FLECTRONICS Australia March, 1970



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National RS255S portable. It looks innocent enough, but it's quite a little earthquake kit. For a start, it pumps out 5 watts in a way that makes it sound like far more.

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volume 31, number 12

- DIGITAL FREQUENCY METER: A full description of the 200KHz version of our new low cost DFM appears on page 62. Offering high performance combined with simplified construction, it would be ideal as a tuitional project.
- AMPLIFIER CIRCUITS: SIMPLE Our younger readers will be interested in the article showing how to build a variety of amplifier circuits using oddment transistors. See page 83.
- WHAT IS SQUEECH? It is a device for speeding up the rate of tape playback, but without altering pitch. The ingenious mechanism with which this is achieved is described in the article beginning on page 109

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ELECTRONICS Australia, March, 1970

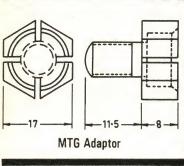
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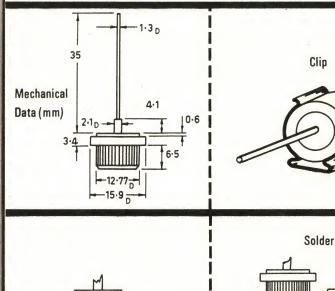


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New units . . .

During the month, the Federal Government announced that Australia would convert to the Metric system of weights and measures during the next ten years. To the scientific and engineering community, this came as no surprise; in fact, most people involved in technical matters are quite accustomed to working in metric units.

Not unexpectedly, writers in the popular press have questioned the necessity for making the change, citing the complications and the cost of so doing: If feet, pounds and pints were good enough for our forebears, they should be good enough for us. If others prefer metres, litres and grams, that's their business — and their business entirely!

Unfortunately, it isn't as simple as that. Industrially and commercially, we are becoming progressively more involved with nations which either use the Metric System, or are in the process of adopting it. To cling to the present system and become the "odd man out" would be to impose a heavy liability on future international trade.

These matters apart, there is a lot of pressure from scientific and technological interests for rationalisation of units and standards on a world basis and adoption of the Metric System is part of this. Our present system has evolved from "standards" which were seemingly quite unrelated, one to the other, and as remote from science as the length of Henry VIII's right foot. It has since become clear that physical parameters are all fundamentally interdependent and the mathematical terms necessary to express their relationship reflect the disparity of the original units and standards.

The Metric System was born out of an attempt to rationalise standards, units, multiples and their relationship one to the other. In retrospect, it is to be lamented that the English-speaking nations saw fit to stay with the old conventions, only to be faced with the necessity for change in the 1970s.

In the intervening decades, conventions for measuring other physical quantities have been introduced, amended and rejected. This has compounded the problem so that, overall, there is a state of massive confusion in technical literature: A variety of measurement systems; different standards for the same units; different meanings for the same word; multipliers with a significance varying with context; literature ostensibly current but nevertheless obsolete.

To try to build a new, rational system around our present foot-poundgallon and the other oddly related quantities would be plainly ridiculous. It would be equally ridiculous to envisage a dual system, with internationally recognised units for all scientific, engineering and technical applications (this of necessity) and traditional units for buying household needs.

I should hope that not too many of our readers will be found chanting: "I hate metres!"

ON SALE THE FIRST MONDAY OF EACH MONTH

On the cover

A view of the low frequency version of our new Digital Frequency Meter project, whose description appears in this issue (page 62). Developed by Technical Editor Jim Rowe, it combines up-to-the-minute circuitry and operating flexibility with straightforward construction and low cost. Spread before the instrument in the picture are some of the components which have made it possible: printed boards, integrated microcircuits, transistors and readout tubes.

EDITOR Neville Williams M.I.R.E.E. (Aust.) (VK2XV)

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3



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- 6. Dual stereo tapehead with hyperbolic contours, providing very good tapehead contact, necessary for drop-out-free playback.
- 7. Multi-play by direct switch.
- 8. Two level controls for individual or coupled stereo level selection.
- 9. Instant-stop button ("pause").
- 10. Recording-mode pilot light.
- 11. Two illuminated VU meters.
- 12. Two mixing inputs with microphone sensitivity for mono recordings.

MODERN ENGINEERING:

The CTG 28 is built to four-track standards in accordance with the newest developments in magnetic sound recording.

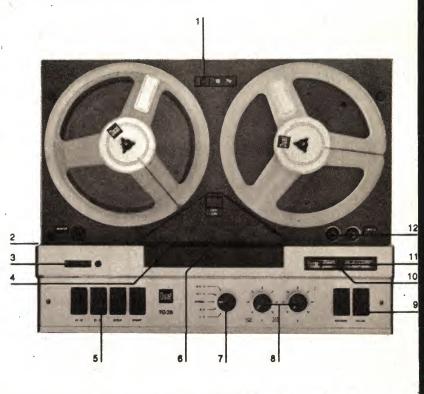
Besides playback of prerecorded tapes, recordings in mono, stereo, and multi-play can be made. With hyperbolic contour tapeheads, modern silicon transistors in the electronic circuits and many other advanced features, optimum recording and playback quality are guaranteed. The newly developed tape drive is



tape deck

Dual, the name synonymous with first class hi-fidelity turntables, now have produced the CTG 28 tape deck . . . a deck that is first class in styling and performance.

Featuring a natural walnut case with dust cover, Instrol are proud to display this deck, together with all other new Dual hi-fi equipment at their spacious showroom. The largest Dual display ever seen—at Instrol during March.



extraordinarily easy on tapes with the brakes controlled by feeler levers sensitive to tape tension. The unit operates on two speeds $-7\frac{1}{2}$ ips for high-fidelity requirements and $3\frac{3}{4}$ ips for less demanding requirements. Tape reels up to 7in diameter can be used. The electronics consist of a combination two-channel recording/playback preamplifier on printed circuits.

FACILITIES FOR CONNECTIONS:

Amplifier, radio, record-player, mono and stereo microphones, headphones and tape recorder. Also auxiliary items such as slide synchronizer, telephone adapter and home movie sound coupler may be used. Microphone and headphone jacks are easily accessible on the front of the chassis.

ELECTRONICS Australia, March, 1970

4





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GE:P548

ENGINEERING

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read what the experts have to say about the **GOLDRING LENCO GL75**

PERCY WILSON

PERCY WILSON Manufactured by Goldring Manufacturing Company (GB) Ltd., 486-488 High Road, Leytonstone, London E11. Manufacturer's specifications: TURNTABLE: AC mains: 200/240 V. 50Hz. Mains switch fully click suppressed 45 and 78 rpm. 9 lb. non-magnetic dynamically balanced turntable, Wow and flutter measured, according to DIN spec., 0.06%. Rumble and Discup the with the specific to the spec., 0.06%. Rumble and the specific to the s

I have now had one of these transcription units on test for over six months; and some of my professional colleagues have made independent assessments which agree with mine. So, let me not beat about the bush, but declare my verdict straight away. This is, quite simply, that * e GL.75 is easily the best integrated turntable • s arm unit that the partnership betwee

Goldring have yet produced. This is, of course, a mouthful, for ship's products have long been kn in the front rank. I have no hesita in declaring that the GL.75 i reckoned with in any company cumstances, anywhere in the w Having made that confession on not merely of faith, I must justify it by stating the resi tests. In this I shall not ju cription that can •be glea ifications. I shall only comm the performance. First of all, I must refer features. This is the tinuous variation of tury icians and others who h perfect pitch, this is a other turntable I know It is secured by having wheel which travels turntable. This idle izontal axis and its times thought that not affect the mo hasty and wrong of design in which angles to the turnts than a design in whi to the turn table.

In my tests I mounted the motor plate on stilts, as it were, above a rather thin motor board, which would resonate quite easily. I found the possibility of rumble all right, but I also found that the makers' recommendations had indicated the answer. In the first place, the motor plate must be mounted, as specified, on a motor board at least % inch thick. Do not on any account go below % inch. If the motor board in your cabinet is slimmer than this, then stick a sheet of Celotex to it so as to damp out any natural resonance

When suitable precautions are taken in mounting; such as the makers specify, the possibility of rumble is avoided. I have enlarged in this report on this possibility, because of the special vulnerability in a vertical drive as compared with a horizontal one; and to make it clear that the makers have safeguarded the position in their mounting instructions.

The second precaution to be taken, and this is vital, is that the motor should always be switched off and on at the switch on the motor plate and never at an independent switch. Otherwise the idler driving wheel would be left in contact with the turntable, and a tiny flat may be created on the rubber driving rim. In order to have accurate control of the turntable sneed this rim b

Hi-Fi News', February, 1969. Frank Jones MANUFACTURER'S SPECIFICATION.

Precision engineered transcription motor and arm. Turntable: Die-cast non-magnetic alloy dynamically balanced. Diameter: 121 in. Weight

din. Turnteste: Diectast non-inginetic alignetic dynamically balanced. Diameter: 124 in. Weight 8-8 lb. Speeds: infinitely variable between 30 and 86 r.p.m.; click-in stops for standard speeds in-cluding 164 r.p.m. Wew and flutter: 0-06% (DIN specification). Rumble: -60 dB. Speed stabi-lity: Within 0-3% for a 10% change in mains voltage; within 0-3% for pickup playing at 6 gm. Lowering device: hydraulic. PICKUP ARM. Lightweight type with decoupled counterweight and separate playing weight counterbalance. Stylus pressure: Infinitely variable between 0-5 gm, calibrated at 4 gm Inter-vals. Total length: 124 in. Effective length: 8-3 in. Overhang: 0675 in. adjustable up to 4 in. at the headhell. Offset angle: 23° 12°. Tracking error: ±0.8°. Height Adjustable. Dimensignes: 15×13×24 in (debve baseplate) × 3 in. (below). Weight: 18-7 lb. GL75/P, on plinth with Perspex IId, as in photo.

Manufacturers: Goldring Manufacturing Co. Ltd., 486-488 High Road, London E.11

PITE its up-to-the-minute appearance ng Lenco GL75 is the latest in a tables and playing desks from hich started, as far as I can he GL56-the first turntable 1 in Hi-Fi News and basically this machine. Since then we with an improved pickup sible layout (the GL56 had ly under the pickup in its r some strange reason), st massive turntable in vith another, improved, and now the GL75 with ter styling and a fine o go with it.

re of all these units is and the unique drive it. It has been pages, but many with the layout requirements, so oints will do no

> ed by a robust ended between o isolate it from This motor is nost precise part act, and runs so

> > 7





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GL 75

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the solid state stereo amplifier that's the right answer for your Hi-Fi problems. Here's 120 watts of IHF standard total music power-a power-packed

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Wide power bandwidth is another outstanding feature with 13 Hz to 30,000 Hz range. IM distortion is almost totally eliminated.

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40-WATT SOLID STATE STEREO AMPLIFIER TK-150U

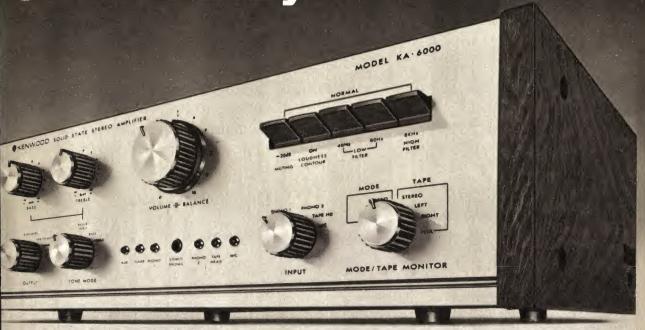
* 5 pairs of input terminals for MAG, AUX 1, AUX 2, TAPE REC and TAPE PLAY.

* Damping factor: 40 (at 16 ohms), 20 (at 8 ohms) * Dimensions: 10¼ "(W), 4¼ "(H), 9% "(D).



60-WATT SOLID STATE STE AMPLIFIER TK-25 * 2 sets of stereo speaker terr and front panel speaker set switch. * Dimensions: 13"(W), 4's "(H), 9

Stereo Family



180-WATT SOLID STATE STEREO AMPLIFIER KA-6000

Special Features of KA-6000

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- 2 pairs of MAG Input Terminals for 2 sets of record players.



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* Dimensions: 141 "(W), 4% "(H), 11% "(D),

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Physicists recognise four natural forces—gravitational, electrostatic, magnetic and nuclear. While the exact nature of these forces is still not fully understood, modern research has uncovered clues which may eventually explain the mutual attraction or repulsion which results.

by L. C. Debnam

A massive solar flare, 160,000 miles high.

One of the first things that any animal becomes aware of in life is the motion of objects. Man, as an animal, is able to perceive motion almost from the first instant his eyes are open, even before the shapes of objects become apparent. A moving object is easier to see than a stationary object and many animals instinctively remain motionless when they sense danger until either the danger has passed or they know that they have been detected.

Studies of the sciences have been aided throughout history by motion. The planets would not have been discovered by early man if they did not move with respect to the background of fixed stars, and subatomic particles, such as electrons, would be undetectable if they did not move.

Greek philosophers of the sixth to second centuries B.C. studied many of the abstract sciences to try to determine the logic behind the operations of nature. In their studies of motion they concluded that motion could be divided into two different types, "natural" mo-tion and "unnatural" motion. Natural motion, i.e., motion due to nature, consisted of motion toward the Earth, as this required no effort on the part of man. Unnatural motion was motion in directions other than downward, as man had to supply effort to move an object or to keep it moving in these di-rections. Some idea of the concept of friction appears in their writings, as horizontal motion through the air was considered more natural than horizon-

tal motion along the ground. For nearly 2,000 years after the time of Aristotle (384-322 B.C.) the concepts of natural and unnatural motion were the only accepted scientific "explanations" of motion. Then, in 1687, Sir Isaac Newton published his now famous three "laws of motion" which may be applied to all motion. The most important of these laws was the first because it introduced a new concept into the ideas of motion. This may be freely translated from the original Latin to the form:

"An object will not change its motion unless it is acted upon by a force."

The second law of motion is the most useful, because it relates force to

mass and acceleration, and may be applied to the solution of practical problems, but the first law combined natural and unnatural motion into the single concept of motion and at the same time resolved problems of friction, effort (in the Greek meaning of the word) and the combined "naturalunnatural" motions.

To explain the "natural" motion of objects, these laws require that the Earth exert a force on all other objects so that such things are accelerated to-ward the ground; to determine this force, Newton's attention was directed to the Moon. The distance to the Moon was known to be about 250,000 miles (384,000 kilometres) and it moved in a circular path around the Earth once every 28 days, which meant that it moved around the Earth at a speed of about 2,300 miles per hour (3,650KM/ hr). By the first law of motion the Moon would continue past the Earth in a straight line at its speed of 3.650KM/hr unless a force acted continuously to change its direction of motion and cause it to move in a circle. (When an object moves in a circle its direction of motion is continuously changing.)

Newton was able to determine that such a force would act toward the Earth and, by comparison with the gravitational acceleration of bodies near the surface of the Earth, he formulated the "Law of Universal Gravitation" which may be expressed as

$$F = G \frac{m_1 m_2}{r^2}$$
 [1]

where F is the force of attraction between two bodies of masses m_1 and m_s separated by a distance r. G is a constant known as the "Universal Gravitational Constant." With the aid of this equation the gravitational attraction between any two objects in the universe may be determined. As may be seen from this equation the more massive the bodies the greater is the attraction and the larger the separation distance the smaller is the attraction.

Gravitation is an attractive force which acts toward the centre of mass ("centre of gravity") of an object. The force acts equally on both objects involved. In the case of the Earth and the Moon the Earth is attracted toward the Moon with as much force as the Moon is attracted toward the Earth. The movement of the Earth is not as great as the movement of the Moon because the Earth is more massive than the Moon, but this force causes the Earth to have a monthly 6,000-mile "wobble" or perturbation in its orbit around the Sun. A readily observable effect of the Moon's gravitational attraction on the Earth is the existence of ocean tides in which the waters are attracted toward the Moon and a lesser known effect is the "ground tide" in which the Earth itself is distorted about 9 inches (23cm) in a regular cycle with the ocean tides.

The Earth moves around the Sun in the same way that the Moon moves around the Earth. As the Sun is much more massive than the Earth, the Earth introduces only a small perturbation of about 560 miles (900KM) per year in the Sun. The most massive planet, Jupiter, introduces a perturbation of 1,970,-000 miles (3 million KM) each 12 Earth years.



Sir Isaac Newton's laws of motion led directly to the formulation of the gravity theory.

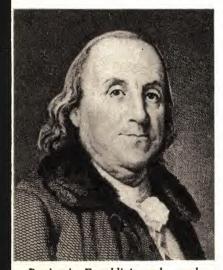
10

OF NATURE

During the preparation for the "Apollo" moon-landings, both manned and unmanned satellites were set into orbit about the moon. It was found that these Lunar Orbiter Satellites did not move at constant speeds in their orbits but travelled faster than they should have done in certain places, mainly over the comparatively flat "seas." Such perturbations in the satellite orbits indicate that generally under the "seas" are high mass concentrations, possibly — but not necessarily — deposits of heavy metals of meteoric origin.

The gravitational attraction of large masses has occasionally hindered Earth surveys. In surveying. a plumb-line is used to determine a vertical line. In most cases, the weight on the plumb line is attracted toward the centre of the Earth, thus the line points toward the Earth, thus the line points toward the Earth's centre. However, in India, the large mass of the Himalayan mountain chain is sufficient to pull a plumbline away from the vertical and much of India and Pakistan is not properly surveyed. This phenomenon has been used to determine the positions of deposits of heavy metals in the ground.

The second natural force, static electricity, was a phenomenon of nature known to the Ancient Greeks. The earliest recorded observations are those made by Thales of Miletus (one of the original "seven sages") about 600 B.C. He noticed that when amber was rubbed with fur it would attract smallpieces of chaff and straw. Systematic studies of this phenomenon were not made until about A.D. 1580 when William Gilbert, court physician to Queen Elizabeth I, performed experiments on this attractive force and published his results in a book entitled De Magnete. He named the phenomenon electricity from the Greek word electron (amber). About A.D. 1650, Otto Von Guericke, Burgomaster of Magdeburg, discovered that there was sometimes a force of re-



Benjamin Franklin's early work on static electricity prepared the ground for later research.

pulsion between electrified bodies. He proposed that there were two types of electricity, "resinous" and "vitreous." In 1747 Benjamin Franklin in-

In 1747 Benjamin Franklin introduced the terms "positive" (for vitreous) and "negative" (for resinous) electricity. Von Guericke had discovered that electric charges of different types attract each other, whereas electric charges of the same type repel each other.

In 1785 Charles Augustin Coulomb published the law of electric attraction and repulsion which bears his name. In modern terminology Coulomb's law is expressed as

$$F = \frac{1}{4\pi \varepsilon_0} \frac{q_1 q_2}{r^2}$$
 [2]

where F is the force of attraction or repulsion between two bodies with electric charges q_1 and q_2 separated by a distance r in a vacuum. E_0 is a constant known as the permittivity of free space.

Although this law was first published by Coulomb it appears that Joseph Priestley and Henry Cavendish — British scientists — were aware of it before Coulomb.

The force given by equation [2] acts along a straight line between the two charges.

The importance of static electricity mainly lay in its development of "Dynamic electricity" until near the end of the 19th Century. At that time many scientists were investigating the properties of electrical discharges in gases the forerunner to the modern fluorescent lamps and neon discharge lighting systems — and some of these noticed that when there was almost no gas in the discharge tube the end opposite the cathode sometimes glowed. This glow could be enhanced by coating the inside of the tube with zinc sulphide. This glow was presumed to be caused by "rays" emanating from the cathode and travelling in straight lines toward the anode.

In 1897 Sir Joseph John Thomson, who was to receive the 1906 Nobel Prize in Physics for his work, successfully determined the nature of cathode rays and showed that they are extremely small particles with a negative electric charge. These small particles were named electrons and were considered to be parts of atoms. Thomson also discovered the existence of particles emanating from the anode which have a charge equal to the charge of an electron but positive and a mass of 1,836 times the mass of an electron. These particles were named protons.

An atom was then assumed to consist of protons and electrons, and in 1911 the New Zealander Ernest Rutherford showed that the protons of an atom are concentrated at the centre in a nucleus and the electrons occupy positions apart from the nucleus.

If the forces of electricity had not been known, the study of the atom would not have been possible, as almost



Lightning over Sydney—a spectacular display of one of Nature's forces.

all knowledge of the interior of the atom has been obtained from the forces which act on charged particles directed into atoms. Even the particles used normally electrons and protons would not have been detected except for the electrical forces that they exert on larger particles.

One of the most common detectors of sub-atomic and atomic charged particles is the ionisation chamber in the form of a Geiger-Muller tube. Fundamentally this consists of a metal tube with a fine wire down the centre. This tube is enclosed in a glass envelope containing a gas such as argon at a pressure of about one-eighth atmospheric pressure. The tube and wire are connected to a DC supply of about 1,000 volts with the positive of the supply on the central wire. When a charged particle passes (usually at high speed) through the tube it can — due to electrostatic forces — dislodge electrons from the atoms of argon, leaving positively charged atoms ("positive ions") and free electrons in the tube. The free electrons are attracted toward the central positive wire and the positive ions are attracted toward the negative tube with the result that a momentary current flow occurs. This current pulse can then be detected, amplified and counted by normal electronic means.

Electrostatic forces are used in cathode ray tubes to control the speed and direction of motion of the electrons which impinge on the screen. For the formation of a picture on a television screen approximately 10¹⁹ (one million million) electrons strike the screen each second, i.e., about 65 million electrons

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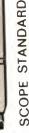
Consumes current only whilst in use. Scope De Luxe performs all the functions of other irons

all the functions of other irons from 40 to 150 WATTS. MINISCOPE—up to 75 WATTS. LABOUR SAVING Fast warm up — always ready, cuts wiping, retinning and filing of tips to a MINIMUM. VERSATILITY

Copes with all soldering jobsfrom miniature components to large solder lugs. Can even be operated from a 6 voltcar battery CONTROL

control at your Temperature finger tips. Heat only when, where and as much as needed.

Ideal for those almost inaccessible spots. No burning of adjacent insulation.



SPEED

ONLY 5 to 6 seconds' initial heating up time from cold, then practically instantaneous.

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Fully guaranteed with tested dependability. time

SAFETY

Low voltage operation. Heat sensitive components protected.

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Longer tip life. NO expensive heating elements to replace. Maintenance without special tools. Spare tips and elements readily available from your Scope Distributor.



are required for the formation of one line of a television picture. Each of these electrons has been accelerated from zero speed to about one-fifth of the speed of light (70,000KM or 44,000 miles per second) over the short dis-tance of 14 inches (36 cm) in less than one-tenth of a picosecond by electrostatic forces. Such acceleration is impossible with gravitational forces or any man-made mechanical forces.

The third force of nature, known to man many centuries ago, is magnetic force. Fragments of magnetite (natural iron oxide) found near the ancient city of Magnes (the modern Manissa, near Smyrna) were found to point in a particular direction if freely suspended. As early as A.D. 120 it was known to the Chinese that an iron rod could be magnetised by rubbing it with magnetite. In the 12th century A.D., Alexander Neckham described a pivoted iron needle that was carried on ships to plot a course.

