    0 compression trimmers
    Long and Medium wave tuner kit
    4 × 465 KC IF transformers
    8 Rocker Switches }40\mathrm{ amp Mains SPST
    6 Rocker Swwithes 10 8mp Mains SPDT 
    4 Rocker Switches }10\mathrm{ amp DPDT
    24 hour time switch mains operated - \s.h.)
    $6 hour clockwork timeswitch
    2 6v operated reed switch relays
    20 neon valves - make good night l
    2\times12v DC or 24V AC 4CO relavs
    1\times12v 2C O verv sensitive relay
    1\times12v4CO relay
    2 mains operated relays 3 x 8 amp changeovers (secondhand)
    0 rows of 32 gold plated IC sockets (torat 320 sockets)
    1 locking mechanism with 2 kers
    5 Dolls' House switche
    2 telephone hand sets incorporating ear piece and mike (p)
    2 flat solenoids - ideal to make curreniece,
    territe rods 4" x 5/16" diameter aerials
    4200 earpieces
    I Mullard Thyristor trigg
    10 assorted knobs % spindles
    5 different mermostats, mainly bi-metal
    Magnetic brake - stops rota
    Heavy duty 4 pole contactor - 24v coil
    2 25 watt pots 8 ohm
    5 wire wound pots - 18,33,50, and 100 ohm
    1 $250 watt dimmer Ultra ref SE2.
    50 1/3 watt carbon film res istorst
    20-2 watt carbon resistors 10 values
    1 time reminder adjustable 1.60 mins
    l
    42a bridge rectifiers 400V
    2 10a bridge rectifiers 30V
    2 30a panel mounting sly dlok fuses
    4 porcelain fuse holders and fuses
    watt
    $ mains shaded pole motor 1/" stack
    25", ali fan blades fit %""shaft
    < 23" plastic fan blades fit %" shaft
    1 mains motor with gear bo }1\mathrm{ rev per 24 hours
    i mains motor with gear box with gear box 1 rev per per }12\mathrm{ hours
    2 mains motor with gear box }16\textrm{rpm
    4 fluorescent starters suit 4-80 w tubes
    411 pin moulded bases for relavs
    5 87G valve bases
    4 skirted B9A valve bases
    1 infra red fire element }1000\mathrm{ watts
    1 motorised stud switch (SH)
    5 assorted ferrite shapes
    3 ferrite magne is
    2%, hours delay switch
    6v mains power supply unit
    4/2v mains power supply unit
    5p\mathrm{ piliex plug and panel soc}
    1 12v vibrating reed bleepers
    5 spetker size radio cabinet with handle
    $ different multi way push switches
    10 stider type volume controls
    -2 musical boxes (less keys)
\12-1 heating pad 200 watts
14-1 1w amplifier Mullard 1172
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are by \(\%\) sockets and three panel mounting fuse holders provide thyristor protection. A four pin plug and socket facilitate ease of thyristor protection. A four pin plug and socket facilitate ease of
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Some of the features are. \(10 n g\) wave band \(115-170 \mathrm{KMz}\),
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connect to ampl fifer or headphones and details of suitable FM zerial (note ferrite rod aerial is included for medium and tong wave bands. All made up on very compact board

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12 volt MOTOR BY SMITHS 12 volt MOTe for use in cars, ere, these are very powerful and eassly reversible. Size
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We have very large stocks of motors from 2 watts \(101 / \mathrm{ho}\). Most at

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Refresh your home, office, shop, work room, etc. with
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3 Channel Sound to Light
Big Ear, listen through walt
Silentsentinel Ultra Sonic Transmitter and receiver
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Matchbox Radio - receives Medium Wave
40 watt amp - hifi \(20 \mathrm{hz}-20 \mathrm{kHz}\)
115 Watt Amplitier 5 Hz 25 kHz
Power supply for 115 watt amp

\section*{EVERYDAY} and computer PROJECTS


\section*{PROJECTS}
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Six channel musical effects box for performers
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Our July-1985 issue will be published on Friday, June 21.
See page 331 for details.

\section*{NEW THIS MONTH}

\section*{SENSING \& CONTROL PROJECTS FOR} TME BBC MICRO*
Have you evor wonderad what all those plugs and book assumes no previous electric knowledge and no soldering is required, bur guides the reader (pupit of teacher) from basic connexions of the user sockets, to quite complex projeccs. The author, an experi enced teacher in this fieid, has provided lots of practical experiments. with ideas on how to follow up the bassc principles. A complete kit of parts for all


\section*{GREENWELD \\ - The Pack People!}

K524 OPTO PACK - a variety of single point and seven segment LEDS (incl. dual types) of various colours and sizes, opto isolators, numicators, multi digit gas discharge displays, photo transistors, infra red emitters and receivers. 25 assorted \(£ 3.95\); 100 £14.95; \(250 £ 36\).
K525 PRESET PACK - Big, Big variety of types and sizes - submin. min and std. MP, slider, multiturn and cermets are all 20 R to 5 M . 100 range of values from £12.95; 1000 £48.
K526 HEATSINK PACK - Lots of different sizes and shapes of heatsink for most diode and transistor case styles. A pack of 25 assorted including several large finned types - total weight over 1 kg £5.50; 100 £ 19.50.
K528 ELECTROLYTIC PACK - All ready cropped for PCB mounting, this pack ofrers excellent value for money. Good \(0.47 \mu \mathrm{~F}\) to \(1000 \mu \mathrm{~F}\). 6 v to \(100 \mathrm{v} £ 3.95 ; 250\) 88.95; 1000 f32

K531 PRECISION RESISTOR PACK High quality, close tolerance R's with an extremely varied selection of values mostly \(1 / 4\) and \(1 / 2 w\) tolerances from \(0.1 \%\) o \(2 \%\) - ideal for meters, test gear etc 250 £3; \(1000 £ 10\).
K532 RELAYS - Wide selection of styies, voltages and contacts. \(4 \mathrm{v}-240 \mathrm{v}\) ACJOC, SP to 4PCO. 20 for £6; \(100 £ 25\) K517 TRANSISTOR PACK - 50 assorted ful spec marked plastic devices PNP NPN RF AF. Type numbers include BC114 117172182183198239251214 255320 BF 198255394 2N3904 etc. etc. Retail cost \(\mathbf{£ 7 +}\); Special low price 275p.
K523 RESISTOR PACK - 1000 - ves \(0001 / 4\) and \(1 / 2\) watt \(5 \%\) hi-stab carbon PCB mounting. Enormous range of pre PCB mounting. Enormous range of pre ferred values from a few ohms to a
several megohms. Only 250p; 5000 several megohm

K520 SWITCH PACK - 20 different as sorted switches - rocker, slide, push, rotary, toggle, micro etc. Amazing value at only 200p.
K522 COPPER CLAD BOARD - AI pieces too small for our etching kits Mostly double-sized fibreglass 250 g (approx 110 sq . ins.). For 100p.
K530 100 ASSORTED POLYESTER CAPS - All new modern components, radiat and axial leads. All values from 0.01 to 1 uf at voltages from 63 to 1000 !! Super value at \(£ 3.95\).
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W4700 PUSH BUTTON BANKS - An assortment of latching and independent switches on banks from 2 to 7 way, DPCC to 6PCO. A total of at least 40 switches for \(£ 2.95 ; 100 \mathrm{£6.50;} 250\) £14.00.

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\section*{TORUS"}

Computer-controlled Robot built around he gearbox described below. Complete kin of parts inc PCB, program listings for BBC cable (min 3 m recommended -5 m better) \(\mathbf{~} 1.30 / \mathrm{m}\). SAE for illustrated leaflet.


\section*{MOTORIZED GEARBOX}

The unit has \(2 \times 3 V\) motors, linked by a magnetic clutch, thus enabling turning of the black ABS housing reducing the final drive speed to approx 50 rpm . Data is supplied with the unit showing various options on driving the motors.
Two new types of wheels can be supplied the aluminium discs and smaller plastic wheels are now sold out). Type A has spokes with a round black tyre and is 100 mm dia. Type B is a solid heaw duty wheel 107 mm dia with a flat rigid tyre 17 mm wide.
PRICES: Gearbox with data sheets: \(\mathbf{E 5 . 9 5}\)
Wheel type A: \(£ 0.70\) ea
\(\mathbf{f 0 . 9 0}\) ea


NH-CAD CHARGER-PANEL
\(177 \times 114 \mathrm{~mm}\) PCB with one massive Varta Deac \(57 \times 50 \mathrm{~mm} \varnothing\) rated 7.2 V 1000 mAH and another smaller Deac \(32 \times 35 \mathrm{~mm} \emptyset\) rated 3.6 v 600 mA . The price of these Ni -cad stacks new is over £20. Also on the panel is a mains input charger transformer with two separate secondaries wired via bridge rectifiers, smoothing capacitors and a relay to the output tags. The panel weighs 1 kgm All this for just \(\mathbf{£ 6 . 0 0}\)
PC8 MOUNTING NI-CADS
Much sought after 4.8 V 150 mA batts with CB mntg tags on 25 mm pitch. Batt size \(25 \times 16 \emptyset\). Ideal for paralleling. 99p ea; \(10+\) \(85 p ; 25+70 p ; 100+60 p\).

NI-CADS: AA 99p; C 199p; D 220p; PP3 \(395 p\).

\section*{1W AMPLFER}

2914 - Audio amp panel \(95 \times 65 \mathrm{~mm}\) whith TBA820 chip. Gives 1 W output with 9 V supply. Switch and vol. control. Just con nect batt. and speaker. Full details supplied Only \(£ 1.50 ; 10\) for \(£ 12\) : \(\mathbf{2 5}\) for \(£ 25 ; 100 £ 75\)

\section*{AM TUNER PANE:}

2916 - For use with mono amp above. Neat panel \(60 \times 45 \mathrm{~mm}\). Only \(£ 1.50\); 10 for \(£ 12.00\) FIBRE OPTICS
Scoop purchase of single and twin cable For use with visible light or infra red. Core 1 mm dia, overall 2.25 mm dia. Single \(50 \mathrm{p} / \mathrm{m} ; 20 \mathrm{~m}\) coil E 6.30 . Twin \(90 \mathrm{p} / \mathrm{m} ; 20 \mathrm{~m}\) coil £ 11.00 .

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4 mm PLUGS - Black and red 15p EACH. Green, Blue - 160 EACH 4 mm CHASSIS SOCKETS Above colours - 15 p EACH 4 mm TERMINAL POSTS Above colours - 44p EACH LASTIC PHONO PLUGS Back, Red, Whie, BiUe,
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DETALLS OF CONNECTORS

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150uF 15p; 220uF 17p; 330uF 20p; 470uF 22p; 000uF 36p; 2200uF 61pi 3300 UF 91 p
63 V :1uF 9p; 1.5uF 11p; 2.2uF \(8 p ; 3.3 \mathrm{uF} 8 p_{;} ;\)
\(4.7 \mathrm{uF} 80 ; 6.8 \mathrm{~F}\) 18p: 4.7uF 8p; 6.8uF 18p;
10uF 12p; 15uF 16p; 22uF 17p; 47uF 17p;
100uF 21p; 150uF 100uF 21p; 150uF 31p;
220uF 29p; 330 F 32p;
470 uF 45p; 1000 l 220uF 29p; 330 HF 32 p ;
\(470 \mathrm{uF} 46 \mathrm{p} ; 1000 \mathrm{~F} 7 \mathrm{7Bp}\); z200uF \(\$ 1.50\) (uF/Nolts)
\(0.1 / 35\) 12p; \(0.22 / 3517 p ;\)
\(0.47 / 3510 ; 2.7617 p\) \(0.47 / 3518 \mathrm{p} p ; 1 / 3519 p ;\)
\(22 / 35\)
\(21 p ;\) 2.2/35 21p; 4.7/16 17p \(101626 p ; 22 / 2563 p ;\)
\(100 / 337 p ; 100 / 10\) DISC CERAMIC TYPE \(0.01 \mathrm{uF} 6 p ; 0.022 \mathrm{uF} 6 p\)
\(0.047 \mathrm{FF} 8 \mathrm{p} ; 0.1 \mathrm{FF} 8 \mathrm{p}\) 1\% POLYSTYRENE TYPE \(10025 p ; 15025 p ; 22025 p ;\)
\(27025 p ; 33026 p ; 39027 p ;\) 470 27p; 1000 28p
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PACK 1: 10 of each value
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\section*{IDEAS}

As I have said before, this is your magazine and your ideas and comments are always valued. We often get interesting views on our contents, from committed hobbyists, from advertisers and teachers and together they help to shape the future developments of the magazine.

One area where you can contribute directly to the contents is Circuit Exchange, this feature is for your circuit ideas. I should point out that we are looking for new ideas, not just a copy of someone else’s circuit. At present we pay \(£ 40\) per magazine page for any ideas published, so good ones could pay for a couple of projects. Keep them coming in-there are a few in this issue to give you the idea of just what we are after.

\section*{TEACH IN}

We are continually being asked for back numbers on the last Teach-In series and unfortunately we are no longer able to supply them all. We would however like to point out that it is now only four months before the start of Teach-In '86 which will continue the tradition of top quality beginners series established by EE over the last fourteen years. The series will be linked to a number of projects and will be backed by software for the BBC and Spectrum-although it will not be essential to use this.

\section*{ACTUALLY DOING IT}

In addition to Teach-In ' 86 we are about to introduce a new page giving the lowdown on actually building projects for all those who are still a little hesitant to take up the soldering iron. These two items will be augmented by a building blocks series which will follow a simple systems approach to building projects of your own design around various circuit blocks. Each circuit block will be fully described and we will provide all the necessary constructional details. The series will also be helpful to AEB ' \(O\) ' level students.

Whatever your level of knowledge and sophistication in electronics, EE will have something of interest.


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\title{
CRAPHIC EQUALISER
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\section*{R.A.PENFOLD}

PROBABLY most readers are familiar with graphic equalisers, as they are now relatively commonplace, and are sometimes incorporated in pieces of equipment such as stereo cassette radios and rack audio systems. The original purpose of a graphic equaliser was to enable any peaks or troughs in the frequency response of the overall system to be ironed out. In particular, compensation could be made to counteract any variations in the frequency response caused by the characteristics of the listening room itself. In order to do this effectively a complex circuit having a dozen or more bands is necessary, and ideally some quite sophisticated test equipment would also be used.


Fig. 1. The basic arrangement of frequency control.

A more recent application for a graphic equaliser is as a sort of musical effects unit. Here the idea is to adjust the controls to modify the sound of an instrument (usually an electric guitar) and give the required sound, rather than to compensate for room accoustics or other frequency response problems. For example, a graphic equaliser can easily act as a bass or treble booster, and gives excellent control over the effect produced. Better in fact, than most bass and treble booster units. Even a fairly simple graphic equaliser enables a wide range of effects to be obtained.

\section*{SPECIFICATION}

This design has six equaliser controls with centre frequencies at approximately \(50 \mathrm{~Hz}, 150 \mathrm{~Hz}, 500 \mathrm{~Hz}, 1.5 \mathrm{kHz}, 5 \mathrm{kHz}\), and 15 kHz . With controls at the extremes of the audio spectrum and four at intermediate frequencies this gives good results with an electric guitar or other electronic instruments. With just six
bands it is less than ideal for use with an audio system, but could be used as a sort of super tone control if desired, but two units would be needed for stereo operation, one to process each channel.

\section*{CIRCUIT OPERATION}

The unit has been kept as simple as possible, and is based on a totally conventional gyrator design. The basic idea is to use gyrators to simulate ordinary L-C tuned circuits, thus avoiding the need for the very large inductors that would otherwise be needed to produce bandpass filters having suitably low resonant frequencies. This gives a substantial saving in cost, as well as enabling easy to obtain components to be used throughout the design. Fig. 1 shows the basic arrangements used in the unit.

Although the operational amplifier has a rather unusual feedback arrangement, it is not very complex in operation. Ra and Rb are of equal value in a practical design, and at resonance the gyrator has a low impedance. If we consider the circuit with the slider of VRa at the centre of its track, a positive voltage applied to the input will take the non-inverting ( + ) input positive of the inverting (-) input. Feedback via Rb will try to counteract this in normal operational amplifier fashion, so as to maintain the two inputs at precisely the same voltage. Due to the symmetry of the circuit the output of the amplifier must go to the same potential as the input in order to maintain this balance. This is true regardless of the impedance provided by the gyrator, and it is essential to the

correct operation of the circuit that there is always unity gain with the slider at the centre of its track.

With the slider moved towards the inverting input of the operational amplifier the symmetry of the circuit is upset. If we assume that the gyrator is at resonance and has a low impedance, the potential divider action across Rb and the gyrator results in only a small fraction of the output voltage reaching the inverting input. On the other hand, the coupling from the input to the non-inverting input is no worse than before, and is actually somewhat better due to the increased resistance to earth through the large portion of VRa's track and the gyrator. Accordingly, the output has to swing to a much greater potential in order to maintain the input voltage balance, and the input signal is boosted.

Of course, at frequencies where the gyrator is not at resonance and its impedance is very high it is effectively not in circuit. As VRa has a value which is low in comparison to that of Ra and Rb the symmetry of the circuit is only marginally affected, as is its voltage gain.

Moving the wiper of VRa to the other end of the track has the opposite effect. The potential divider action across Ra and the (resonant) gyrator gives a relatively poor coupling from the input to the non-inverting input of the operational amplifier. However, there is slightly reduced voltage drop from the output to the inverting input since the full track resistance of VRa is in series with the gyrator as far as this signal path is concerned. A relatively large input signal voltage is therefore needed in order to produce a given output level, and the circuit provides attenuation.


Fig. 2. The complete circuit diagram of the Graphic Equatiser.

Again, if the gyrator is off-resonance and has a high impedance it does not have any significant affect on the circuit, which consequently still has approximately unity voltage gain.

\section*{PRACTICAL CIRCUIT}

The full circuit diagram of the unit appears in Fig 2, and IC4 is the operational amplifier at the heart of the unit. R4 corresponds to Ra of Fig. 1, while R17 is the practical equivalent of \(\mathrm{Rb} . \mathrm{C} 2\) and C15 are d.c. blocking capacitors at the input and output of the unit. R1, R2 and C1 produce a centre tap on the supply so that a single 9 volt battery supply can be used, and the need for two batteries to provide a dual balanced supply is avoided.

In Fig. 1 only a single gyrator and potentiometer are shown, but in practice several potentiometers connected in parallel (VR1 to VR6) are required, with each one having its slider feeding into a separate gyrator circuit. This produces little interaction between the various gyrator/potentiometer stages since each gyrator only has a low impedance over its own frequency band, and has a very high impedance at the centre of any other bands. Interaction is not totally absent, but out of band, each control affects the gain of the unit by a relatively small amount, and in practice this type of circuit gives excellent results.

Although each gyrator is extremely simple, using just a single operational amplifier plus two resistors and two capacitors, this type of circuit is quite complex in the way that it operates.

However, the basic scheme of things is to have the operational amplifier, one capacitor, and the two resistors to simulate an inductor, which is then connected in series with the remaining capacitor. This gives what is effectively a conventional series L-C tuned circuit, which provides the required low impedance at or near resonance and a high impedance at other frequencies.

The maximum degree of boost and cut is about 15 dB , and the sample frequency response of Fig. 3 was obtained using full boost at 150 Hz , maximum cut at 5 kHz , and the other controls set for about unity voltage gain.

S2 can be used to bypass the unit and switch out the filtering when it is not required. In practice this is a heavy duty push button type so that it can be

\section*{COMPONENTS}
\begin{tabular}{|c|c|}
\hline \multicolumn{2}{|l|}{Resistors} \\
\hline R1, R2 & 4k7 (2 off) \\
\hline R3 & 100k \\
\hline R4,R17 & 470k (2 off) \\
\hline R5-R16 & 15k (12 off) \\
\hline All resist & ors \(\frac{1}{4}\) W \(5 \%\) carbon film \\
\hline \multicolumn{2}{|l|}{Potentiometers} \\
\hline VR1-6 & 100 k lin. carbon (6 off) \\
\hline \multicolumn{2}{|l|}{Capacitors} \\
\hline C1,C16 & \(100 \mu 10 \mathrm{~V}\) radial elect (2 off) \\
\hline C2 & \(1 \mu 63 \mathrm{~V}\) radial elect \\
\hline C3 & 100 n carbonate \\
\hline C4 & 470n carbonate \\
\hline C5 & 33 n carbonate \\
\hline C6 & 150n carbonate \\
\hline C7 & 10 n carbonate \\
\hline C8 & 47 n carbonate \\
\hline C9 & 3 n 3 carbonate \\
\hline C10 & 15 n carbonate \\
\hline C11 & 1 n carbonate \\
\hline
\end{tabular}

C12 4n7 carbonate
C13 330p ceramic plate
C14 1 n5 carbonate
C15 \(10 \mu 25 \mathrm{~V}\) radial elect

\section*{Semiconductors}

IC1-3 \(\begin{array}{ll}\text { 1458C dual op amps } \\ \text { (3 off) }\end{array}\)
IC4 741C op amp

\section*{Miscellaneous}

S1 Part of SK1
S2 SPDT heavy duty push button type
SK 1 Standard jack with
SPST contacts (S1)

\section*{SK2 Standard jack}

\section*{B1 9 volt (PP3 size)}

Case, 180 by 120 by 39 mm , printed circuit board EE8506-01, battery connector, small control knobs with pointer line ( 6 off), 8 pin di.i.l. i.c. holders ( 4 off), wire, solder, etc.