William Gilbert was the first to sys-William Olibert was the flast to sys-tematically study magnetism, as well as electricity, but he found no connection between the two phenomena although he did find that "like poles repel and unlike attract." Before Newtons time it was sometimes considered that gravity was a magnetic effect — but this raised the problem of non-magnetic materials being bound by gravity.

Although suggestions were made that electricity and magnetism might be related, it was not until 1818 that this was proven, when the Danish scientist Hans Christian Oersted observed that a compass needle was deflected when placed near a wire carrying an electric current. Twelve years later Michael Faraday and Joseph Henry independently discovered that movement of a magnet near a conductor produced an electric current in the conductor.

In 1820 Jean Baptiste Biot and Felix Savart measured the force between two current-carrying conductors and the equation for this force in a vacuum may be expressed in modern terminology by

$$F = \frac{\mu_o}{2\pi} \frac{I_1 I_2 \ell}{r}$$
 [3]

where F is the force between two conductors of the length 1 separated by a distance r, carrying currents of I1 and I_a respectively. The constant μ_0 is known as the permeability of free space. This equation differs from equations [1] and [2] in two important respects. The first is that the source of magnetism (the currents) cannot be regarded as points, and the second is that the separation distance (r) is not squared in equation [3] so that magnetic forces may be detected over greater distances than electrostatic or gravitational forces.

If the old idea of "pole strength" for magnetic forces of permanent magnets is used however, where a "pole" is simply the collection of magnetic forces to a point source, equation [3] could be expressed in the form

$$F = K \frac{P_1 P_2}{r^2}$$
 [4]

where K is a constant and P1 and P2 are two pole strengths separated by a distance r. This equation is very similar to equations [1] and [2].

Some useful data

To compare the electrostatic and gravitational forces in the nucleus of a helium atom the following information is required.

mass of proton	
charge of proton	
diameter of nucleus	2
E	1
G	

1.67 \times 10^{-sr}kilogram 1.6 \times 10^{-sr}kilogram 2.4 \times 10^{-sr}coulomb 2.4 \times 10^{-sr}metre 8.85 \times 10^{-sr}coulomb²/(newton-metre^s) 6.67 \times 10^{-sn}metron-metre^s/kilogram²

The gravitational force of attraction between two protons in a helium nucleus is, by equation [1]

$$F = \frac{6.67 \times 10^{-11} \times 1.67 \times 10^{-27} \times 1.67 \times 10^{-27}}{2.4 \times 10^{-16} \times 2.4 \times 10^{-16}}$$
 newton:

= $3 \cdot 2 \times 10^{-33}$ newtons of force.

The electrostatic repulsion is given by equation [2] as

 $\frac{1}{4\pi \times 8 \cdot 85 \times 10^{-12}} \frac{1 \cdot 6 \times 10^{-19} \times 1 \cdot 6 \times 10^{-19}}{2 \cdot 4 \times 10^{-16} \times 2 \cdot 4 \times 10^{-16}}$ newtons

= 4000 newtons of force.

thus the electrostatic force of repulsion is about 10⁴⁰ times as great as the gravitational attraction.

One newton is approximately equal to the downward force exerted by 4oz at the surface of the Earth.

Magnetic forces are now known to be caused by electric currents - even the "permanent" magnets obtaining their forces from inter-atomic currents. Although at first sight natural magnetic forces may appear to be very weak as suggested by the Earth's magnetic field which has far less effect than gravitation — some natural magnetic forces are extremely powerful. Some of the most powerful natural magnetic forces observed have occurred on the forces observed have occurred on the Sun, which is composed of fast moving (high temperature) hydrogen and he lium atoms. At the high temperature of the sun the gas atoms decompose by losing electrons to form positively charged ions, and the motions of such charged particles constitute electric cur-rents which form gigantic magnetic fields.

These gigantic magnetic fields are thought to be the source of solar flares in which a globule of solar material some twenty thousand miles in diameter is accelerated away from the gravitational forces of the sun to a speed of (1,000KM/sec) in less than two min-utes. The energy release in such flares is a thousand million times as much as that of the atomic bomb exploded over Hiroshima in 1945.

During the International Geophysical Year of 1957-58, such flares occurred often. At one period, from late 1957 to late 1958, the Sun was observed to have two "North" poles — no "South" - existing at either of the poles. Such a phenomenon apparently occurs every eleven years, to some extent coinciding with the major sunspot and solar flarecycle, but magnetic measurements of the Sun have not been carried out for a long enough period to determine this with certainty.

It is known that throughout the galaxy, and probably the whole uni-verse, space is not a perfect vacuum but contains between ten and one thousand atoms per cubic centimetre. Many of these atoms are ionised and are in motion, thus creating magnetic fields. These magnetic fields appear to be re-sponsible for the spiral shape of the galaxy, which cannot be explained by gravitational forces.

Since the mid-1950s a new field of

physics - magnetohydrodynamics has arisen from the study of charged particles and magnetic fields, and their interactions.

The fourth natural force which was unsuspected until the early years of the 20th century is nuclear force. The nu-cleus of an atom consists of protons and neutrons—the protons being posi-tively charged particles and the neutrons uncharged particles. Electrons do not exist in the nucleus but are separate. The diameter of an atomic nucleus is known to be about one million millionth of an inch, so that this would be the greatest separation distance of the two protons in the nucleus of a helium atom. (For other atoms the separation distance would have to be less.)

By using this separation distance as r in equation (2), and the charge of each proton, the electrostatic repulsion force may be determined. As both protons are positively charged, the nucleus tends to break into separate protons. The mass of a proton is known, and as this is extremely small, it may be imag-ined that the gravitational attraction between protons is small-but the separation force due to electrostatic repulsion is about one-half ton. (See the data above for the mathematics of this calculation.) Consideration of these forces led to the belief in the existence of a short range "nuclear force" which would be required to hold the nucleus together against the electrostatic repulsion force.

To date no general equation such as the equations for gravitational, elec-trostatic and magnetic forces has been developed for the nuclear forces but the energy required to hold the nuclear particles together is generally consid-ered to be obtained from a mass deficiency. This mass deficiency is a measurable quantity of most atomic nuclei and may be determined by adding the masses of the individual nuclear particles (protons and neutrons) of which the nucleus is composed and comparing this mass with the measured mass of the nucleus. It is found that the measured mass of the nucleus is LESS than the normal mass of the constituent particles, the difference being known as the mass deficiency. The energy can

(Continued on page 174)

13

ELECTRONICS Australia, March, 1970

Here are the famous names in INSTRUMENTATION

together with the standard of service to match

A SELECTION FROM THE OUTSTANDING RANGE OF INSTRUMENTS AVAILABLE FROM JACOBY MITCHELL:



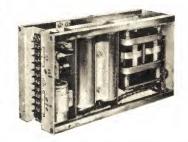


(Above) Advance TC9 Timer Counter is a 6-digit instrument capable of measuring frequencies up to 32 MHz with 0.1 Hz resolution. Freq. Measurement: 2 Hz to 32 MHz. Time Measurement: 1 μ S to 10 S in decade steps. Sensitivity: 3 position attenuator providing 10 mV, 100 mV, and 1 V RMS.



(Above) Advance TC11 & TC12 Timer Counters are designed to measure frequencies up to 15 MHz. TC11 has 4-digit display with 1 Hz resolution. TC12 has 5-digit display with 0.1 Hz resolution. Freq. Measurement: 2 Hz to 15 MHz. Time Measurements: TC11 10 μ S to 1 S, TC12 10 μ S to 10 S. Sensitivity: 10 mV, 100 mV and 1 V RMS. Tick for further details.





(Above) Advance PM Series Stabilised Modular Power Supplies are designed in modular form to be used as integral parts of other equipment, either singly or in multiples. Voltage Range 0-50 volts. Current capability 500 mA to 10 A. Fully transistorised, with silicon semi-conductors which permit operation up to $+60^{\circ}$ C.

Tick for further details.





(Above) Jayem S100 Tr Multitester provides AC and DC measurements, also resistance, capacity and level. Also measures the more important parameters of transistors, both NPN and PNP types. DC 100,000 o.p.v. A 3" anti-parallax scale and sensitive 7.5 μ A meter. Shockproof suspension and full overload protection.



(Above) Jayem JM-01 Micromegmet is designed for the rapid and accurate testing of insulation resistance such as motors, generators, power-lines, etc., and for voltage detection and continuity checks. Rated voltage is 500 V and measuring range is 0.01-100 Megohms. Fully transistorised with 1 transistor and 4 diodes. Only 6" x 31/8" x 15/8", in soft leather carrying case with 1 pr. of test leads.

KOVO

(Right) Kovo Megmet is a portable insulation tester for measuring insulation resistance of DC and AC mains, machines and appliances. The generator is driven by 2 sets of gears, the tooth wheels being of



bronze and the pinions of steel. Models Available: Megmet 500 500 V, Resistance: 50 Kohms to 50 Megs; Megmet 1000 1000 V, Resistance: 100 Kohms to 100 Megs. Tick for further details.

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ELECTRONICS Australia, March, 1970

Computer Graphics in Engineering Design

New storage and display techniques developed in the U.K. to allow direct access to computers by engineering staff will eliminate the administrative bottlenecks which occur when all computer work is channelled through computer operators.

By A. H. Thomas, B.Sc., M.I.E.E.

Since their earliest days, computers have been used in the solution of have been used in the solution of specific engineering problems; that is those problems which can be expressed in mathematical form (perhaps of great complexity) and are capable of solu-tion, given the necessary data, by a continuous run of the computer without human intervention. The delays associ-ated with the operation of most comated with the operation of most computer installations mean that several hours or tens of hours may elapse between the submission of a problem and the receipt of its solution by the engineer. Much, perhaps most, engineering design work is repetitive in nature, requiring several solutions of the same mathematical formulas with slightly different input data. This means that the total time required to complete a design is determined by the delays in the computing department rather than by the time needed for the designer to make the necessary decisions at each step in the procedure, or by the actual time needed for calculation by the computer.

Sometimes it is possible to incorporate the necessary repetitions in the computer program, where the choices involved are sufficiently predictable, for example in the design of transformers. In many cases, however, the judgment of the designer is needed at each stage. For instance, a choice between several possible courses of action may be needed, involving a logical procedure too complex to program or requiring value or aesthetic decisions. An example of this is the design of the interconnection patterns for printedwiring boards or integrated circuits. Whereas it is relatively easy to program the computer to route most of the conductors, it is very difficult to make it route them all satisfactorily. The intervention of the designer simplifies the process greatly and makes use of a human skill not possessed by a computer, that of comprehending an overall pattern.

The efficient use of computers for engineering design thus requires that the designer has instant access in order to eliminate his waiting time. This can be provided simply by connecting a typewriter directly to the computer, so that the designer can feed in data, call up or feed in the appropriate program, and receive output in printed form. Since, however, a single designer would not occupy fully even the smallest computer because of the slow speed of the typewriter but principally because of the time needed for thought before calling for a calculation many terminals must be connected to the computer so that overall it is satisfactorily loaded. Multi-access systems of this type are now becoming commonplace and are, of course, useful for other iterative procedures such as program writing and information retrieval.

An engineering designer does not, however, communicate only or even mainly by the printed word. He expresses his ideas in the form of drawings, so that the use of a tele-typewriter requires a translation into alphabetical and numerical form.

The computer output may sometimes best be expressed in the form of a graph or histogram rather than as a single numerical value or table of values. The designer will wish to study this and if necessary modify his original drawings and call for a recalculation.

A graph or drawing may, of course, be delivered by a computer using a mechanical plotting machine and if no further steps in the iterative design procedure are needed, this may be quite satisfactory, particularly where great precision in draughting is required. But when the designer wishes to alter the design and call for further work by the computer, he needs first to get the drawing from the computer quickly so that he is not kept waiting unproductively, and second to be able to modify the drawing directly or to specify new numerical values.

An engineering designer therefore requires a combined input and output device attached to the computer having this graphical and interactive capability. Such a device is the graphic display, in which the drawing and alphanumeric information are presented on a cathode-ray tube.

The high writing speed of a cathoderay tube enables drawings to be presented rapidly, complete with all necessary annotation. Although the resolution-value of the screen limits the complexity and accuracy of the drawing that can be produced, it is possible to cause part only of a complex drawing to be displayed, either by scalechanging, to magnify a detail of particular interest, or by regarding the screen as a "window" through which any desired portion of a large drawing can be seen.

The designer must in the first place make his drawing on the cathode-ray tube. The position of the cathode-ray spot on the screen is controlled by the computer, and some means must be provided to allow it to be moved about by the designer. This can be done simply by typing appropriate x and y co-ordinate values on a keyboard connected to the computer, but unless great precision is needed this method is too slow.

More direct movement of the spot can be achieved by means of a tracker ball, in which the movements of a freely rotatable sphere are signalled to the computer and cause the spot to execute corresponding movements; a control column may be used in a similar fashion. An analogue of the screen may be set up consisting of a plate over which the movement of a stylus causes a corresponding movement of the spot.

The most commonly used device for moving the spot is the light-pen. This consists of a holder containing a photoelectric cell connected to the computer in such a way that the instant at which



Employing a light-pen for plotting design data on the display screen of an Elliot computer.

NO OTHER GENERATOR PROVIDES 0.1% DISTORTION PLUS THESE FEATURES FOR ONLY \$76 MODEL bwd 140A VERY LOW DISTORTION SINE & SQUARE WAVE GENERATOR.

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A light-pen may thus be used to make drawings in two ways. In the first of these, the computer is caused to present on the tube a grid or matrix of spots. The light-pen is used to indicate two of these spots to the computer, which, on the pressing of a key on an associated keyboard, will cause a line to be drawn between the two spots. Proceeding in this way, a complete drawing may be built up; if the grid of spots is too coarse, a finer grid may be drawn locally in the area where greater precision is needed. Circles and arcs may be drawn by various methods, such as by indicating three points, by indicating one point and typing in the required radius on the keyboard, or by indicating the ends of an arc and typing in the radius.

In the second method, no grid of spots is presented. To draw a line, the light-pen is used to move the tracking symbol to the position required for one end of the line, then to that of the other end. Depression of appropriate keys causes a line to be drawn between the two points. Circles and arcs may be drawn in a similar way to that of the first method. This method is similar to freehand drawing, and it is possible for the computer to apply constraint such that, for example, lines can only be drawn horizontally or vertically.

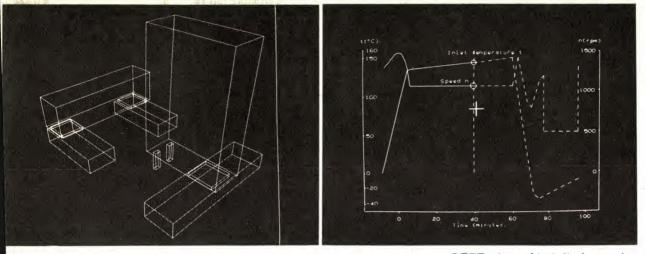
Many drawings, particularly symbolic ones such as electronic circuit diagrams, contain repeated elements and repeated groups of elements. To save work, it is important for the designer to be able to draw a certain element once, to move it as a whole about the screen and cause it to be repeated as often as required. It should also be possible to combine certain elements into a group and then to treat the group as an element in itself which may be repeated as required. For convenience, it is desirable that it should be possible to invert elements or make mirror images of them and to expand or contract elements to different sizes.

Alteration of a drawing requires that it be possible to delete an element by pointing at it with the light-pen, without deleting other similar elements but at the same time deleting other associated elements, such as the wires connected to an electrical resistor or the dimension lines belongings to a group of holes. Further requirements are those mentioned above for windowing and scale-changing of the complete picture. Scale-changing may call for the deletion of detail too fine to be resolved on the screen.

The process of building up a picture and subsequently modifying it is thus complex and requires an elaborate system of storing the data in the computer. This is called the "data structure," and its design represents one of the most complex problems in the creation of graphical display systems.

BWD/7

A light-pen may be used, as mentioned earlier, for pointing at elements



of drawings which are to be deleted or amended. It may be used directly in its tracking mode to alter a picture by moving the ends of lines or the junction of groups of lines. In the pointing mode, it may be used as the "key" of a "keyboard" in which the "keys" are symbols or words in plain English displayed on the screen of the cathode-ray tube. In this way, an infinite number of key functions may be provided rather than the finite number available on a mechanical keyboard. This arrangement of "light buttons" is often preferred for convenience to the use of the keyboard for the insertion of numerical data, since it is not necessary for the designar to take his eyes from the screen or to attempt to operate the keyboard with his free hand.

Having made the drawing, the deigner may call for a calculation to be arried out — perhaps of the stiffness of a structural member, the complex ross-section of which has been drawn, or of the electrical characteristics of a ircuit of which the diagram has been trawn. An immediate answer may be resented to the designer, in the light of which he may if necessary modify the trawing and call for further calcuations. These calculations, as are all ther functions, are set in motion by lepressing keys on the keyboard or electing light-buttons with the lighten.

The computer must be provided with he appropriate software to operate the isplay, cope with light-pen and keyoard outputs, establish the data strucure and call up the appropriate rouines to carry out the design calcuations. The provision of adequate softvare and applications programs is the ey to the achievement of a successful omputer graphics system for comuter-aided design.

The computer must have a store of ifficient size to hold the complete data ructure relating to the task in hand, lus the programs and any data needd in the calculations. Since one deigner cannot occupy a machine continously, in order to load it economically must be capable of carrying out other vork while he is occupied in thought. his other work may be a background ob or jobs of low priority run in the ormal batch-processing mode, or it nay be that of designers using other isplays connected to the machine. his requires a further allocation of omputer storage and the provision of a backing store of the disc or drum type.

Most displays require that the picture be presented on the screen between 15 and 50 times/second, to avoid flicker. The repetition rate used is dependent on the type of phosphor employed. To avoid loading the computer with this surely repetitious task, a small buffer store is usually provided for the display which is cyclically read at the required rate. However, such a buffer is very like part of a computer and it is found useful to expand it into a small computer so that it can carry out some of the minor functions which would otherwise have to be performed by the main computer, such as handling signals from the light-pen and managing that part of the data structure corresponding to the portion of the total data structure visible on the screen. The main computer is then left to carry out calculations, to hold the major portion of the data structure and perhaps to hold common data files and common programs of use to more than one display.

When this is done, the transmission rate of data between the central computer and a display is reduced, and it therefore becomes easier to site the display remotely. Such remote siting is necessary in large organisations with a number of design offices, or for smaller organisations having their own displays but connected to a large, shared machine for major calculations and common data storage.

The concept thus emerges of a satellite system, consisting of a central computer of high capability and having substantial storage capacity, connected over private wires or the public telephone system to a number of satellites, each consisting of a small computer. display, light-pen and keyboard. Some systems of this kind are in operation, but no clear rules can yet be stated to indicate precisely what work should be done in the central and satellite computers and what rate of data transmission should be employed. Much depends on the relative economics of computers and data transmission.

Displays can be used for work outside the immediate design area; for example, information retrieval, stock control and the drawing and amendment of program evaluation and review technique (PERT) charts for project control. Some of these tasks do not need the capability of presenting drawings, LEFT: A graphical display used to apply perspective to a furniture design drawing.

RIGHT: Visual display giving input and output characteristics of equipment under test.

for example, stock control and much information retrieval work. Simpler displays having the ability only to present alphanumeric data may therefore be used. They are electronic versions of the tele-typewriter, having the advantage of high writing speed and noiseless operation but also the disadvantage of not providing a printed record, or "hard copy." This type of display, with an associated keyboard, has, however, enjoyed the greatest volume of sales, mainly in applications outside engineering design and particularly for airline seat booking.

Application of computer graphics to engineering design is still in an early stage of development. It is clear, however, that the technique is of great potential benefit, not necessarily, if at all, in design work of the highest creativity, but in helping with many of the routine design and drawing office tasks which are needed between the initial conception of a product and its readiness for production.

The ability of a display to provide two-way communication between designer and computer means that the designer can be guided through a complex, though routine, design procedure, and be given access to computation power or standard data just when he needs it. The main benefit of this is likely to accrue from the shortening of the design period, reduction in errors in procedure, and improved accuracy. It is also possible to generate component or material lists automatically, and for modifications of the design to be reflected immediately in amendment of these lists. Reduction in design time and eventually of cost means that a design can be prepared in response to a customer's inquiry which is both accurate and precisely costed, thus probably allowing a more competitive price to be quoted.

Pioneer work in industry and research establishments shows that computer graphics has an assured place in computer-aided design. Further development of the hardware and software, and of the techniques of application to practical problems, will ensure its eventual use throughout industry. AUTOMATIC EQUIPMENT TESTER

30,000 **ELECTRONIC** TESTS IN LESS THAN TWO MINUTES



The CATE computer controlled equipment tester.

Fully automatic post-production testing of complex digital and analog electronic equipment can be carried out by computer controlled test systems developed in the U.S.A. by the Convair Division of General Dynamics. Up to 30,000 separate tests can be completed in one minute 50 seconds.

Called Convair Automatic Test Equipment (CATE), the new systems are controlled by Varian 620/i general-purpose computers with 16K memory which allow the single technician operator required by each system to initiate a test merely by typing in the part num-ber of the item to be tested.

According to Electronics Group Engineer, B. A. Penners, the CATE systems now in operation at Convair each have testing capability of 10,000 units (ranging from electronic modules to rack-size systems) per month on a twoshift basis.

The requirement for automatic test-ing arose with the F-111 AGE logic modules. After evaluating the buy or build decision, Penners' group chose the latter course in order to achieve the following unique equipment characteristics:

- 1. a system totally under computer control;
- 2. internal loading and switching by computer controlled switching systems:
- 3. a universal adapter configuration to accommodate 550 or more types of modules and subsystems.

The CATE 1082 product was the first system developed with the above characteristics. It contains a general purpose integrated circuit digital com-puter and related peripheral devices, computer interface electronics for con-tablication that activity the statement of the statement to the statement of the statem trolling the station, test stimuli sources, signal measurement and detecdevices, an automatic matrix tion switching device, test loading devices, an adapter subsystem for the devices to be tested, and an extensive software package to fully utilise all hardware components.

The test set computer that supervises and controls all testing is a Varian 620/i with peripherals. The standard

test stimuli supplied are fixed loads, fixed voltage sources, programmable power supplies, addressable registers and flip-flops, and pulse lines. Signal measurement and detection devices include a 32-channel analog-to-digital converter, a pulse timer, addressable registers, and sense lines.

Subsequent requirements arising from the F111 AGE program dictated the need for a second (and more versatile) test system, designated CATE 1109. Like its logic-oriented predecessor, this nearly universal test system centres on the Varian 620/i minicomputer as a controlling element. In addition to duplicating the logic test capability of CATE 1082, the new system also fully utilises the capabilities of such versatile instruments as a waveform analyser, a pulse generator, a waveform generator, a volt-ratiometer, seven programmable power supplies, and others.

In spite of the impressive capabilities listed above, Penners feels that the system's real strength resides in a Convair designed switching system which allows simultaneous interconnection of any (or all) test instrument(s) to any part of the unit under test. Additionally, electrical loading for each UUT pin may be automatically set under program control.

Test programs are written in a sim-plified form of Fortran which can be learned easily in about two weeks with no prior programming experience re-quired. An extensive software library reduces the test writer's task essentially to calling library sub-routines in the proper order. The test programmer is not required to understand digital computer hardware or system software to write complex and detailed test programs.