Fig. 3. A sample frequency response obtained from the Graphic Equaliser.
operated by foot. S1 is the on/off switch, and on the prototype this is a set of normally open contacts fitted to the input socket, SK r.

The unit is therefore automatically switched on when the plug is inserted into SK 1, and switched off again when it is removed. Of course, SI can be an ordinary switch such as a toggle or push button type if preferred. The current consumption of the circuit is approximately 5.5 mA , and a small 9 V battery is adequate as the power source.

\section*{CONSTRUCTION}

The unit is most easily constructed using printed circuit mounting rotary potentiometers as these can be mounted direct onto the printed circuit board. Details of the p.c.b. and component layout are provided in Fig. 4 and Fig. 5. An alternative is to hard wire ordinary (tag connection) rotary or slider type potentiometers to the board. If this method of construction is used it is important to keep the connecting leads reasonably short. It will be assumed here that the unit is built using rotary printed circuit mounting potentiometers, but it is obviously not difficult to modify construction to suit other types if desired.

Construction of the board is very straightforward, but make sure that each potentiometer is pushed right down into position before soldering it in place, using a generous amount of solder. Construction of the board will probably be easiest if the potentiometers are fitted last. It is advisable to use the carbonate capacitors where specified in the components list as these have a suitably close (5\%) tolerance for this application, and the lead spacing on the printed circuit has been designed to suit this particular type of capacitor. The use of radial (vertical mounting) electrolytics rather than vertically mounted axial types will give a neater finish, and a
board of greater resilience. Connect single-sided pins to the board at the points where connections to the sockets and switches will be made.

\section*{PLASTIC CASE}

A 180 by 120 by 39 mm plastic. Verocase having aluminium front and rear panels makes an attractive and adequately tough housing for this application. The front panel must be drilled with six 10 mm diameter mounting holes for the potentiometers, and these holes must be spaced 0.9 inches ( 22.86 mm ) apart to match the potentiometer spacing on the printed circuit board.

The board is mounted inside the case only by way of the mounting bushes and nuts of the six potentiometers, but this produces a very rigid assembly. There are mounting pillars moulded into both the top and base sections of the case, and

\section*{SOCKETS}

SK 1 and SK2 are fitted at opposite ends of the rear panel. \(\mathbf{S} 2\) must obviously be mounted on the top panel of the case so that it can be foot operated. Note that this component must be a heavy duty type as an ordinary push button switch is unlikely to be physically strong enough to withstand repeated operation by foot.

It might be difficult to obtain a single pole changeover heavy duty push button switch, but one pole of a double pole type can be used if a single pole type should prove to be elusive. Be careful to position this switch over a vacant part of the case. Otherwise, due to the very limited height of the case, it will probably prove to be impossible to fit the lid into position. The unit is completed by adding the small amount of hard wiring, as detailed in Fig. 5.

\section*{IN USE}

In use the unit simply fits between the guitar or whatever other instrument is being used, and the amplifier. Standard jack leads are used to carry the input and output connections. As explained earlier, the unit is automatically switched on when a plug is inserted into SK 1, and switched off again when the plug is removed.

The unit can introduce large irregularities into the frequency response of a system, and experimenting with the controls should soon determine whether or not the circuit is functioning correctly. Provided the instrument producing the input signal generates signals over a
 some of these will almost certainly obstruct the potentiometers and the board. This problem can be overcome by carefully drilling away the offending mounting pillars using a drill of about 9 mm in diameter. Due to the restricted height of the case it might also be necessary to trim off the ends of the potentiometer's pins, which with most components protrude well beyond the surface of the board.
reasonably wide frequency range it will be possible to considerably alter its sound. However, bear in mind that controls which operate below the fundamental frequency of the input signal can not have any significant effect on the output signal. For instance, if the instrument is generating a note at 300 Hz plus harmonics throughout the part of the audio range above this frequency, the 500 Hz , \(1.5 \mathrm{kHz}, 5 \mathrm{kHz}\) and 15 kHz controls will


Fig. 4. The p.c.b. design of the Graphic Equaliser. This board is available from the EE PCB Service, code 8506-01.


Fig. 5. Component layout and wiring diagram of the Graphic Equaliser.


Component and potentiometer mounting details.
be effective. There will be no output at frequencies below the 300 Hz fundamental, rendering the 50 Hz and 150 Hz controls ineffective.

When using any form of high frequency tone control it is necessary to bear in mind that a large amount of boost can produce excessive powers for the tweeters in some loudspeakers. This is more likely to be a problem with hi-fi loudspeakers than with types intended for the reproduction of electronic music.

The circuit does not have a very high noise level, and an excellent signal to noise ratio will be obtained using an input level of about 200 mV peak to peak or more. The maximum amplitude that can be handled without clipping occurring is about 4 V peak to peak.

\title{
HICH IMPEDANCE MULTIMETER
}

\section*{L.S.COOK}

WHEN measuring voltages using a conventional multimeter, the meter itself requires some current for its operation. If this is substantially greater than the current flowing in the circuit under test, the voltage levels are significantly altered when the meter is connected and a misleading reading is obtained. Even the once-popular \(20 \mathrm{k} \Omega / \mathrm{V}\) meter requires too much current for a circuit involving just a few microamperes.

The meter featured here has an input impedance to suit almost all applications where low-level d.c. voltages and currents are to be measured. It is designed mainly for experimental work, such as investigating the characteristics of devices.

\section*{CIRCUIT DESCRIPTION}

The circuit diagram is shown in Fig. 1. Apart from the two highest ranges, the high impedance for voltage measurement is provided by the LF441 op-amp (IC1). This is similar to the popular 741, but has an input impedance of \(1 \mathrm{~T} \Omega\) ( 1 Teraohm \(=10^{12}\) ohms), and draws a much lower current, a point strongly in its favour if small batteries are used. This i.c. has JFET inputs and needs no special handling precautions unlike many MOS devices.

The meter winding, together with R26 and R27, provides a total resistance of \(50 \mathrm{k} \Omega\) so a potential of 2.5 V across these produces a current of \(50 \mu \mathrm{~A}\) through the meter. The meter specified is a \(50 \mu \mathrm{~A}\) fullscale deflection type with an internal resistance of \(1.4 \mathrm{k} \Omega\). A different type can be employed with the value of R26 and R27 modified to obtain full-scale deflection at 2.5 V .

The different voltage ranges are obtained by varying the gain of IC 1 , which is used in the non-inverting mode; the basic arrangement for this is shown in Fig. 2. R18 to R25 (Fig. 1) constitute RA and \(\mathrm{R}_{\mathrm{b}}\) (Fig. 2) and switch Sle taps this resistance chain at selected points to vary the gain. For example, with Sic in the position indicated, \(\mathrm{R}_{\mathrm{B}}=250 \Omega, \mathrm{RA}_{\mathrm{A}}+\mathrm{R}_{\mathrm{B}}\) \(=25 \mathrm{k} \Omega\), so gain \(=\)
\[
\frac{25000}{250}=100
\]

Therefore for an output of 2.5 V the input must be 25 mV , since input voltage \(\times\) gain \(=\) output voltage.

Diode D1 prevents the meter attempting to swing negative which would occur if the input were incorrectly polarised or left floating. With the output taken from the cathode of D1, the calculation of gain is unaffected by the inclusion of this diode. C1 improves the stability of the circuit.

Table 1 shows the voltage ranges available, and the corresponding gains of IC1. For the 10 V and 25 V ranges, the input is taken to a chain of resistors totalling \(100 \mathrm{~m} \Omega\) with a \(\operatorname{tap}\) at \(10 \mathrm{~m} \Omega\) providing up to 1 V or 2.5 V respectively at this point. The voltage is then applied to the main circuit on the 1 V or 2.5 V range with S1a carrying out the necessary switching. R11 prevents high currents flowing through IC1 in the event of an excessive voltage being applied at the input; this could be destructive if the polarity was reversed. Compared with the high impedance of \(I C 1\), the drop across R11 is negligible. VR1 provides a means for zero-setting as explained later.

Current measurements are made by placing shunts across the input, comprising R12 to R17. In order to keep the voltage drop to a minimum the highest gain setting is used for IC1 where practicable, this being selected by switch S1d which is brought into play by \(\mathbf{S} 2 \mathrm{~b}\). The values of R12 to R17 are chosen to provide the ranges shown in Table 2. For example, with S1b and S1d set as shown, gain \(=\)
\[
\frac{25000}{25}=1000
\]
so the voltage across the input for full-scale deflection is
\[
\frac{2.5}{1000}=2.5 \mathrm{mV}
\]

The resistance across the input is \(25 \Omega\), hence the current required for full-scale deflection is
\(\frac{2 \cdot 5}{25} \times 10^{-3}=100 \mu \mathrm{~A}\)

The multimeter has a JFET input to provide the very high impedance.

Table 1: Voltage Table 2: Current ranges and opamp gain
\begin{tabular}{|l|r|}
\hline Range & \multicolumn{1}{|c|}{ Gain } \\
\hline 2.5 mV & 1000 \\
10 mV & 250 \\
25 mV & 100 \\
100 mV & 25 \\
250 mV & 10 \\
1 V & 2.5 \\
2.5 V & 1 \\
10 V & 2.5 \\
25 V & 1 \\
\hline
\end{tabular} measurement and voltage drop
\begin{tabular}{|l|c|}
\hline Range & \begin{tabular}{c} 
Voltage \\
drop
\end{tabular} \\
\hline \(10 \mu \mathrm{~A}\) & 2.5 mV \\
\(25 \mu \mathrm{~A}\) & 2.5 mV \\
\(100 \mu \mathrm{~A}\) & 2.5 mV \\
\(250 \mu \mathrm{~A}\) & 2.5 mV \\
1 mA & 2.5 mV \\
2.5 mA & 2.5 mV \\
10 mA & 10 mV \\
25 mA & 25 mV \\
100 mA & 100 mV \\
\hline
\end{tabular}

\section*{CONSTRUCTION}

Many of the resistors are mounted directly on S1, a 4 -pole 9 -way rotary switch. The connections to this switch are indicated in Fig. 4 with each section (pole) shown separately for clarity: the actual "Makaswitch" has two wafers each containing two poles, one each side of each wafer. It requires close scrutiny to obtain a thorough understanding of its operation, and this is essential before attempting the wiring.

Two small pieces of 0.1 inch matrix stripboard are required for the remaining


Fig. 2. Basic op-amp circuit.
small components, one of them holding the \(10 \mathrm{M} \Omega\) resistors. These are shown in Fig. 3. Attach a plug to one end of each test lead and an alligator clip to the other.

\section*{CASE}

A plastic console-style case with appropriate dimensions is suitable; alternatively, a case can be made from 3 mm plywood and covered with plastic fabric. The prototype, shown in the photograph, has a plywood case. Small wooden blocks glued inside the vertical corners enable a base panel to be screwed on. The circuit boards can be fixed in position using small screws and insulated spacers if necessary.

\section*{METER SCALE}

The meter is likely to have a scale reading up to \(50 \mu \mathrm{~A}\). This can be replaced


Fig. 3. Layout of components and drilling details for the two pieces of stripboard (shown actual size). The integrated circuit is mounted with its associated diode and resistors, and all the 10 M resistors (R1 to R10) are mounted separately. Refer also to Figs 1 . and 4.
by a scale showing markings up to 10 and 25.

Carefully remove the transparent cover and stick a piece of white card or plastic adhesive film over the scale, having first cut out an area corresponding to the position of the graduations on the original scale. Add the numbers using dry transfers.

\section*{POWER SUPPLY}

A dual power supply is required: the i.c. will operate from \(\pm 3 \mathrm{~V}\) to \(\pm 18 \mathrm{~V}\), but obviously the higher the supply voltage, the higher will be the meter current in the event of overload. Two PP3 batteries are ideal and can be held in place by stiff wire fastened by the meter fixing screws.



EE1660
Fig. 4. Interwiring details, viewed from the back. The four poles of S1 are exploded for clarity: S1c is nearest the front (knob), and S 1 b is nearest to the back. The photograph below shows the interwiring of the prototype.

\section*{TESTING AND USING}

Although calibration should not be necessary it is wise to check performance against an existing meter if possible. Voltage and current readings for all ranges should be checked, with the meters connected in parallel for voltage readings and in series for current. The impedance
of the existing meter is of no great importance.

When using the meter try to avoid touching the positive connection as this can cause the output of the op-amp to swing to maximum. It may be advisable to switch on only when the connections have been made.

To set zero correctly, select the lowest voltage range and with the test leads
plugged into the ' \(V\) ' and ' \(O\) ' sockets, connect both clips together. With VR1 towards the clockwise limit a reading will be shown on the meter. Turn VR1 back to the point at which a zero reading is just obtained and no further. Note that a negative reading cannot be indicated owing to the presence of D1. Accurate setting of this control is important, particularly for the lower ranges.


\section*{}


\title{
FOR YOUR ENTERTATNMENT \\ BY BARRY FOX
}

\section*{Hi Fi Video}

Everyone is talking about hi fi video. You can buy hi fi machines in both the Beta and VHS formats.

On a conventional machine the sound is recorded on a linear track along the edge of the tape. Quality is limited by low tape speed (under one inch a second) and the narrow track width, especially in stereo.

For hi fi video the audio is converted to f.m. and fed to extra heads mounted on the rotating video drum. These lay down f.m. signal tracks across the tape which are almost immediately over-written with video signals from the conventional video heads. Because the video signals are at higher frequency and lower drive current than the audio f.m. only the top layer of audio recording is erased and replaced with video.

The result is a two layer sandwich, with video on top and audio below. Hence the term depth multiplex recording. The audio and video heads are set at different angles or "azimuth", so that on playback the audio heads read only audio and the video heads read only video.

Both the Beta and VHS hi fi systems work in the same way in Europe, although the Beta hi fi system works rather differently in America. Over there the audio and video signals are mixed and fed to the same heads.

The hardware firms are busily advertising hi fi video and promising more and more pre-recorded cassettes in the new format. These will of course also have a conventional soundtrack for owners of conventional machines.

All the major duplicators have installed hi fi machines-except one. CBS-Fox is holding back. This is particularly surprising because in America CBS-Fox led the hi fi scramble. I asked David Harris, head of duplication at the CBS-Fox plant in Greenford, Middlesex, why he wasn't joining in.
"Hi fi has come too early," he told me. "It's a major benefit for the hardware industry which can sell at higher prices. But it's no benefit yet for software companies like us.
"Pre-recorded tapes won't sell better because they are in hi fi. We've sold 30,000 copies of The Empire Strikes Back. If we'd sold ten more because of hi fi we'd have been lucky.'
"I don't believe hi fi quality can be achieved for the same price," he went on, "you need different mastering, different quality control standards, different technology. You can't do that for nothing. So who will pay? We've been asking that question for 18 months.
"The hardware firms should have knocked a million or so off their multimillion advertising budget for video hi fi machines, and helped pay for the duplication equipment. Sony has been markedly more helpful over providing video hi fi equipment at reasonable price than the VHS manufacturers.
'The CBS-Fox plant in America needed new equipment," Harris explained, "so it made sense to choose hifi and launch with
plenty of razzmatazz. At Greenford we've got around 800 or 900 machines, we never say exactly how many, and they don't need replacing yet.
"Hi fi machines cost more and I can't justify that extra expense. We've got some machines on test and are learning about the problems. But we are doing it without upsetting our customers. Other firms are learning publicly."

\section*{Right Approach}
"What the industry needs," Harris goes on, "is a standard approach to hi fi mastering. Some duplicating houses are set up to issue hi fi tapes with the sound sourced from a digital recording sync-locked to a master video machine, but others are equipped only to source the sound from ordinary video machines with linear soundtracks.
"In America they use DBX noise reduction on the master machine, but not over here. So what happens if a film company wants to shift work from one duplicator to another with different equipment? The industry isn't even talking about a standard yet. Hi fi video in Britain won't really happen for another eighteen months.'

\section*{Cable Vision}

Although there is much talk about cabling Britain in the future, around six per cent of the country is already hooked up to cable. A total of 1.2 million homes get their TV programmes down wires from local "headends" or distribution points. That's in addition to people who live in blocks of flats and get their TV signals from a communal master aerial.

Ten years ago 2.5 million British homes were on cable. The number then stood still and has been falling since 1980. Cable began in Britain back in 1925, when some homes did not have mains power and could not receive radio. Enterprising companies piped in radio signals at high enough voltage to run a loudspeaker without an amplifier.

In 1950 the Home Office licensed three companies, EMI, Rediffusion and British Relay to distribute 405 -line TV along cable radio lines. The systems were then upgraded to take colour TV. Around 70 per cent of these 1.2 million homes in Britain now receiving TV by cable, rely on relatively primitive twisted wire pairs of the type originally designed for radio signals.

The radio signals were distributed over long distances at 500 V and reduced to 55 V for home use. The TV signals run into the home at 30 V on an 8.9 MHz carrier. Trunk cables are coaxial and then split for home service into twisted wire pairs, with one channel per pair.

In theory it is possible to stack or multiplex (this happens in Jersey) but in practice, the losses are too serious. The higher the frequency carried, the quicker the signal is lost on a twisted wire pair. At the moment repeaters are needed every 1500 metres.

All the fuss about cabling Britain centres on the Government's enthusiasm for making the UK a wired society with high technology, two-way interactive cable links. That way homes of the future will be able to bank, shop and browse through mail order and estate agents' catalogues by cable link.

The snag is that interactive systems need cables wired in switched star configuration, not conventional tree and branch layout. Although the Government wants a wired
society, it won't subsidize switched star installation.

The cable companies know there is a limited market for interactive systems. British Telecom's Prestel viewdata service still has only 50,000 subscribers, many of them business users. Only a few are domestic subscribers who use Prestel to shop and shuffle money by viewdata. So the cable companies certainly don't want to spend extra on laying a high technology system simply to offer interactivity. They would rather try to make money out of simple one-way entertainment services.

As far as 1 can see, no-one has yet thought seriously about a possible compromise between these two extremes; high technology switched star interaction on one hand and one way, low technology tree and branch on the other. The answer, surely, is to link cable with a telephone.

Already Oracle the commercial TV teletext service is experimenting with personalized teletext transmission. Pages of data are given address codes which means they can only be received by a set which incorporates a decoder with matching access codes.

Oracle will use this system to transmit semi-confidential information nationwide. for instance a running update on pricing for department store chains and a list of stolen credit card numbers for shops and restaurants to keep checking. Extra memory in the receiver will give rapid access to long lists of data.

If a cable system, even of the old twisted pair types, were to use addressed teletext messages, then the subscriber's conventional telephone could provide the other half of the interactive link. A simple modem would let the subscriber key instructions down the line direct into the cable teletext computer.

The use of a home computer would make the system even more flexible. This would make it possible to upgrade existing cable systems, without ripping out old wires from under the ground. But no-one seems to be seriously investigating the possibility. Could it be that no-one has thought of it?


\section*{CATALOGUES RECEIVED}

Not so much a catalogue as a bulletin received from Midwich concerning the company's special offering of a number of items, including IDC strip headers, low power Schottky TTL (LS series) i.c.s, low profile di.i.l. sockets and wire-wrap sockets with turned pins. Prices are too numerous to quote, but further information may be obtained from Midwich Computer Co., Ltd., Gilray Rd., Diss, Norfolk IP22 3EU. 03794131.

If you have a connector problem, STC's Five Star Connector service might be your escape route. The 1985 catalogue (Issue No. 1) is out now, and you can order using your credit card, or c.w.o. There's no minimum order charge, and if you are not an account holder with STC your first order will automatically open one. Five Star carries over 4000 lines, and the catalogue includes illustrations to assist selection: Five Star Connectors (STC), Edinburgh Way, Harlow, Essex CM20 2DF. \(\int 0279\) 442851.

Another catalogue received is that of Rose, whose enclosures are available in many shapes, sizes and materials, including aluminium, polyester, polycarbonate and \(A B S\). This 52 page catalogue is rich in dimensional information, and available from Radiatron Ltd., 76 Crown Rd., Twickenham, Middlesex TW1 3ET. /01-891 0156.

\section*{Magic Washers}

A revolutionary thermal jointing compound which changes state from solid to liquid when the equipment is switched on is available from Charcroft Electronics Ltd. Called Crayotherm, the compound automatically "wets" the contact area to a high level of thermal conductivity, and never hardens, no matter how many thermal cycles it undergoes-a feature contributing improved reliability.

The "no-mess" compound is available in the form of ready-coated insulating film rolls, and in sheet form, making it an ideal replacement material for power transistor mica
washers. Crayotherm is in fact available ready-stamped into washers to suit TO-3, TO-36, TO-66, TO-220 and DO-4 devices.

If you would like free samples of the material please write to Charcroft Electronics Ltd., Charcroft House, Sturmer, Haverhill, Suffolk CB9 7XR. 60440705700.

\section*{Passcards}

Shown below is an example of the 'Key Facts' Passcard 'modular' revision system for students following the AEB ' O ' Level Electronics course. The card pack serves as a very quick reference for the student during revision, and for the beginner. The cards measure \(75 \times\) 125 mm and fit inside a plastic wallet. Further details from: Charles Letts \& Co Ltd., Diary House, Borough Rd., London SE1 1 DW.
```

suocession of pulses (pulse train) is used as the crerrier wav
Of the laller type there are four main forms (Fig. 45):
(i) Pulse amplitude modulation (PAM): the amplitude of the
(ii) Pulse is modulaled by sampies or me modulating signal
(ii) Pulse duration modulation (PDM): the duration of each
pulse is modulated by the signal.
or position of pulses is modulated by the signal
(iv) Pulse code modulation (PCM): only certain values of the
amplitude of the modulating signal are allowed. and
each sample is assignod a numerical value. A pattern of
pulses that represents this value is transmitted as a coded
010
Л\OmegaT\ULU\Omega %ow
M\&STOLL...
|||||||||||.
Figure 45
Information Transmission
Whercver information needs to be transmitted from one point to another, as in telecommunications, computer ystems, radio and television, certain fundamental elements These elements are the source, modulatot, transmite propagation medium. recsiver, demodulator and receptor (Fig propa
46).

```

\section*{Terrific Tori}

What advantages have toroidal power transformers over their conventional stacked lamination counterparts? Toroidals are about 50 per cent lighter and smaller. They are magnetically more efficient. They
radiate less electrical and audible hum.
Cotswold Electronics Ltd. stocks a "budget" range of these transformers, costing around £9 for a 30VA unit to around \(£ 25\) for a unit rated at a little over 500VA, at one-off prices. Details from Cotswold Electronics Ltd., Unit T1, Kingsville Road, Kingsditch Trading Estate, Cheltenham, Gloucester GL51 9NX. 『0242 41313.

\section*{CONSTRUCTIONAL PROJECTS}

\section*{Across The River}

The p.c.b.-mounting buzzer for Across The River is available from RS Components (RS 249-794).

\section*{Caravan PSU}

Switch S2 used in the Caravan PSU is assumed to be the Maplin Electronics 4P3W slide switch, in the wiring diagram. The 317 M variable voltage regulator IC1 is available from Greenweld Electronic Components, 443 Millbrook Rd.. Southampton SO1 OHX. \& 0703 772501.

\section*{Electronic Doorbell}

The PB2720 piezoelectric transducer used in the Electronic Doorbell is available from Cirkit (stock number 43-27201) for the princely sum of 55 pence. There should be no difficulty in procuring the remaining components. Cirkit, Park Lane, Broxbourne, Hertfordshire EN10 7NQ. \(\int 0992444111\).

It was mooted in the EE office that this project would make an ideal "pocket doorbell" for calling on houses without their own fitted. You would simply dangle it through the letter-slot, on the end of its wire, push the button and retrieve it. But is this a truly original idea?

\section*{Graphic Equaliser}

There are no components in the Graphic Equaliser that should present any buying difficulties, although it should be pointed out that S1 is integral to SK1, which is a 0.25 in. jack socket with a "make" switch. A suitable socket is available from Electrovalue Ltd., 28 St. Judes Rd., Englefield Green, Egham, Surrey TW20 OHB.

\section*{High Impedance Multimeter}

The \(50 \mu \mathrm{~A}\) f.s.d. panel meter \((1.4 \mathrm{k}\) resistance) used in the High Impedance Multimeter is available from Maplin (order as RX54J), for \(£ 8.95\). See page 209 of the Maplin catalogue, or contact Maplin Electronic Supplies Ltd., PO Box 3, Rayleigh, Essex SS6 8LR.

The LF441 CMOS op. amp. can be obtained from Macro Marketing Ltd., Burnham Lane, Slough. Berkshire SL1 6LN. 06286 4422. If you do not have an account number with Macro, your first order will set one up.

\section*{Computerised Shutter Timer}

All of the components in the Computerised Shutter Timer were found to be readily available when checked.

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Size 1212 mm dia \(£ 4.37\)


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Multicore Solder Cream Mixture of powdered \(60 / 40\) (tin/lead metal alloy and rosin flux) Uses: Micro electronics and printed circuits Handy Tube: Size BCR 10 £ 1.73


Bib Audio/Video Products Limited. (Solder Division).
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\({ }^{1}\)n COMMON with most of the ready-made Spectrum interfaces, many of the projects which we shall be describing in On Spec will derive their power directly from the Spectrum. We shall, therefore, start this month with an important note concerning the d.c. supply rails available at the Spectrum's edge connector.

\section*{Power Supply}

Whilst it would appear to be expedient to use the Spectrum's own internal supplies, the would-be experimenter should first be made fully aware of the limitations of these voltage rails. Failure to do so may not only result in unpredictable behaviour of the computer but may also cause permanent damage to the Spectrum's own internal power supply.

It should be noted that there are definite limitations to the current which may be safely drawn from the Spectrum's internal supply rails. This is particularly true in the case of the nominal +12 V and -5 V rails which are internally generated from a simple d.c.-to-d.c. converter, the reliability of which has been a consistent cause for concern with early issues of the Spectrum. (Sinclair have, in fact, taken steps to alleviate these problems with the introduction of a series of modifications and improvements to the circuitry around the d.c.-to-d.c. converter, TR4).

For the sake of readers who may have missed March's On Spec we will just summarise the power rails to which we have access at the rear connector: refer to Table 1, above.

The +9 V unregulated line consists of nothing more than the unregulated d.c.
input from the mains unit and, although an appreciable current may be safely drawn from this rail, the voltage may vary anywhere between 9 V and 11 V depending upon the mains input, load current, and particular mains unit employed.

The +5 V regulated rail is derived from a single monolithic three-terminal regulator (marked REG on the p.c.b.) In early versions of the Spectrum (Issue 1 and Issue 2) this regulator was somewhat prone to overheating and, from Issue 3 onwards, was relocated to the rear of the p.c.b. and accorded the benefit of a much larger heatsink. It should be noted that, by virtue of the 7805 's internal foldback over-current protection, this device will usually survive the ravages of a temporary short circuit placed on the +5 V rail.
point (shown, for the benefit of the curious, in Fig. 1) comprises a high frequency component of typically 100 kHz or more, superimposed on a d.c. level of approximately 10.5 V . The peak-to-peak value of this decidedly non-sinusoidal waveform is of the order of 20 V or so. Permanent damage to TR4 can be caused by an inadvertent misconnection or temporary short-circuit placed on the \(\sim 12 \mathrm{~V}\) rail and hence this particular voltage rail is best left well alone!

\section*{Solution}

Generally the most satisfactory solution to the problem of delivering power to an external interface (at least where any appreciable current is involved) is that of providing an additional 7805 regulator within the interface unit. This, in turn, should derive its power from the

Table 1. Voltage levels available at the Spectrum rear connector
\begin{tabular}{|c|c|c|c|}
\hline Designation & \begin{tabular}{c} 
Connector \\
Reference
\end{tabular} & \begin{tabular}{c} 
Typical \\
voltage
\end{tabular} & \begin{tabular}{c} 
Max. recommended \\
current
\end{tabular} \\
\hline 9 V unregulated & 4 B & +10.5 V & 300 mA \\
5 V regulated & 3 B & +4.9 V & 50 mA \\
12 V & 22 A & +11.5 V & 10 mA \\
-5 V & 20 A & -4.5 V & 5 mA \\
\(\sim 12 \mathrm{~V}\) & 23 A & (see Fig. 1) & do not use! \\
\hline
\end{tabular}

The +12 V and -5 V rails required by the lower 16 k of RAM (IC6 to IC13) are produced by the on-board d.c.-to-d.c. converter, TR4. The +12 V rail is regulated by means of d.c. feedback in the converter whilst, in later issues the -5 V rail also has the benefit of an additional shunt zener diode regulator. Unfortunately, neither of these rails can deliver much in the way of current.

\section*{High-Frequency Waveform}

The \(\sim 12 \mathrm{~V}\) line is connected directly to the collector of the d.c.-to-d.c. converter, TR4, and the normal waveform at this


Fig. 1. Waveform at the collector of TR4
unregulated 9 V line. Not only is this arrangement flexible but it also helps to minimise the effects of loading on the already well-used internal supply rails of the Spectrum.

\section*{Four Channel Output Interface}

Having started on a cautionary note, let's turn our attention to a simple four channel output interface. This unit has a wide variety of applications and complements the four channel input interface described in April's On Spec.

The complete circuit diagram of the interface is shown in Fig. 2. An eight-input NAND gate, IC1, together with the inverter formed by IC2b, provides address decoding so that the interface is selected whenever address line A6 is low and all other address lines (A0 to A7) are high. This corresponds to a decimal address of 191. If desired, the address may be changed to 255 by simply omitting IC2b and linking address line A6 directly to pin 11 of IC 1 .

The address decoded from ICl is combined with the \(\overline{I O R Q}\) and \(\overline{W R}\) lines using IC2a so that the output of IC2a (pin 6) goes high whenever the Spectrum writes to port address 191 (or 255 if IC2b is omitted). This has the effect of clocking
COMPONENTS
Resistors
\[
\begin{aligned}
& \text { R1 to R4 } 270 \text { (4 off) } \\
& \text { R5 } 1 \mathrm{k} \\
& \text { All } \frac{1}{4} W \pm 5 \%
\end{aligned}
\]

\section*{Capacitors}
\begin{tabular}{ll}
C 1 & \begin{tabular}{l}
\(10 \mu 16 \mathrm{~V}\) p.c. \\
electrolytic
\end{tabular} \\
C 2 to C4 \\
100 n polyester (3 off)
\end{tabular}

\section*{Semiconductors}
\begin{tabular}{ll} 
D1 to D4 & Red I.e.d. (4 off) \\
IC1 & 74LS30 \\
IC2 & 74 LS27 \\
IC3 & 74 LS175
\end{tabular}

\section*{Miscellaneous}
14-pin low-profile d.i.l. sockets (2 off); 16-pin low-profile d.i.l. socket; 28 -way open end doublesided 2.54 mm pitch connector (e.g. Vero part number 83824826A); terminal pins (12 off) or four 3 -way 2.54 mm pitch connectors; 2.54 mm hole pitch stripboard measuring approx. \(80 \mathrm{~mm} \times\) 80 mm (minimum 28 strips).
Approx. cost Guidance only
the data which appears on the least significant four data lines (D0 to D3) into the data latch formed by IC3. The "Q" outputs of the four latches will then retain the state of their respective data input lines until the latch is again written to.

The Q and \(\overline{\mathrm{Q}}\) outputs of each data latch (which are, of course, TTL compatible) are both made available. This not only allows an l.e.d. indicator to be connected to each channel but also permits direct connection of sensitive di.l. reed relays since the \(\overline{\mathrm{Q}}\) output is capable of sinking currents in the order of 15 mA or so.

\section*{Construction}

Construction of the four-channel output interface follows the same broad principles as that adopted for the fourchannel input interface described in April's On Spec. The interface components are assembled on a small piece of Veroboard measuring approximately \(80 \mathrm{~mm} \times 80 \mathrm{~mm}\). Whilst the precise dimensions of the board are uncritical, it must have a minimum of 28 tracks aligned in the vertical plane.

The 28 -way double sided edge connector is mounted along the bottom edge of the board and will require approximately


5 rows of holes across the full width of the stripboard. The board will thus stand vertically when the connector is mated with the Spectrum.

Before soldering any of the components to the stripboard, it is important to leave some clearance for the rear "overhang" of the case. For the Spectrum this gap should correspond to 8 rows of holes ( 20 mm approx.) whilst for the Spectrum Plus the gap should be increased to 12 rows of holes ( 30 mm approx.).

Whilst component layout is generally uncritical, care should be taken to ensure that the supply decoupling capacitors, C2 to C 4 , are distributed around the board (each preferably associated with an individual integrated circuit supply). Great care should be taken to ensure that all unwanted tracks are cut (including those which link the upper and lower sides of the 28 -way connector). A purpose designed "spot-face" cutter may be used for this purpose or, if such a device is not available, use can be made of a small sharp drill bit.

Links on the underside of the board are best made using appropriate lengths of miniature insulated wire of the type normally employed for wire wrapping. Readers requiring further information on
the connector should refer to March On Spec.

When the stripboard wiring has been completed, the three integrated circuit devices should be inserted into their sockets (taking care to ensure correct orientation) and the entire board should be carefully checked before connecting to the Spectrum. Note that the Spectrum should always be disconnected from its supply before either connecting or disconnecting any interface module. If all is well, when power is re-applied, the normal copyright message should appear. If not, disconnect the power, remove the interface and check again.

Any comments, queries, or suggestions for inclusion in On Spec should be sent to:
Mike Tooley,
Department of Technology,
Brooklands Technical College,
Heath Road,
WEYBRIDGE,
Surrey KT13 8TT.
And don't forget to include a stamped addressed envelope if you would like a copy of our latest "Spectrum Update".
NEXT MONTH: We shall provide some example uses for the fourchannel output interface.


The lack of I/O facilities is undoubtedly one of the Sinclair Spectrum's weakest points. This is unfortunate since many other low-cost personal computers provide some form of parallel I/O which is available for use by the experimenter. Even with the simplest interface hardware (i.e. one which is not itself programmable) the possibilities are immense, ranging from controlling your model railway to running your domestic central heating system.

An interface, therefore, must be considered as an essential pre-requisite when connecting your Spectrum to the outside world. Happily, a few hardware suppliers are beginning to cater for this need. One such supplier, Datel Electronics (no newcomer to the field of Spectrum interface design) have recently introduced their Robotek interface as an addition to their existing range of 'add-ons' which includes such devices as joystick interfaces and light pens.

\section*{I/O CHANNELS}

The Robotek interface has four output channels (labelled A to D) and eight input channels (labelled A to H). The interface is mapped to a decimal port address of 63 (address lines A6 and A7 both low). The output channels appear as relays, each of which has a single set of changeover contacts and, therefore, has three associated lines; common, normally closed, and normally open. In the nonenergised state the common connection is linked to the normally closed contact whereas, in the energized state, the common connection is linked to the normally open contact. A relay may be energized by simply writing a logic 1 to the output channel concerned. It is important to note that all of the output channels have a latching action (i.e. once energised the relay will stay that way until a logic 0 is written to the channel concerned).

Besides the flexibility of relay outputs, this also provides a measure of isolation for the Spectrum controller. Each relay
can switch up to 50 V at 1 A . It should, however, be stressed that the Robotek is not suitable for directly switching a.c. mains supplies. This is a task which can be easily accomplished using an appropriately rated external relay or solidstate switch. (It would have been nice to see a few hints as to how this can be done in the instructions!)

One further point to note is that the wiring of output channel \(D\) differs from that of the other channels in that the normally open contact is also used as the common ground connection for the eight input channels. The reason for this anomaly is the use of a 20 -way IDC connector for terminating all the I/O lines. With three lines devoted to each relay (making a total of twelve output lines) and eight input lines devoted to inputs, the common ground connection has to be shared. Whilst in many applications this may be unimportant, it may restrict the usefulness of output channel D where a degree of isolation is required.

\section*{SOFTWARE}

Software control of the output is extremely easy. Each channel is associated with a particular data line hence, to switch channel A 'on' from BASIC you need simply key:

OUT 63,8
and, to switch channel A 'off again, you need only enter:

\section*{OUT 63,0}

The eight input lines are all TTL compatible and are not isolated. The lines are internally pulled-up so that, in the absence of any external connections, they all adopt a logic 1 state. If a switch is now connected between an input line and common ground, when 'open' a logic 1 input will be sensed and when 'closed' a logic 0 will be perceived. Obviously the user is not restricted to using mechanical switches as inputs and any TTL compatible switching device (such as a TTL optoisolator) could be employed.

\section*{DATA VALUES}

Just as a data value is associated with each output channel, a value is associated with each input channel. Thus, if we had a single input switch connected to channel A (value \(=4\) ) we could sense its state by keying:

\section*{PRINT IN 63}

If this returns a value of 255 (all input lines high) the switch would be 'open'. If a value of 251 were to be returned we would surmise that the switch was closed (all lines EXCEPT that used by channel A are high).

The Robotek is neatly housed in an ABS case measuring approximately 110 \(\times 77 \times 28 \mathrm{~mm}\). The case is fitted with a double-sided edge connector which mates directly with the expansion connector at the rear of the Spectrum. It is important to note, however, that this case will not mate directly with the Spectrum Plus!

The external lines are terminated in a 20-way IDC connector which emerges from the upper edge of the ABS case. A matching connector (assembled on a 620 mm length of 20 -way colour coded ribbon cable) is supplied with the Robotek. Two main criticisms followthe cable was not really long enough (they never are!) and the ribbon cable colour codes did not correctly agree with the pin assignment of the IDC connector!

The unit is supplied with two A4 pages of instructions. These explain the electrical properties of the input and output channels and provide brief details of how they can be controlled from BASIC. Also included are tables giving the values associated with each input and output channel (these are useful since the values do not follow the logical sequence of weighting) and a chart showing the ribbon cable connections. My only comment on the instructions are that a few sample programs could have been usefully included for the benefit of the inexperienced programmer. These could, for example, show how the four output channels can be controlled independently and how the status of the input lines can be repeatedly sensed.

\section*{CONCLUSION}

The Datel Robotek offers the experimenter tremendous scope for expanding his Spectrum beyond the confines normally associated with a games/entertainment machine. The few minor criticisms voiced in this review in no way detract from the usefulness of the interface which is both competitively priced and excellent value for money. So, whether you are building a robot or intelligent security system, there are no longer any excuses; this interface will help you do it!

The Robotek interface costs \(£ 29.99\) (post free). It is available from: Datel Electronics, Unit 8, Fenton Ind. Est., Dewsbury Road, Fenton, Stoke-on-Trent. (0782 273815).

\title{
ACROSS THE RIVER
}

\section*{W.D.PHILLIPS BSc PhD}

THIS easy-to-build hand-held electronic game can provide fun for all the family. It is based on a very old problem in which a farmer has to cross a river to get his goods to market; the snag is that he can take only one item at a time, and he has to be selective if he is to get all three safely across.

\section*{THE PROBLEM}

A farmer takes to market a hen, some corn, and a fox. On the way to town he has to cross a river. There is a boat but the farmer can take only one of the three,


Fig. 1. 16-bit data selector.


Fig. 2. 8-bit data selector.
either the hen, the corn, or the fox, across at a time. This unlikely scenario creates a nice little problem in logic.

When the farmer is there to keep order, everything is under control but, if he leaves the hen with the corn, on either side of the river, the hen will eat the corn, while if he leaves the fox with the hen, the fox will eat the hen. The problem is how exactly does the farmer cross the river safely with all three of his possessions and continue on his way to market?