To start a test sequence, the operator types in the part number of the item to be tested on the teletypewriter key-

The resident portion of the board. supervisory program that is always in the computer interprets this request and searches the magnetic tape on which all test programs are stored. After the appropriate program is After the appropriate program in found, it is loaded into the computer

found, it is loaded into the computer and testing begins. Each test begins with a confidence self-test of CATE 1109 or CATE 1082 before proceeding to the device being tested. During testing, messages may be printed which direct the operator to take some particular action, such as plugging in the unit to be tested and making an adjustment. The specific op erator communication during any test-ing situation is determined by the test program. This communication will vary greatly from situation to situation. For example, in one large failure diagnostic application of CATE, the particular test number and test values which failed examples of the situation of the s failed are printed out along with voltages occurring at all other test points a the time of failure.

This information is used in diagnos ing the failure and determining correc tive action. However, operator communication capability can take on any de-gree of complexity depending on how the test programmer designs his pro-

gram. The specifications for the CATE computers are:

cycle 1.8-microsecond memory time.

- 16-bit word length.
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- Eight priority interrupt levels.
- Direct memory access.

• Single and double word instructions with direct, indirect, relative, and indexed addressing.

 Buffered interface controller allowing simultaneous computation and input/output.

Computer peripherals include a magnetic tape transport (25-ips. 556 or 800 bpi), teletype, and a 300 CPS paper tape reader. The entire CATE 1109 test system, excluding teletype console, mea sures 117 inches wide by 81 inches tal by 33 inches deep with a 68-inch-wide work shelf. The system requires no stringent environmental controls.

ELECTRONICS Australia, March, 1970

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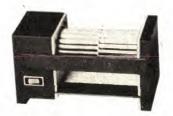
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POST OFFICE PREPARES

The advent of colour TV to Australia will require that the TV relay systems provided by the P.M.G.'s Department be capable of handling a much more complex signal than is needed for monochrome TV.

In February, 1969, the Postmaster-General, Mr Hulme, announced in the House of Representatives that the PAL (Phase Alternation Line) colour television system would be used when colour television transmissions were introduced in Australia.

The PAL system was recommended by the Australian Broadcasting Control Board after careful assessment of the relative advantages of the three main systems (NTSC, PAL and SECAM) now in use in other parts of the world.

The NTSC system was introduced in the U.S.A. early in 1953 following a recommendation of the National Television System Committee. A tribute was paid to the NTSC system by Dr W. Bruck of Telefunken, who was largely responsible for the development of the PAL system, when he stated in a lecture to members of the Institute of Electrical Engineers in London in 1965, that the NTSC system belongs to the outstanding physical and technical masterpieces of our century.

The PAL system is a variant of the NTSC system. The main virtue of the PAL variation is its ability to com-

Based on an article by R. W. Harnath, F.I.R.E.E. (Aust.), A.R.M.T.C. (Divisional Engineer, Long Line Equipment Section, P.M.G.'s Dept.) pensate for some of the distortion which inevitably occurs between the studio where the signal is generated and the domestic colour television receiver picture displayed. The PAL system advantages and the significant improvements in circuit design and manufacturing, which have become possible largely through solid state devices, now promise that the colour television receivers for the coming Australian service will be many times more reliable and stable than the valve-operated receivers in use when the NTSC system was first operated.

The SECAM (sequential and memory) system is, like PAL, very tolerant of distortion in the transmission system. A choice between SECAM and PAL depends not only on an engineering evaluation, but also on a subjective comparison of both systems. A final subiective comparison by human observers is necessary because the PAL and SECAM systems differ in their characteristic errors which, therefore, cannot be related by objective measurements. The television studio equipment, relay systems and transmitters of the

The television studio equipment, relay systems and transmitters of the present Australian black and white television service are now being evaluated in terms of their suitability for colour television. To allow time for the conversion of equipment and the production of colour television receivers, the Postmaster-General has also said that 18 months' notice would be given of the date of commencement of colour transmissions.

In the case of the P.M.G.'s Department, with its extensive network of video relays and national television transmitter stations throughout the Commonwealth, this 18-month period would not allow all the conversion, upgrading and installation of equipment which must be accomplished before the colour "on-air" date. Preparations must therefore commence as soon as possible if the work is to be completed within reasonable time. In fact, considerable work has already been done in preparation for the changeover.

This article does not include the difficulties applying specifically to television transmitters, which it is hoped will be covered by a subsequent article, but concentrates on the difficulties arising in relaying colour television signals.

Monochrome or black and white television signals contain two basic types of information. The first is synchronising information which sets the time pattern for the display. The second type of information provides the luminescence signal which controls the brightness of the cathode ray tube to provide the picture. Colour uses similar basic synchronising information, but includes two additional types of information. The first of these is the "colour burst" which is an addition to the synchronising information and which allows the extraction of the correct colour signal phase relationships at the receiver. The second is the "chrominance" signal—conveying information as to colour (hue) and intensity (saturation)—which is additional to the lumi-

Convertible Colour TV Camera

A new monochrome broadcast TV camera which can be converted to colour at any time has been announced in the U.S.A. by Ampex Corporation.



The new camera, Model BC-210M, is designed for studio or outside broadcast use. It uses a single Plumbicon pickup tube, and is basically a one-tube version of the Ampex two Plumbicon colour camera Model BC-210. The BC-210M can be converted to full broadcast colour capability by the addition of a single colouring channel.

The BC-210 colour camera has a simple optical system which splits the visible spectrum into luminance for one of the tubes, and red-blue, in alternate fields, for the other, by means of a revolving two-colour filter wheel locked to vertical sync. The missing colour fields are replaced by using a 262-line delay in conjunction with field frequency switching. Each colour field is thus used twice, once as the original signal and once as a delayed signal. The three signals (red, blue and luminance) are then fed into a matrix in which green is obtained by subtracting appropriate proportions of blue and red from the luminance signal.

The BC-210M is expected to be used by small commercial stations and by educational networks which may want to convert to colour operation at a future date. When converted, the BC-210M performs identically with the BC-210.

FOR COLOUR TV

nescence signal used in monochrome transmission.

To retain about the same overall frequency bandwidth for the colour signal as for the black and white, the colour information is carried in the high frequency end of the normal television signal, using two-phase amplitude modulation of a sub-carrier signal. As far as a black and white signal is concerned this added colour signal is a spurious signal. However, by choosing a sub-carrier frequency with a precise relationship to the line and field scanning frequencies of the television system, a fine spatially interleaved interference pattern is produced which, with the persistence of vision effect of the eye, has minimum visibility.

In the PAL system, the sub-carrier has a frequency of approximately 4.43MHz which, when modulated with colour information, produces side band signals at frequencies up to 1.3MHz above and below the carrier frequency.

This means that the energy distribution of a colour signal is very different to that of a monochrome signal, particularly at the high frequency end of the band, and also that the bandwidth requirement for a colour television signal is approximately 5.7MHz instead of the 5MHz commonly used for monochrome.

It should not be implied from this that a colour TV receiver needs to have a video bandwidth of 5.7MHz. In fact, his would not be practical, because the bound carrier occurs at 5.5MHz and ransmitters and receivers are both deigned so that the video bandwidth loes not extend significantly beyond 5MHz for either black and white or colour. In the case of a colour signal, he full 1.3MHz lower sidebands from he chrominance sub-carrier (from 4.43MHz down to 3.13MHz) are transnitted but, of the upper sidebands, only he lower frequencies are transmitted, is permitted by the approximate 5MHz imitation.

Thus, the chrominance signal uses a restigial sideband system, very similar o the vestigial sideband system used by he luminance or monochrome system. This means that both the transmitter nd receiver response curves must be ailored to satisfy these requirements.

As far as relay systems are conerned, it is necessary to transmit the ull 5.7MHz bandwidth, in order that he transmitter will be presented with a ignal which is as nearly perfect as posible. Whatever tailoring is to be done nust be done at the transmitter. Any ttempt to do this within the relay netvork, when the transmitter is already lesigned to do the job, could result in erious complications and degradation of the picture quality.

There are two results arising from he need to accommodate the chromiance sub-carrier. The first is that reponse of video circuits above about MHz, which previously was relatively ess significant than the lower frequeny performance in terms of picture uality from the television receiver, ow becomes highly significant.

The second is that caused by the

larger signal frequencies, due to the colour signal components, which require parts of television amplifiers and other equipment, where the high frequency load impedance is largely capacitive, to have a much greater power or voltampere capability to carry colour signal without distortion. For example, it can be shown that an amplifier which has a flat frequency response to 5MHz can be completely inadequate in handling this high frequency power requirement.

In order to ensure that the equalisation of relay equipment is adequate, a new test signal is being introduced. Monochrome transmission circuits were lined up using a 2T pulse and bar. The energy distribution of a 2T pulse falls off progressively above 2.5MHz and approaches zero at 5MHz, so that systems lined up using this signal can have significant equalisation errors above about 3MHz. The new test signal, in addition to 2T pulse and bar, incorporates a "20T" pulse, modulated with the colour sub-carrier frequency. The 20T pulse has exactly the same sine squared shape as the 2T pulse, but has 10 times the duration.

The extended duration 20T pulse provides heavier loading, and therefore a more exacting check, at the lower frequency end, while the colour sub-carrier provides a heavier loading and more exacting check of the high frequency end. The use of this combined signal gives an energy spectrum which is much more uniform over the whole band and thus provides critical testing of the equipment performance at all frequencies.

To test the capabilities of the transmission equipment for high frequency power performance, a method usually known as "differential gain and phase" testing is being introduced. This test uses the same sawtooth or staircase linearity testing waveform previously used for monochrome circuits, but in place of the 1MHz modulation frequen-cy previously applied uses the cy previously applied, uses the 4.43MHz colour sub-carrier frequency the as a modulating signal. By means of a special receiving equipment which compares the phase of the colour burst and of the recovered modulated signal, it is possible to obtain information regarding the change of phase at this frequency which occurs when the information signal varies from black level to max-imum. Differential gain is also mea-sured by the same test gear, in a similar fashion to previous non-linear tests at 1MHz. These two factors are important because they change the "hue" and "sa-turation" of the observed colour signal from the original states impressed on the relay.

Most long distance radio relay systems have adequate bandwidth to cope with the 5.7MHz colour requirement, but the early types of cable video systems used in Australia cut off fairly sharply above 5MHz. To change the equalisation capabilities of these systems would be prohibitive in cost, and it will therefore be necessary to replace older equipment gradually with new equipment which has an intrinsic bandwidth exceeding 7MHz.

The reference to "old" and "new"



The repeater station at Madden's Plains, south of Sydney, is typical of similar broadband repeaters all over Australia. These must be capable of handling the more complex signals when colour TV is introduced.

cable video systems introduces an interesting sidelight into this overall story. Cable video systems, as distinct from "radio" or "carrier" systems, transmit video information directly, at the video frequencies. They are used for relatively "short haul" applications, as between a capital city terminal and a switching centre a few miles away, or from a switching centre to the TV studios. Repeaters are required every five or six miles and the maximum distance is normally limited to the use of a maximum of three repeaters.

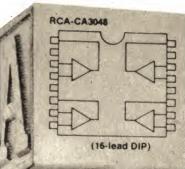
The "old" cable video equipment used by the P.M.G.'s Department was imported and used valves. When this was due to be replaced the Department looked around for something more modern, using solid state techniques. It transpired that there was nothing offering on the world markets which would meet the Department's specifications, so the Department went ahead and developed its own equipment, in conjunction with a leading Australian manufacturer, and this equipment has subsequently been manufactured in quantity.

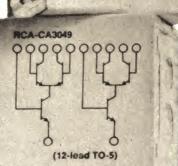
One benefit arising from the replacement of the older valve equipment is that the operating costs of the new equipment are very low. Also, the cost of providing no-break AC power for the older rack could exceed \$700 per annum, depending on the no-break plant being used. An additional advantage is the elimination of valve aging, which in the older equipment caused changes in the equalising characteristics thus requiring re-equalisation of the system at random intervals. (From "Telegen," December, 1969.)

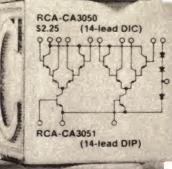
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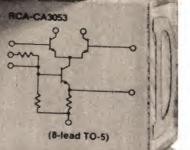
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P.M.G. Conducted Survey

Do Bushfires Impair Radio Communication?

Post Office researchers have reported that they have found no significant interference to radio transmission during recent investigations into the problems of radio communications during bushfire fighting.



The experiments were carried out during "Operation Euroka" in Queensland last October, and followed requests for an investigation into apparent radio failure during last summer's fatal fires at Lara, Victoria.

The Post Office Research Laboratories report says that the overall conclusion from the Euroka investigations was that fire-edge to fire-edge radio communications between mobile transceivers fitted to trucks, and fire-edge to base station communication were not affected significantly.

However, in other bushfires, different atmospheric conditions, different fuels and strong winds may produce substantially more severe temperature patterns to those experienced in the Euroka fire. It is therefore not impossible that the subrefractive conditions observed at Euroka could become more marked, and have significant effects on communication between a fire-edge vehicle and a distant base station with low aerials. Under such conditions, radio waves curve upwards, thus weakening signals received at a distant base.

The Post Office team's experiments covered the radio frequency bands used by bushfire fighting organisations and also the frequency bands used in the national trunk telephone microwave radio systems.

For the microwave measurements, special equipment was available, some of it produced by Standard Telephones and Cables Pty. Ltd., and the rest developed by the Post Office Research Laboratories.

However, there was no comparable equipment available for measuring HF and VHF and in the brief preparation time before Operation Euroka these units had to be made up from transceivers normally used for point-to-point communications by Post Office research field teams. They were assembled from Treager and S.T.C. mobile sets.

Collaborating with the Post Office team was a three-man team from the University of N.S.W., led by Professor P. Angus-Leppan, of the University's Department of Surveying.

For the HF and VHF measurements, the Post Office team set up three units in a simulated bushfire fighting situation. There were two "near" stations, each 140 yards from the fire edge and transmitting a distance of 800 yards, including 500 yards across the flames. Aerials for these units were mobile "whips" on vehicles adjacent to instrumentation shelters.

Transmissions were also received at a "fire brigade base" station 15 miles away, with a Yagi aerial mounted on a 120ft tower and with long-wire vertical HF aerials run down from the tower summit.

Measurements at the trunk system frequency of 450MHz and 4,000MHz were made using transmit and receive aerials 25ft above the ground on masts beside the instrumentation shelters at the "near" stations. Transmit and receive aerials were also installed at the top of the mast at the remote station.

At the "near" receiving station, the vertical angle-of-arrival of the 4,000MHz signal was measured continuously.

The University of N.S.W. party made precision measurements across the fire testing optical refraction and range. Ranging was done with three MRA101

Amateurs Please Note

The results obtained from "Operation Euroka" can only be regarded as inconclusive. The situation exists, therefore, where more data is required. Amateur operators may be able to provide such data, and thereby undertake a public service, by making observations during actual bushfire conditions of fluctuations in normal reception behaviour over paths they are accustomed to working.

tellurometers, now a standard measuring instrument in precision surveying. These instruments measure the transmit time of 10GHz radio signals between "master" and "slave" units and had an accuracy of about half-a-centimetre at this range.

During the fire, the Post Office radio signal strengths varied slightly both above and below the levels before the fire was lit, but signal minima were rarely more than 5dB below the "preburn" levels. Averaged over the eight major attenuation measurements made (five on the short path, three on the long) the total range of signal variation was below 11dB. For the long path it was below 7dB.

The Post Office measurements of the angle-of-arrival showed a decrease at 4,000MHz — the apparent position of the transmitting aerial being lowered. This effect was more marked in the university measurements with tell-urometers, which were employing a lower ray height across the flames.

A ray about 4ft above the piled timber showed a maximum range "shrinkage" of 5cm, due to an increase in radio wave velocity, while similar measurements at about nine feet above the timber showed no change at a time when the lower path appeared shortened by 3cm.

Brief tests were also made with a laser beam across the fire and first indications are that it could offer useful qualitative data on the degree of turbulence and on mean refraction (hence temperature gradients).

The six-man Post Office research team went into Operation Euroka at short notice, when it was learned that the Department of Supply was to conduct the experiment with 6,000 tons of bulldozed brigalow scrub to test fire patterns.

The Post Office saw it as a unique opportunity to study the effects of bushfires on radio propagation in circumstances wherein many aspects of fire and weather behaviour were being accurately measured simultaneously.



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FIRST AUSTRALIAN FARADAY LECTURE

The 1968-69 Faraday Lecture, entitled "Microelectronics," originally presented in U.K. by Mullard Ltd. for the Institution of Electrical Engineers, is to be staged in four Australian capital cities, during March, by the Institution of Radio and Electrical Engineers Australia.

The Faraday Lectures are an annual event in the U.K., organised by the Institution of Electrical Engineers. They are held to commemorate the great British physicist Michael Faraday, whose research into the principles of electromagnetic induction laid the founlations upon which the science of elecrical engineering was subsequently puilt. Arrangements have now been completed for the I.R.E.E. Australia to present the 1968-69 lecture in Australia. The I.R.E.E. is the first body to sponsor Faraday Lecture outside the U.K.

The 1968-69 lecture in the U.K. was elivered by Mr Peter Trier, director of esearch and development, Mullard td. It was given 29 times in the U.K., n 12 major centres, to audiences otalling about 60,000. The Australian ectures will be given by Mr Edward . Emms, who is head of the Mullard lentral Applications Laboratory, and tho was deputy lecturer for the U.K. resentations. He will be assisted by Ir David G. Dewdney, manager of the Iullard Electronics Centre in London. The lecture has been most carefully

The lecture has been most carefully repared, and involved months of work y a team of planners in the U.K. In ddition to numerous slides and film lips, which are used at every stage of he lecture to add visual impact, the cturer is aided by elaborately nounted large-scale models, which are nanipulated by a team of assistants.

The lecture begins with a brief hisprical survey of the techniques which re-dated the transistor revolution. ransistor theory is covered next, and t this section of the lecture use is ade of an elaborate model using ploured balloons to represent elecons and "holes" which move about trough the three sections of the odel representing the emitter, base and collector. This is designed to show the audience what really happens to electrons in transistor action, and how their wanderings can be controlled at will to provide not only current amplifiers, but also other solid state devices—switches, resistors, capacitors and diodes.

This section leads readily into the miniaturisation of electronic devices, the need for which is illustrated graphically by the complex circuitry associated with the flight deck of an airliner, a modern telephone exchange and a rocket launching. The planar technique is discussed, and its application to microcircuits techniques is shown with the aid of another large scale model, prepared in great detail, which allows the various stages of manufacture to be built up a step at a time. The last section of the lecture is concerned with the application of microcircuits to modernday electronics, showing how they are already being used in computers and other complex equipments, and giving a glimpse into the future, when they will be used in everyday domestic equipment.

It should be obvious from the foregoing that the lecture is pitched at a popular rather than an engineering level. In fact, the subject matter has apparently been very carefully prepared to cater for the widest possible audience, and even those with little or no prior knowledge of the subject should have no difficulty in understanding the material presented. Accordingly, no restrictions have been placed on attendance.

Even those to whom the subject matter is not new should find the methods of presentation, involving special lighting effects and staging techniques, a most interesting spectacle. People in the electronics industry will also be presen-



Mr. Edward T. Emms, B.Sc., C.Eng., F.I.E.E., A.R.C.S., F.I.M.A.

ted with an opportunity to introduce their families and friends to the matters with which they are closely involved each day.

The lectures are to be presented in accordance with the following program:

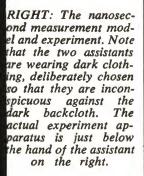
SYDNEY: Friday, March 6, at 12 noon, 2.30 p.m. and 8 p.m., and Saturday, March 7, at 10 a.m., 2.30 p.m. and 8 p.m., in the Science Hall, University of N.S.W.

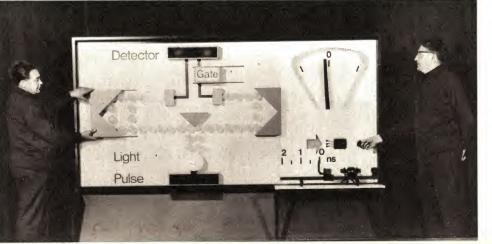
MELBOURNE: Tuesday, March 10, in the Storey Hall, Royal Melbourne Institute of Technology, at 11 a.m., 2 p.m. and 8 p.m.

ADELAIDE: Friday, March 13, in the Brookman Hall, South Australian Institute of Technology, at 10 a.m., 2 p.m. and 8 p.m.

CANBERRA: Wednesday, March 18, in the Canberra Theatre, at 10.30 a.m., 1.30 p.m. and 8 p.m.

In Sydney, arrangements for attendance can be made with Mr K. Knight, secretary of the Institution of Radio and Electronics Engineers, simply by phoning (27-1039). Similar arrangements will apply in Melbourne, where reservations can be made through Mr R. Crow, principal of the Royal Melbourne Institute of Technology (34-0234); in Canberra, Mrs Schultz, 44-361; and in Adelaide, Mr D. Cox, 233-866.





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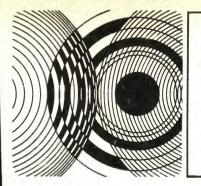
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TECHNICAL DIGEST

Laser Altimeter used as calibrating tool

A pulsed laser altimeter developed in U.K. by Elliott Brothers (London) Ltd. will be used as a calibration tool for radio altimeters, which suffer from inaccuracies due to terrain penetration effects at radio frequencies.

It is not possible to use a laser equipment as a prime altimeter due to the degradation in performance under poor visibility conditions as a result of backscatter and attenuation of the laser energy. The equipment has been designed to operate in the environment of a combat aircraft and is at present undergoing acceptance trials in a Comet system is an altitude range of 15 to 2,000 feet and an accuracy of ± 5 feet or $\pm 1\%$ whichever is the greater.

A block diagram of the system is shown in figure 1. The transmitter is mounted coaxially with the receiver to avoid parallax problems and make maximum use of the circular window area available in the trials aircraft.

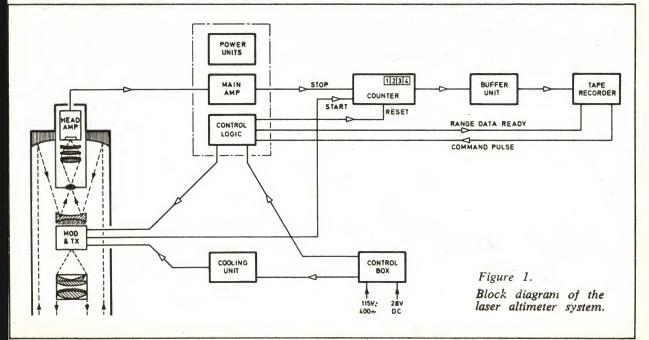
The transmitter employs a gallium arsenide semiconductor laser diode which is mounted inside a vacuum Dewar flask and cooled to around 80°K. The vacuum envelope ensures low heat transfer from the outside of the Dewar to the cold laser, thus allowing high cooler efficiency and preventing misting of the Dewar exit window. It is necessary to operate at low temperatures in order to achieve a high laser efficiency — the quantum efficiency of the diode rises from 5% at room temperature to about 30% at 80° K. This high efficiency means that high peak laser output powers can be achieved with a reasonably low input current drive which can be generated by a practical drive circuit.

The laser requires a pulse drive current of 200A to achieve the maximum peak power output of 50W. The laser driver must further be capable of generating_pulses of short rise time to achieve good accuracy of altitude measurement. These pulses are generated by discharging a low inductance capacitor bank, charged to 1KV, through a fast cold cathode switching tube. It is imperative in the design of this circuit that stray inductance is kept to a minimum if short duration, high current pulses are to be achieved. The circuit developed achieves a peak current of 200A, pulsewidth 30nS, and a pulse repetition frequency from 0 to 100 p.p.s.

The energy emitted from the laser diode is collimated by a transmitter lens of 6.5in (165mm) focus and 3.25in(82.5mm) aperture which produces a beam divergence of 6 by 2 mrad. The optical aberrations through the transmitter lens are minimised by the use of a four-element lens, the radii of curvature and the thickness of these elements being optimised to give minimum aberration. This optimisation was achieved with the aid of a computer program for ray tracing through the optics.

Energy emitted from the transmitter is reflected by the ground and collected by the receiver which takes the form of a Cassegrain telescope cf 12 inches (30cm) aperture. After reflection by the primary and secondary mirror, the received light is brought to a focus at the field stop which defines the receiver field of view at 10 by 6 mrad. Light from the stop is then refocused on to a silicon photodiode of 2.5mm diameter.

The combination of the silicon photodiode detector and its associated pre-amplifier is designed to have a fast, low noise performance. The detector behaves as a current source and thus the pre-amplifier must have a low input impedance to achieve fast detection.



ELECTRONICS Australia, March, 1970

New Rola 12U50 speaker with 50 watts RMS power!

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ARIS

A virtual-earth amplifier therefore represents an ideal choice, an operational amplifier being the most convenient form of this circuit. The optimum choice of input device is a low noise FET which provides the best noise performance and adequate speed of operation. The detector/pre-amplifier assembly achieves an equivalent input noise power of 50nW RMS at a bandwidth of 25MHz.

Output from the pre-amplifier is further amplified with a video amplifier which raises the voltage level to around 5V for driving the counter (see below). The amplifier gives a voltage gain of 10^5 and will deliver 8V into 50 ohms with a rise time of 10nS. This amplifier employs a common base input stage giving an input impedance of 50 ohms. The remainder of the amplifier consists of cascaded shunt feedback pairs and the low output impedance is provided by a double emitter follower.

The height accuracy required for the altimeter is ± 5 feet which dictates an accuracy of transit time measurement of approximately ± 10 ns. This may be achieved with a high speed count-er/timer (i.e. around 100MHz) or by the use of an analogue technique where the height reached by an accurate ramp function is used as a measure of transit time. Available systems using the latter technique operate in a "search and lock" mode which prevents the tracking of rapid height changes. For the present application the digital approach was adopted and employs a high speed counter which has the necessary 10nS resolution. This provides a facility for height measurement each time the transmitter operates (i.e. integration over a number of pulses is not required) and will therefore readily follow step changes in height. The digital tech-nique provides the further advantage of an ergonomic, high accuracy digital altitude display and a b.c.d. output suitable for driving computer interface equipment.

The counter is started by a sample from the transmitter current pulse and stopped by the returned signal pulse from the video amplifier. A counter clock frequency of 98.3312MHz is used which results in a readout in feet. The velocity of light under typical conditions is .983312 \times 10° feet per second. Therefore, light travels 10 feet in 1 count and with the go and return path for the laser beam one count represents an altitude of 5 feet. The accuracy of the relationship, that one count equals 5 feet, depends on the stability of the crystal clock and the variation in the velocity of light. The clock is accurate to one part in 10° per day and likely atmospheric variations will only affect the velocity of light by one part in 10⁴. It is obvious that these errors are negligible in comparison with the allowed system accuracy. The counter resolution is ±1 count which gives an altitude resolution of ±5 feet.

The instrument also provides a BCD output which is used for feeding height information to the aircraft tape recorder. It is necessary to reset the counter on completion of each height measurement and this is provided by a reset pulse which is generated by auxiliary logic, synchronised to the altimeter transmitter pulse. The BCD output is reset to zero but the display has a memory such that the indication is only updated when the altitude changes. If

COMPUTER-SIMULATED ACCIDENT STUDIES

Cornell University's Aeronautical Laboratory (CAL) in the U.S.A. is conducting studies of road accidents using computer-simulated models representing various accident situations.

One project concerns a three-year study sponsored by the Bureau of Public Roads. This study looks at the performance

This study looks at the performance of the driver by simulating his possible. courses of action in accident situations at intersections on the computer. The computer describes numerically and in detail the driver's processes of perception, decision-making and response as he passes through the intersection. By these means it can suggest techniques for training drivers, establishing traffic regulations and designing roads at intersections. Features are represented in the computer on a mathematical model, which reproduces in terms of equations and formulas the relevant characteristics of the vehicle, driver and highway.

The model deals with two simple crossroad intersections with stop signs or traffic light control. Fourteen characteristics of the intersection can be represented, including type of traffic control, road conditions, max. detection distance of the intersection and speed limits. Other factors which can be taken into consideration relating to the vehicle and the driver include the speed, acceleration and deceleration of the vehicle, the driver's braking tendencies, and braking response time.

The model can deal with a whole string of vehicles Nonetheless it cannot completely simulate a real situation and certain limitations are imposed for the sake of simplicity. For example, all roads are twolane, no overtaking, and no pedestrians, the intersection is on level ground and visibility is a constant. The model is, however, still being developed and may eventually be modified to incorporate some of these features.

The simulation of a particular incident involves the use of a number of routines, which together build up a picture of the relationship between the various factors involved.

The driver enters the central program when he is 600 feet from the intersection. At this stage his only concern is with the traffic ahead of him, and this situation continues until he observes the intersection. Once the driver detects the intersection, he slows down and prepares to pass through it. Here again, the distance and rate of deceleration are determined

by a number of variable factors. When the intersection is reached the driver will stop, scan the road for other cars and proceed when it is clear.

The model has been validated from data gathered in laboratory experiments, investigations using real cars and drivers, and real-life observations at intersections.

In another CAL project a computer model is being used to study the causes and nature of accidents to pedestrians. The particular field of this study is the dynamics of the impact of the car on the pedestrian and is sponsored by the National Highway Safety Bureau.

The computer was used to simulate impact speeds of 5, 10 and 15mph under emergency braking conditions and of 20mph without braking, to define the trajectory of the "pedestrian" after impact. At 20mph the pedestrian somersaulted, hitting the bumper, the leading edge of the bonnet, the bonnet, windscreen and roof as he did so.

Although this is a preliminary study, results suggest that it can provide insight into the fundamental relationships involved in pedestrian collisions and thus lead to methods of reducing pedestrian accidents.

Another part of the research project was the behaviour of cars and their occupants in various accident situations.

The computer's results were produced in the form of animated cartoons, comparable to frames on motion-picture film. The time interval between frames could be varied, with a minimum in the region of 1/1000th of a second.

There are obvious advantages in using computer simulation for this work once its accuracy is satisfactorily established notably the greatly reduced cost and the ease with which experiments can be repeated. ("Electronics Weekly," 10/12/69.)

Computer simulated frames showing the body motions of a dummy in a collision. Compared with films of an actual crash, the computer results proved remarkably accurate.



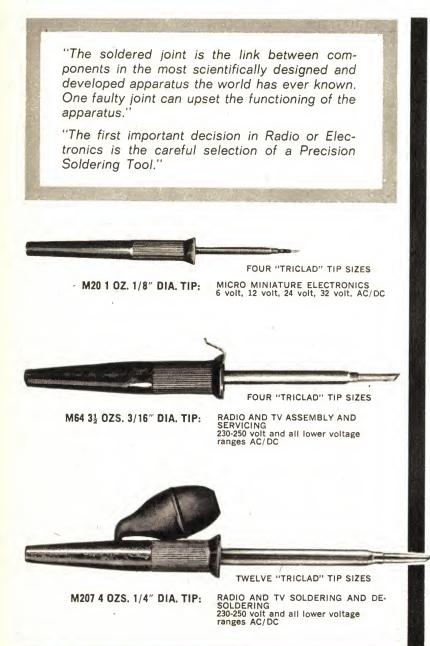
the counter exceeds its full count of 9995 feet without a receiver stop pulse being detected, then the counter automatically resets to zero to indicate "out of range." The counter gate cannot be opened and closed in an interval of less than 30nS and this prevents the counter being stopped by electrical or optical breakthrough from the transmitter to the receiver. The instrument was converted to operate from aircraft supplies.

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The height measured by the laser altimeter, together with that simultaneously measured by the radio altimeter, is recorded on the aircraft tape recorder. The recorder is also provided with aircraft attitude information which is required to correct for the slant height measured by the laser system which is rigidly mounted to the airframe. These altitude measurements are synchronised with a photographic record of the terrain thus allowing a comparison between the altimeters under known conditions. ("Marconi Instrumentation," Vol. 12, No. 3).

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ALTERNATIVES FOR THE JERVIS BAY ATOMIC POWER STATION

Overseas countries are vieing for the contract to build Australia's first atomic power station to be located at Jervis Bay (130 miles south from Sydney). This article explains some of the alternatives available — the various systems from which the final choice will have to be made.

Current nuclear reactors can be conveniently classified under three headings, according to whether they use:

• Light water, heavy water or graphite for moderation.

• Gas, light water or heavy water as the coolant.

• Natural or enriched uranium for fuel.

In a nuclear power station's radioactive pile, atoms of the uranium isotope U235 are split by the impact of neutrons (nuclear particles carrying no electric charge), producing in the process more neutrons to carry on the chain reaction. The neutrons emerge at speeds of about 6,000 miles a second, too fast to carry on the reaction efficiently.

Their most efficient speed, as far as splitting lots of P235 nuclei is concerned, is about one mile a second. To slow them down to this speed, some material is needed to moderate their velocity — hence the term moderator. Graphite, water and beryllium are particularly good materials for this; and the first two are the most commonly used substances. The water can be ordinary tap water ("light water" in the trade) or a variant known as heavy water.

The ordinary hydrogen atom, the simplest element there is, consists of one proton in the nucleus and one electron circling around. In a rare isotope of hydrogen, the central proton is joined by a neutron to form heavy hydrogen (or deuterium). In ordinary water, perhaps one molecule in 5,000 has heavy hydrogen instead of ordinary hydrogen. And if these molecules are separated out (by a fairly expensive process) you have heavy water. If you don't want the expense of a heavy water plant, you can use light water but at a price.

Heavy water soaks up just the right proportion of neutrons for a pile run on natural uranium — that is, one where the fuel rods contain only 0.7 percent of the fissile U235. Light water soaks up too much — to keep the pile going satisfactorily you have to step up the proportion of U235 by using enriched fuel.

The choice thus becomes natural uranium and expensive heavy water moderation, or enriched fuel with light water or some other relatively inexpensive moderator. The coolant is needed to transfer the heat from the pile to the actual generating part of the station.

The American General Eelctric reactor uses boiling light water as the moderator and also as the coolant. while the Westinghouse version uses pressurised light water (preventing boiling) to take the heat to a heat exchanger for production of steam. Both are thus light water systems, using heavily enriched fuel. They are also on the low side as far as capital costs are concerned — \$100 million has been quoted as a rough estimate of the possible cost of an American 500 megawatt station at Jervis Bay.

Enrichment of uranium, for a pressurised light water 500MW station on high load factor (that is, running continuously) to about 3 per cent U235, would cost about \$2 million a year, if done in the U.S.

Very roughly, the total cost of enriched fuel runs out at one-third for the original uranium oxide, one-third for enrichment and one-third for processing into fuel elements. So the total cost of fuelling might be around \$6 million a year.

Britain over a number of years built 10 nuclear power stations using natural uranium fuel, graphite as the moderator and carbon dioxide as the coolant; these are the gas graphite stations. They now have an improved version known as the advanced gas cooler reactor, still using graphite and carbon dioxide, but with slightly enriched uranium fuel.

Work has also been going on in Britain on a prototype 100MW station using a hybrid system — heavy water moderation, to reduce the amount of fuel enrichment needed, light water as the coolant, and slightly enriched uranium as the fuel. This is the Steam Generating Heavy Water Reactor, or SGHWR.

The Australian Atomic Energy Commission had high hopes that this system could be modified to work on natural uranium, meeting the Commission's requirement of independent Australian nuclear fuel supplies. Twenty Australian experts spent two years in the U.K. working with the British on this prospect, but the results were disappointing. However, with the possibility that Australia might acquire access to the newer, much cheaper method of fuel enrichment known as the gas centrifuge ("Electronics Australia," August, 1969), British chances of putting the SGHWR into Jervis Bay have revived.

The package deal would be more economic than alternative proposals for natural uranium reactors — provided a series of reactors are built. this point needs underlining — if the enrichment technology is available and is acquired, then Australia will pretty well be committed to erecting a series of nuclear power stations to make economic use of the enrichment plant.

Unless, that is, export contracts for

the enriched fuel suplus can be negotiated — or military uses are found for the surplus production. It is a point to be looked at very carefully between March this year, when the official tenders are finally expected to be called, and September when, on present plans, the contract will be awarded.

Natural uranium reactors are possibly available from Canada, Siemens in West Germany, A.S.E.A. in Sweden and Gesell in France. However, only the Canadians and the West Germans have actually exported or contracted to export working systems. A 500MW nuclear station to the CANDU (for Canadian Deuterium Uranium) design could cost between \$125 million and \$150 million.

CANDU reactors use natural uranium and heavy water moderation, largely through historical accident. With two moderation systems available — heavy water and graphite — the U.K., France and Canda at the beginning of World War II got together as much heavy water as possible and carried it to safety in Canada. The Canadians have stayed on that

The Canadians have stayed on that line of development since. They now have eight nuclear power stations using the CANDU system built or committed.

They include a 3,000MW station made up of four 750MW units for Ontario, and installations for India and Pakistan.

Australia would need about 500 short tons of heavy water to start off a CANDU reactor, for a cost estimated at \$22 million.

This assumes a price of \$22 a lb, compared with current prices of \$28,50 a lb, on the argument that increases in the supply of heavy water will bring down prices.

At current prices, it would cost \$28.5 million.

A natural uranium power station would need about eight tons of heavy water a year to make good operational losses, costing about \$350,000 a year.

The Canadians claim that the total cost of fuelling a CANDU reactor is one-half to one-third the fuelling cost of any other big commercial reactor in the world.

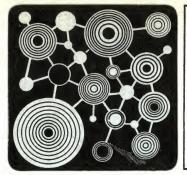
It will take a lot of savings on fuel over a long period of time to make up for the difference between just over \$50 million for a coal-fired unit and \$150 million as the upper limit for a CANDU nuclear reactor.

The relative advantage of the coalfired stations lessens as you move away from the coalfields.

Either transmission lines lengthen, with resultant power losses, or coal has to be transported to a local power station for a cost which increases with distance.

For this reason, industrial centres in southern Australia look better prospects for nuclear power than do Queensland and N.S.W., which are well supplied with major black coal deposits. (Condensed from an article by Christopher Jay, "Financial Review," 7/1/70.)





SCIENTIFIC AND INDUSTRIAL NEWS

Laser communications

Aerojet-General Corp., Calif., has been awarded a contract by the National Aeronautics and Space Administration (NASA) for the development of a laser communications experiment. It will be aboard NASA's Applications Technology Satellite-F (ATS-F) scheduled for launching from Cape Kennedy into a synchronous (stationary) orbit in 1971. Aerojet-General is required to develop the spacecraft laser equipment and ground equipment necessary to conduct laser communications experi-ments between the craft and a ground station. The system will require smaller antennas and may need less power and weight than is required for microwave systems.

In 1974 when ATS-G is launched, the experiment could be expanded to include spacecraft-to-spacecraft laser communica-tions (teletype, voice, facsimile, colour TV and still photo-graphs) between ATS-F and G spacecraft.

UHF power diodes

An unexplained phenomenon in a solid-state device has been harnessed by RCA scientists to produce high power pulses of energy in the UHF band. The effect occurs in certain silicon avalanche diodes when they are placed in a circuit tuned to oscillate at frequencies lower than those at which the diodes are supposed to be able to oscillate. For reasons still not fully underticed when electrical pulses are new earlied to the diodes are supposed to be able to oscillate. For reasons still not fully understood, when electrical pulses are now applied to the diodes, they abruptly enter an "anomalous mode" of operation and begin to produce microwave oscillations with powers and efficiencies comparable with electron tubes. Discovery of the anomalous mode and the development of the diodes is credited to a team of scientists in the RCA Microwave Research Laboratory headed by Dr Kern K. N. Chang.

By combining five PN diode junctions in one package, the By combining five PN diode junctions in one package, the team has succeeded in producing microwave pulses with peak powers above 1.2KW at frequencies up to 1GHz and with efficiencies above 25 per cent. Avalanching of the junctions is triggered by 130V pulses, but once microwave oscillations begin, 94V, 10A, 1uS pulses with 0.1 per cent duty cycle are used on each junction to achieve the 1.2KW output. Diode samples have been operated at the RCA laboratories without failure for more than 15,000 hours.

Diagnosis by CCTV

A new medical use for closed-circuit television has been pioneered by the Department of Surgical Neurology of Edinburgh University and the Emergency Department of the Edinburgh Royal Infirmary. A television link, now operational, enables new patients at the infirmary to be examined by a specialist three miles away. If necessary, the specialist can direct the surgical staff to prepare an operation ready for his arrival. In this way, rapidly deteriorating conditions can be detected and treatment started with the maximum speed.

Professor John The new system was developed by Profess Gillingham, neurosurgeon at Edinburgh Western

Heart/lung membrane

Research in the U.K. to design a heart/lung machine Research in the U.K. to design a heart/lung machine which is smaller safer and more efficient than current machines has resulted in the development of a new membrane. Known as "Silestofilm," the rubber silicone membrane makes it possible to mimic the functions of the alveolar membrane within a living lung by eliminating the direct contact of oxygen and blood during oxygenation. The membrane's high permeability to oxygen and carbon dioxide makes it ideal for the type of machine under consideration. (Midland Silicones Ltd., Reading Bridge House, Reading, Berks., England.)

A research worker positions a sample of the mem-brane on a manometer prior to testing its permeability to different gases.

Hospital, together with the South-Eastern Regional Hospital Board, Scotland and was engineered and installed by the Marconi Electro-Optical Systems Division. The Marconi V322A vidicon television camera in the Royal Infirmary accident unit is carried on a movable boom above the patient trolley, and has full facilities for panning, tilting and zooming. It can view the whole patient, or zoom in enough to inspect just one eye, as the specialist directs. The television signal is carried three miles from the Royal Infirmary to Professor Gillingham's office in the Western General Hospital by a GPO link. There is a permanent telephone link between the infirmary and Professor Gillingham's office on which he can be told of a new admission, direct the camera movements, or give instructions to prepare for an operation if necessary. to prepare for an operation if necessary.

Geological survey of Australia

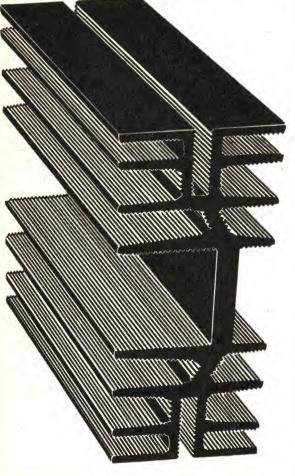
Westinghouse Electric Corporation is to conduct a geological mapping survey of about 50,000 to 70,000 square miles in Australia and New Guinea using "Side Look Radar." (See "Electronics Australia," June, 1969, page 21.) The survey was due to begin in Western Australia early this year. Preparation of the radar mosaic maps and the geological interpretation of the maps will be done by the Automatic Operation of the Raytheon Company. Side look radar has been used to map 6,000 square miles of the Darien Province of the Republic of Panama, where the area is constantly covered by clouds making aerial photography impossible. aerial photography impossible.

Westinghouse flew its specially equipped DC-6 aircraft to Australia to carry out the survey. The aircraft is a self-contained mapping unit. Every step of the process from the pulse transmission to film processing and evaluation is done aboard the plane by a highly skilled crew. Flying at 20,000 feet, the plane can map 1,500 square miles in an hour and can be used in adverse weather. The ability to rapidly collect images by day or night through all kinds of weather greatly shortens the initial exploration period for mineral and oil firms.



ELECTRONICS Australia, March, 1970

FOR TRANSISTORS, DIODES, THYRISTORS

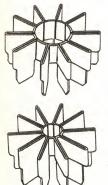


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WITH Hexafit mounting FOR MEDIUM POWER DIODES & THYRISTORS

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ELECTRONICS Australia, March, 1970



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Darwin booster station

The high power Radio Australia boos-ter station established at Darwin com-menced regular transmissions on Decem-ber 20, 1969. This date marked the 30th anniversary of the inauguration of Radio Australia. The first transmissions emanat-ed from Lyndhurst in Victoria on Decem-ber 20, 1939 The three transmitters at Darwin are all rated at 250KW and all should be operating on full power by should be operating on full power by March, 1970. The Darwin station is located on Cox Peninsula, and was established at a cost of \$8 million. It picks up Radio Australia programs "off air" from Shepparton in Victoria and retransmits them at greatly increased power to in-crease the effectiveness of Radio Australia transmissions to south-east and eastern Asia.

Radio and TV expansion

A low-powered national television translator station is to be established on Mount Devlin, a ridge overlooking Collinsville in Queensland. The station will relay the programs of ABMQ at Mackay. It will use channel 11 with horizontal polarisation. It is hoped to have the station operating by the end of 1970, when it will provide an adequate service to the 2,000 residents of the town. The establishment of a commercial translator station is being considered.

A national broadcasting station to be established in north-west New South Wales will be located at Byrock between Nyngan and Bourke on the Mitchell High-way, about 79 miles north-west of Nyngan. It will operate with power of 10KW and use a directional aerial. It will take the regional third network pro-grams of the A.B.C. It will provide a service to about 16.000 people in an area ervice to about 16,000 people in an area outside the service areas of 2CR Orange and 2NB Broken Hill. The station is expected to be operating within three

Split screen CRT

Westinghouse Electric, of the U.S.A., has developed a cathode ray tube with a split screen — one part displays informa-tion in real time while the other displays information stored electronically by the ube. It thus combines the functions of a conventional CRT and a display storage tube in a single device. Both areas of the tube can be used for continuous display, however, as the tube storage is done by an internal screen rather than by the persistence of a phosphor. The ratio of stored to non-stored area can be varied at the time of manufacture to suit the tube's the time of manufacture to suit the tube's application.

Sounding rocket

A new type of sounding rocket for high-altitude geophysical research has been developed by Svenska Flygmotor, of Sweden. Called SR-1, the rocket can carry over 100lb of scientific instruments to a height of 120 miles. Main features of the unit are the hybrid rocket engine with superior handling characteristics and the attitude control system which radically decreases impact dispersion. In the SR-1 safety is ensured by the separation of the oxidiser from the fuel. The latter, develop-ed by Flygmotor, has a high melting ed by Flygmotor, has a high melting point is smokeless, can be easily stored, and is easy and cheap to manufacture.