Table 1: Truth table for the problem.
\begin{tabular}{|c|c|c|c|c|}
\hline \begin{tabular}{c} 
farmer \\
\(D\)
\end{tabular} & \begin{tabular}{c} 
hen \\
\(C\)
\end{tabular} & \begin{tabular}{c} 
corn \\
B
\end{tabular} & \begin{tabular}{c} 
fox \\
A
\end{tabular} & output \\
\hline 0 & 0 & 0 & 0 & 0 \\
0 & 0 & 0 & 1 & 0 \\
0 & 0 & 1 & 0 & 0 \\
0 & 0 & 1 & 1 & 0 \\
0 & 1 & 0 & 0 & 0 \\
0 & 1 & 0 & 1 & 1 \\
0 & 1 & 1 & 0 & 1 \\
0 & 1 & 1 & 1 & 1 \\
\hline 1 & 0 & 0 & 0 & 1 \\
1 & 0 & 0 & 1 & 1 \\
1 & 0 & 1 & 0 & 1 \\
1 & 0 & 1 & 1 & 0 \\
1 & 1 & 0 & 0 & 0 \\
1 & 1 & 0 & 1 & 0 \\
1 & 1 & 1 & 0 & 0 \\
1 & 1 & 1 & 1 & 0 \\
\hline
\end{tabular}
\(D=0\) : Farmer on first side of river. \(D=1\) : Farmer on second side of river.

Table 2: Truth table for an 8-bit data selector.
\begin{tabular}{|c|c|c|c|c|}
\hline \multicolumn{3}{|c|}{SELECT INPUTS} & OUTPUT & QUTPUT \\
\hline \[
\begin{gathered}
C \\
(f o x)
\end{gathered}
\] & \[
\begin{gathered}
\hline \text { B } \\
\text { (hen) }
\end{gathered}
\] & \[
\begin{gathered}
\mathrm{A} \\
\text { (corn) }
\end{gathered}
\] & \((\mathrm{F}=0\) ) & \((\mathrm{F}=1)\) \\
\hline 0 & 0 & 0 & 0 & 1 \\
\hline 0 & 0 & 1 & 0 & 1 \\
\hline 0 & 1 & 0 & 0 & 0 \\
\hline 0 & 1 & 1 & 1 & 0 \\
\hline 1 & 0 & 0 & 0 & 1 \\
\hline 1 & 0 & 1 & 0 & 0 \\
\hline 1 & 1 & 0 & 1 & 0 \\
\hline 1 & 1 & 1 & 1 & 0 \\
\hline
\end{tabular}

\section*{TRUTH TABLE}

The first step in designing an electronic circuit to model this situation is to construct a truth table for the problem, as shown in Table 1.

In the truth table, a ' 0 ' in the farmer column shows the farmer on the first side of the river, while a ' 1 ' shows him on the second side. In the same way, 0's and 1's are used to represent the position of the hen, corn, and fox. In the output column, a 0 corresponds to a safe overall position, while a 1 indicates that either the corn or the hen, or perhaps both, are about to be eaten!

\section*{DATA SELECTOR LOGIC}

The truth table is turned into a practical circuit using a simple but elegant technique called data selector logic. A 16bit data selector is shown in Fig. 1. The select inputs, \(\mathrm{A}, \mathrm{B}, \mathrm{C}\), and D , are decoded to provide the "address" of one of the data inputs, numbered 0 to 15 . The logic level available at the selected input is then transferred to the single output pin. A complete solution to the hen, corn, fox problem is obtained simply by connecting 0's and l's to the data inputs as illustrated.

A more economical solution using an 8 -bit data selector is shown in Fig. 2. In this case there are just three select inputs: these are chosen to correspond to the hen (input B), the corn (input A), and the fox (input C ). By referring to the truth table of Table 1, the correct logic level to be connected to each of the data inputs can be determined and a revised truth table (Table 2) can be drawn up.

The method is as follows: consider, in Table 1, the lines for which select inputs \(\mathrm{A}, \mathrm{B}\) and C are all 0 . In one case, select input \(D=0\), corresponding to the farmer on the first side of the river, and for the other \(\mathrm{D}=1\). The output is 0 for the first case and 1 for the second.

For the 8 -bit data selector, it is simply necessary to arrange for the data inputs to act as the fourth select line. Hence when \(A, B\) and \(C\) are all 0 , data input 0 is routed to the output \((\mathrm{Z})\) : the logic level at data input 0 needs to be 0 when the farmer is on the first side of the river ( \(\mathrm{F}=0\) ) and 1 when he is on the other side \((\mathrm{F}=1)\). This is achieved by switch \(\$ 2\), as shown in Fig. 3. The process continues similarly for the other seven possible combinations


Fig. 3. Circuit diagram of the electronic game "Across the River"
of select inputs A, B and C, and is summarised in Table 2.

In the case when A, B and C are all 1, for example, in Table 1, when \(\mathrm{D}=0\) the output is 1 and when \(\mathrm{D}=1\) the output is 0 . Hence for the 8 -bit selector, the inverse of the input from S2 \((\bar{F})\) needs to be connected to data input 7. This is done by TR1.

The appropriate logic levels for the other data inputs are chosen in a similar way. Depending on the desired truth table, some inputs are permanently connected to logic 0 , or to logic 1. The remaining data inputs will then be connected either to the logic level for the variable \(F\), or to its inverse, \(\bar{F}\). In this case, three of the inputs are connected to farmer ( \(\overline{\mathrm{F}}\) ). In two cases (data inputs 2 and 5 ), the output is 0 whichever side of the river the farmer is. This corresponds to the (safe) situation in which the fox and the corn are together without supervision on either side. Hence these two data inputs can be connected directly to 0-see Figs. 2 and 3.

\section*{CIRCUIT DIAGRAM}

The complete circuit diagram for the game is shown in Fig. 3. IC1 is a cmos integrated circuit, the 45128 -bit data selector. The s.p.d.t. switches, S3, S4, and S5, represent the hen, the corn, and the fox, and each can be switched to logic 1 or logic 0 , thereby providing the select inputs required by the data selector.

At the same time l.e.d.s are illuminated to indicate the current position: red on one side of the river, and green on the other. S2 represents the farmer and the logic level obtained is inverted by TR1 to provide the farmer variable connected to data inputs 3,6 , and 7 . The output, pin 14 of the data selector, drives the audible warning device, WD1, via TR2.

\section*{COMPDNENTS appoximatio Gust £13.50}


\section*{COMPONENTS}

\section*{Resistors}
\begin{tabular}{ll} 
R1,R2,R5 to & 750 (8 off) \\
R10 & \\
R3 & \(47 k\) \\
R4 & \(4 k 7\) \\
R11 & \(15 k\)
\end{tabular}

All \(\frac{1}{4}\) W carbon film \(\pm 5 \%\)

\section*{Capacitor}

C1
\(47 \mu 25 \mathrm{~V}\) elect. axial leads

\section*{Semiconductors}

D1,D3,D5, TIL 220 red l.e.d. D7 (4 off)
D2,D4,D6, TIL221 green l.e.d D8 (4 off)
TR1,TR2
BC108 silicon npn (2 off)
IC1 4512 cmos 8-bit data selector

\section*{See}

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\section*{Miscellaneous}

S1-S5
s.p.d.t. min. toggle ( 5 off)
WD1 p.c.b. audible
warning device
Printed circuit board: single sided size \(114 \times 60 \mathrm{~mm}\), available from the EE PCB Service (order code 8505-02), ABS box, \(150 \times 80 \times\) 50 mm , 16 pin d.i.I. socket, l.e.d. fixing clips ( 8 off), PP3 battery clip.


Fig. 4. Top, component layout for "Across the River". Above, actual-size p.c.b., available from the EE PCB Service, order code 8505-02.


The completed circuit removed from its case. Note that when completing the assembly of the unit, all components except the l.e.d.s should be soldered in position. The ABS case lid should have 13 quarter-inch holes drilled in it to match the positions of the switches and l.e.d.s, and one additional quarter-inch hole directly over the centre of the audible warning device WD1. The I.e.d.s should first be fixed by their clips in the case lid, and then their leads threaded through the appropriate holes in the p.c.b. Finally, the switches should be secured by their fixing nuts, and then the l.e.d.s soldered in position.


Use of the printed circuit board available for the project is strongly recommended. This has been designed to eliminate interwiring and simplifies construction considerably. Begin by soldering all the components, as shown in Fig. 4, with the exception of the eight l.e.d.s, which are kept separate until later. The five s.p.d.t. switches are mounted directly on the p.c.b. and care should be taken to fix them in an exactly vertical position: switches with pins spaced at 0.2 in . intervals are required.

The circuit should be tested at this stage by fitting IC1 in its socket and connecting a battery. Using S2, S3, S4, and S5, work through the complete truth table, checking that the audible warning device sounds whenever there is a 1 in the output column.

Next drill the lid of the case to accept the switches and the l.e.d.s. It is easiest to do this working in 0.1 in . intervals, corresponding to the spacing of components on the p.c.b. Lettering and decoration of the case are best done at this stage.

Complete the assembly by fixing the l.e.d.s in position in their clips on the lid of the case, and then threading their connecting leads into the appropriate holes in the p.c.b. Cutting one lead on each l.e.d. slightly shorter than the other will facilitate this operation. Tighten the nuts fixing the switches and finally solder the l.e.d.s in position. This method of assembly avoids strain on the p.c.b. and produces a neat overall effect.

Table 3: Move-by-move solution.
\begin{tabular}{|c|c|c|c|c|c|}
\hline move & Farmer & \begin{tabular}{c} 
hen \\
C
\end{tabular} & \begin{tabular}{c} 
corn \\
B
\end{tabular} & \begin{tabular}{c} 
fox \\
A
\end{tabular} & output \\
\hline 0 & 0 & 0 & 0 & 0 & 0 \\
1 & 1 & 1 & 0 & 0 & 0 \\
2 & 0 & 1 & 0 & 0 & 0 \\
3 & 1 & 1 & 1 & 0 & 0 \\
4 & 0 & 0 & 1 & 0 & 0 \\
5 & 1 & 0 & 1 & 1 & 0 \\
6 & 0 & 0 & 1 & 1 & 0 \\
7 & 1 & 1 & 1 & 1 & 0 \\
\hline
\end{tabular}

\section*{THE SOLUTION}

It is expected that constructors will discover the solution to the problem for themselves; for the record, the correct sequence of moves is given in truth table form in Table 3.

\title{
COMPUTERISED SHUTTER TIMER
}

\section*{R.A.PENFOLD}

Electronic shutter timers are much used by photographic magazines when preparing camera reviews, and are also a standard piece of test equipment in camera repair workshops. Such a unit would obviously be very useful for a camera enthusiast as well, but the cost of even a home constructed shutter timer would probably be prohibitively expensive for most camera owners. However, with the aid of a suitable home computer an accurate shutter timer can be produced for a very modest outlay, and all that is required is a simple optoelectronic interface plus suitable software.

\section*{BBC INTERFACE}

This shutter timer interface was built for use with a \(B B C\) model \(B\) microcomputer, and it connects to the user port of this machine. The user port is basically an 8-bit input/output port plus two handshake lines, and it is provided by port B of a 6522 VIA (Versatile Interface Adaptor). In addition to the ten input/output lines it has a serial shift register and two 16 -bit counter timers which can be accessed via certain of the lines. In this case it is the two timers that are of interest. These count down at a rate of 1 MHz , and therefore give a resolution of one microsecond. In practice the level of accuracy this would suggest is not usually achieved, and this application is no exception, but more than adequate accuracy to permit checking of shutter times from about \(1 / 1000\) th of a second to several seconds is obtained. The unit is powered from the user port of the computer and does not need any other power source.

\section*{VIC-20 INTERFACE}

The Commodore VIC-20 computer has a user port that is also provided by port B of a 6522 VIA, and which therefore offers virtually identical facilities to the equivalent port of the \(B B C\) machine. This timer interface has been tried with the VIC-20 and operates perfectly well with the computer, and software plus connection details for both computers are included in this article.

Of course, although intended for use as a shutter timer this interface and (or) the method of timing suggested in this article could be used in other applications that require accurate split-second timing. Possible applications range from an ultraaccurate lap timer for a slot-car race track, to scientific experiments in schools.

\section*{OPERATING PRINCIPLE}

Fig. 1 shows the system in block diagram form. The interface consists of just the light detector and trigger circuit, while the rest of the hardware is part of the computer.

The 1 MHz clock of the computer is applied to a 16-bit binary counter via some control logic. In practice the 16 -bit counter is possibly better regarded as two 8 -bit counters connected in series, since the 8 -bit data bus of the computer means that it is only possible to read or load one half of the counter at a time. It should perhaps be explained that although the BBC computer has a 2 MHz clock, this is divided by two to give a 1 MHz clock signal for input/output circuits, including the 6522 VIA. The clock frequency of the VIC-20 is actually marginally more than \(1 \mathrm{MHz}(1.08 \mathrm{MHz})\), and although we will ignore the small error this produces in this application, if required some mathematics in the software could be
used to correct it.
In the "free-running" mode the counter continuously counts down to zero, whereupon it is reloaded with the maximum value of 65535 and count down recommences. Software can be used to set the counter to any desired value and at any time. The most simple way of using the counter to time an external event is to use the two handshake lines of the user port (CB1 and CB2) as inputs to detect the beginning and end of the event. When the beginning is detected a short assembly language routine is used to load the counter with a value of 65535 , and when the end is detected the counters are read by another assembly language routine. Assembly language (or machine code in the case of the VIC-20) must be used as BASIC is far too slow for this application, and would produce hopelessly inaccurate results. Of course, the number read from the counter is not the answer in microseconds as the counter is a "down" type. However, simply deducting the number from 65535 effectively inverts the counter action and gives an answer in microseconds.

A problem with this basic arrangement is that a clock frequency of 1 MHz plus a maximum count of 65535 gives a maximum timing period of only about \(1 / 15\) th of a second. This is sufficiently long to cover most shutter speeds, but many

cameras these days have maximum shutter times of around one to four seconds. In order to accommodate longer shutter times one section of the other counter in the 6522 VIA is used to count the overflow pulses from the first timer. The first timer can provide an output on line PB7 of the user port, and this line is toggled each time the counter reaches zero. The other counter can count input pulses on line PB6, and can therefore count the overflow pulses of the first timer if lines PB6 and PB7 are linked.

By using just the least significant bit of the second timer the maximum shutter time that can be accommodated is boosted to just over half a minute, which should be more than adequate for the present application. By also using the most significant byte the maximum timing period could actually be boosted to more than an hour if required.

The interface to drive the two handshake lines is very simple, and it merely needs to provide a positive output pulse while the shutter is open. This is accomplished by positioning a photocell behind the shutter, and having a light source in front of the camera. The latter can be provided by a torch, or even just the light from a window will often suffice. The photocell provides an output pulse while the shutter is open and it is subjected to a higher light level, but this pulse must be processed by the trigger circuit to give an output that is compatible with the handshake inputs of the user port.

\section*{THE CIRCUIT}

Refer to Fig. 2 for the circuit diagram of the interface. The photocell is phototransistor TR1, and virtually any silicon photo-transistor can be used here. The unit was found to work well using types BPY62, TIL81, BPX25, BPX29, and even the Maplin "low cost phototransistor" gave good results. Other types of photocell are unlikely to give usable results. Cadminium sulphide photoresistors and photo-Darlington devices are likely to have inadequate response

Fig. 2. Circuit diagram


time, and a photo-diode would almost certainly have inadequate sensitivity.

In this circuit it is the collector to emitter leakage current of TR1 that is utilized, and the base terminal is left unconnected. This leakage current is very low under dark conditions, being typically about \(1 \mu \mathrm{~A}\), but it increases substantially as the light level received by the device is increased and can reach several milliamps. This results in a negative output pulse being generated from the pulse of light caused by the shutter operating. VRI enables the sensitivity of the circuit to be adjusted so that a wide range of ambient and light pulse levels can be accommodated.

IC1 is an operational amplifier which is connected as a straightforward Schmitt trigger having hysteresis provided by R4. This helps to give a "clean" output pulse which is free from noise spikes that could give spurious results. The trigger circuit is an inverting type so that the negative output from TR 1 gives the required positive output pulse from IC1. the use of a substitute for the CA3130E specified for IC1 is not recommended since few (if any) other devices would operate properly on the 5 volt supply from the user port, and would give a large enough output voltage swing to drive CB1 and CB2 of the port correctly. The CA3130E has a CMOS output stage which enables it to operate efficiently from a 5 V supply and to give a large output voltage swing.

When the output of ICI goes positive TR2 is switched on, and this in turn activates l.e.d. indicator D1. D1 plays no active role in the circuit, but is very helpful when setting up the system as it will flash on while the shutter is open if the equipment is set up correctly.

\section*{CONSTRUCTION}

Most of the components fit onto a small printed circuit board, as detailed in Fig. 3. The board is constructed using the normal techniques, but note that IC 1 is a MOS device and consequently requires the appropriate handling precautions. Fit this device in an 8 -pin d.i.1. i.c. socket, but do not fit it into place until the board and wiring have been completed. Leave it in its protective packaging until then, and handle the device as little as possible. Fit Veropins to the board at the places where connections to off-board components will be made.

Fig. 1. Block diagram

A plastic Verobox having dimensions of \(100 \times 50 \times 40\) millimetres makes a neat but tough housing for the unit. The board has been designed to fit onto the mounting pillars moulded into the base section of this case and suitable selftapping mounting screws are supplied with the case. The board could easily be mounted in another case though, by drilling four mounting holes at suitable positions on the rear panel of the case and using M3 or 6BA fixing screws. VR1 and Dl are mounted on the front panel of the case. TRI must be mounted off-board, and one way of arranging things would be to mount this component on the front panel of the unit. With the interface positioned behind the camera and the light source positioned in front it should then be possible to align things to give good results. An alternative method, and the one adopted for the prototype, is to fit a 3.5 mm jack socket on the front panel of the unit, and to then connect TR1 to the board via this and a screened lead about 0.5 metres long and terminated with a 3.5 mm jack plug. TR 1 can then be easily positioned for use with any camaera shutter or in-lens shutter.

The board connects to the computer by way of a four-way lead about 0.5 to 1 metre long, and an exit hole for this is drilled in one side of the case. Connection to the BBC computer requires a 20 -way IDC header socket, while a \(2 \times 12\)-way 0.156 inch pitch edge connector is required in the case of the VIC-20. In either case the terminals connecting to PB6 and PB7 must be linked. Connection details for both computers are provided in Fig. 5.

\section*{TIMERS}

Timer 1 is used as the 16 -bit counter fed from the machine clock, and this is controlled by bits 6 and 7 of the auxiliary control register at \&FE6B (37147 in the VIC-20). Both bits are set high to give the free running mode with output on PB7 enabled. Timer 2 provides the most significant byte, and this timer is controlled by bit 5 of the auxiliary control register. This bit is set high to give the mode where input pulses on PB6 are counted. Data is written to or read from timer 1 at \&FE64 and \&FE65 (37140 and 37141 for the VIC-20). The
equivalent addresses for timer 2 are \&FE68 and \&FE69 (37144 and 37145 for the VIC-20). Note that even though the high byte of timer 2 is not used, data must still be written to this byte in order to load the low byte (which is stored in the 6522 and loaded into the counter when the high byte is loaded).

The operating mode of CB1 and CB2 is controlled by the peripheral control register at \&FE6C (37148 in the VIC20). Bit 4 controls CB 1, and this bit is set high so that it is activated by a low to high transition (i.e. the leading edge of the signal from the interface). CB2 is controlled by bits 5 to 7, and of these only bit 5 is set high so that CB2 is activated by a high to low transition (i.e. the trailing edge of the pulse from the interface).

Active transitions on CB1 and CB2 set bits 4 and 3 respectively of the interrupt flag register at \&FE6D (37149 in the VIC-20). Writing a 1 to each of these bits resets them.

The basic action of the software must be to first set CB1, CB2, and the two timers in the correct modes. Then the program loops until the CBI flag is set, at which point the timers are loaded with the maximum values. The program then loops until the CB2 flag is set, after which the timers are immediately read and the figures obtained are stored in zero page addresses. The stored values are then processed and used to calculate the shutter time which is printed on-screen. After the CB1 and CB2 flags have been reset the program loops back to the point where the CB1 flag is monitored so that it is ready to take another timing. A slight improvement in timing accuracy might be obtained by disabling interrupts during each timing run, but this does not seem to be essential, and has not been included in the suggested software.