The attitude control system of the rocket Ine attitude control system of the rocket removes the risk of descent anywhere but in the chosen area. Necessary side forces are generated by secondary injection of the liquid oxidiser in the supersonic part of the exit nozzle. The attitude - sensing device is a pneumatic floating-ball gyro-scope, developed by the Swedish Defence Descence Institute Research Institute.

Survey of WWV users

The National Bureau of Standards (N.B.S.) of the U.S.A. is considering changing the format of radio stations WWV and WWVH, two of four radio stations operated by the Bureau to prostations operated by the Bureau to pro-vide accurate time and frequency informa-tion. N.B.s. is seeking the opinion of users on the present format and asking for suggested changes. A questionnaire has been sent to many users of the services, and information about the survey is broad-cast on WWV once each hour. The ques-tionnaire is on a machine-readable punch card, and participants punch out a "Yes," "'No," or "No Opinion" in answer to 16 questions concerning the present format of the broadcasts. Additional comments are invited on a separate sheet of paper. invited on a separate sheet of paper.

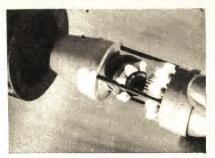
Station WWV has been transmitting standard radio frequencies on a regularly announced schedule since March, 1923.

Computer service in Melbourne

The IBM Call/360 shared computer service (see "Electronics Australia," May, 1969 page 18) has been extended to Melbourne to provide an identical service to that previously operating in Sydney. Several terminals in Victoria were con-nected to the Sydney-based IBM System/ 860 Model 50, but the relatively high ong-distance line costs restricted this service. To handle the work load of terminals installed and planned in Vic-toria, IBM has installed a second System/ 360 Model 50 costing \$1.5 million in the company's data centre in St. Kilda in addition to the model which has been at the centre since February, 1967. (IBM Australia Ltd., Bradfield Highway and Kent Street, Sydney, 2000.)



The original IBM System/360 Model 50 installed at the IBM data centre in St. Kilda.



A closed-circuit television camera, no bigger than an electric torch and complete with its own miniature lighting set, has been developed in the U.K. It can be inserted into a 2¹/₂ in diameter pipe (as shown) to examine a weld. For this it is fitted with a 90-degree viewing head, using a 45-degree mirror to see round a right angle corner. The head can be rotated by a remotely controlled miniature electric motor built into the camera viewing head. Pictures inside tubes of only $\frac{1}{2}$ in diameter are possible using an introscope attach-ment. The range of screw-in attachments includes a waterproof head that can be operated at depths up to 500 feet for forward or right-angle viewing and fitted with quartz-iodine lighting. (Seer TV Surveys Ltd., Old Woking, Surrey, England.)

It first operated on the grounds of the Bureau in Washington, D.C. The station was moved several times, but remained in Washington until 1966, when it began broadcasting from its present location near Fort Collins, Colorado. Station WWVH began supplementing the services of WWV from Maui, Hawaii, in 1948. Both WWV and WWVH broadcast the same services on HF. N.B.S. also operates a LF and a VLF station (WWVB and WWVL) at the Fort Collins site.

All users of WWV who wish to receive the questionnaire should write to: WWV 1969, National Bureau of Standards, Boulder, Colo. 80302, U.S.A.

W.A. radio and TV

A national television station and a national broadcasting station commenced op-erations recently in Western Australia. A television station to serve Geraldton began regular transmissions on December 8, 1969. A radio station to serve the Bun-bury/Busselton area began transmissions on December 22, 1969. In the past 13 years, the Government and private enterprise between them have provided 140 TV stations throughout Australia.

The TV station at Geraldton, ABGW 6, is located on Moresby Range, seven miles north-east of Geraldton. It operates on 10KW of power, and takes its programs on relay from Perth over the recently installed c o a x i al cable system. The Bun-bury/Busselton radio station 6BS, oper-ates on 2KW and covers not only the Bun-bury/Busselton area, but also parts of the Margaret River/Augusta district, providing a service for about 26,000 people.

The commencement of television trans-The commencement of television trans-missions in the Kalgoorlie area, scheduled for December 29, was delayed due to last-minute equipment failures. The station, ABKW 6, is sited on Peter Hill, two miles north of Kalgoorlie. It will operate on 4KW and be beamed towards Kambalda and Coolgardie. It will take its programs from Perth via the completed section of the East-West microwave link.



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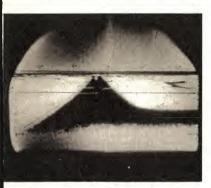
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Visual approaches in bad visibility

A radar device that would enable pilots of Lockheed's L-1011 TriStar jetliner to "see" airport runways while landing in rain and fog has been successfully demon-strated in flight tests. The device, called an independent landing monitor (ILM), displays a realistic picture of the airport and runways on a screen in the cockpit. It is being developed by Texas Instruments and runways on a screen in the cockpit. It is being developed by Texas Instruments Inc., of Dallas, Texas to meet require-ments for "new generation" wide-bodied jetliners, such as the TriStar, which will begin entering airline service late in 1971. It is claimed to be the first system permitting a pilot to visually monitor performance of an aircraft's automatic landing system during approach and touchdown under low visibility conditions.



The display screen of the Texas ILM system showing clearly a runway's image.

Smog study in U.S.A.

Los Angeles is installing automated Los Angeles is installing automated equipment to measure atmospheric pollu-tion and weather conditions at 12 key sites once every 20 seconds. The system, de-signed by Litton Industries' Guidance and Control Systems Division, will automati-cally measure atmospheric changes and telemeter the information over telephone lines to Los Angeles County Air Pollution Control District. There it will be contin-Control District. There it will be contin-uously analysed by computer and present-ed in instant pre-digested form to a con-trol officer who will be able to issue public warnings if needed.

The system — Litton Industries Model 512 Quality Data Acquisition System — is designed for remotely measuring, tele-metering, recording, processing and dis-playing information related to air and water quality parameters. The system achieves high reliability and ease of maintenance through the use of solid-state components and plug-in printed circuit boards. A typical monitoring program in-cludes measurement of such phenomena as wind speed and direction, air temperature and concentration of sulphur dioxide, car-bon monoxide, hydrocarbons, oxides of nitrogen and other contaminants. Output data is available for recording on magnetic tape, punched paper tape, typewritten page, visual displays or for connection to an external processor for subsequent data handling. The system - Litton Industries Model

The I.T.U. in 1969

The number of member countries of the International Telecommunication Union (I.T.U.) increased to 137 with the admis-sion of Nauru (10 June, 1969) and Mau-ritius (30 July, 1969). The Study Groups of the International Consultative Committees held numerous meetings during the year. Among topics discussed were: the possible application of satellite techniques to direct proadcasting from satellites to aeronauticbroadcasting from satellites, to aeronautic-al and maritime navigation; traffic control communication; space communications; problems concerning standard frequency

Other sensing systems besides radar were evaluated for the TriStar's ILM, such as infra-red, low light level television, and image intensifiers. But radar appears to offer the best overall promise for over-coming restrictions imposed by bad weather, according to John Gorham, Lock-beed's engineer in charge of TriStar flight heed's engineer in charge of TriStar flight guidance and controls.

Gorham emphasised that the ILM "is not intended in any way" to substitute for the TriStar's fail-operative automatic for the TriStar's fail-operative automatic landing system, which will be a standard feature of the aircraft's avionics. The range of the display in clear weather is about five miles. Reduction in range caused by fog, rain or snow will be measured during flight tests. Lockheed's minimum ILM range requirement is two miles. Resolution of the display must be of such quality that a pilot can instantly recognise the runway, other air-port features and any hazards in the approach and landing path. The ILM display will also show airport taxiways, permitting the pilot to taxi off the runway under low visibility conditions.

An ILM system, when fully developed by Texas Instruments and adopted by Lockheed, will be offered as an option to airlines ordering the TriStar. Lockheed believes the ILM's advantage for airlines will be to virtually eliminate costly go-arounds that could arise when jetliners begin landing at airports in poor visibility. Under such conditions, a pilot could mis-interpret fleeting views of the ground in the final stages of landing and elect to circle the airport for another approach before touching down. before touching down.

and time broadcasts; and the possibility of

standard time broadcasts based on an atomic standard. Further work was done to improve the standards for low cost

to improve the standards for low cost sound and television receivers for use in new and developing countries. Work prog-ressed on the preparation of a handbook to be used by monitoring stations in ob-

to be used by monitoring stations in ob-serving transmissions by all nations to check that they conform to the Inter-national Radio Regulations. The I.T.U. continued to assist in technical co-oper-ation by sending experts to study special telecommunication problems, to train staff, and to operate some 15 training schools including an experimental earth station to train space radiocommunication

Radio-telephone links

cember, 1969, page 16.)

vices becoming available.

\$39,000 worth for installation in selected areas. (See "Electronics Australia," De-

A.W.A. has also found considerable interest in South-East Asia and the Middle East, where earlier types of radio-phones have been supplied in quantity often for use by industrial establishments in the out-

er suburbs of cities where there was no immediate prospect of normal telephone ser-

America.

Electrical exhibition

Electrex '70, the 15th International Elec-trical Engineers' Exhibition, will be held in Earls Court, London, England, from April 8 to 15, 1970. The organising committee has announced a new award for Electrex '70. Formerly awards have been made for the best items in the industrial and domes-tic portions. New 2010 and a constant will be the best items in the industrial and domes-tic sections. Now a third award will be made for accessories. Among exhibits eli-gible for this section are switches, fuses, plugs, socket outlets, lampholders, ceiling roses, and other electrical accessories. During the exhibition, the British Elec-trical and Allied Manufacturers' Associ-ation is sponsoring a three-day Inter-national Conference on Electrical In-sulation. sulation.

Broadcasting convention

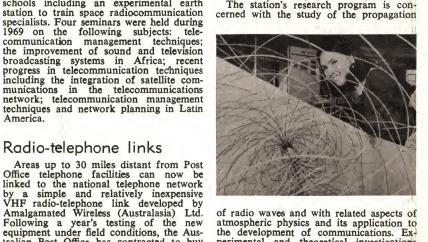
The third London International Broad-The third London International Broad-casting Convention, IBC '70, will take place from September 7 to 11, 1970, at Grosvenor House, Park Lane, London. It is sponsored by several professional bod-ies, including the Electronic Engineering Association, which is organising the exhi-bition aspects of the convention on behalf of the other unproper of the other sponsors.

of the other sponsors. The scope of IBC '70 takes in all aspects of television and sound broadcasting including: operational experience; receivers; studio design; propagation and service planning; origination equipment; recording; films; signal distribution, including wire relay; satellites; automation aspects of broadcasting; transmitters and transposers; aerials; digital techniques in broadcasting; technical management. All inquiries should be addressed to The Secretariat, International Broadcasting Convention, c/o I.E.E., Savoy Place, London W.C.2, England.

Magnetospheric model

A magnetospheric model based on the theory of the interaction of the magnetised solar wind plasma with the earth's magnetic field was exhibited at a recent open day at the Science Research Coun-cil's Radio and Space Research Station in southern England. The line pattern is assumed to resemble the superposition of two simple vacuum fields namely a dipole field, corresponding to the earth's field, and and external uniform field corresponding external uniform field corresponding and to the interplanetary (solar wind) field.

The station's research program is con-cerned with the study of the propagation



of radio waves and with related aspects of atmospheric physics and its application to the development of communications. Ex-perimental and theoretical investigations include the effects of electromagnetic and particle radiation from the sun on the ionosphere and the influence of meteoro-logical factors on the propagation of very logical factors on the propagation of very short radio waves through the troposphere. Rockets and satellites are used as experi-mental tools; the station provides services for its own space science research groups and those elsewhere, notably in British universities. (Radio and Sapce Research Station, Ditton Park, Slough, Bucks., England.)

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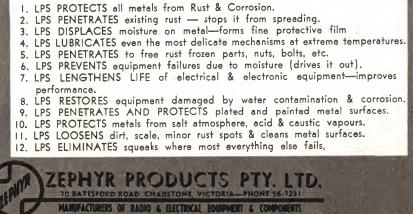
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Yacht race communications



Mr R. Young, radio operator of the Cruising Yacht Club of Australia (left), and C.Y.C. assistant secretary, Mr D. Goode, with the Goode, with the A.W.A. communications equipment in-stalled in the 75ft yacht Bali the official relay ship motor H'ai. radio which accompanied competitors in the 1969 Sydney-Hobart yacht race.

Noise abatement

The Department of Civil Aviation will stablish Airport Noise Abatement Com-nittees in Sydney and Melbourne as a fur-ner step to help overcome present and fu-ure aircraft noise problems. The Com-nittees will comprise representatives of CA local comprise representatives of C.A., local government, and the airlines, gether with State Government representives whenever they desire to be repreented.

Terms of reference for the Committees clude: informing the public on aircraft of problems and the action being taken alleviate the nuisance; maintaining a ontinuous liaison with airlines, commu-ty groups, and other interested authories about possible noise nuisance to protes about possible noise nuisance to pro-osed housing and other community proj-ts; discussing current aircraft noise roblems and seeking satisfactory answers; ting as a clearing house for all specific oise nuisance complaints relevant to lascot, Tullamarine and Essendon airorts and co-ordinating resolution of com-aints; recommending appropriate addional investigation and research into comunity noise problems associated with airraft operations at these airports.

Ergonomics conference

The Ergonomics Society of Australia and New Zealand is holding its Seventh Annual Conference at the University of New South Wales on August 13 and 14, 1970. The conference theme is Ap-plied Ergonomics. Papers on selected top-ics from the fields of environmental stud-ies, training and skills analysis, road safe-ty, and ergonomics in medicine will be les, training and skills analysis, road safe-ty, and ergonomics in medicine will be presented. People interested in attending or contributing papers to the conference are requested to write to the Conference Secretary at the following address: D. Goodridge, c/- School of Mechanical and Industrial Engineering, University of New South Wales, P.O. Box 1, Kensington, N.S.W. 2033.

Spectroscopy courses

Analchem Consultants, in conjunction with Perkin-Elmer Pty. Ltd., are organ-ising three-day training courses in atomic absorption spectroscopy, commencing in Sydney on April 6, 1970, and in Mel-bourne on April 27, 1970. The courses will cover both theory and practical work. Interested persons should contact Analchem Consultants, 18 Kendal Cres-cent, Collaroy Plateau, N.S.W. 2098, for further details or registration forms.

Inderwater rescue

The U.S. Navy is to manipulating ave ms on its deep subersible emer scue vehicles. emergency cles. This ill enable the rescue shicles to pick up bjects weighing up to old, dobain to attack olb, to remove much nd debris, to attach ables, and to cut lines. he 10ft-long arms developed by he 10ft-long arms ere developed by /estinghouse for Lock-eed, the prime con-ractor for the Navy's ubmersibles.

Movement of an arm partly manual and artly programed. Elec-onic controls, ydraulic actuators. nd servo-valves cause he arm's six joints to ptate in a manner

hich ensures precise positioning. The arm hay be jettisoned as a safety measure, parating at the shoulder joint. The rm's terminal device can also be



jettisoned. Stowing and unstowing of the arm is completely automatic. The bay into which the arm folds is out of the pilot's visual range. -



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PART THREE

Our New Communications Receiver

This is the third and final article describing our new receiver. It deals with the RF stages, the dial assembly, general assembly and inter-wiring, testing and alignment. In regard to the latter particular attention is given to the filter blocks in the IF system.

By lan Pogson

Before proceeding with the description of the receiver, there are some errors which unfortunately crept into the parts list. We suggest that readers modify their parts list in accordance with the information given in Errata and Notes elsewhere in this issue.

The first mixer is assembled on a piece of tag board, with seven pairs of tags. As the layout is identical with that for the second mixer, we are not repeating the diagram. Sufficient details should be available in the under-chassis picture. The same comments and procedures as before apply for the transformers and the wiring of the diodes.

The RF amplifier components are mounted on two boards, each having 13 pairs of tags, and these in turn are fixed to a two bank, 2-pole 5-position rotary switch. Before proceeding with any further assembly, check the dimension between centres of the screws holding the switch decks. This should correspond approximately with the dimension between the third hole in from one end of the boards and the fifth hole in from the other end. More than likely, the holes on the boards will be a little too close together. These should be eased out to the right dimension with a slim taper file.

The four coils, L1, L2, L3 and L4, are mounted and terminated on one of the boards, according to the wirning diagram. The ends of the windings are terminated at convenient adjacent tags on the board. In the case of the lower frequency coils, which are wound with relatively fine wire, this is not enough to fix the coil securely to the board. This can be done simply by tying the toroid to the board with a piece of nylon or other suitable cord. While not so necessary with the coils wound with heavy wire, it is a good idea and ensures that they do not shift.

Next, the main component board is wired according to the diagram. Make sure that all the interconnecting wires are complete before any attempt is made to take the assembly of this board any further. The two capacitors in series with the tuning capacitor are not wired in at this stage.

The two boards, as assembled to this stage, are mounted on the end of the range selector switch and separated from each other and the switch with *in-long spacers*. The first step in assembly involves fitting the first pair of spacers to the rear ends of the two switch retaining screws. Generally, there is about 1-16in of thread protruding beyond the nuts. The screws used in MSP type H switches are 5BA and the threaded spacers which are readily available are 1-8in Whitworth. These dissimilar threads do not mate very well but, due to the short length of thread, it is possible to screw the spacers on, provided due care is taken. If you can substitute Whitworth screws, so much the better.

The board with the coils is mounted against the spacers at the end of the switch, with the coils away from the switch. The second board is spaced away from the coil board with the second pair of $\frac{1}{2}$ in spacers. Two roundhead screws, 1-8 in $\frac{3}{2}$ in are used to secure the two boards to the spacers on the switch.

The assembly is now ready for the outstanding wiring and components. The various sections of the switch are used as follows. Only one section is used on the wafer nearest the clicker plate and this is used to switch the aerial into the primaries of the coils. The corresponding section on the other wafer switches the tuning capacitor to the relevant series capacitors. The third section selects the top of the secondary of each coil. The wiring involves the interconnections between the various contacts on the switch and coils, to gether with the series capacitors. When there is no series capacitor, a length of wire is substituted.

The dial system is the same as the one described for the 1967 All Waw series of receivers, but with a differen scale. The basic movement is the plan etary dual ratio unit, made by Jackson Bros., and distributed in Australia by Messrs Watkin Wynne Pty. Ltd. A backing plate, 6-3/8in x 32in, wa made from 16 gauge aluminium sheet

The dial scale is the same size as the backing plate and we used a piece of Formica board, one face finished in matt white. All lines are drawn with drawing instruments and Indian ink Correct size photographic reproductions of the scale will be available through the Information Service, at 50 each. The alternative is to do the whole job yourself, along with the calibration which will be discussed later.

To add a finishing touch, we made up an escutcheon from a piece of 1 gauge aluminium. The outside dimensions are the same as the backing plate The inside dimensions are $5\frac{1}{2}$ in : 3-1/8 in. The latter dimensions correspond with the cutout in the fron panel, with four mounting holes also corresponding with holes in the fron panel and backing plate. The escutcheon was given a coat of glossy black enamel.

This takes care of all the dial com ponents, except the pointer. We made ours from a piece of 16 gauge coppet wire, as follows. Take a piece of tinned copper wire, about 24in long. This is hammered flat, leaving about 3 in round at one end. Use a hammer with a good smooth face and a hard, flat surface, such as part of a vyce. Use care and patience and keep hammering, not too hard, until a reasonably flat surface is obtained on one side. Turn the wire over and treat it in the same way. When the wire bends, it can be straightened, to allow the job to proceed properly.

Having done a reasonably good job

up to this point, there will be undulations, due to uneven hammering. These are removed by carefully filing both flat faces. The edges can also be straightened up by a little filing. When you are satisfied with the finish, solder the round end to a small solder lug, with the pointer edge at right angles to the lug. Cut the pointer to length, with a 45-degree bevel and then give it a coat of black paint. The hole in the lug is used to fix the finished pointer to the movement, with one of the two screws supplied.

Although we did not fit a sheet of perspex over the dial, some readers may prefer to do so. A piece may be cut to the same outside dimensions as the escutcheon. The perspex is then fitted between the escutcheon and the front panel.

Assembly of the dial unit is quite simple but it is desirable to do it in a logical sequence. The movement is fixed to the back plate with two screws, using the holes adjacent to the 13/16in hole. Brass spacers can be used but this is not necessary. We used brass screws \ddagger in long and six nuts to give the right spacing. This method has the advantage that fine adjustment can be made to the spacing.

The backing plate is immediately behind the scale and the distance between the scale face and the back of the panel will need to be between 1/8in and 3/16in, according to space desired between the pointer and scale. One nut used as a spacer may be just insufficient and two nuts probably too much. A combination of one nut and one or more washers should give the desired spacing.

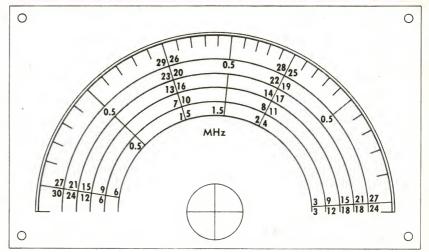
Push the four screws through the corners of the escutcheon and include the Perspex if used. The screws are then pushed through the corresponding holes in the front panel. Run a nut (with the washers) on to each screw. The nuts should not be tightened at this stage. Offer the back plate assembly over the four screws and tighten the nuts. Four more nuts behind the back plate hold the complete dial in place. Screw the pointer to the movement.

The dial which results is one which is capable of smooth, fine tuning control. This can be further improved by using a very large knob, which helps the vernier action.

As mentioned before, the dial movement is a dual ratio arrangement. This allows a quick transition form one end of the dial to the other, or to any desired point. The high ratio can then be used over a limited range, which is slightly less than one turn of the knob. Some readers may like this arrangement as it is. On the other hand, others may not like the rather heavy feel of the low ratio. This can be dispensed with permanently, leaving only the high ratio, by simply removing one of the two "dogs" which engage for the low ratio. In point of fact, we did alter ours by cutting off one of the dogs with a jeweller's saw. Travel across the dial is very little impeded by this change and feels rather better. Before making up your mind, remember that there is no turning back!

We are now in a position to undertake the final assembly. This is largely a matter of common sense, but it is possible to run into some traps, whereby an item already fixed has to be removed so that another item may be as-

CALIBRATIONS FOR ALL BANDS



Dial calibrations provide for ten ranges, all of 3MHz. The smaller divisions are 100KHz apart. Any one range has all figures on one side only of each MHz division, i.e., all on the anti-clockwise side or all on the clockwise side. The lowest range (up to 3MHz) runs clockwise, the 3 to 6MHz range runs anti-clockwise (it being the tunable IF), and all the following ranges up to 18MHz run clockwise. The system crosses over at this point and all ranges from 18 to 30MHz run anti-clockwise. The 100KHz divisions on the outer radius apply to all ranges. Full size, glossy photographic reproductions of this scale are available through our Information Service for 50c, post free.

sembled. To avoid this as much as possible, here is a suggested order of assembly, with appropriate comments as we go along.

The main chassis partition should be among the first to be fixed, with grommets fitted to holes where leads are to be passed through. The single gang capacitor for the RF stage should be fitted next. Remember to provide a lead of hookup wire from the stator plates, running the lead through a hole immediately below the gang. The front panel is next. This is held in place by the components which are fixed along the front skirt of the

The front panel is next. This is held in place by the components which are fixed along the front skirt of the chassis. These include two toggle switches, pilot lamp, function switch, a bush for the extension spindle for the crystal selector switch, and the RF amplifier assembly. The crystal selector switch can also be fitted at this stage.

When screwing the power transformer in place, we suggest that you use 5/32 in Whitworth screws. We also stood the transformer feet off the chassis by placing an extra nut between the foot and the chassis. This reduces the transfer of heat from the transformer to the chassis, This is done to avoid undue chassis temperature rise, with less heat conduction to the oscillator coil in particular.

cillator coil in particular. The rest of the major front end components, such as the crystal sockets, first mixer assembly and L5, may now be fitted together with the components along the back skirt of the chassis. The tunable IF assembly and the

The tunable IF assembly and the 3-gang capacitor should be mounted in conjunction with each other, as screws for each are fairly close to the respective alternative item. Three leads from the stator plates of the gang should be provided, the input section lead being dropped through immediately below the lug on the gang. The other two leads are brought through holes drilled about 3/8in from the respective coil cans or L7 and L8. These two coils, with L6, may be mounted now. These may be followed by the noise silencer assembly, which is straightforward.

The filter block assembly, on its printed board, is mounted upside down, i.e., with the copper uppermost. This is to permit final adjustments during the alignment process. This is followed by the largest assembly of all, the IF amplifiers, AGC and BFO. However, before fixing it, we suggest that you decide which leads may be better soldered in place, to avoid an awkward situation later on.

The audio amplifier and power supply are the only remaining major items to be fixed under the chassis. These are stood off with $\frac{1}{2}$ in diameter, $\frac{1}{2}$ in long spacers. Flag heat sinks for the two output transistors and the AC128 regulator transistor are held under the appropriate spacers.

Assuming that the dial has already been fitted to the front panel, as described earlier, the three potentiometers, meter and aerial capacitor may be fitted. The wiring board for the back of the meter may also be included.

The aerial capacitor, which is a 140pF maximum in the prototype, must be insulated from the panel. If the 140pF is not readily available, then one with a maximum of 100pF would do. The purpose of this capacitor is to afford control over the signal level into the receiver and so avoid blocking and cross-modulation on very strong signals.

On the other hand, it may sometimes be desirable to feed as much signal as possible into the receiver, particularly at the lower frequencies. A switch is shown across this capacitor in the main



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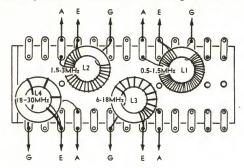
(A DIVISION OF ELECTRONICS INDUSTRIES) 116-118 CLARENCE ST., SYDNEY 29-4451 443 CONCORD RD., RHODES 73-0211 BOTH STORES OPEN SATURDAY MORNING FREE PARKING SPACE AT RHODES FOR CUSTOMERS circuit diagram. This is to short out the capacitor for this condition. We provided the "switch" by applying a small bridge of solder across the outer ends of three of the rotor plates. When the capacitor is fully meshed the solder short circuits the rotor plates to the stators. This provides wide control over incoming signals, from the short-circuited position to the minimum capacitance position at the other end of the scale.

Having completed the major assembly, the remaining constructional task is to do the interwiring between units and add a few other items in the process. Most of the procedure will suggest itself at this stage but a few guiding comments may be of assistance.

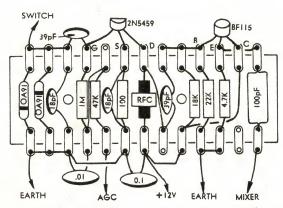
In addition to the speaker outlet socket, which is the two-pin version of this line of miniature sockets, we have made optional provision for a five-pin section of the switch is wired so that, on the STANDBY position, the leads are open, but are bridged in the RE-CEIVE position. Another section of the function switch is used to switch one lead of the mains to the primary of the power transformer. This is wired so that the mains lead is broken only in the OFF position, but bridged for both STANDBY and RECEIVE.

Although it may be a small point, the type of power transformer used may call for mention as to how it should be connected. Where there is one secondary winding of 12.6 volts, there is no problem. However, if there are two secondary windings of 6.3 volts each, they will be connected in series. In the case of two 12.6 volt windings, these should be connected in parallel, in the correct phase relationship.

The leads between the detector and the audio volume control are best run



This board is mounted nearest the switch and accommodates the four toroidal coils. The suggested terminations are clearly indicated and each coil should be firmly anchored, as mentioned in the text.



This board which is stood off from the coil board, includes all other components for the RF amplifier. All wiring can be followed easily from this diagram.

socket as an outlet for the 17.5 volts unregulated, 12 and 9 volts regulated, and earth. These voltages can be used for ancillary equipment associated with the receiver, provided the demand is within the current capabilities of each voltage.

A third socket, with four contacts, is reserved for any control leads which may need to be taken from the receiver, such as for muting. We have arranged a simple muting arrangement which breaks all the 12 volt supply to the rereceiver. The 12 volt lead from the power supply is terminated at one point on the socket. Another socket point is the feed point for all the 12 volt supply to the receiver. These two points may be taken externally to where contact may be made or broken, thereby activating or silencing the receiver.

So that this facility can also be controlled at the receiver, leads are taken from this socket to the function switch on the front panel. This is marked, OFF, STANDBY and RECEIVE. One in shielded or coaxial cable (the light weight variety) to ensure that no hum problem arises from this source. We earthed the ends nearest the detector to a lug on the audio amplifier fixing screws. We also connected the coaxial shield lead to the case of the volume control. This point is also used as the earth connection for the S meter circuits, which are nearby.

The wiring of the two toggle switches on the front panel could be a little confusing and so we have drawn wiring diagrams for each. The selectivity switch presents no particular problem, but the SSB1, AM, SSB2 switch could take some working out. By following the wiring diagram, no troubles should arise.

The 14 volt indicator lamp on the front panel, should be wired directly across the 12.6 volt AC supply to the rectifiers.

Although the greater number of components for the tunable IF and VFO are on the assembly unit, in addition to



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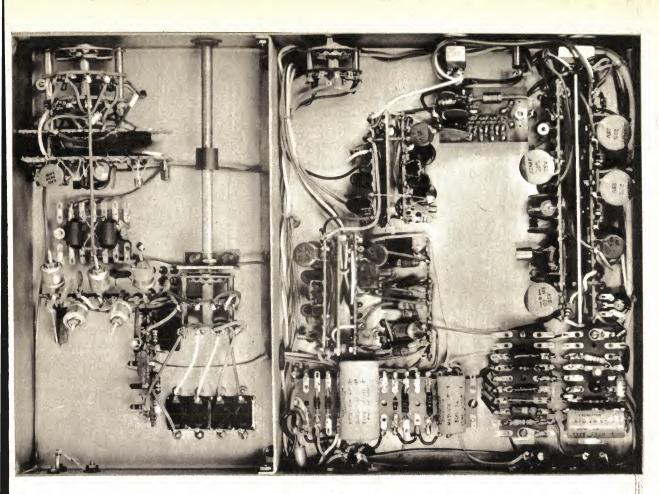
-tisk

	15'' Guitar Speaker P-382	
	Voice Coil Impedance:	8 Ohms (P382B).or 15 Ohms (P382A)
	Nominal Power:	60 watt
	Frequency Response:	` 60 - 5000 c/s.
-	Sensitivity:	103 db./watt.
	12'' Guitar Speaker 30-35Q	
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the three coils, there are a number of other components which are wired between tag strips and the coil lugs. A 2-tag strip is held under the oscillator coil screw, with 3-tag strips similarly mounted for the other two coils. Make sure that all wiring and components for the VFO are quite firm, to avoid instability due to vibration. All other leads should be kept as short as possible.

The crystal oscillator and amplifiermultiplier stages are so disposed as to keep leads as short as possible. The resistors and closely associated capacitors for both transistors are wired to a 10tag strip and this is orientated so that it is conveniently located with respect to the switch, crystals, etc. This can be seen in the under-chassis picture.

Another 10-tag strip accommodates the five 3-30pF trimmers, and shunt capacitors where used, for tuning the amplifier-multiplier output. This tag strip is mounted at right angles to the other one, as may be seen in the photograph. One mounting foot of this tag strip, the one nearest the coil, is not used. We found it more convenient to cut it off and support the tag strip by soldering it directly to the earth lug of the coil.

Having completed the whole of the assembly and wiring, the receiver is all but finished, except for adjustments. Before carrying out the adjustments a careful check should be made of the whole wiring, to make sure that there are no omissions or errors. If all is well, switch on the power and check for any signs of distress. If none appears, we can proceed. First, make sure that the noise silencer is totally disabled, by turning off the switch on the silencer control. This is very important. With no signals being fed into the

Underchassis view showing the relative positions of the various modules which have been described in detail. At right of the partition are the power supply and audio amplifier at the bottom, the IF strip at the right, and the ceramic filter board at the top. To the left of the filter is the noise silencer, with the tunable IF just below it. Details of the front end, to the left of the partition, are shown in a separate picture on the next page.

receiver, set the S meter to zero with the 1K tab pot. The first step of align-ment is to tune L5 to 24MHz, 21MHz, 18MHz 15MHz, 12MHz and 6MHz. Two methods may be readily used to obtain an indication of resonance. One is to use an RF probe with a VTVM, set to its lowest range. The probe is connected across the low im-pedance secondary of L5, which is the injection for the first mixer. This method has the disadvantage that it does not indicate the frequency of the output voltage.

The second method is to use a dip oscillator, set to its "wavemeter" position; i.e., the oscillator not working and the unit set to detect an RF field. This method gives a peak reading on the meter for tuning and it also gives the frequency of output. The choice is up to the resources of the reader. If you use a VTVM, connect the probe across the output winding and if you use a GDO, hold the coil close to the same lead from the coil to the mixer. The GDO will need to be set to the expected frequency each time.

Set the Tuning Range switch to 30-27 and set the dip oscillator to 24MHz. Adjust the slug in L5 for maximum deflection of the dip meter. If you are using a VTVM, tune for maximum deflection also. Set the Tuning Range switch to 27-24 and set the dip os-cillator to 21MHz. Adjust the appropriate trimmer for maximum response. Set the Tuning Range switch progres-sively to 24-21, 21-18, 6-9 and 0.5-3 and adjust each trimmer in turn, for maximum response on 18MHz, 15MHz, 12MHz and 6MHz, respectively.

If it is not possible to adjust the slug or trimmer through the wanted frequency it may be necessary to make a small change in the value of the shunting capacitor. Inability to reach resonance at 24MHz, with the slug right out, would require that the 10pF capacitor be changed to 8.2pF. Once this slug is set it must not be touched when adjusting trimmers to the other frequencies.

The next job is to sweep align the IF strip, with the two filter blocks. Equipment needed is a sweep generator which sweeps 455KHz, and a CRO. These are set up in the usual way. A marker generator is not necessary, the object being to get the pass bands of the correct shape. Any deviation from the nominal frequency of 455KHz has to be accepted but will not amount to more than 1KHz or so anyway.

The AM detector of the receiver is used for this operation and its output may be taken from across the volume control, across the speaker voice coil, etc. and is fed to the CRO via a shielded lead. It should be noted that after the alignment of the IF strip no changes can be made to circuit values which could upset the pass-band shape.



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TUNERS

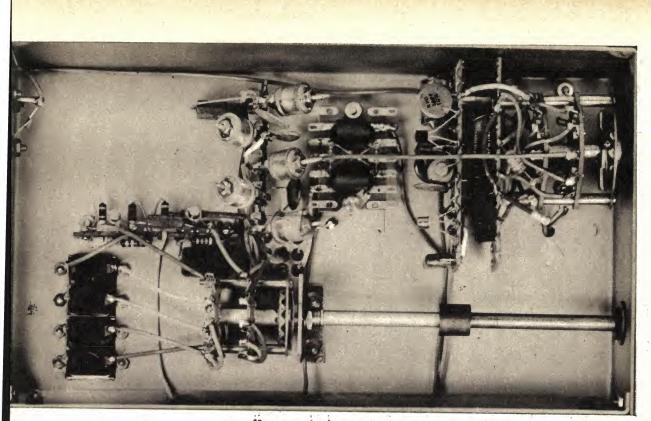
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t changes are made in the future, the lignment should also be checked and djusted if necessary.

We suggest disposing of the broad osition first, involving the single SFD-55B, as this is the simplest. Feed the utput of the sweep generator into the ase of the silencer amplifier. Adjust he level of the display on the screen to convenient size and make sure that here is not so much signal being fed no the system as to cause overload nywhere along the line. This could pok like an ideal curve but is not the rue story.

In all probability the display on the creen will look "lopsided." The techique is to use resistors and capacitors f various sizes to make exploratory hecks. The resistor values will normaly range between about 10K and 1K, nd the capacitors from about 22pF to 00pF or more. Start with either a apacitor or a resistor of any value in he above range. Connect it between hassis and pin 1 or 2 of the resonator n the filter block, and note the effect on the screen. Careful observation, tother with a few tests, will indicate the orrect value of resistor or capacitor, nd the terminal to which it must be onnected, to give the best pass-band hape.

Note that at no time should the two esonators used for interstage coupling be subject to any of these adjustments.

More than likely, a resistor will give he best result. In some cases it may be necessary to connect a resistor or capacitor to both pins. We had one case where it was necessary to connect a 6.8K resistor and a 100pF capacitor, n parallel, from one pin to chassis, with a second resistor of 12K from the other pin to chassis. This was an extreme case.

Now switch to the sharp filter position, which brings in the block of four SFD-455B filters. It may be necessary to readjust the gain of the CRO vertical amplifier. The same principles apply as before, but the procedure is someHere are the layout details of the front end. The four crystals are at the left, with the switch immediately to the right. Above these two items are the oscillator and amplifier-multiplier tag strip and the trimmer tag strip. To the right of the trimmers is the ring mixer, with the RF amplifier assembly at the top right corner.

what more involved in that there are many more combinations possible. However, this may sound worse than it really is in practice. Proceed as before, with a resistor or capacitor from each of pins 1 and 2 to chassis, and note the effect.

At this point, a certain amount of guesswork as well as judgment must be applied. Connect the component which looks most promising, in that it results in an improved, if not a correct, pass band shape. If improvement is still called for, proceed as before. More than likely, a component will be found which gives the final correction. If not, connect the most promising component into circuit and proceed along the same lines. When the final pass band is achieved, all the corrective components



THE MARK OF DISTINCTION

NO.	NOM. WATTS				MTG.	H.	₩.	L.	
OPM1A	5	7000, 5000	S.É.	15, 8, 3.7, 2	W	2¼ x	23/4 >	(21/4	
OPM19A	5	7000, 5000	S.E.	500, 250, 166; 100	W	2¼ x			
DPM20A	5	10000, 8000	S.E.	15, 8, 3.7, 2	W	21/4 X			
DPM2A	7	10000	P.P.	15, 8, 3.7, 2	W	21/4 X			MEDIUM FIDELITY
DPM3A	10	4000, 2500	S.E.		VC	3¼ x			40-30000 CPS
DPM4A	10	4000, 2500	S.E.	500, 250, 166, 100	VC	31/4 X			
PM5A	15	5000, 3000	P.P.		VC	31/4 X			± 2 db.
PM6A	15	5000, 3000	P.P.	500, 250, 166, 100	VC	3¼ x			1
PM7A	15	(10000) 8000, 7000		15, 8, 3.7, 2	VC	31/4 X			
PM8A	15	(10000) 8000, 7000		500, 250, 166, 100	VC	3¼ x			1
PM10A	25	(8000) 6600	P.P.	15, 8, 3.7, 2	VC	3¼ x			
PM9A	25	(8000) 6600	P.P.	500, 250, 166, 100	VC	31⁄4 X	25% >	(31/2	
PM14A	35	(8000) 6600	P.P.	15, 8, 3.7, 2	VC	41/8 X	31/4 >	(31/8	() Impedance
DPM11A	35	(8000) 6600	P.P.	500, 250, 166, 100	VC	41/8 X			in brackets indicate
PM13A	55	3500	P.P.	15, 8, 3.7, 2	VC	4% x	3% >	31/8	
PM12A	55	3500	P.P.	500, 250, 166, 100	VC	41/8 X	3%)	(31%	screen taps available.
PM21A	100	(4500)	P.P,	500, 281, 125, 31	VC	41/8 X	3% x	(43/4	
DPM16A	10	500		15, 8, 3.7, 2	W	2¼ x	2¾ >	(2¼	LINE TO VOICE COIL
DPM18A	25	500		15, 8, 3.7, 2	VC	3¼ x	25% x	(3	_ 40-30000 CPS ± 2 db.
DP412	7	9000 + Screen Taps	P.P.	15, 7.5, 3.7, 2.	W	2½ x	23/4 >	(3	MULLARD STEREO PLAYMASTER UNITS
)P308/15	12	8000, 6000	P.P.	15, 3.75	VC	4¼ x	31/ Y	31/	HI-FI FOR MULLARD
DP308/8.4	12	8000, 6000	P.P.	8.4, 2.1	VC	41/4 X	31/4 x	(31/2	5-10 AMPLIFIER
0P301/15	12	8000 + Screen Taps	PP	15, 3.75	VC	4¼ x	31/2 >	31/	
DP301/8.4	12	8000 + Screen Taps		8.4, 2.1	VC	41/4 X			-
DP312/15	25	6600 + Screen Taps		15, 3.75	VC	5 x			ULTRA-LINEAR
P312/8.4	25	6600 + Screen Taps		8.4, 2.1	VC	5 x			
)P387/15	12	8000 + Screen Taps	P.P.	15, 3.75	VC	3½ x	3 ×	(3	
P387/8.4	12	8000 + Screen Taps		8.4, 2.1	VC	31/2 X			For 6BQ5's (EL84's)
P447/15	12	8000 + Screen Taps	P.P.	15, 3.75	VC	3½ x	3 >	(3	-
DP447/8.4	12	8000 + Screen Taps		8.4, 2.1	VC	3½ x			For 6GW8's (ECL86's)
P499/500	60	4000	P.P.	500	W	2½ x	4½ x	(3	PHILIPS
)P499/15	60	4000	P.P.	15	W	21⁄2 x			60 WATT AMPLIFIER
DP499/8.4	60	4000	P.P.	8.4	W	2½ x	41/2 >	(3	(6CA7's)(EL34's)
)P541	40	3300		15, 8, 3.7	VC	41/8 X	33/4 >	33/4	GUITAR AMPLIFIER
)P542	60	2600		15, 8, 3.7	VC	4¼ x			ELECTRONICS AUSTRALIA
PS10K3	5	1 0000	S.E.	3	HEI	GHT			
DPS7K3	5 5 5	7000	S.E.	3 >	1-5/1 e	ГН 1/,			
DPS5K3	-5×-	5000	S.E.	3 × 4 × 4 × 4 × 4 × 4 × 4 × 4 × 4 × 4 ×		GTH 1	-		SPEAKER
OPS10K15	-5 X -	And the second sec	<u>3.E.</u> S.E.	15 ZZ		NTING	-		TRANSFORMERS
OPS7K15	5 MON	7000	3.E. S.E.	15 00		TRES			
OP\$5K15	5 ¥	5000	<u>S.E.</u>	15 wz	UEN	INCS.	-		

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are wired permanently to the copper side of the board.

This description may give the impression that the task is a tedious one. This s not the case and the correct shape can normally be obtained in a shorter ime than it has taken to write the deailed instructions!

The next adjustment is to introduce he correct amount of attenuation at he output of the broad filter, so that when switching from broad to sharp, here is no change in gain. This can be lone readily, with the sweep still set ip. Adjust the low value resistor shown as 150 ohms) to a value which equalises the gain.

Using the sweep setup the BFO can be set, at least approximately, to the correct frequency on each side of the bass band of the sharp position. Assuming a capacitor of 68pF or so across he 1mH inductor, switch on the BFO and see where the centre frequency lies. A good place to start is at about the end near the bottom of the pass band. Adjust the capacitor to give this result. Now add another capacitor, 100pF or berhaps more, across the capacitor just lecided. The new value should shift the BFO centre frequency to the correponding point on the other side. These positions may be subject to some thange under listening conditions. This completes the sweep alignment. Turn the tunable IF capacitor to its jully meshed position. Set the dial pointer so that it coincides with the cale horizontal base line. On our dial

Turn the tunable IF capacitor to its ully meshed position. Set the dial pointer so that it coincides with the cale horizontal base line. On our dial cales the 3MHz point will be alredy narked in, about 5-32in above the base ine. The 6Mhz point, on our scale, is bout 3-8in above the base line at the ther end of the scale. If you are makng your own scale, these two points hould be fixed at this stage.

ng your own scale, these two points hould be fixed at this stage. Set the RF Band and Tuning Range witches to 3-6MHz. Set the dial pointr precisely to 3MHz. Feed in a signal rom a signal generator, or other ource, at precisely 3MHz. Adjust the lug in the oscillator coil, L8, until the signal gives maximum deflection on the meter. Adjust the slugs in coils L6 and L7 for maximum response on he S meter. If necessary, reduce the generator input level so that the S neter does not reach full scale. Set the dial pointer to precisely MHz and the generator to the same requency. Adjust the trimmer on the

Set the dial pointer to precisely MHz and the generator to the same requency. Adjust the trimmer on the soillator section of the gang until the ignal gives maximum response on the S neter. Peak up both of the other two rimmers on the gang. Return to the MHz point and repeat the process, as t will be found that the position will have shifted a little. The 6MHz point nust be checked and this process must be repeated until both the 3MHz and MHz points are in the correct positions.

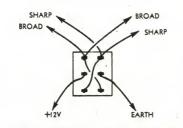
We are now in a position to do the tather exacting job of calibrating the dial. Fortunately, it is only necessary to calibrate from 3-6MHz, the rest of the ranges will automatically come in their right positions, assuming that the crystals are on frequency. A reliable source of accurate frequencies over the 3-6MHz range is required, the final result being only as good as the original reference. Signal generators are usually quite good, but they often are a little off calibration and ths will be carried over to the new dial. If you have a source of 1MHz and/or 100KHz spot frequencies from crystals, then these

should be used. The alternative is to use the best available.

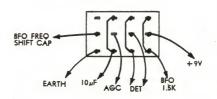
With the 3 and 6MHz points already set, the 4 and 5MHz points should be marked in next. Then it is a good idea to mark in the 500KHz points. This done, it is an easy matter to set and mark in the 100KHz points in between. Mark these points first in pencil, then in ink or other permanent fashion.

Set the dial pointer to 6MHz and set the RF Band switch to 6-18MHz and the Tuning Range switch to 9-12MHz. Feed a signal into the aerial terminal at

SELECTIVITY SWITCH



The selectivity switch is wired according to this diagram. SSBI, AM, SSB2 SWITCH



This is how the AM-SSB switch should be wired.

9MHz and make any necessary adjustment to the trimmer across L6.