\section*{USING THE UNIT}

Suitable software for the BBC model B and VIC-20 computers is provided in the form of the accompanying listings. In order to use the unit as a shutter timer it is not necessary to understand the operation of the timers in detail, and even if you do not understand the explanation given above, it is merely necessary to load and run the appropriate program for your computer. There should be no difficulty in finding a suitable light source, and aligning the shutter and photocell with this source. Any torch will provide a suitable light, and the prototype equipment even worked properly just using the light from a window. It might be necessary to adjust VRI in order to obtain satisfactory results, and D1 (which should flash on when the shutter is open) helps to make setting up very much easier. D1 may not operate properly until the program is running and CBI/2 have been set to the correct operating mode. Until this is done DI will probably just light up continuously.


Fig. 3. P.c.b. track layout (actual size)


\section*{}

Approx. cost Guidance only
£14


Resistors
\begin{tabular}{ll} 
R1 & 1 k \\
R2, & 4 k 7 (2 off) \\
R4 & 39 k \\
R5 & 680 \\
All \(\frac{1}{4} W\) & carbon \(5 \%\)
\end{tabular}

Potentiometer
VR1 47k 1 in

page 312

\section*{Capacitor}

C1 \(100 \mu 10 \mathrm{~V}\) radial elect

\section*{Semiconductors}

IC1 CA3130E CMOS op amp
TR1 TIL81, BPY62, or similar npn photo-transistor
TR2 BC549
D1 TIL209 red panel l.e.d.
D2 BZY88C3VO 3 volt Zener diode

Miscellaneous
Plastic case about \(100 \times 50 \times\) 40 mm . Printed circuit board (available from EE PCB Service, order code 8506-021. 20-way IDC socket or \(2 \times 12\)-way 0.156 inch edge connector. Control knob. 8 pin di.i.t i.c. socket. Wire, solder, etc.

If the camera has an interchangeable lens it is probably best to remove it, but this is by no means essential, and the unit seems to function perfectly well with the lens in place, or even with a large format lens having a built-in (leaf type) shutter. Something that does seem to be important is to have the photocell as close to the shutter blades or curtains as possible. This helps to keep the ambient light received by the cell to a minimum. In practice there is usually no problem in opening the back of the camera and placing the photocell close to the shutter, although the exact set-up used will obviously depend on the type of camera concerned. However, with any camera great care not to damage the delicate shutter mechanism must be taken.

It is quite likely that the shutter speeds will show significant errors, but large errors are quite tolerable (a 10\% error is considered to be a commendable level of accuracy). In particular, with a focal


Fig. 5. BBC (upper) and VIC-20 (lower) connectors.
plane shutter and speeds of about \(1 / 500\) th to \(1 / 2000\) th of a second the measured shutter times are likely to be significantly longer than the nominal speeds. One reason for this is simply that most cameras (even expensive types) do not seem to achieve their shortest shutter times. Another reason is that the photocell is not monitoring a single point behind the shutter, but is monitoring a small area. Due to the way in which a focal plane shutter operates this tends to slightly stretch the shutter speeds, but only to a noticeable extent on the fastest speeds. This effect can be minimised by either masking off the front end of the photocell to reduce the sensitvie area, or by using about the lowest light level that will reliably trigger the interface.


\section*{VIC-20}

\footnotetext{
5 REM VIC SHUTTER TIMER
1O FOR M=6144 TO E137
20 READ \(v\)
39 POKE M, N
4 M NENT
5 DRTR \(169,16,44,29,145,240,251,169,255,141,24,145,141,25,145,: 41,29\)

76 DATA \(89,173,20,145,133,87,96\)
TS POKE 55, QIPOKE 56, 24
80 POKE 37147,224
ge FOKE 37148,48
1 106 FOKE 37143,24
110 Sis 6144
120 POKE 99,PEEK (S9) + (PEEK(89)-255)
130 R=PEEK ( 87 ) +255 *PEEK ( 88 ) +65535 *PEEK ( 89 )

150 PRIHT ME:" MILLISECONDE.
150 GOTO 10ด
}

3


\section*{by ithekeray}

thenso3gs
We areall familarwith the 'Abacus as being rows of baads sliding on medal rods but the ORIGINAL ADacus was a flat tray of sand. Marks weremade in the sand with a thin snarp sticle. (Abacus'strakenfrim the Greak mord'Abax
The'Abacus'as he Rnow it is still used todayand is considered by some to De faster than the modern computer for simple calculations.


\section*{Fown Capick}

Publication ofa work by John Napier in 1617 showed a method of multiplying and dividing by the use of"RODS" or "BONES"-combined with the use of onginol datatadies mares one of the historical contributionsto combeveritileyy
by mechanical means.


\section*{0; Sa, \\ Hins the Frenchman Baise} Pascal bull adicital calculating machine in \(1642^{6}\) to assist with his father's business accounts.
The machine was able to perform addition during which contisyanas


\begin{tabular}{|c|c|}
\hline & Werio \\
\hline & B－－C \\
\hline & ．E．．． \\
\hline & ．－cum＿ttation \\
\hline & D．－．L．D．C．G． \\
\hline & DE－－．．．－ \\
\hline & C．．．．．．\({ }^{\text {To }}\) \\
\hline & PA－ \\
\hline & FL． \\
\hline & M \\
\hline
\end{tabular}


＂Actually，this machine doesn＇t count for you but it does slap your hand if you get it wrons．


In1694 the German mathematician G．W．Leioniz completed the stepped Reckoner that could COUNT，MULTIPLY，DIVIDE and extra－ ct SQUARE ROOTS．
The major contribution was how he showed the advantages of binary over the decimal system for mecha－ nicalcomputers．I wonder if he rea－ lized that the binary system would be used today．

The software for＂Seekers Of The Gold Seal＂is continued from the last Computer Club below．
S3ODEFFROCar \(W \%=n \%\) ：Q\％：T\％＝W\％DIV19：IFV\％＝2 V\％＝SGN（T\％－N\％DIV19）+242
540 IFV \(=1\) T \(\%=W \%-T \% * 19: W \%=N \% D V 15: V \%=S G N(N \%-W \% * 18-T \%)+245\) 5SOPFDCWr：ENDPROC
560DEFFROCtw（H\％）UDU4， \(28,0,31,19,28:\) COLOUR \(131:\) CLS：COLOUR129：COLOURH\％：ENDFFOC
 5BjDEFFNSV：\((X \%, C \%, F \%, F \%)\) LOCALY\％：T \(\%=0\)
590 FORX\％＝X\％TOC\％STEPB：FORY\％＝F\％TOR\％STEF4：V\％＝FNpt： \(1 F V \mathrm{~F} \% \mathrm{~T} \%=\mathrm{V} \%\)
GOONEXT ：NEXT：\(=\mathrm{T} \%\)
S1ODEFFROCSE PROChd
 8BOO： \(6 \%=\%\) E 20
ozoDATAGloom．Towers．Bat．Crat，Arches，Zeen，Soram，Flent，Hidden ，Arrowed，Sealed＂S 1ipped，Fallen！．＂Empty＂

G5ODATA1，5，9，15．21，17．25
6́0 FFOCz 5 FOFF\％＝1 TO7：READG\％？P\％：NEXT
 680 FOF \(5 \%=0\) TO4：T戠＝＂＂：W＝＂
G9OREFEATFORQ\％＝1 TQS：IFQ\％＝2T \(\%=G \%\) ？RND（5）EL．SET \(\%=F F N a\)
700 IFQ\％＜\({ }^{2}\) 2ANDFND（5）＜2THEN720

720 NEXT：UNTILLENT＊＞2：K \(⿻=\)

74OREFEEATH韦 \((S \%)=H *(S \%)+M I D+(T ⿻ 三 丨\)

760 VDU \(23,252,0 ; 0,124,61438 ; 71,23,253,64,64,64,120,60540 ; 196 ; 25,254,0 ; 0 ; 0,16,56\) \(, 16,23,255,2,7,2,3,1,0,23,239,26,58,107,75,72,72,216,23,240,0: 24,126,24,24,24,25\)
4
770 VDU23， \(246,8,24,26417: 49,24,8,23,245,0,17022,66,66,66,126,23,244,16,24,59020\) \(; 140,24,16 ; 23,243,16,56,50796 ; 16,16,124 ; 23,242,0,17022 ; 66,66,66,126: 23,241,4220 ;\) 16．27846：56．16；

780 VDU23， 238,\(65535 ; 65535 ; 65535 ; 65535 ; 23,237,60,50022 ; 56319 ; 39321 ; 153,23,236,36\) ， \(50022 ; 66,231,189,153 ; 23,235,126,90,65499 ; 65535 ; 48615 ; 23,234,130,43670 ; 65278 ; 238\) ，238；23，233，65278；27756；254，238，238；


81 ODATA \(18,0,1,252,253,8,8,18,0,2,254,254,8,8,18,0,3,255,5,7,12,9,14\)
82OFORF \％＝ 1 TOS：READE \(\%\) ？P\％：NEXT
BSOREPEATT \(\%=0: 5 \%=0: 0 \%=5500:\) FROCC
84OREFEAT \(5 \%=5 \%+1\) ：IFS \(\%=5 \quad 0 \%=2700\)
85OFEFEATPFOCe ：\(V \%=1\) ：FOFP \(\%=0\) TOS \(\%-1\)
\(860 \mathrm{~V} \%=\mathrm{ABS}(x \%\) ？ \(5 \%-x \% ? P \%): W \%=A B S(y \% ? S \%-V \% ? P \%): I F V \% * V \%+W \% * W \%<2 \% \quad V \%=0\)
870 NEXT：\(T \%=T \%+1\) ：UNTIL \(Y \%=1\) ORT \(\%=300:\) UNTIL \(5 \%=7\) ORT \(\%=300\)
日80 IFT\％＝300 UNTILFALSE ELSEUNTILTRUE
890FEFEATPFIMTTAB（0．20）＂Mappings in Frogress＂：FROCl（404）
900 PFOC \(=G \%\) ？ \(0=127: G \%\) ？ \(1=153: G \% ? 2=231: G \% ? J=255: I \%=10: M \%=40: N \%=9: 5 \%=0\)
910 FEEPEATI \(\%(5 \%)=I \%:\) IFS \(\%=5 \quad \mathrm{M} \%=32: \mathrm{N} \%=5\)
\(920 x \%=27+F N D(3): Y \%=19+F(N D(4):\) PROCIn \((M \%)\) ：PRDCin \((N \%)\) ：FROCin \((X \%)\)
\(930 \mathrm{~T} \%=1 \%: I \%=I \%+1: W \%=0\) ：REFEATW\％＝W\％＋FND（54）
940 FROCin（ \((x \%-\) RND（ 7 ））＊COSRADW\％）：PROCin（Y\％＊SINRADW\％）

960 FORP \(\%=0\) TO4：REFEAT：T\％＝RND（64）：UNTILG\％？（T\％＋3）\(>1: \mathbf{G} \%\) ？\((T \%+3)=1\)
970 FORQ \(\%=0\) TO2：\(W \%=G \%\) ？（T \(\%\) MOD 4 ）：PROCin \((W \%): T \%=T \% D I V 4\) ：NEXT \(:\) NEXT： \(5 \%=5 \%+1\) \＆URIT ILS \(\%=\)
98OIFI\％＞380 UNTILFALSE ELSEUNTILTFUE
990 FROC \(5 t(0): \mathrm{C} \%=8: \mathrm{F} \%=128: \mathrm{a} \%=1\) ：FROCgt（उO）：ENDFROC
100ODEFFROCz FOFP\％＝0TO246：G\％？P\％＝255：NEXT：ENDPFOC
\(1010 D E F F N a\) LOCALO\％：REPEATT \(\%=\) RND \((25): W \%=1:\) FORG \(\%=2 \quad\) TO7：IFT \(\%=G \% ? 0 \% \quad W \%=0\)
1020 NEXT：UNTILW\％＝1：＝T\％
1030 DEFFROCg （T\％）FFOCer（O）：＊FX15．1
1040 IFT\％＝30 PROCl（96）
1050 PRINTTAE（1．T\％）＂press bar to play＂：K\％＝GET：ENDFFOC
106ODEFPFOCC \(x \% ? 5 \%:=28+R N D(203): v \% ? 5 \%=55+F N D(163)\) ：ENDFFROC
107ODEFPROCin \((V \%) \quad D \%\) ？ \(1 \%=A B S V \%-128 *(V \% 60): I \%=I \%+1\) ：ENDFFGC
 the Seal＂：FROCl（912）：ENDFROC
1090DEFFFROCtab LDCALS\％，V\％：FROChd
1100 COLOUFi 132 ：COLOUR2：FRINTTAB \((1,5)\)＂KEY．TEMFLE Find＂：\(Y \%=6: F O R S \%=0\) TO4 \(=Y \%=Y\) \(\%+2\)
1110 FRINTTAB（1，Y\％）C \((5 \%\) ）TAB（ \(10-L E N N *(5 \%) / 2, Y \%)\) N本（S\％）：FFOCL（19）：NEXT
1120 FRDC1（448）：COLOUR128：COLOURG：FFINTTAB（2．18）＂TOMBS Find＂： \(\mathrm{Y} \%=22:\) FORS\％ \(=5107\)
 1140DEFFROCVI
1150 PROCV19（0，1）：PFOCV19（1，2）：PROCV19（2，4）：FOFP\％＝4 TO15：FROCV19（F\％．1）：NEXT
1160 CDLOUF128：CLG：F\％＝O：FDFS\％＝0 TO7： 1 FL \(\%\) ： \(5 \%\) PROCGrd \((S \%+4,1): F \%=F \%+1\)
1.170 MEXT：VDU24，8；128： \(1271 ; 1023 ;: K \%=8: 0 \%=104: \times \%=C \%: Y \%=F \%\) ：PROCshft（E \(\$\) ，J\＃）：ENDFFO

\section*{T. R. de Vaux Balbirnie}

ALthough portable equipment is useful to take on a caravanning holiday, it proves expensive on batteries. Assuming the caravan has a 12 -volt system supplied by either an independent car battery or through a hook-up lead from the towing vehicle, items such as radios. cassette recorders. games and keyboard musical instruments may be operated at practically no cost.

This project accepts a nominal 12 V input and supplies a regulated \(6 \mathrm{~V}, 7.5 \mathrm{~V}\) or 9 V output at up to 300 mA . This suits a wide variety of battery powered equipment. Precision resistors are used to preset the output voltages so it is not necessary to have a volt meter available at the testing stage.

Special features of this circuit are switched polarity reversal of the output leads and the ability to make input connections either way to the supply. This is useful where the caravan is fitted with non-polarised sockets, or where battery clips are to be used.

Examine each piece of equipment to be powered by the unit. Check that it requires one of the above input voltages, and that it is fitted with a d.c. power-in socket. Such sockets are usually used for connecting mains operated power supplies. Although some items are fitted with 2.1 mm or 2.5 mm connectors, or 2.5 mm or 3.5 mm jack sockets. DIN or other types of socket may be found. If no such d.c. input socket is fitted it will be necessary to make direct connections in the battery compartment and the feasibility of this should be investigated before proceeding.

\section*{CIRCUIT DESCRIPTION}

The circuit for the Caravan Power Supply unit is shown in Fig. 1. With S1 on. current flows through FSI to the bridge rectifier RECI. Whatever the polarity of the input connections, the bridge rectifier will direct current correctly to the rest of the circuit-that is, with the positive and negative as shown. D1, a light emitting diode with current limiting resistor RI shows that the circuit is switched on. 1 CI is a voltage regulator which gives a steady output voltage whose value depends on R2 in conjunction with either R3(9V). R3+R4 (7.5V) or \(\mathrm{R} 3+\mathrm{R} 4+\mathrm{R} 5\) (for 6 V ) as selected by the 3-position switch S 2 . S 3 sets the out-
put polarity. When switched the opposite way to that indicated in the diagram the output leads will assume opposite polarity.

\section*{VOLTAGES}

The output voltages are preset to approximately \(90-95 \%\) of their nominal values. This allows for the precision resistors R2. R3. R4 and R5 being at the extremes of their tolerance, and for the fact that even a new battery does not produce its nominal voltage on account of its internal resistance. In the prototype, the voltages were \(8 \cdot 2 \mathrm{~V}, 7 \cdot 1 \mathrm{~V}\) and 5.7 V for \(9 \mathrm{~V}, 7.5 \mathrm{~V}\) and 6 V settings respectively. Tests with several pieces of portable equipment proved these to be entirely satisfactory. It will be noted that the higher the resistance between the adjustment and output pins of IC1, the lower will be the output voltage. This particular arrangement of R3. R4 and R5 was chosen so that the circuit defaults to a low output voltage in the event of \(S 2\) failing to make proper contact or wires detaching from its terminals.

Operates battery-powered equipment from a 12 V supply


\section*{CONSTRUCTION}

Since most of the circuitry is already inside IC 1 , construction is made very straightforward. Due to variations in size in components of the same specification, readers are advised to check their layout before buying the case. The prototype was made to take up as little space as possible but some readers will wish to use a larger box to give more working room.

IC I becomes warm in use so must be mounted on an aluminium panel which acts as a heat sink. Begin by cutting this part from thin aluminium sheet to fit tightly in the runners of the case. Its width should be 4 mm less than the height of the box to allow connecting wires to pass over the top. Cut short the centre connection and bend the tab of IC1 so that this component will lie flat on the panel. Drill a small hole and attach it using a small fixing. Note the solder tag which is secured under the nut. Cut the tag panel to fit the runners of the case tightly-there must be at least 10 tags available in two rows. Refer to Fig. 2, and solder the components in position noting the polarity of C1. It is essential to use only high quality close-tolerance resistors for R2-R5 as specified in the components list. Neglecting this could possibly result in output voltages which are too high. Prepare the case by making holes for the switches, l.e.d. indicator, fuse holder and the input and output leads. Mount the offboard components noting that it helps to place some packing under S2 and S3 to level the slides with the face of the case. This will make accidental operation less likely. Refer to Fig. 2 and complete all wiring. Take care over the connections to S2 and S3 so that the output voltages and polarity are predictable. Although \(\mathbf{S} 2\) is a 4 -pole switch only one pole is used in this circuit. Note that the connections between the adjustment pin of IC 1 and R2, and between R2 and the negative supply line demand special care. WARNING: If any of these should become detached, the output voltage will rise to the full 12 V of the supply with possible damage to external equipment.

Tape a piece of thin cardboard to the back of the tagboard to provide insulation. Insulate any other exposed connections where they could short-circuit to the metalwork. Use 3A 2-core mains wire for the input and output leads and tie string tightly around each on the inside of the

case to provide strain relief. Slit a piece of scrap insulation along its length and use it to protect the top edge of the aluminium panel. Fit appropriate connectors to the input and output leads. In the prototype, a 4 -way Universal Connector was used for the output.

\section*{TESTING}

Although not essential, some readers may wish to use a multitester to check the polarity and output voltages. A simpler test can be made with a small 12 V bulb. Connect this to the output lead, adjust S2 to 6 V , connect the supply and switch on. The l.e.d. should light and the test bulb glow dimly. At 7.5 V and 9 V settings it should increase in brightness but never become as bright as it does when connected directly to the 12 V supply. If there is any doubt about the polarity of the output wires, check by connecting a diode in series with the test bulb (Fig. 3). With the diode connected as shown the test bulb should light.

Fig. 1. Circuit diagram.

It only remains to label the switches and to check that they cannot be operated accidentally. Where young children are present it would be a wise precaution to tape over S2 and S3 since a higher voltage than that required, or switching to the wrong polarity could damage equipment.

\section*{USING THE UNIT}

Before connecting a particular piece of equipment to the power supply, determine the operating voltage and polarity. Do not use trial and error. Always switch of SI when the unit is not actually being used since it draws a small current (about 20 mA ) even with nothing connected to the output. Switch off also before changing the settings of S2 or S3. Note that it is normal for the case to become slightly warm in operation.

Fig. 2. Tag-board layout and wiring.

[EE148


Fig. 3. Polarity tester.

\section*{COMPONENTS}

\section*{See
S201 \\ page 312}

\section*{Resistors}
\begin{tabular}{ll} 
R1 & 680 \\
R2 & \(1 k\) \\
R3 & 180 \\
R4 & 36 \\
R5 & 68
\end{tabular}

All resistors 0.4 W metal film \(\pm\)
\(1 \%\) (R1 may be \(\frac{1}{4} \mathrm{~W}\) carbon \(\pm 5 \%\) )

\section*{Capacitors}

C1 \(1 \mu 15 \mathrm{~V}\) electrolytic

\section*{Semiconductors}

IC1 317 M voltage regulator
REC1 W005 50V 1 A bridge rectifier
D1 TIL220 5 mm redi.e.d. with panel mounting clip

\section*{Miscellaneous}

S1 miniature SPST rocker switch
S2 miniature 4P3W slide switch (Maplins 4-pole slide switch
S3 miniature DPDT slide switch
FS1 500 mA fuse and fuseholder to suit

Sub-miniature tag board; Plastic box (see text); 3A mains type twin wire; Aluminium panei; Universal power-in connector, plugs and sockets for input and output leads as required; Fixings; Solder tag.