Disable the BFO by removing the 9 volt lead from the 6.8K resistor. Switch to either SSB1 or SSB2 and with the generator set as before, switch on the modulation. Adjust the 100K potentiometer on the product detector for a null in the modulation. Restore the 9 volt lead and the alignment is complete.

Having completed your receiver and attached an aerial to it, a little practice will soon help in mastering the controls. Perhaps a short lesson would be in order.

Set the Tuning Range and RF Band switches to the positions which include the wanted frequency. Tune the wanted station on the dial and peak up the signal with the RF Tune control. Due to economy in design, it is possible to adjust the RF Tune control to another frequency than that of the wanted signal, thereby reducing its strength and possibly favouring an interfering signal. This situation should be avoided.

When a signal is tuned in the aerial capacitor should normally be set towards "max" so that a relatively large amount of signal is fed into the receiver. However, very strong signals could cause overloading, and this control should be turned back until the problem disappears. The higher the received frequency, the further towards "min" will this control have to be set. When trying to receive a medium strength or weak signal in the presence of a very strong adjacent one, the strong signal may cross-modulate the wanted one. Again, the aerial capacitor should be set towards "min," until the problem is resolved. Generally, the noise silencer will be set to the disabled, or completely off position. This is essential when receiving very strong signals, or even when receiving lower strength signals in the presence of a very strong adjacent signal. The reason for this is that the silencer is fitted before the sharp selectivity of the receiver and the strong signal, even with the silencer control operative but turned well back, can be suicidal. In short, the strong signal can turn off the gate and nothing is allowed through.

Under conditions where it is desired to receive a medium to weak signal, in the presence of noise, the Noise Silencer control should be advanced to a point where the noise is reduced or eliminated. The limiting point comes where the peaks of the wanted signal modulation are clipped off. The control should be backed off to avoid this condition. Noise silencing is often complete in the presence of impulse noise, but the effectiveness against hiss and similar overlapping noise is limited.

When receiving SSB signals, the detector must be set to either SSB1 or SSB2. As the heterodyning crystals in the front end are used for injection both above and below the frequency of the incoming signal, it is not possible to mark the switch in the more conventional manner as USB and LSB. For any particular band the correct position may be quickly determined on a trial and error basis.

So there it is. We have set out to produce a receiver which would give a reasonably high performance, at a modest cost. We think we have succeeded and we hope you like it.

Before even completing this series of articles we have been asked for sensitivity and signal-to-noise ratio figures. So far, all we can say is that the internal noise is extremely low, giving a practical sensitivity which is very good. There are three main factors contributing to the low noise; the FET RF amplifier, the ring mixer, and the high "Q" of the RF coils. We have attempted to measure the signal-to-noise ratio but all the figures obtained so far appear to be "too good to be true." Until we can double check our equipment, or have the measurement made by an independent organisation, we would prefer not to quote them.



item	Symbol	2SF	2SF	2SF	2SF	2SF	2SF	2SF	2S 658	Unit	<u>M</u>
*Non Rep. P.R.V.	VR surge	101	102	104 300	400	108	656 75	657 150	300		TT
*Rep. P.R.V.	V R surge	50	100	200	300	400	50	100	200		
*Rep. PK. Fwd. Blocking Voltage	VFOM	50	100	200	300	400	50	100	200	v	
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Non Rep. P.R.V.	VR surge		75		50	300		600		V	
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Fundamentals of SOLID STATE

Chapter 10

The bipolar transistor — NPN and PNP forms — basic configuration — equilibrium conditions — collector-emitter bias alone — the effect of forward emitter-base bias minority carrier injection — base diffusion, and collection — the device as a power amplifier — factors affecting the gain — the gain factors alpha and beta — characteristic curves — the common base characteristic — the common emitter characteristic.

Let us now turn our attention to a fourth basic semiconductor device, one whose development in fact marked one of the most important milestones in the history of the electronics industry: the **bipolar transistor.**

Although in earlier chapters we have examined other "transistor" devices such as the unijunction and the FET prior to the present introduction of the bipolar transistor, this order of presentation has been arranged by the author mainly in an effort to assist the reader by dealing with concepts and devices in a logical and progressive manner. In consequence, the presentation order is quite unrelated to the chronological order in which the devices made their appearance.

Actually the bipolar transistor was the first practical transistor device to be developed. The first crude working model was built in December, 1947, at the Bell Telephone Laboratories by physicists William Shockley, John Bardeen and Walter Brattain, and announced in the "New York Times" of July 1, 1948. This despite the theoretical proposition of the FET device some 20 years earlier, as noted previously in chapter 8. In fact the name "transistor" was coined by Bell Labs expressly for the bipolar device. It was intended to detrick the coartige of the device

In fact the name "transistor" was coined by Bell Labs expressly for the bipolar device. It was intended to describe the operation of the device, being a contraction of the words "Transfer" and "resistor." However, although the term "transistor" is still widely used to signify the bipolar device in particular, it has also become widely used as a generic name applied to any three-element semiconductor device capable of power amplification. The result has been ambiguity, and accordingly it has become common practice to use the term "bipolar transistor" to signify the specific device. For this reason the latter term will be that used in the present and subsequent chapters.

Basically, the bipolar transistor consists of a device having three functional semiconductor regions. The three regions are arranged such that there are two adjacent and approximately parallel P-N junctions, sharing one of the three regions as a thin common region. Naturally this means that the unshared or "outer" regions of the device must both be of similar semiconductor type, because they will both be of opposite type to the shared common region.

From this definition and from the somewhat schematic representations shown in figure 10.1 it may be seen that, like the unijunction and the FET, bipolar transistors may be constructed in either of two complementary forms. One form is that having an "NPN" configuration, in which the shared common region is of P-type material while the outer regions are of N-type material. The other or "PNP" form has the converse arrangement.

As one might well expect from previous chapters, both varieties of the device operate in virtually identical fashion except that the polarities of operating voltages and currents are opposite, and the roles played by the various current carriers are reversed. In the case of the NPN variety, conduction band electrons play the major part in

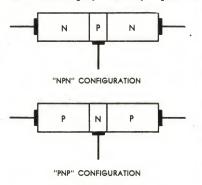


Figure 10.1

device operation, whereas with the PNP variety it is valence band holes which play the major role.

Because they operate in virtually identical fashion, the performance of NPN and PNP bipolar transistors of the same semiconductor material and geometry is almost identical. It is true, h o we ver, that there are subtle differences in performance due to such theoretical factors as the differing mobilities of electrons and holes. It is also true that there are practical manufacturing problems which tend to make it harder to achieve some aspects of device performance with one form compared with the other.

by Jamieson Rowe

Despite these factors, at the present state of the semiconductor art there are many types of bipolar transistor which are available in NPN and PNP versions sufficiently comparable in performance to be virtually interchangeable in a large number of applications. The appropriate power supply polarities must be provided in each case, of course.

Although the foregoing might seem to suggest that one form of the device could perhaps be adopted for universal use, and the other virtually ignored, there are a number of reasons why this is not done. One is that there are many applications in which a particular combination of circuit configuration and power supply polarity strongly favours one form compared with the other. Broadly speaking, there are as many such applications favouring one form as there are favouring the other, so that in general it is both convenient and economical to have devices available in both forms.

A further reason is that in critical applications demanding high performance in terms of certain parameters, one device form can offer distinct advantages compared with the other as a result of the subtle differences between the two noted above. An example is in UHF power amplifiers, where NPN devices tend to be more attractive largely as a result of the higher mobility of electrons relative to that of holes. In other cases PNP devices may be more attractive.

There is also the important reason that with both varieties of the device available, it becomes possible to produce novel and highly efficient circuitry which employs both types of device and exploits their complementary behaviour. This is a very worthwhile and dramatic advantage which the bipolar transistor and other semiconductor devices, such as the unijunction and the FET, offer in comparison with the thermionic valve.

As with the other semiconductor devices which we have examined in previous chapters, the bipolar transistor may be fabricated from a variety of semiconductor materials; although to date only germanium and silicon have been used to any appreciable extent. Germanium was used for the first devices developed. and for those first marketed, and is still used to a small extent for very high current switching devices and very high frequency amplifiers. However, the great majority of bipolar transistors now manufactured and used are fabricated from silicon, largely because of the superior leakage behaviour and high temperature performance offered by this material.

Because of the similarity between the NPN and PNP forms of the bipolar

transistor, it is really only necessary to consider one form when examining the fundamentals of device operation. Once the basic concepts of device operation are grasped with respect to one form, the operation of the other form may be deduced simply by exchanging the roles of the current carriers, and reversing the polarities of all voltages and currents.

In the treatment which follows, the PNP form of the device is used as the basis for discussion, primarily to assist the reader in becoming more familiar with the behaviour of holes as current carriers. However, upon completion of the chapter the reader may care to deduce for himself the corresponding picture of NPN device operation, in order to test and reinforce his understanding.

An elementary PNP bipolar transistor is shown in figure 10.2 (a). It may be seen that the thin central N-type region shared by, and between the two P-N junctions, is called the base (B), while the two outer P-type regions are called the emitter (E) and collector C).

The same names are used for the corresponding regions of the NPN variety of the device. In both cases the term "base" refers to the thin central region, which is lightly doped, while the terms "emitter" and "collector" refer respectively to the heavily and lightly doped end regions. The significance of these terms should become apparent later in this chapter.

Superficially, as may be seen, the bipolar device consists basically of two P-N junctions arranged in a "back-toback" or inverse series configuration, with the common connection brought out as the base electrode. From this the reader might be led to infer that its behaviour would be very similar to that of a pair of simple P-N diodes connected in a similar manner. However this is only true in a very limited sense indeed.

If one simply ignores either of the two device junctions and its associated P-type region, and proceeds to examine the behaviour of the remaining junction alone, then that behaviour will in general be identical with that of a normal P-N diode. The results of such a test will be the same for either junction, so that in this rather artificial and limited sense the device is in fact equivalent to a pair of simple diodes connected back-to-back. Yet almost the only practical significance of this fact is that it may be used as the basis of simple tests for device damage.

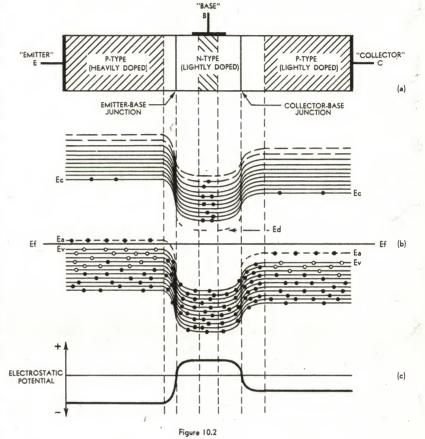
Of far greater significance is the fact that as soon as both junctions are permitted to play an effective part in determining device behaviour, its behaviour tends to depart quite markedly from that of a pair of simple diodes. And the reason for this is that the thin base region shared by both junctions causes a significant interaction between the two.

It is, in fact, this interaction between the behaviour of the two junctions which is responsible for virtually all of the highly useful properties of the bipolar transistor, and which therefore we must proceed to examine in some detail. But before we do so, it may be worthwhile for the reader to refresh his understanding of P-N junction behaviour by referring to the diagrams of figure 10.2 (b) and (c).

Figure 10.2 (b) shows the energy level diagram corresponding to the equilibrium condition of the elementary transistor shown in (a). As before, the equilibrium situation represented is that which applies with zero external bias applied to the device electrodes, and is thus the dynamic balance reached between the "internal" carrier movements due to the opposing mechanisms of diffusion and drift. The average carrier energy level or Fermi level (Ef) is constant throughout the material.

As part of the equilibrium, depletion layers are formed in the vicinity of "up-hill" slope of the nearest junction.

Similarly the majority carriers (electrons) in the base region effectively "see" themselves at the bottom of a potential "valley" in the centre of the device, as may be seen if the diagram is viewed upside-down. In order to pass from the base to either of the two other regions, in the equilibrium situation, these carriers must surmount the "uphill" potential slope of the junction concerned.



each junction, extending into the material on either side to a degree inversely proportional to the doping levels. Drift fields are set up across the depletion layers, as before, with the P-type side of the depletion layers acquiring a negative charge, and the N-type side a positive charge. This produces a distribution of electrostatic potential throughout the device, of the shape shown in figure 10.2 (c).

From previous chapters, the reader may be able to recognise that this potential distribution has two important implications regarding the movement of current carriers within the device.

One important implication is that, in the equilibrium situation, both P-N junctions of the device represent potential barriers to the MAJORITY CAR-RIERS in each of the three semiconductor regions.

Hence the majority carriers (holes) in both the emitter and collector regions of the PNP device shown effectively "see" the base region as a potential "mountain" separating these two regions, this "mountain" having the crosssection suggested by the curve of figure 10.2 (c) viewed normally. In order to pass from one P-type region to the other under equilibrium conditions, such carriers must first surmount the In short, then, any flow of majority current carriers across the device junctions constitutes a movement of these carriers in opposition to a depletion layer potential barrier. It may be recalled from chapter 4 that this type of majority carrier flow is normally known as a **diffusion current**.

The second important implication of the diagram of figure 10.2 (c) is really the converse of the first. In the same equilibrium situation, both P-N junctions of the device represent "downhill" potential slopes to the MINORITY CARRIERS in each of the three device regions.

Hence in the PNP device shown, minority carrier holes in the base region "see" themselves at the top of a relatively high potential "plateau," and can "roll down" a potential slope into the emitter or collector regions if they diffuse into the depletion layer region of the appropriate junction. Similarly, minority carrier electrons in the emitter and collector regions "see" the base region as a narrow "gorge" running between the two outer regions, and can accordingly roll into the base if they diffuse into the appropriate depletion layer.

Minority carrier flow across the junctions of the device may thus be de-

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9	151628	2.320	1.350	1.560	9	151637	1.560	1.350	Type
12	151629	2.788	1.818	2.028	12	151638	2.028	1.818	Housings
15	151631	3.256	2.286	2.496	15	151640	2.496	2.286	available
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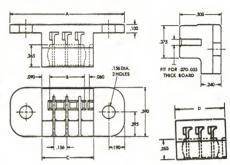
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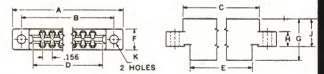
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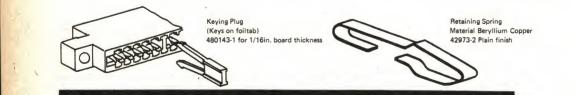
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42717-3	42840-3	22 18	.120 max Sum of Insul. Diameters		Gold/Standard	900
	66067*	two 16 max.			Gold/Standard	

Part No. 582501-1 Inter Control Keying Plug Contact Extraction Tool Part No. 465195-1 for 15-22 Pos. Part No. 465195-2 for 18 Pos. Contact Extraction Tool



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ELECTRONICS Australia, March, 1970

С D Е scribed as drift currents, as they represent a carrier flow influenced by and in the direction of the "inbuilt" electric field across each junction depletion layer.

From previous chapters it may be recalled that the only minority carriers present in a doped semiconductor region under equilibrium conditions are those generated by the "intrinsic" excitation mechanism. Hence in the bipolar transistor for the equilibrium conditions, the minority carrier drift currents moving "down" each depletion layer potential slope will be at a very low level, and saturated in the sense that they are determined almost completely by the number of carriers produced by excitation.

Since by definition there can be no nett current flow in a device in the equilibrium condition, the foregoing implies that the majority carrier diffusion currents moving in opposition to the minority carrier currents, or "up" each depletion layer slope, must also be at a very low level.

Thus while there are currents flowing across both junctions of the bipolar transistor in the equilibrium situation, as an integral part of the equilibrium, these currents are quite small and consist in both cases of equal and opposite majority and minority carrier currents. In this respect the bipolar transistor does not differ from the other junctions semiconductor devices examined in earlier chapters.

It is hoped that the foregoing review of the equilibrium condition of the device has assisted the reader in refreshing his understanding of basic P-N junction behaviour. Now let us turn to consider what happens when the equilibrium of the bipolar transistor is disturbed by the application of external bias voltages.

If one connects a DC bias voltage between the emitter and collector electrodes of the device of figure 10.2, of either polarity, only a very small current is found to flow. This is perhaps not surprising, because in this case we are effectively connecting the external bias across both junctions in series, and for either polarity of the bias one of the junctions will be reverse biased.

The internal situation of the device will, in fact, be only slightly different from that for equilibrium. The depletion layer of the reverse biased junction will widen to correspond to the increased electric field across it. This in turn will cause a small nett current to flow, as there will be a reduction in the majority carrier diffusion currents while the minority carrier drift curtents will remain fixed at their saturation values.

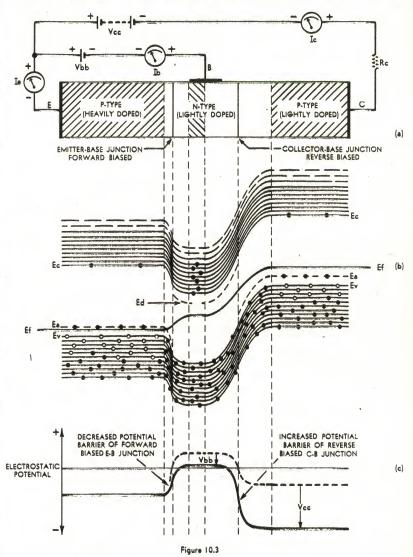
The small current which flows through the reverse-biased junction will cause a very small voltage drop to appear across the other junction, which will naturally be forward biased. Accordingly the depletion layer of this junction will narrow very slightly, and its majority carrier diffusion currents will increase to correspond to the small nett current flow.

It may be seen that when a single external DC bias is connected between the collector and emitter electrodes of a bipolar transistor, the device behaviour for both applied polarities is basically very similar to that of a normal P-N junction diode when reverse biased. However the small current which flows through the device in this situation is actually slightly greater than the reverse bias current of a normal P-N diode, or of either device junction alone. And although the difference in current levels is only slight, it is of great significance, for it provides the key to the really interesting and unique aspects of bipolar transistor operation.

aspects of bipolar transistor operation. The alert reader may have already noticed an interesting fact about the small current which we have seen to flow through the device when biased between emitter and collector. This is that the current which does flow effectively "changes its nature" during its passage through the device, even though its magnitude necessarily remains constant. When passing a P-N junction, of necessity they undergo a reversal in terms of population statistics — simply because the majority/minority roles in each type of semiconductor material are the opposite of those in the other type.

site of those in the other type. Hence a carrier initially belonging to the majority population of one region will automatically become a minority carrier when it crosses a junction into a region of opposite type; and vice-versa.

Perhaps the most obvious implication of this, in the case of our foregoing biased transistor, is that the minority carrier currents flowing across the reverse-biased junction actually consist of the same types of carrier moving in the same directions as the majority carrier currents flowing across the forwardbiased junction. Only the "labels" ap-

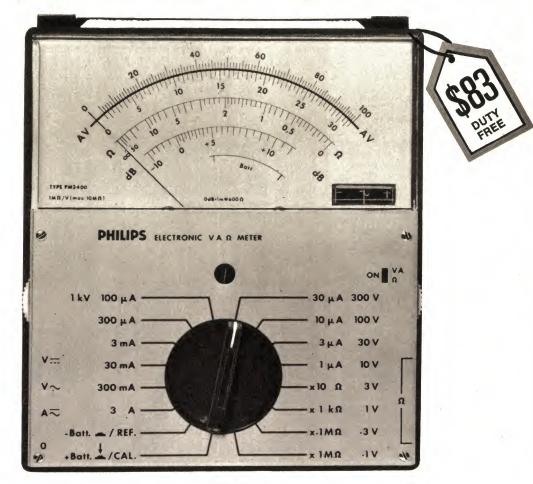


through the depletion layer of the reverse-biased junction, we saw it to consist of drift currents derived from the minority carrier populations of the two adjacent regions; yet when it passes through the depletion layer of the forward-biased junction it then consists of diffusion currents derived from the adjacent majority carrier populations.

At first sight this may seem not only confusing, but downright contradictory. Yet the explanation is really quite simple: when carriers move from one semiconductor region to another across plied to the carriers change, in other words. This should clear up the apparent contradiction.

However, a second and more important implication is that those majority carriers (holes) which diffuse across the forward-biased junction into the base region will naturally then become minority carriers in that region, boosting the minority carrier population of the base above its normal level. And because the base region is relatively thin, many of these additional minority carrier holes will be able to diffuse across to the depletion layer of the re-

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verse-biased junction before their passage can be interrupted by a recombination with a majority carrier electron.

Naturally those holes which do reach the reverse-biased junction depletion layer will be "grabbed" by the electric field of the latter and will accordingly drift into the far P-type region. The minority carrier hole current of the reverse-biased junction will thus be boosted to a value greater than its normal saturated value, and this ex-plains why the net current passed by the device is higher than that of a normal reverse-biased junction. The mechanism just described may

be seen to involve a novel type of interaction between the two junctions of the device: the current passed by one junc-tion in the reverse-blased state is in-creased significantly from its "normal" saturated value as a result of excess minority carriers injected into the narrow base region by the forward-bias of the adjacent junction.

This is, in fact, the precise "inter-action" mechanism which is responsible for the really important behaviour of for the really important behaviour of the bipolar transistor, and to which ref-erence was made earlier. The ability of one forward biased junction to influence the conduction of the other reverse-biased junction gives the device the ability to perform power am-plification, although of a slightly different type to that of the thermionic value or the field effect transistor. valve or the field effect transistor.

In figure 10.3(a) is shown an ele-mentary PNP transistor with external bias voltages applied to it, in a fashion which should help in understanding how the device is capable of amplification.

One of the applied voltages, that abelled "Vcc," may be seen to cor-respond to the collector-emitter bias which we have just considered in the foregoing discussion. With this bias applied alone, as we have seen, the device will draw only a small current slightly arger than the current drawn by a reverse-biased P-N junction. We might thus expect the meter measuring collector current Ic to register only a current of this low order.

The other bias voltage applied to the device is labeled "Vbb," and may be seen to be applied between the base and emitter with a polarity which forward biases the base-emitter junction. Superficially one might therefore ex-pect a considerable current flow to be registered by both the meter measuring base current Ib and that measuring emitter current Ie.

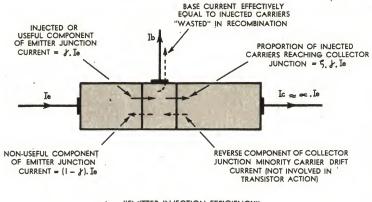
Perhaps surprisingly, this is not quite what is found. The meter in the emitter ead is certainly found to register an appreciable current, as expected. How-ever, the meter in the base lead is found to register only a small fraction of the emitter current, while instead the meter in the collector lead is found to register virtually the same current as the emitter meter, despite the reverse bias on the collector-base junction!

The reason for this behaviour is simply that the majority carrier hole current passed by the forward biased base-emitter junction "injects" excess minority carrier holes into the base, as before. Because of the narrowness of the here preserved the base region, a major proportion of these holes are able to reach the de-pletion layer of the reverse biased collector-base junction before being stopped by recombination with a majority

carrier electron. Those which do reach the second junction will naturally "roll down" the potential gradient into the collector.