Approx. cost Guidance only \(\mathbf{£ 8 . 0 0}\)

\section*{New Laboratories for Graduates}

Opening the new Advanced Telecommunications Laboratories in the Department of Electrical and Electronic Engineering at Queen Mary College, University of London, Dr John Alvey CB FEng, Engineer-in-Chief British Telecom offered his congratulations to the Principal, Sir James Menter, FRS, on the College initiative in setting up the laboratories.

In his speech Dr Alvey referred to the increasing shortfall in the number of graduates being produced to meet the needs of the Electronics and Telecommunications Industries and spoke of the facilities at Queen Mary College as being just the sort required to provide graduates with the skills they will need to help British industry establish a leading role in the many aspects of Information Technology. These facilities are probably unique in the UK and establish the Department of Electrical and Electronic Engineering as one of the leading departments in the country.

He particularly appreciated the combination of technologies provided for undergraduates within the Department. For instance, the VLSI Design Laboratory which gives students the opportunity to design on silicon and see some of their integrated circuits made and tested. Also the provision of a range of real telecommunications systems throughout the laboratories to enable undergraduate students to experience the application of the principles they have learnt on real systems.


Dr Alvey speaking to Mr Lomer, Technical Director Racal Electronics, over the digital telephone system built by a third-year project student.

Welcoming the guests, the Head of Department, Prof. Peter Clarricoats, FEng, explained that whilst the visit was primarily concerned with undergraduate activities, the Department played a leading role in research. The current value of grants held by the Department is almost one million pounds.

\section*{COMPETITION}
 FOR BIRDBRAINS

The advance of migrant birds across the British Isles as shown on BBC Telesoftware's high resolution maps.

27th March 1985


\(Y\)OUNG computer enthusiasts have a chance to win a microcomputer and help scientific research in a new competition launched by BBC CEEFAX and the Young Ornithologists' Club (YOC) of the Royal Society for the Protection of Birds.

The latest data on the spring migration of birds arriving in Britain is being collected by members of the YOC, who are reporting the first sightings of spring migrants throughout the country. BBC CEEFAX is displaying maps and information to show how birds are travelling across the country, on page 295 on BBC 2. More detalled information is also being transmitted through the BBC CEEFAX Telesoftware Service, which will be updated weekly until the end of this month (May).

The competition winner will be the person who makes the most imaginative and innovative use of the data transmitted by Telesoftware. The programs based on the Telesoftware data will be judged in September, and the winner will receive a BBC Micromputer; three runners-up will receive Electron Microcomputers, and there will be consolation prizes of binoculars.

\section*{ALL AT SEA}

Questions and answers will be bouncing back and forth across the Atlantic by satellite as The Times Network for Schools puts UK schools in direct touch with the Operation Raleigh flagship, sailing off the coast of Panama.

The Sir Walter Raleigh is at present in the Caribbean, acting as a base for extensive community work and diving exploration and in the cause of conservation. TTNS's representative Lakh Singh, has just joined the ship and will be sending twice-weekly bulletins to the schools network via the satellite link.

Schools in the UK will be able to ask Lakh specific questions on projects they are undertaking and he will reply via the Network. A team of scientists will also be using the Sir Walter Raleigh as a base.

This will provide schools with immediate access to new research information and the opportunity to question scientists as they carry out their work in the field.

Oil and gas production platforms in the North Sea will have their own satellite communications system next year. The system will be called SatStream Offshore and contracts for the provision of a permanent service to a floating production platform in June ' 86 have been signed by British Telecom and the North Sea Sun Oil Company.

A new satellite earth station near Aberdeen, using an 8 m ( 26 ft ) diameter dish, is to be built by British Telecom.

This earth station will work to the European Communications Satellite, EUTELSAT 1-F2. It will offer satelite facilities to platforms in any part of the UK's offshore exploration areas.

Philips is to supply 115 million Guilders worth of colour television sets to the People's Republic of China. The contract was signed by the Consumer Electronics Division and a Chinese Purchasing Delegation.

\section*{lectronics}

\section*{AGREEMENT ON EDUCATION}

THE City and Guilds of London Institute (CGLI) and the Scottish Vocational Education Council (SCOTVEC) have announced that they have reached agreement on the terms of a formal Memorandum of Agreement covering the establishment of equivalences between particular certificates awarded by the CGLI and particular modular programmes of study, leading to the award of the SCOTVEC National Certificate.

Announcing the agreement Mr. H. M. Neal, Chairman of CGLI, and Dr Peter Clarke, Chairman of SCOTVEC, made the following observations:
"The agreement provides the framework of procedures within which individual equivalences can be established and detailed work has now begun on taking these matters forward.
"The new agreement has been reached after careful and detailed discussions. We believe it will be mutually advantageous to both parties in assisting the establishment of the new SCOTVEC National Certificate and in making a major contribution towards the success of the 16 -plus Development Programme being implemented in Scotland."

\section*{OFFSHORE DEAL}

Thorn EMI Electronics has been awarded a contract by Humphreys and Glasgow on behalf of Britoil, to supply a sophisticated environmental monitoring system for the Britoil Clyde field.

The microcomputer-based equipment will display all the current weather information on a number of VDUs situated in various parts of the platform. Displays can be modified 10 include special customer requirements or any new legislation that might arise; further sensors can also be added if required.

The monitoring system, which can be linked to a telemetry facility and interrogated at inter. vals, can also be connected to a tape recorder or other data logging system to provide a permanent record. A part from the sensors it is claimed that the system reguires no maintenance.

\section*{MICRO TRENDS}

Barely two thirds of UK micro suppliers have been in the market for more than a year and nearly a third are likely to withdraw before the year is out. This is one of the more startling conclusions which can be drawn from the third NCC Microsystems Centre's survey of the UK micromarket.

This survey is based on the files used to support the NCC Microsystems Directories of Hardware, Software and Training. These files are updated daily as new products are identified and old ones withdrawin, or suppliers go out of business and noone is willing to take over the product.

Of the 629 hardware suppliers known to be active in the UK market as at March 1st, only 386 (61 per cent) had been identified as at September 1 (when the first NCC-computing survey was drawn up). However, of those active in September, 65 (14 per cent) have since withdrawnimplying an annual rate of nearly 30 per cent. Part of the reason for the rate of entry is that over twothirds of the products on sale are imported and many new suppliers are merely agents for American organisations (over half of all systems) or Japanese (who dominate the market for most types of peripheral).

Under the terms of a deal worth \(£ \frac{1}{2} \mathrm{M}\), Microvitec will manufacture switched mode power supplies and colour monitors for the RM Nimbus computer which was launched recently by Research Machines.

A graphics utility package for the Amstrad CPC464 is the latest software release from Kuma.

Entitled "Artwork" (£9.95), it enables the user to draw pictures and includes the facility for circle, ellipse, line and box drawing
and allows full use of available screen modes and colours.

Options for fast colour fill and complete screen scroll in all directions are included, plus the ability to load and save completed pictures to either tape or disc.

\section*{MOBILE REPAIR SERVICE}

THORN EMI Electronics have recently received an \(£ 18 \mathrm{M}\) contract from the British Army for the supply of a number of its general purpose thermal imager repair facilities (GPTIRF).
The GPTIRF will allow the British Army to test and repair complex thermal imaging equipment in the field and in base workshops rather than returning the equipment to civilian contractors.
The contract, which was secured by the company's Electro Optics Division, is the the third major contract for thermal imagers and associated equipments to be awarded by the MOD to THORN EMI Electronics in the last eighteen months.


Pictured here (top) is an interior view of the GPTIRF container body, showing a thermal imager being tested on the optical test bench, and (bottom) an exterior view of the vehicle with a towed generator altached.

\section*{MICROCOMPUTERS AND THEIR INTERFACING}

\author{
Author R. C. Holland \\ Price £6.95 Flexicover, £15 Hardcover \\ Size \(\quad 210 \times 147 \mathrm{~mm} .193\) pages \\ Publisher Pergamon Press \\ ISBN 0080311253 (Pbk.)
}

THERE is no shortage of books on this subject, but Microcomputers and their Interfacing is not an unwelcome addition.

When choosing a book on this topic, an important criterion (apart from cost) is likely to be the particular microprocessor that the author has used for explanation and examples. For although the various different 8 -bit microprocessors have much in common, their differences are particularly evident when it comes to interfacing, and real-time control applications using assembly-language. Mr Holland uses chiefly the 8085 and the related \(\mathbf{Z} 80\) chip for his examples, and this is a fair choice, as they are the most popular 8-bit microprocessors for industrial use and personal computers, respectively.

The opening chapters are given over to fundamentalsbinary and hexadecimal arithmetic, logic, CPU architecture and memory organisation. This approach is common, but ought by now to be assumed prior knowledge, especially for a book concerned primarily with interfacing, rather than the fundamentals of microprocessor design. It would have been better to have devoted this space to the hardware of standard programmable and non-programmable I/O devices, establishing the distinction between memory-mapped and isolated I/O.

Following his introductory chapters, Mr Holland covers, in a very general way, standard methods for interfacing microprocessors to the outside world, using both digital and analog techniques. This is well-presented, and a useful and comprehensive summary. The section on 'Special Peripherals' will be of widespread interest, as floppy discs, keyboards, and VDUs are the media used by the majority of people for communicating with their CPUs. The hardware is shown in block-diagram form, which is appropriate to the approach taken in the text-widely applicable principles rather than specific instances-and makes for clarity.

The chapter on high- and low-level languages is ill-considered; it is probably impenetrable to those not already familiar with the use of different languages, and different assemblers and compilers, and of little value to those who are.

For the engineer who wants to know how to use his microprocessor to monitor and control external events, the final chapters are those of real interest: the 8085, Z80, and 9980 each have their own section. This is very useful, and although the manufacturers' own literature would still need to be consulted in order to implement a real system, their data sheets can be cursory or confusing to the novice. Mr Holland provides a beneficial service in explaining the function of control and timer registers, publishing full instruction sets, and giving examples. Also valuable are the explanations of the user ports on the Apple II and BBC computers, again with examples.

This book will no doubt find its way into college libraries and onto the bookshelves of many students and engineers. But as Mr Holland himself indicates by his (excellent) bibliography, he is up against stiff competition.
D. A. B.

\section*{EXPERIMENTS WITH YOUR COMPUTER}
\begin{tabular}{ll} 
Author & Helen Davies \\
Price & \(£ 4.50\) hardback, \(£ 2.25\) paperback \\
Size & \(240 \times 170 \mathrm{~mm} .48\) pages \\
Publisher & Usborne Publishing Ltd \\
ISBN & 0860207919
\end{tabular}

HJow can a computer be educationally useful? One approach is to make use of the speed and graphics capabilities of the computer to model real situations, using well-established mathematical modelling techniques. These techniques can be used for the optimisation of transportation systems, for example, or for investigations into rocket flight, population growth, or the national economy.

The reason that the computer is invaluable for such investigations is two-fold. Realistic models require hundreds (or thousands) of recalculations as parameters are varied in order to give a useful result; and the results are best displayed graphically. Both these tasks are ideally suited to a computer's capabilities. Once the analytical and the graphics programs are stored, parameters can be changed, and a new display obtained, saving hours of time and eliminating mistakes in recalculation.

A related area in which a computer is invaluable is the analysis of data. Are events positively or inversely correlated? At what level are test results statistically significant? What is an "average" result? The problem with all this is that the mathematics involved is not trivial, and the programs can be tricky to write properly. The solution is Experiments With Your Computer. This splendid book has listings for investigations into the effects of gravity on different planets, simple transportation problems, and an excellent "Running an Airline" model. The calculations are (rightly) presented in the body of the programs without comment. This means that the situations can be investigated immediately, while those who have the inclination can follow up the mathematics if or when they wish.

There are also some elementary but useful ideas for using thermistors and light-dependent resistors to directly monitor real-world conditions. The hardware involved here is minimal, and the interfacing instructions are clear and unfussy.

This is the way books for computer users ought to be written. No specialist prior knowledge is necessary; the machine's capabilities are properly exploited to allow real-life investigations. For young children, the presentation is so good that it will be possible to work from the text with minimal supervision; for older children (and adults) it is an invaluable springboard for further development of ideas.
D.A.B.

\section*{MICROMANIA}
\begin{tabular}{ll} 
Author & Charles Platt \\
Price & \(£ 7.95\) Hardback \\
Size & \(235 \times 142 \mathrm{~mm} .184\) Pages \\
Publisher & Victor Gollancz \\
ISBN & 057503419 X
\end{tabular}

THIS is an excellent book, because the author fully achieves his purpose, namely, to remove the mystique surrounding the Home Computer. A "Micromaniac" himself, he skilfully pilots us through the maze of Hardware, Software and Buzz Words. He sums up the good points and the bad points of most of the well known makes of Home Computers and he pulls no punches. He even evaluates the many and varied Computer Magazines. It is not written for the expert, but for those who don't know a "Bit" from a "Byte" or a "Dot" from a "Daisy Wheel", and although after reading it, you won't be an expert on "Boolean Algebra", you will at least know how the Binary Code works. It is a "Must" for beginners, and they should not venture within ten miles of a computer shop before reading it.

Illustrated with an abundance of helpful diagrams and amusing cartoons, the author adds just that touch of humour which makes the book a pleasure to read.
A.S.


The Amstrad CPC464 computer has proved reasonable cost and with a minimum of hardware.


All model train enthusiasts will want to build this signal controller. The red signal stops a train from entering a zone in which there is already another train. When the line is clear, the signal changes to green and the train can move.

\section*{Actrally doing it!}

Spread out before you are the following items: One magazine constructional article, a selection of small tools, a soldering iron and reel of solder, a p.c.b. and packets of electronic components. What do you do next? If you are a beginner, the answer is simple. Read this new regular column.



ATRANSISTOR is a cleverly-processed bit of semiconductor material. To make use of it, the engineer needs to know how it behaves electrically. This entails inventing an equivalent circuit, in which the electrical activity of the device is represented by an assembly of familiar elements.

\section*{ACTIVE DEVICES}

Transistors are active devices. This means that in order to describe how they work, any circuit which serves as a model must contain a generator of some kind. The rest can then be made up of passive elements: resistors, capacitors, etc.

Note that I'm talking about a model for what goes on inside the transistor, not a complete circuit with external elements such as collector loads and base bias resistances. That comes later.

There are two kinds of models. One is concerned with the d.c. conditions in which the transistor operates. The other kind assumes that the d.c. operating conditions are satisfactory and deals only with small a.c. signals. Small means not so large that the signals interfere with the d.c. conditions.

Assuming that the transistor is operating in the common-emitter configuration (i.e. with the emitter earthed or common to both input and output) the simplest a.c. equivalent circuit is shown in Fig. 1. Here the input impedance of the device is modelled by resistance \(R\). When an input current flows (between base, b, and emitter e), this causes a corresponding collector current to flow. Because the device amplifies, this collector current is greater than the base current. The amount by which it is greater is called the current amplification factor. It is typically 100, but very variable. For small (a.c.) signals, this number is given the symbol hfe.

If the polarity of the signal is such that current flows into the base, then amplified current flows into the collector. Of course, a.c. signals alternate between inwards and outwards, but for convenience it is usual to consider only one polarity at a time:

\section*{MICROPHONE AMPLIFIER}

Now let's use the model in a practical situation and see (Fig. 2) what happens. Suppose we have a microphone whose internal impedance is \(500 \Omega\) and which produces an audio signal of 3 mV . We connect this to a transistor whose input resistance \(R\) is 2.5 k . (Never mind how we know this, for now.) The transistor is given a collector load of 10 k , so the current generator is driving current through 10k. If hfe \(=100\) this current is 100 times the base current.

What's the base current? By inspecting Fig. 2 it is clear that the microphone's 3 mV must drive current through its own impedance ( \(500 \Omega\) ) and \(R\) in series. We have 3 mV and 3 k . This gives a base current, ib, of \(1 \mu \mathrm{~A}\). The collector current is therefore \(100 \mu \mathrm{~A}(0.1 \mathrm{~mA})\). In flowing through the 10 k load this sets up a voltage of 1 V \((1000 \mathrm{mV})\). The voltage gain, overall, is \(1000 / 3=333\).


\section*{CLOSER TO REALITY}

Our model has told us the voltage gain, but of course it is not a full working circuit, with d.c. supplies, input and output coupling capacitors and so on. Never mind. It has in fact already given a vital pointer to the d.c. conditions needed. If the a.c. collector current is \(100 \mu \mathrm{~A}\) then in order that the a.c. will not interfere with the d.c., the d.c. collector current must be more than \(100 \mu \mathrm{~A}\). How much more depends on commonsense considerations.

If the microphone gives out 3 mV on an average sound, what will it give on a loud one? Maybe 10 times as much. So to handle the loudest sounds the collector current must be at least ten times \(100 \mu \mathrm{~A}\), i.e. \(1000 \mu \mathrm{~A}\) or 1 mA . We have selected one d.c. operating condition already!

\section*{INPUT IMPEDANCE}

The input impedance of a transistor can be estimated. At audio frequencies, and with small d.c. collector currents, the common-emitter input resistance is approximately:
\[
\left(\frac{\text { hfe } \times 25}{\text { lc }(\mathrm{mA})}\right) \text { ohms. }
\]

In our case we have selected \(\mathrm{Ic}=1 \mathrm{~mA}\), and our transistor's hfe \(=100\). So the input resistance is roughly \(25 \times 100 / 1=2500 \Omega\), or 2.5 k , which is the value actually given

All very well, but hfe is a very variable quantity, even among nominally identical transistors. What if our particular specimen had hfe \(=200\) ?

Let's see. The input resistance would then be \(25 \times 200 / 1=5000 \Omega(5 k)\). With the microphone's \(500 \Omega\), the 3 mV signal now sees a total of \(5 \cdot 5 \mathrm{k}\). The base current reduces to \(3 / 5.5 \mu \mathrm{~A}=0.545 \mu \mathrm{~A}\). This is now amplified by hfe \(=200\), giving ic \(=\) \(109 \mu \mathrm{~A}\). This is 9 per cent more than before so the gain and output increase by a mere 9 per cent even though hfe has doubled.

Inspection of the diagrams shows why. Since the microphone impedance is small compared with \(R\), in effect \(R\) controls the input current. As hfe increases, \(R\) also increases, reducing the input current in such a way as to keep the output current fairly constant.

\section*{SUPPLY VOLTAGE}

With a d.c. collector load of 10 k and current of 1 mA the load drops 10 V . The collector voltage must be more than this: it must be able to deliver the required output voltage. Suppose the amplifier drives a mixer whose input impedance is 10k. The amplifier "sees" 5 k -the load resistance and mixer impedance in parallel. With a "loudest sound" microphone output, the output voltage into 5 k (RL and the mixer) is 5 V . So the d.c. supply must be at least 15 V . If the microphone output is in r.m.s. volts rather than peak volts the peak output will be much more than 5 V , so the supply voltage must be increased further. A fairly common voltage is 20V: you can see why.

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\(\mathrm{N}_{\mathrm{t}}\)o, this is not an article about various types of housing accommodation for horses, but about three building blocks that are used time and time again in electronics, and yet never fail to cause confusion in the minds of newcomers to the hobby. The stable part comes from the same root word as stability, so the three words of this article's title refer to different types of circuits dealing with electronic stability. The three, known as multivibrators, will be explained separately, and examples given with various circuits using both transistors and i.c.s. Finally a simple test-bed circuit will be described that can be built and experimented with.

All the circuits are shown using a 9 V supply, but in fact the CMOS circuits will operate from approx. 5 to 15 V , and the transistor circuits from approx. 3 to 12 V . All the component values are only suggestions, and modifications are encouraged. None of the CMOS circuits show the supply connections ( +V pin 14, and 0 V pin 7), and if they are tried, don't forget to tie any spare input pins from unused gates to either supply line, as the text will explain.

\section*{MONOSTABLE (Transistor)}

Any word starting with mono usually refers to something single, and similarly a monostable multivibrator is stable in one condition only, either on or off (high or low). The circuit can be forced to assume a different state but after a period of time it will revert to its original stable condition where it will remain indefinitely.

Consider the circuit in Fig. 1. Transistor TRI is normally on, pulling its

collector down close to 0 V , taking with it the base of TR2, consequently keeping TR2 turned off. Also note that R3 and R5 keep both sides of C 1 high so that it is fully discharged.

If however we temporarily short the base of TR 1 to ground, this transistor will be turned off, allowing the collector voltage to rise, turning on TR2. The temporary short to base will also take with it the -ve side of Cl . However after a period of time determined by the charging circuit involving C1 and R3, the base voltage of TR1 will gradually rise, and it will turn back on again, turning off TR2, and the circuit is once more stable. Note though that if the base of TR 1 is held low, shorted to ground, then the outputs will remain in their changed condition until the short is removed, after which the monostable will then complete its cycle. Outputs can be taken from either collector.



Fig. 3. CMOS 4011 B pin connections.

\section*{MONOSTABLE (CMOS)}

Fig. 2 shows a circuit that does exactly the same job as the transistor circuit above, but this time it is performed by two gates of an i.c., the CMOS 4011 quad NAND gate. The quad means that within the i.c. are four identical circuits, symbolised by Fig. 3. The truth table is shown opposite, and these tables are extremely important for any logic circuit designer, because they show what the gate will do given certain conditions.

A logic gate can normally only assume two positions, referred to as high (1), i.e. close to the \(+V\) supply voltage, or low ( 0 ), close to 0 V . The output state of the NAND gate will depend on the states of the two input pins, \(A\) and \(B\), so that if both inputs are high, the output will be low. However if only one input is high, it doesn't matter which, then the output will be high, as it will be if both inputs are low. A final point to remember about any CMOS logic gate is that all the input pins must go somewhere; they cannot be allowed to float, i.e. not connected to anything, because the output won't know whether they should be high or low. Consequently you will read in circuit descriptions of pins being tied with resistors to +V or OV as appropriate.


Fig. 4. Differentiator circuit.
Before we examine the circuit in more detail, it is worthwhile just looking at what happens at the junction of Cl and R2. This is called a differentiator, and if the input (the left hand side of Cl in Fig. 4) is a positive going transition, low to high, the junction of the capacitor and resistor will immediately go high, and then gradually fall to 0 V via the resistor, irrespective of whether the input is still high or low.

Normally the output at pin 4 will be high. This is because R2 is pulling both IClb inputs low. Because the output is connected to one of the inputs of another NAND gate (IC1a) and R1 is holding the other input of IC la high, the output at pin 3 will be low, as shown by the truth table. Consequently both sides of the capacitor are low and it is fully discharged.

When a low-going trigger pulse is applied to pin 2, the output of ICla will switch states, causing a high pulse, gradually decreasing to 0 V on the two inputs pins 5 and 6 , the junction of Cl and R2. Thus pin 4 goes low, taking with it pin 1. The output of IC la will now stay high, even if the trigger pulse is removed. Eventually the decreasing voltage falls below the threshold of pins 5 and 6 , and IC1b output reverts back to its original high state.

This takes pin 1 high, and assuming the trigger pulse is no longer there, the output of ICla will return low. If however the trigger pulse is still present, then IC 1 a

Table 1. NAND gate truth table.
\begin{tabular}{|c|c|c|}
\hline \(\mathbf{A}\) & B & OUT \\
\hline 0 & 0 & 1 \\
0 & 1 & 1 \\
1 & 0 & 1 \\
1 & 1 & 0 \\
\hline
\end{tabular}


Fig. 5. Simple monostable timer.
output will stay high until it is removed. This is an important difference with the transistor circuit, namely the output (pin 4) changes back, irrespective of whether the trigger pulse has finished.

Monostable circuits are very useful as for example, simple pulse stretchers. As the name implies these lengthen a normally very short pulse to one slightly longer. Normal switches don't in fact switch over very cleanly, and produce more than one pulse, hence they are called noisy; this can totally upset logic circuits. To counteract this, pulse stretchers are used so that the monostable output lasts slightly longer than the complete switchover operation, ensuring that no extraneous pulses get through.

Another use for monostables is as a simple timer, and because of the high impedance of CMOS gates, high value resistors and capacitors can be employed to give very long time delays, a disadvantage with the transistor circuit incidentally. A practical circuit might well be based on one like Fig. 5.

The input to pins 8 and 9 is normally high. going low for the timed period. The truth table shows that the output will consequently be normally low, going high for the timed period, and thereby turning on the transistor. D1 is included to protect the transistor from back e.m.f. when the coil de-energises.

\section*{BISTABLE (Transistor)}

Any word starting with "bi" normally means two, and a bistable multivibrator is one that is stable in either the high or low (the on or off or the ' 1 ' or ' 0 ' state). These types of circuits are useful as latches, i.e. sensing an input pulse, and changing the output accordingly. The advantage over normal switches is, as with the monostable above, that they can be made clean, so avoiding glitches in the circuit. The simple circuits shown here have two input pins, normally known as SET and RESET, but brief details will be given later of a specialised flip-flop i.c., the 4013.


Fig. 6. Transistor bistable.

On pressing S1 the output will switch on TR1, which energises the relay. The changeover terminals can then control an appliance, turning it on or off after a predetermined length of time. Increasing the value of R 2 or C 1 will lengthen the time delay. You will note that an extra gate ICIC has been used. This was deliberately done rather than use a transistor to show that a 4011 gate can be used as a simple inverter.

Consider the circuit in Fig. 6, assuming that TR1 is on. The effect of this will be to pull the collector of TR1 down close to 0 V , taking with it the base of TR2, turning that transistor off. If we now short the base of TR 1 to earth, it will turn off, allowing its collector voltage to rise, past the point at which TR2 will turn on. This takes the TR2 collector voltage (and the TRI base) down, thus ensuring that the base of TR 1 is low, and this transistor is


Fig. 7. CMOS bistable.
tion of all the possibilities available would take too long. However one of the principle advantages is that it only requires one pushbutton to set and reset. This has interesting applications in the field of frequency division, as Fig. 9 will show. Each rising edge of the input waveform will cause the output to change state. Thus it requires two input pulses to cause the output to rise and fall once, which means it has divided the input frequency by two. The 4013 has two identical circuits inside it (see Fig. 10) and the output of the first can be connected to the input of the second, which will further divide the frequency by two.

This technique is often used in simple musical instruments that need to generate frequencies for the different octaves: Usually what is.involved is, creating the
kept turned off. The circuit is now stable, but with the on and off transistors transposed. Another shorting to 0 V , this time the base of TR2, will reverse the process. Outputs can be taken from either collector.

\section*{BISTABLE (CMOS)}

The CMOS equivalent of the bistable circuit is shown in Fig. 7. Again two NAND gates are used, so that the same truth table applies. Assume that gate ICla output (pin 3) is high. This means that IC1b pin 5 is high, and because pin 6 is tied high by R2, then IC1b output at pin 4 will be low, holding pin 2 low. R1 is holding pin 1 high, so IC1 a output will stay high and the circuit is stable. If S2 is now closed briefly, IC1b output will switch high, taking with it pin 2. Now both IC la inputs are high, so pin 3 will switch low, taking with it pin 5, and the circuit is once more stable, but with the outputs transposed. Closing S1 will reverse the process.

You will notice that there is no capacitor in either of the two bistable circuits. This is because capacitors normally introduce an element of timing, which is not required in this application, unlike monostables or astables. We want the switch over to be clean, and usually as fast as possible.

Fig. 8 shows a very simple application

[EEIMM
Fig. 8. Simple bistable application.
of a bistable, again using a relay which can be used to turn on household appliances, (but check the power rating!). It is a latching relay circuit, i.e. a simple pushbutton will cause the relay to turn on, and stay on. It will only turn off when the second pushbutton is pressed. Projects always look a bit more impressive with a couple of very small pushbuttons on the front panel to control something rather than a large toggle switch.

The 4013 is a more specialised CMOS dual flip-flop i.c., and a detailed descrip-


Fig. 10. CMOS 40138 pin connections.
top octave's frequencies, then dividing them by two each time for the lower octaves.

An experimental circuit is given in Fig. 11 and consists of a sound generator, feeding into the 4013 , which produces the two lower octaves. The output is fed into a piezo transducer, connected in what's known as a bridge circuit to increase the output power. This circuit can be built either on Veroboard or on a small p.c.b. Varying the resistance of VR1 will alter the pitch, and by switching in either the pure signal, or divided by 2 , or 4 , the dif-


EE116M

Fig. 11. Simple sound generator and frequency divider

\section*{ASTABLE (CMOS)}

The CMOS version of the astable circuit is shown in Fig. 14, a nd the explanation of how this circuit works tends to get rather complicated, involving the charging of C1 via R1, and then the discharg ing through the internal input protection diodes, actually contained within the i.c. Detailed explanation is outside the scope of this article, and readers should look to the various reference books on CMOS

The really nice thing about this circuit is that it only needs two other compo nents apart from the i.c. gates, and because the i.c. contains four identical gates, two oscillators can be built from one i.c., two resistors, and two capacitors. As a bonus one oscillator can control the other. One point to note: because the capacitor charges in both directions, only
ferent octaves will be heard. Looking at the latter two waveforms in particular will reveal a very clean square wave with fast rising and falling edges.

\section*{ASTABLE (Transistor)}

Modern music is often referred to as atonal, without tonality (sounding dischordant to many people). Similarly "astable" circuits, being without stability, are those which are deliberately designed to be unable to remain in either the on or off state. They stay in one condition for a period of time, but the operating conditions change, normally caused by rising or falling voltages due to a capacitor, and the multivibrator has to change state, when conditions again start to alter back, and the process continues ad infinitum.


Fig. 13. Frequency alteration circuit.


Fig. 12. Transistor astable.
[EEII5M

The circuit in Fig. 12 bears some slight resemblance to the transistor monostable circuit and this is not surprising, because it can be considered as two monostables, working opposite to, and continually triggering, each other. For this reason there are now two capacitors in the circuit, one for each transistor. The operation is very similar, with the capacitors alternately charging and discharging, switching on each transistor in turn. The speed of switching is controlled by R2, C1, and R3, C2. If the two resistors and the two capacitors are the same value, a square wave with equal mark-space ratio (i.e. each transistor is off and on for the same amount of time) should be obtained. To make the circuit variable whilst maintaining the equal mark-space ratio requires that R2 and R3 be altered as in Fig. 13.

non-polarised capacitors may be used; electrolytics are not suitable. Values for the resistor can vary from a few kilohms to several megohms, and for the capacitor from a few picofarads to hundreds of microfarads; thus the operating frequency of the oscillator is vast.

If pin 1 is not joined to pin 2 , but is instead tied high via a resistor, then by


Fig. 14. CMOS astable.
shorting this pin to 0 V , the oscillator will stop. This is called a gated oscillator, and the pulling down to 0 V can be achieved either mechanically, with a pushbutton, or with another logic circuit, as in Fig. 15.

If controlled by a logic circuit, then the tie-up resistor is not required, because the previous circuit element holds it high or low. Gates ICla/b are connected as an astable multivibrator, switching high and low quite slowly. The output is connected to one of the pins of the astable using IClc/ICld, switching much faster (approx. \(1 \mathrm{kHz}, 1000\) times per second), producing an audible sound. The effect of the first astable is to keep switching off


Fig. 16. Positive triggered monostable.
the second, so we hear a pulsed bleep tone, which can be speeded up by reducing the value of R2 or C1, and can be raised in pitch by reducing the value of R3 or C2.

\section*{NOR GATES}

All of the CMOS circuits so far described have used the 4011 quad NAND gate, but there does also exist the 4001 quad NOR gate, the truth table of which is shown below.

Table 2. NOR gate truth table.
\begin{tabular}{|c|c|c|}
\hline A & B & OUT \\
\hline 0 & 0 & 1 \\
0 & 1 & 0 \\
1 & 0 & 0 \\
1 & 1 & 0 \\
\hline
\end{tabular}


Fig. 17. Positive trlggered bistable.
EE120M

You will observe that the difference is a low ( 0 ) output when either input is high. All 3 types of multivibrator can be built with this i.c., but because the truth table has changed, the polarity is opposite. Also note how the drawing of the gate is different to distinguish it from a NAND gate. The variations from the NAND circuits are listed below:
a) The monostable requires a positivegoing trigger pulse, and the output (pin 4) will normally be low (Fig. 16).
b) The bistable requires positive-going pulses to change the states of the outputs (Fig. 17).
c) The astable requires pin 1 to be tied high to stop the oscillator (Fig. 18).


Fig. 18. Astable requiring \(+V\) to stop.
Finally Fig. 19 shows a test-bed circuit, consisting of two monostables, with short timing periods to act as pulse stretchers, a bistable and a gated astable operating in the audio range. All the circuit elements are separate, but link positions have been provided on the p.c.b. so

\section*{EXPERIMENTER'S TEST BED}


\section*{COMPONENTS}

Resistors
\begin{tabular}{ll} 
R1,R3,R5-R7 & 10k (5 off) \\
R2,R4 & 47 k (2 off) \\
R8 & 680 k \\
All \(\frac{1}{4} \mathrm{~W}\) carbon \(5 \%\)
\end{tabular}

All \(\frac{1}{4}\) W carbon 5\%

\section*{Capacitors}

C1

C3 \(\quad 1000\) p Disc
Semiconductors
IC1,IC2 4011 CMOS quad NAND gate (2 off)


Miscellaneous
S1,S2

WD1 ush-to-make pushbutton switch (2 off)
electric transducer
Printed circuit board: single-sided \(86 \mathrm{~mm} \times 50 \mathrm{~mm}, E E P C B\) Service, code 8506-03; Veropins; connecting wire; link wire; battery connector.

Approx. cost
Guidance only
£6.00
that they can be combined together in various ways. e.g. if the two monostables control the two trigger pins of the bistable, the output of which gates the oscillator, then S1 and S2 will turn the audio on and off. This is rather a case of over-kill but it does use all the elements!


A p.c.b. design is given in Fig. 20, with the overlay in Fig. 21. Insert the resistors, capacitors, and veropins for the various link pads. CMOS i.c.s are sensitive to static, though the more recent B -series are more robust. However the legs should be handled as little as possible, and insert the i.c.s last in any p.c.b. When construction is complete, check carefully, then switch on. If connected as suggested above, then the switches should control the audio.

Try experimenting with different permutations, and different component values. R5, R6 and R7 are tie up/down resistors and in fact are unnecessary in the configuration example illustrated. Each section has been labelled in and out so that the operation can be understood more easily.

\section*{CONCLUSION}

It is hoped that this article will have shown how useful the three types of multivibrators are. They crop up time and again, in various guises, and readers are well advised to read more information about them to gain a greater understanding.

\section*{EXPMRIMPNTHR'S TEST BED}



Fig. 20. P.c.b. design of the Experimenter's Test-bed.
This board is available from the EE PCB Service; order code 8506-03.


Fig. 21. Component layout of the Experimenter's Test-bed

\section*{all in your}

Projector and photoflood lamps have a very short life, and are expensive io replace. This project reduces the switchon current surge, so extending the life of the lamp: the savings made in this way mean that the circuit will pay for itself many times over.

\section*{MTX 8 CHANNEL} Ato D
No more electronic lonelinessnow your MTX can listen the the real world it hes hundren A \&o applications and cen cater for applications wide range of extra peripherals

\section*{nnoe enne}

NED REGMLAR robotics review

With the ever increasing range of robotic products and producers we feel it is time to introduce a regular page which will keep an eve on the activity, bring you news from the industry and generally look at where it is all leading.
In this second part we look at current design techniques and typical circuit elements. The all important Eritish Telecom "Approved Design" specification for construction and connection will also be dealt with.

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\title{
CIRCUIT EXCHANGE
}

This is the spot where readers pass on to fellow enthusiasts useful and interesting circuits they have themselves devised. Payment is made for all circuits published in this feature. Contributions should be accompanied by a letter stating that the circuit idea offered is wholly or in significant part the original work of the sender and that it has not been offered for publication elsewhere.

\section*{LIGHT CHASER/SEQUENCER}

THE circuit is designed around the 4 -bit shift register, 74LS95. The clock pulses are provided by the 555 timer. When S1 is depressed all the four outputs ( \(13,12,11\) and 10 ), of the shift register will go low, so that the output of IC3c will be held high; the seria data input of IC2, pin 1, will also go high. Clock pulses from the 555 timer will then successively make the outputs of IC2 go high, one after the other. When IC2 pin 10 goes high its serial data input will go low so that the
next set of clock pulses will make the IC2 outputs to go low, one after another, after which the first sequence will be repeated.

Connected to the shift register outputs are four exclusive-OR gates. The output from the NOR gate, IC3d will go high only if both pins 13 and 10 of IC2 are high, or low. IC 4 c gives a high output only when pins 13 and 12 of 1C2 are high and low or vice versa. IC4b gives a high output when pins 12 and 11 of IC2 are high and low or vice versa and IC4a output
goes high when pins 11 and 10 are high and low or vice versa. These events take place sequentially so that the net result is a 1 to 4 decimal counter.

The outputs from the shift register and gates are connected to l.e.d.s. via an octal buffer. When the slider switch \(\mathbf{S} 2\) is in its normal position the l.e.d.s. will simulate a light chaser.

The original version was interfaced with triacs to drive higher power lights.

Gerald Kotonya, Kenya


Circuit diagram of the Light Chaser/Sequencer,


\section*{SIMPLE BURGLAR ALARM}

THis simple alarm circuit uses just one i.c. wired as a flip-flop and multivibrator. The flip-flop, ICl a and ICl b is wired to give a normally low output which is switched high whenever the loop circuit is broken, via the switches or cut wire. This will cause the l.e.d., D1 to light and the multivibrator, IC1c and IC1d to be activated.

The output from ICld is amplified by the Darlington pair, TR1 and TR2 which supply current to drive a loudspeaker or relay.

A Reset switch S 1 is provided which will reset the alarm when the loop has been reestablished. The frequency of the alarm. signal can be modified by changing the components associated with ICIC and IC Id.

> K. A. Khiavi,
> Tehran,
> Iran.

\section*{MODEL EMERGENCY VEHICLE SIREN}

0
NCE again we see a simple oscillator application circuit. This design is used to

\section*{ZX SPECTRUM JOYSTICK}

\section*{INTERFACE}

THIS simple Joystick Interface for the ZX Spectrum consists of a few discrete components and five readily available i.c.s. It is addressed when A0 to A4 are at logic 1. With this condition true and the \(\mathbf{Z 8 0}\) control lines, \(\overline{\mathrm{RD}}\) and IORQ low (logic 0 ), the hex buffer i.c., IC5 is enabled and the device is ready to transmit.

The Joystick conditions are fed to data lines, D0 to D4 and are read as left, right, up, down and fire respectively. RI to R5 are pull up resistors and the Joystick signals should be switched to ground to provide the required voltage levels.

> A. Moran, Reading,
> Berks.

For more circuit ideas for the Spectrum, see our regular feature, On-Spec, Page 314
simulate an emergency vehicle siren for model cars or alternatively it may be used in conjunction with an amplifier to drive a burglar alarm.

IC1c and ICld form a simple oscillator whose output is modulated with the output from the oscillator formed by IC1a and IC1b running at about 1 Hz , to give an alternate high and low signal.

There is nothing new about this circuit but a useful 'switch' is provided by the input to ICla. When ' \(A\) ' is at logic 1 the circuit is on, when at logic 0 the circuit is off and it draws negligible current. This makes it idea! for use with computers or remote controlled models.
W. A. Adam,

Kettering,
Northants.


\title{
COUNTER NTELICENCE \\ BY PAUL YOUNG
}

\section*{On Trial}

Being an avid reader, the first thing I did on moving to my new district was to join the library. My previous library was the old fuddy-duddy type which issued tickets, but it had certain advantages. You were given six tickets, so if you looked in your pocket and only found five you knew you had a book to return, even old Young can count up to six

Contrast this with my present library. You are issued with one ticket, which has a rectangle on the bottom surrounding a series of vertical lines (as used in some Supermarkets for pricing). Having selected your books, the librarian rubs a special collector across the appropriate part of your ticket, and also across a similar marking fixed to the inside cover of each book. On returning the books, they only rub the collector across the marks in the books.

It seemed to work well enough until last week, when I received a letter requesting me to return Systematics by John Gall. I was convinced in my own mind that I had returned it. To be certain, I turned Schloss Young inside out, though to no purpose.

Finally I went to the library and asked the lady if their electronic wonder ever made mistakes. "Oh! yes" she said, "You see it is very old". This rather surprised me as I thought they were the latest thing, so 1 explained my predicament and she went off to investigate. She returned beaming, and said, "I wrote to you at the beginning of the week and you came in and returned it'
'Madam' | replied, trying to appear cross, which is difficult if the recipient is an attractive young lady, "I have not returned any books this week, I returned that book a month ago, it has obviously been sculling around your library and you have only just found it.'

While I was sitting at home cogitating on this fracas | fell asleep and had a dream which finished up as a nightmare. It was evidently some time in the future, and Young was in the dock charged with some dreadful crime

The Jury consisted of twelve good computers and true, and my learned friend, the computer for the defence, was giving his final summing up speech. Unfortunately due to a bad joint on one of his chips he became thoroughly confused and thought
he was the computer for the prosecution Consequently poor old Young was sentenced to be hung. Luckily I woke up just before the sentence was carried out. It was a narrow squeak and all due to a faulty joint.

I don't wish to appear as an alarmist, but remember this could happen. To repeat myself once more, computers are wonderful, except when they go wrong.

\section*{Mature Guard}

You would imagine that any firm responsible for the security of 700 million pounds worth of maturing whisky would have the latest and most sophisticated type of electronic alarm system. In the case of George Ballantyne and Sons, you would be wrong. They employ a flock of Chinese geese who patrol the barbed wire perimeter and racks of casks twentyfour hours a day. Any intruders start them cackling so loudly that they wake up the two human guards.

The geese were the idea of the late Tom Scott managing director of the company af ter studying Roman history. He decided that as the geese successfully aroused Rome in time to counter the Gauls offensive in 390 B.C. they could probably frighten off Bill Sykes, or perhaps I should say Mac Sykes, bearing in mind they are situated North of the border.

Apart from the minimal running costs, another advantage is, that they can reproduce themselves, something still beyond the scope of any electronic device-I always say you can't beat these old fangled ideas!



\section*{LOGICAL STEP}
\(\Delta^{\mathrm{N}}\) oscilloscope companion that will enable most scopes to have the facilities to function as a real-time eight channel logic analyser is the latest product from Heaviside Industries.

This relatively low-cost add-on is capable of allowing the scope to display high speed signals from d.c. to 10 MHz , and is compatible with all \(\pm 5 \mathrm{~V}\) logic. No a.c. outlet is required, the unit taking power directly from the circuit under test and drawing typically 50 mA .

Allowing the scope to display up to eight simultaneous traces on the screen, the unit is supplied with 750 mm eight channel probe complete with E-Z hooks for easy i.c. connection.

The Real-Time Logic Analyser (RTLA) is expected to sell for

around \(£ 150\), including VAT. This includes operating instructions, full one year warranty on parts, postage and packing.

For further information contact:

Heaviside Industries LId., Dept EE, 45 Woodstock Road, London, NWII 8ES.

\section*{TRANSFERS}

Avallable to amateurs wishing to design and make their own one-off p.c.b.s, as well as for the professional, Pelltech are marketing a new range of ALFAC "rub-down" dry transfers.
The range includes selfadhesive black flexible crepe paper tapes with a non-reflective matt finish for quality photographic reproduction work. It is claimed that the use of a quality adhesive allows easy correction and resiting of "tracks" as necessary.
Included is a comprehensive selection of circular and d.i.1. pads, connectors and elbows, track conductors and relay symbols. A further addition is a range of solder mask symbols, component outlines and round plane grids. These are printed in inactinic transparent red (photographically opaque) which, it is claimed, permits accurate positioning in relation to the prin ted circuit layout.

\section*{CASE FOR ENCLOSURE}

The first of a new range of durable enclosures moulded in rigid polyurethane is now available from Plastek.

Designed as a medium sized desk console, the EC21 can be used with a range of components including key pads, meters, liquid crystal displays, and ZIF sockets to produce stylish assemblies for desk and laboratory applications.

Being moulded from polyurethane, the case lends itself to a variety of fixing arrangements such as inserts, self-tapping screws, through bolting and epoxy adhesives, and can be cut, drilled or routed using ordinary tools.

Features include a brushed aluminium mounting plate, moulded-in mounting guides for circuit boards, provision for Perspex display face, large cable entry/outlet plate and non-slip rubber feet.


The case is finished in polyamide spatter textured paint with black base and grey top and is claimed to be impervious to most forms of chemical and environmental attack. Other colours are available to special order.

For details of prices and range of cases available contact:

\section*{Plastek,}

Dept EE, Units 1,2 \& 7. The Midlands Industrial Estate, Holl, Trowbridge. Wilts, BAI4 6 RU.

\section*{DRIVE FOR SINCLAIR OL}


A3.5in floppy disc drive system to operate with the Sinclair QL is announced by Micro Peripherals.
The system has been designed and manufactured in the UK and is available in three separate units which can be purchased individually. The package consists of an interface module and first and second disc drives.
The two drive system has a total formated capacity of 1.44 MB and provides fast file handling using the multitasking feature of the QL .

The interface which supports up to four drives on a standard
multibus provides a whole host of resident utilities including a screen editor, job control as well as additional file handling commands.

The interface module has a recommended selling price of \(£ 99\) and the first and second Disc Drives are available for \(£ 189\) and £159 respectively (ex VAT).

For more details and addresses of nearest stockists contact:

\footnotetext{
Micro Peripherals Ltd., Dept EE, Unit 3 Intec
Hassocks Wood, Wade Road, Basingstoke, Hants, RG24 ONE.
}


\section*{1180DEFFROCL (T\%) IFT \(\%=19 \mathrm{~W} \%=1.32\) ELSEW \(\%=128\)}

1190 IFL\%?S\% COLOUFW\% ELSECOLOUF135
1200FFTNTTAB (T\%-LENHF ( \(5 \%\) ) , Y\%) HF ( \(5 \%\) ) : COLOUFW\%: ENDFROC
 U255: NEXT: EMDPROC
122ODEFFFOCDrd (H\%,M\%) LOCALX\%, Y\%, C\% :GCOLO. H\%

\(=1 \%+1\).
1240 VDU2 \(9 \%\) Y\%: \(5:\) MOVEFNOut, 0:FOFF\% \(=1 \%\) TOI\%+FNOut/M STEF2
1250 DRAWF Nout. FHout : NEXT: IFM\%ANDS\% SMOVE-5.2. 16: VDU2 \(33+5 \%\) \(1260 \cup D U 26,5:\) IFM\%ENDFFROC

1280 GCOLU. 2: FQFiv\%=128 TO896 STEP \(64: X \%=24:\) T \(\%=\) TFUE
\(12 马 O R E P E A T F E F E A T: X \%=X \%+4: W \%=F r g t:\) UNTILABSW\%=1:IFW\%=1 T\%=T\%+1:T\%(T\%)=X\% 1300 REFEAT \(X \%=x \%+4: W \%=\) FNDT: UNTILW \(\%<1: T \%=T \%+1: T \%(T \%)=X \%\)
\(1310 U \mathrm{WT}\) ILW \(=\) = TRUE DRT \(\%=3: ~ V \%=T \%(1): W \%=T \%(2)\)
132OFGR \(\%=64\) TO1213 STEF64:N\% \(=\mathrm{N} \%+1:\) IFT\%<3THEN1 360
1330 IF \(X \%<\mathrm{V} \%\) ORX \(\%+64\) ) W\% GFFOINT \((X \%, V \%-64)<2 T H E N 137 O\)
\(1340 \mathrm{C} \%=\mathrm{C} \%+1: \mathrm{F} \%=5: \mathrm{FEFEAT}: \mathrm{Q} \%=\mathrm{C} \% \mathrm{MODE} \%\) ? \(\% \%: \mathrm{F} \%=\mathrm{F} \%-1\) : UNTTLQ \(\%=0\) OFF \(\%=0\)
\(1 \geq 50 \quad \mathrm{~T} \%=32\) : IFQ \(\%=0 \quad \mathrm{~F} \%=F \%+1: T \%=24 \mathrm{C}+\mathrm{F} \%\)
1360 G\%NN\%=F\%:MUVE \% \% \% UDUT\% IFT\% S2 UCDLO, 1: VDUB, 10, 23E: GCOLO, 2

1. ZBONEXT : NEXT: \(C \%=0:\) REFEATN \(\%=0\) : REFEATN \(\%=\mathrm{N} \%+1\)

), (1\%, 1)
1400 UNT ILN \(\%=240:\) UFT I LU \(:=M \%:\) VDU24, \(32 ; 68: 1216 ; 896:\) ENDFFRC
1410 DEFFFIDt \(=F\) OINT (X \(\%\), Y \% )
\(1.420 D E F F N o u t \quad V \%=D \% ? I \%: I \%=I \%+1: I F V \% ; 128 \quad v \%=128-V \%\)
\(1430=\mathrm{V} \% * \mathrm{~F}\)
1440 EFFFRDCV19 ( \(V \%\), W\%) VDU17, \(V \%\), W\%, 0:0: : ENDPRDC \(1450 D E F F F O C 1(V \%)\) MOVEO, U\%ッDFAN \(1279, V \%\) : ENDFF:DC
146ODEFFROCCR (V\%) VDU1279:V\%:0;0;0: ENDFROC

\title{
ELECTRONII DOORBELI
}


THE purpose of this project is to construct a doorbell with the ringing sound of the conventional electromechanical device, but taking advantage of the reliability and compactness of electronic techniques. It is batteryoperated with the batteries housed in the unit, so the only external connections are those to the bell-push.

\section*{POWER}

The two PP3 batteries providing the power may seem uneconomical but they minimise the physical size, and with only intermittent use they should last an acceptably long time.

The current drain is about 5 mA , and just one battery could be used, but the loudness would be reduced. The supply must not exceed 18 V , as this is the maximum that the i.c. can handle.

\section*{CIRCUIT DESCRIPTION}

The circuit diagram is shown in Fig. 1. IC1c and and IC1d, together with R3,

R6, VR1 and C3 produce a square-wave at the resonant frequency of WDI, adjustable by VR1. TR2 and TR3 drive WD1 using a simple push-pull arrange-ment. IC Ia, IClb and associated components produce very short zero-going pulses when pin 1 of ICla is high (bellpush pressed), which switch on TRI and charge C4. The capacitor, prevented from discharging through IC1b by D2, gradually discharges through the baseemitter junction of TR 1 , thereby steadily reducing the current available to the output stage, and effectively giving rise to damped oscillations between each pulse from IC1b.

When the power is disconnected (push released), CI maintains a supply to IC1, and with pin 1 now low, the output: of IC1b is low, holding on TR1. C5 then supplies a diminishing voltage to power WD1, again simulating damped oscillations.

D3 and D5 ensure that C1 and C5 respectively discharge only along the required paths. D4 provides a voltage drop


Fig. 1. Circuit diagram for the Electronic Doorbell.
to roughly match that across D3 so that the input at pin 1, IC1, is not harmfully above the supply voltage to this i.c.

\section*{CONSTRUCTION}

The sixteen breaks to be made in the copper tracks of the circuit board are shown in Fig. 2. This also shows the positions of the wire links on the underside and the layout of the components and links on top of the board.

Complete the trackside first, then mount the i.c. holder, VR1, and add the links on the upper side. Solder in the remaining components leaving the semiconductors until last. Use sleeving, such as the insulation from connecting wire, on the leads of DI to prevent electrical contact with VRI.

Attach the flying leads, battery connectors, and WD1 to the circuit board as shown. Check the orientation of Cl and C5 and ensure there is no copper or solder shorting adjacent tracks.

\section*{CASE}

A box made specially ( 3 mm plywood is suitable) enables the circuit board, batteries and terminal block to fit exactly (see photographs) so that the unit can be. kept as compact as possible. WDI is screwed to a strip of wood which is then screwed across the top of the box. The prototype, as shown in the photographs, was constructed in this way.

Alternatively, a plastic box could be utilised to give a more professional finish, with WDI screwed to the outside of its lid, holes being made in the lid to take the leads. Holes would also be needed in one side for the leads to the bell-push. A box with dimensions \(95 \times 71 \times 35 \mathrm{~mm}\) is suitable.

The circuit board is screwed to the bottom of the wooden box using small-gauge screws in the positions indicated in Fig. 2 and the terminal block screwed to the side as shown. Make screw holes in the base for mounting the box, if it is to be secured in a fixed position. The two battery connector leads which are joined together are anchored on a solder-tag positioned between the terminal block and box.



If required, a cover can be made for the unit. The prototype made use of an empty margarine tub, painted with silvercoloured enamel paint. A small hole (about 5 mm diameter) was made in the centre of the tub, immediately above the hole in WD1, and pieces of foam rubber glued round the inside of the tub fixed the cover in position.

\section*{ADJUSTING}

Insert IC1, connect the batteries and bell-push. With the device in operation, adjust VR1 to provide the best sound and loudest output.

Finally, fix the bell and push in the desired positions, with an appropriate length of twin flex connecting them.

Fig. 2. Component layout and Veroboard drilling details for the Electronic Doorbell (actual size). Note that the collector of TR1 is the centre pin. Use thin insulated wire for the underside links.


View showing the layout of the circuit board and batteries within the case.
\begin{tabular}{|c|c|}
\hline COMPONENTS & Approx. cost Guidance only \(\mathbf{E} 5.00\)
\(\qquad\) \\
\hline Resistors & Semiconductors \\
\hline R1 47k & D1 to 1 N4148 silicon (5 off) \\
\hline R2 8M2 Se & D5 1 BC214L pno sillicon \\
\hline \(\begin{array}{lll}\text { R3 } & 2 \mathrm{M} 2 & \text { Se } \\ \text { R4 } & 3 \mathrm{k} 9 & \end{array}\) & TR2 2N3906 pnp silicon \\
\hline R5 3M9 & TR3 2N3904 npn silicon \\
\hline R6 560k & IC1 4011 смоs quad 2-input \\
\hline R7 330k & NAND gate \\
\hline All \(\frac{1}{6} \mathrm{~W} \pm 5 \%\) carbon page 312 & Miscellaneous \\
\hline & WD1 PB 2720 piezo-ceramic transducer \\
\hline Potentiometer & B 1,B2 9V battery (PP3) (2 off) \\
\hline VR1 220 kmin . horizontal preset & S1 Push-to-make switch 15 \\
\hline & rows \(x 16\) holes; 14 -pin di.i.l. \\
\hline \multirow[t]{2}{*}{Capacitors} & socket; 2A terminal block, two \\
\hline & sections; PP3 battery connectors \\
\hline C1 \(100 \mu 25 \mathrm{~V}\) radial elect. & - 12 off). Case-minimum internal \\
\hline C2 12 n polycarbonate & dimensions \(68 \times 57 \times 28 \mathrm{~mm}\); \\
\hline \(\begin{array}{ll}\text { C3 } \\ \mathrm{C} 4 & 150 \mathrm{p} \text { polystyrene } \\ \text { 100 polycarbonate }\end{array}\) & push; 6BA solder-tag; fixing \\
\hline C5 \(\quad 10 \mu 25 \mathrm{~V}\) radial elect. & screws. \\
\hline
\end{tabular}

\section*{BACK NUMBERS and BINDERS}


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\begin{tabular}{|c|c|c|}
\hline PROJECT TITLE & Order Code & Cost \\
\hline \begin{tabular}{l}
- JULY'83 - \\
User Port Input/Output M.I.T: Part I User Port Control M.I.T. Part 1
\end{tabular} & \[
\begin{array}{r}
8307-01 \\
8307-02
\end{array}
\] & \[
\begin{aligned}
& £ 4.82 \\
& £ 5.17
\end{aligned}
\] \\
\hline \begin{tabular}{l}
\(\qquad\) \\
Storage 'Scope Interface, BBC Micro Car Intruder Alarm High Power Interface M.I.T. Part 2 Pedestrian Crossing Simułation M.I.T. Pt 2 Electronic Die
\end{tabular} & \[
\begin{aligned}
& 8308-01 \\
& 8308-02 \\
& 8308-03 \\
& 8308-04 \\
& 8308-05
\end{aligned}
\] & \[
\begin{aligned}
& £ 3.20 \\
& £ 5.15 \\
& £ 5.08 \\
& £ 3.56 \\
& £ 4.56
\end{aligned}
\] \\
\hline \begin{tabular}{l}
\(\qquad\) SEPTEMBER '83 - \\
High Speed A-to-D Converter M.I.T. Pt 3 \\
Signal Conditioning Amplifier M.I.T. Pt 3 \\
Stylus Organ \\
Distress Beacon \\
Distress Beacon Pocket Version
\end{tabular} & \(8309-01\)
\(8309-02\)
\(8309-03\)
\(-8309-04\)
\(8309-05\) & \[
\begin{aligned}
& £ 4.53 \\
& £ 4.48 \\
& £ 6.84 \\
& £ 5.36 \\
& £ 3.98
\end{aligned}
\] \\
\hline \begin{tabular}{l}
- OCTOBER'83 \\
D-to-A Converter M.I.T. Part 4 High Power DAC Driver M.I.T. Part 4 Electronic Pendulum
\end{tabular} & \[
\begin{aligned}
& 8310-01 \\
& 8310-02 \\
& 8310-03
\end{aligned}
\] & \[
\begin{aligned}
& £ 5.77 \\
& £ 5.13 \\
& £ 5.43
\end{aligned}
\] \\
\hline \begin{tabular}{l}
- NOVEMBER '83 - \\
TTL/Power Interface for Stepper Motor M.I.T. Part 5 \\
Stepper Motor Manual Controller M.I.T. Part 5 \\
Digital Gauss Meter Speech Synthesiser for BBC Micro Car On/Off Touch Switch
\end{tabular} & \[
\begin{aligned}
& 8311-01 \\
& 8311-02 \\
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& 8311-04 \\
& 8311-05
\end{aligned}
\] & \[
\begin{aligned}
& £ 5.46 \\
& £ 5.70 \\
& £ 4.45 \\
& £ 3.93 \\
& £ 3.11
\end{aligned}
\] \\
\hline \begin{tabular}{l}
- DECEMBER 83 - \\
4-Channel High Speed ADC (Analogue) \\
M.I.T. Part 6 \\
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M.I.T. Part 6 \\
TRS-80 Twin Cassette Interface Environmental Data Recorder \\
Touch Operated Die (Dot matrix) \\
Touch Operated Die (7-segment) \\
Continuity Tester
\end{tabular} & \[
\begin{aligned}
& 8312-01 \\
& 8312-02 \\
& 8312-03 / 09 \\
& 8312-04 \\
& 8312-05 / 06 \\
& 8312-05 / 07 \\
& 8312-08
\end{aligned}
\] & \[
\begin{aligned}
& £ 5.72 \\
& £ 5.29 \\
& £ 7.43 \\
& £ 7.24 \\
& £ 4.34 \\
& £ 4.34 \\
& £ 3.41
\end{aligned}
\] \\
\hline \begin{tabular}{l}
- JANUARY '84 \\
Central Heating Pump Delay \\
Biological Amplifier M.I.T. Part 7 \\
Temp. Measure \& Control for ZX Comprs \\
Analogue Thermometer Unit \\
Analogue-to-Digital Unit \\
Games Scoreboard
\end{tabular} & \[
\begin{aligned}
& 8401-01 \\
& 8401-02 \\
& 8401-03 \\
& 84011-04 \\
& 8401-06 / 07
\end{aligned}
\] & \[
\begin{array}{r}
£ 3.33 \\
£ 6.27 \\
£ 2.35 \\
£ 2.56 \\
£ 9.60
\end{array}
\] \\
\hline \begin{tabular}{l}
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Oric Port Board M.I.T. Part 8 \\
Negative Ion Generator \\
Temp. Measure \& Control for ZX Comprs Relay Driver
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\(8402-02\)
\(-8402-03\)
\(8402-04\) & \[
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£ 8.95 \\
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\hline Mini Workshop Power Supply & 8412-04 & £2.78 \\
\hline & & \\
\hline Power Lighting Interface & \[
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& 8501-01 \\
& 8501-02
\end{aligned}
\] & \[
\begin{aligned}
& f 8.23 \\
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\end{aligned}
\] \\
\hline Games Timer Spectrum Amplifier & \[
\begin{aligned}
& 8501-02 \\
& 8501-03
\end{aligned}
\] & \[
\begin{aligned}
& \text { £ } 1.86, \\
& £ 1.70
\end{aligned}
\] \\
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\hline Computerised Train Controller & 8502-02 & £3.38 \\
\hline \begin{tabular}{l}
- MARCH '85- \\
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\hline Insulation Tester & 8504-02 & \(£ 2.53\) \\
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