As the emilter region is relatively heavily doped whereas the base region is quite lightly doped, the majority car-rier diffusion current passed by the emilter-base junction consists mainly of boles moving from emilter to have rathholes moving from emitter to base rather than electrons moving from base to emitter. Also the light doping in the base region results in a relatively low population of majority carrier electrons in the base, so that most of the minority carrier holes injected from the emitter escape recombination and do actualrent (and hence low power) conditions at the base of the device can thus be arranged to cause large changes in both the voltage and current levels at the collector. From this it may be seen that the bipolar transistor is capable of pro-

viding appreciable power amplification. It should now be fairly clear why the names "emitter" and "collector" are used for the two end regions of the bipolar device. The name "emitter" is surely quite appropriate for the region concerned, which does effectively emit or inject carriers into the base region. Similarly the name "collector" is quite appropriate also, for the region con-cerned does effectively collect those of



5 = "BASE TRANSPORT EFFICIENCY" 1.5 ~ ~ ~ = "COMMON BASE GAIN FACTOR" Figure 10.4

ly end up in the collector region. This explains why the emitter and collector currents are almost equal.

The base current is actually equal to the slight difference between the two, because in effect it consists only of the small number of electrons necessary to replace those majority carrier electrons in the base region which do actually meet and recombine with an injected hole. This accordingly explains why the base current is very small.

From the foregoing it may be seen that the operation of the bipolar transistor is basically a combination of three simple processes: injection, diffusion and collection. The forwardbiased emitter-base junction **injects** minority carriers into the base, where-upon these carriers **diffuse** away through the base, because of the local-ised concentration. Those which manage to reach the reverse biased collector-base junction without recom-bining with a majority carrier are then collected by that junction.

The effect of forward bias Vbb applied across the base-emitter junction, then, is to cause a marked increase in the current flowing through the reverse biased collector-base junction. And as one might expect, the increase in col-lector current is highly dependent upon the magnitude of the applied base-emitter bias. In fact only a small bias Vbb is found sufficient to produce quite a large collector current Ic, and relatively small variations in Vbb tend to produce large variations in Ic.

As the collector-base junction is reverse-biased, the collector supply voltage Vcc may be considerably larger than Vbb. This allows a fairly large load resistor Rc to be connected in series with the collector, as shown. Changes in the low voltage/low curthe injected carriers which diffuse

The name "base" is applied to the central region of the device largely as a historical carry-over from the very first type of bipolar transistor, the long ob-solete "point contact" variety. With this type of transistor the base region did in fact form the physical base of the func-tional device. However, with most mod-ern forms of the bipolar transistor this is not the case, and the term "base" is merely a conventional label.

At this point the reader may find it worthwhile to examine the diagrams of figure 10.3 (b) and (c), which show respectively the energy band diagram and electrostatic potential distributions for the biased transistor of figure 10.3 (a). Comparison of these diagrams with the corresponding diagrams for the equilibrium situation, given in figure 10.2, may help in clarifying the foregoing discussion.

As we have seen, the base current of a biased bipolar transistor consists basically of the small number of electrons necessary to replace those majority car-riers in the base region "absorbed" by recombination with injected minority carriers. As such, it is numerically equal to the difference between the emitter and collector currents. From this it follows that the larger can be made the fraction of emitter current reaching the collector, the smaller will be the base current and the higher the potential amplification of the device.

Naturally one factor which has an important effect on the proportion of emitter current reaching the collector is the actual composition of the emitter junction current. From the foregoing discussion, it should be fairly clear that it is only the component of emitter current which consists of carriers moving from emitter to base which plays a part

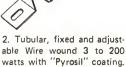
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in the operation of the device; the component which consists of carriers moving in the opposite, direction plays no useful part.

It is for this reason that the ratio between the emitter and base impurity doping levels is made very high, ensuring that the emitter junction current consists almost entirely of carriers moving from emitter to base. In the PNP transistor, as we have seen, these car-riers are holes; conversely in the case of the NPN transistor they are elec-trons. The ratio of the emitter-to-base component of emitter current to the total emitter current is known as the emitter injection efficiency or ratio, which term the reader may recall was also used in chapter 7, in connection with the unijunction.

Apart from the emitter injection ratio, a second important factor governing device amplification is the number of minority carriers injected into the base which are able to diffuse through to the collector junction depletion layer without meeting with a majority carrier and "falling by the wayside" due to recombination. Expressed as a proportion of the total injected carriers, this is known as the base transport efficiency.

It is to ensure a high base transport efficiency that the base region is made very narrow; the shorter the distance which the minority carriers must travel through the base, the lower the likelihood of recombination. The base transport efficiency is also improved by making the impurity doping level of the base as low as possible, to ensure a relatively small population of base region majority carriers.

The schematic diagram of figure 10.4 may help the reader to visualise the significance of the emitter injection efficiency and base transport efficiency factors in terms of basic device operation.

It is possible to express the am-plification action of the bipolar transis-It is tor in terms of two different gain factors, both of which are actually current increment ratios. One of these, and the earliest to be used, is called α (alpha), and is simply an expression of the ratio between collector and emitter currents, in terms of changes or small increments:

$$\alpha = \frac{dIc}{dIe} (dVcb=0) \dots (10.1)$$

Here "dIe" is a small change in emit-ter current, "dIc" is the corresponding change in collector current, and the expression in brackets specifies that the collector-base voltage is defined as constant.

Fairly obviously alpha is always less than one, because the collector current is always less than the emitter current. In fact alpha is a fraction which approaches unity asymptotically as the amplification increases: a very low gain device may have an alpha of 0.91, while a very high gain device might have an alpha of 0.998.

The numerical values of alpha for practical devices tend to be restricted to the range between these two examples, and are progressively cramped for increasing orders of amplification. Be-cause of this it is usually more con-venient to use the second gain factor called alternatively β (beta) or hfe. Beta is simply the device amplification

expressed as the ratio between collector

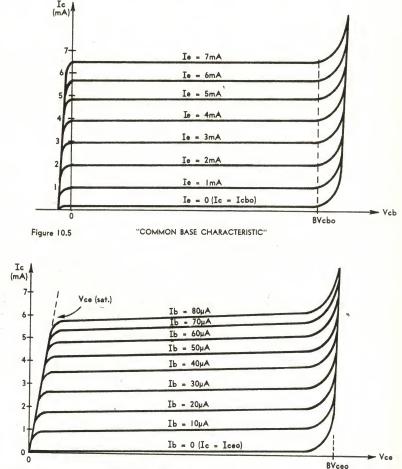
and base currents, again in terms of small increments:

$$\beta = \frac{dIc}{dIb} (dVce=0) \dots (10.2)$$

Here "dIb" means a small change in base current, "dIc" again means the corresponding change in collector current, and the expression in brackets has a similar meaning to that in (10.1).

Naturally since Ib is simply the difference between Ie and Ic, alpha and beta have a fixed relationship to tor characteristic, which in this case displays the amplification behaviour of the device in terms of the relationship between collector current and voltage for various values of emitter current. As may be seen, this is known as the common base characteristic.

Perhaps the first thing which the reader may note from the diagram is that the major portion of each curve in the characteristic "family" is almost horizontal, at a collector current value which corresponds in each case to a fraction alpha of the emitter current



"COMMON EMITTER CHARACTERISTIC" Figure 10.6

one another. A short calculation reveals that the relationship is as follows:

$$\beta = \frac{\alpha}{1-\alpha} \qquad \dots \qquad (10.3)$$

Beta normally has a value somewhat greater than unity, and does not become cramped at high orders of am-plification. For example, devices having alpha values of 0.91 and 0.998 quoted above would have corresponding beta values of 10 and 500 respectively. The reader may care to work these out for himself using equation 10.3.

Just as there are two different gain factors which may be used to express the amplification action of the bipolar transistor, there are also two main ways of representing the behaviour of such a device in terms of graphical characteristics. These will now be briefly examined.

Figure 10.5 illustrates one of the two main types of bipolar transistor collec-

value. The curves thus bear a strong resemblance to those of the FET and the thermionic pentode valve, and indicate that like these devices the bipolar transistor has a relatively high output resistance.

The curves have this basic shape be-cause the injection-diffusion-collection mechanism which we have seen to be responsible for device operation is basically almost independent of the magnitude of collector voltage. As long as the collector-base junction is not forward biased, its depletion layer is capable of "collecting" virtually all of the injected carriers which diffuse across the base. The collector current which flows as a result of forward emitter-base bias is thus effectively "saturated."

If the collector-base junction is in fact forward biased, normal device operation does naturally cease. This explains why the curves of figure 10.5 drop down sharply on the left-hand side. All curves in the family fall to

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zero current when the forward collector-base bias has been increased to approximately 0.3V for germanium, or 0.6V for silicon.

The other limit to the "pentode" region of device operation occurs when the reverse bias on the collector-emitter junction is increased to the point where this junction enters avalanche breakdown. As with any other P-N junction, the current then increases rapidly due to avalanche carrier collision. Normal device operation again ceases, and the device enters a high dissipation mode of operation. The collector-base voltage at which avalanche begins is called the collector-base breakdown voltage, symbolised BVcbo.

In the "common base" configuration in which the curves of figure 10.5 are measured, the collector-base junction is biased by a voltage applied directly between collector and base (Vcb). Because of this, the device does not amplify its own reverse bias current when the external base-emitter bias is zero (Ie = 0). The lowest of the curves therefore corresponds to the "normal" reverse bias current of the collectorbase junction, known as the collectorbase saturation current (Icbo).

It may be noted that the curves of figure 10.5 actually slope upward slightly in the direction of increasing collector voltage. The reason for this is that as the collector-base voltage is increased, the depletion layer of the collector-base junction naturally widens, and this reduces the effective thickness of the base. The amplification therefore increases slightly, due to lower carrier recombination and increased base transport efficiency.

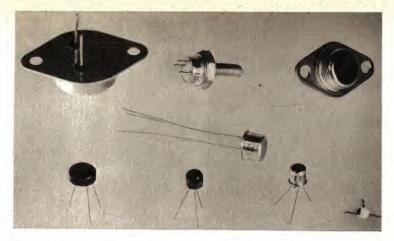
A further point to note is that although the curves for low values of emitter current are spaced apart by almost exactly the same intervals of collector current, those for higher values become cramped together. In other words, the amplification action of the bipolar transistor droops at high values of emitter and collector current.

The primary reason for this is that at high current levels the emitter injection efficiency of the device tends to fall as a result of the large number of minority carriers present in the base region. In effect, the number of minority carriers becomes so great that the emitterbase diffusion current component tends to fall, the base-emitter component rising to compensate.

The other main type of collector characteristic used for the bipolar transistor is that known as the common emitter characteristic, illustrated in figure 10.6. As may be seen, this displays the amplification action of the device in terms of the relationship between collector current and voltage for various base currents.

The common emitter curves are rather similar to those for the common base configuration, as may be seen, the main difference being that the value of base current corresponding to each curve is very much smaller than the value of emitter current. In effect, the common-emitter curves display beta, whereas the common base curves display alpha.

The curves may be seen to have a more pronounced slope than those of the common-base characteristic, and this is again due to the reduction of the effective base thickness as the collector-base junction depletion layer extends with increasing collector voltage.



An array of modern silicon transistors, reproduced approximately actual size. The largest device, when bolted to a suitable heatsink, is capable of dissipating up to 120 watts. The smallest shown is a subminiature type for VHF use, capable of dissipating only a few tens of milliwatts.

The effect is more dramatic in this case merely because beta is a more sensitive indicator of the amplification mechanism.

As before, the curves may be seen to cramp together at higher collector current levels, indicating the droop in amplification due to falling emitter injection efficiency. Again the effect appears more marked in this case, due to the greater sensitivity of beta as an indicator of the device amplification mechanism.

When the curves of figure 10.6 are measured, the collector bias voltage is applied between collector and emitter as shown in figure 10.3. As we saw earlier, this allows the device to amplify its own reverse bias current even when no external forward bias is applied to the base-emitter junction.

As a result the lowest (Ib=0) curve of the family in this case represents a collector current level somewhat greater than the normal reverse bias current of the collector-base junction. Known as the **collector-emitter saturation current** (Iceo), it is actually very close in value to Icbo multiplied by beta.

Whereas the curves of the common base characteristic maintained their value of collector current down to zero collector voltage Vcb, the curves of the common emitter characteristic may be seen to fall away at a low value of collector voltage, the value rising slightly with collector current. The reason for this is that because the collector bias voltage is applied between collector and emitter, it cannot be reduced below a certain value without effectively for ward-biasing the collector-base junction. Naturally when the latter occurs collector action falls, so that collector current drops as soon as the effective collector junction voltage reverses.

The voltage level at which the collector current of the device begins to fall is known as the collector saturation voltage, symbolised Vce(sat). The slight rise in this voltage with collector current results from the reduction in effective collector junction voltage due to resistive voltage drop in the relatively high resistivity collector and base material.

As before the collector bias voltage of the device cannot be increased indefinitely, for at a certain voltage avalanche breakdown occurs and the device current rises sharply. The avalanche breakdown of a bipolar transistor in the common emitter configuration occurs at the collector-emitter breakdown voltage, symbolised BVceo. Because the device amplifies its own

Because the device amplifies its own leakage current in this configuration, the amplification and avalanche effects are cumulative and this generally causes BVceo to be somewhat lower than the collector-tase breakdown voltage BVcbo.

At this stage of our discussion of the bipolar transistor it is hoped that the reader has gained a reasonably clear and satisfying concept of basic device operation. If this is not so, a glance back through the chapter may be advisable, as the concepts which have been presented are quite important and will be necessary for an adequate understanding of the following chapters.

SUGGESTED FURTHER READING

BURFORD, W. B., and VERNER, H. G., Semiconductor Junctions and Devices, 1965. McGraw-Hill Book Company, New York.

CLEARY, J. F. (Ed.) General Electric Transistor Manual, 7th Edition, 1964. General Electric Company, Syracuse, New York.

PHILLIPS, A. B., Transistor Engineering, 1962. McGraw-Hill Book Company, New York.

SHIVE, J. N., Physics of Solid State Electronics, 1966. Charles E. Merrill Books, Inc., Columbus, Ohio.

SURINA, T., and HERRICK, C., Semiconductor Electronics, 1964. Holt Rinehart and Winston, Inc., New York.

Also "The Transistor: Two Decades of Progress," a special review section in Electronics, V.41, No. 4, February 19, 1968.

ELECTRONICS Australia, March, 1970

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A low cost 200KHz Digital Frequency Meter

The "low frequency" version of our new digital counter design. It uses the same counting section as the high frequency version yet to be described, so that it can measure to beyond 40MHz if an external timebase is used. Integrated microcircuits and printed wiring boards make assembly quite straightforward.

by Jamieson Rowe

Taking advantage of modern components and circuit techniques, the basic digital counter-frequency meter described in this article offers a high standard of performance at a very modest cost. It provides the facility for making rapid, unambiguous frequency measurements and event counts of high accuracy and resolution. As a result it should be very suitable for use in equipment servicing, production testing, research and development, and by amateur radio operators.

It may also be of interest to universities and technical colleges, both as a means of providing low-cost digital frequency meters for student use, and also as a constructional project for engineering and science students. The design would be well suited for the latter application, as it combines low cost and ease of construction with the use of modern integrated microcircuits and printed wiring boards.

The design uses solid-state devices throughout, with the exception of the gas-discharge tubes used for numerical readout display. It uses a total of 29 microcircuits, 8 discrete transistors, 9 diodes and a silicon rectifier bridge. The digital microcircuits used include devices of the RTL, DTL and ECL variety, and together represent some 525 functional transistor elements and 34 functional diode elements. This may give some idea of the order of wiring simplification and cost reduction which has been made possible with microcircuits.

The instrument has a counter consisting of three full decades plus single digit over-range, and is also fitted with overflow detection and indication. The readout display is via side-viewing, gasdischarge display tubes for the full decades, together with a matching neon lamp for the over-range "1." Counter capacity is 1,999, giving a display resolution of .05 per cent.

Three frequency measurement ranges are provided, together with an "events counting" range and an "external timebase" range. The frequency ranges are nominally 0-2KHz, 0-20KHz and 0-200KHz.

The limitation of the self-contained frequency range of the instrument to 200KHz arises from the fact that this version of our DFM design uses a low cost mains-derived timebase system. A 50Hz signal from the power mains is doubled in a modified full-wave rectifier circuit, and then fed to a flip-flop divider chain to provide timebase frequencies of 100Hz, 10Hz and 1Hz. This system offers a considerable cost saving compared with a crystal oscillator and divider chain, and it is for this reason that we have adopted it for the low frequency version of the design. However, as 100Hz is the highest frequency which may be easily derived from the 50Hz AC mains, this means that 10mS is the shortest internal gating time available for frequency measurement.

A further consequence of the use of mains-derived timebase signals is that the measurement accuracy of the instrument for the ranges concerned is quite modest—typically only in the order of 0.5-1 per cent. However, it is believed that there are many applications in which this limitation and that of restricted frequency range will be outweighed by the low cost and freedom from reading ambiguity provided by the instrument.

The frequency response of the input signal shaping, gating and counter sections of the instrument is considerably better than the figure of 200KHz which corresponds to maximum capacity of the counter for a 10mS gating time. In fact, these sections will typically be capable of operating reliably to beyond 40MHz, as they are identical with the corresponding sections of the high frequency version.

high frequency version. All that is necessary in order to realise this "latent" frequency performance is to supply the instrument with the appropriate higher frequency timebase signals. These may be supplied from any suitable source of stable reference signals having a peak-to-peak output of about 3-4 volts. A suitable source would be the "Solid State Crystal Calibrator" described by the author in the September, 1969, issue. The selected timebase signal from such a



SPECIFICATIONS

A low cost digital frequency meter employing integrated microcircuits and gas-discharge readout tubes. The readout display provides three full decades plus single digit over-range. A panel lamp indicates counter overflow.

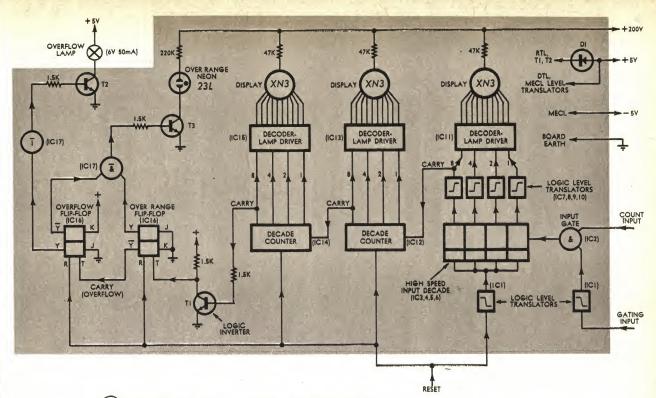
Basic frequency range of the instrument is 200KHz, but this is limited not by counter response but by the limitations of the internal mains-derived timebase. The response of the counter itself extends to beyond 40MHz, and this range may be realised if an external timebase is used.

The three internal frequency ranges cover 0-2KHz, 0-20KHz and 0-200KHz. An "events" position permits manual control of the counter gate for event counting. External gate control for this mode is also possible using a +3V/0 logic convention. Similarly an external timebase may be used for extended range measurements and frequency ratio measurements.

Two internal sampling rates are provided, 5 per second and 1 per 4 seconds, together with a manual sample facility and provision for external sampling input (+3V/0 convention).

Input impedance of the instrument is approximately 2K ohms, with an input sensitivity of approximately 30mV P-P up to 200KHz rising to better than 300mV P-P at 40MHz. The input sensitivity is adjustable and the input circuitry is protected from overload damage for inputs up to 100V peak-to-peak.

Power consumption of the instrument is approximately 40 watts.



(EA) DIGITAL FREQUENCY METER - COUNTER BOARD

Figure I

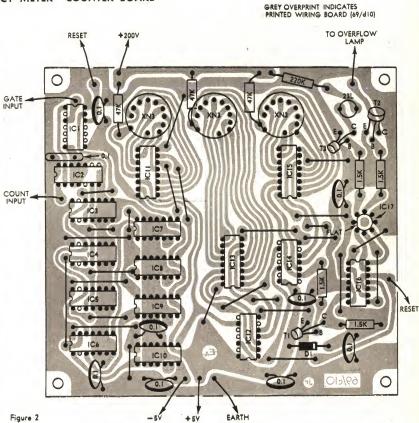
source is simply fed to a connector provided at the rear of the counter, and the function switch turned to the "external timebase" position.

Naturally the accuracy of the instrument when used with an external timebase source will be somewhat greater than with the internal mains-derived timebase signals. When the September, 1969, calibrator is used, for example, the accuracy will be in the order of .01% or better depending upon the care taken in standardising the calibrator, and upon the resolution of the effective range involved.

The same rear connector and function switch position used for higher frequency measurements may also be used to enable the instrument to perform frequency ratio measurements, or measurements in special units. Thus, by using appropriate timebase signals, it is possible to arrange the instrument to measure an unknown frequency in terms of a ratio to a known frequency, or to express a pulse rate in terms of beats per minute, firings per revolution, etc.

In the "events count" mode the instrument will perform normal counting, the gate being controlled by a manual pushbutton on the front panel. An indicator lamp is provided to display the "gate open" condition. The logic circuitry is arranged so that first the depression of the button following instrument reset will open the gate, while the second depression will close it. Further depressions have no effect until the instrument is reset, ensuring that readings are quite unambiguous. The input pulses counted in this mode may have any repetition rate up to 40MHz,

Remote command events counting is also possible, using the "external timebase" facilities. In this case a pushbutton and bounce-suppression circuit



would merely take the place of the external timebase generator to which reference was made earlier.

Naturally for convenient remote command operation a remote reset facility is also necessary, and provision has been made for this also. The instrument in fact provides four sampling modes: two automatic recycling modes, in which measurements are made at 5 per second and 1-every-4 seconds, respectively, a "manual" mode allowing reset when required using a second push-button on the front panel, and the "external" mode in which reset is initiated by a +3V/0V pulse applied to a rear panel connector.

The two internal sampling modes employ reset pulses of 5Hz and 0.25Hz repetition rates, which are derived from the mains timebase system. This obviates the cost of an independent free-running sampling generator, and involves only a slight restriction in terms of operating flexibility. The lower rate must be used for the 2KHz

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and 20KHz internal ranges because of the gating times used for these ranges; however, either sampling rate may be used for the 200KHz internal range and for higher-ranges employing external timebases.

The input sensitivity of the instrument is better than 30mV P-P between about 100Hz and 3MHz, falling to better than 300mV P-P at 10Hz and 40MHz. The sensitivity may be reduced if necessary, for the measurement of signals in the presence of noise. Input impedance is approximately 2K ohms.

Overload protection is incorporated into the input circuitry, and the instrument is thus able to accept signals up to approximately 100V peak-to-peak without damage.

Apart from the power supply wiring, all of the circuitry of the instrument is mounted on printed wiring boards. This simplifies the construction considerably, so that, despite its relative complexity, the instrument should be capable of being constructed rapidly, easily and with confidence even by those with little experience of equipment construction.

There are three wiring boards, the largest of which supports the complete counting section including decoding and readout display. A smaller board, mounted beneath the counter board, provides the mains-derived timebase frequencies, while the smallest board mounts behind the input connector and main front panel controls and supports the input shaping, gating logic and reset circuitry.

The logic/circuit diagram of the counter board is shown in figure 1. As may be seen, it includes some 17 microcircuits, three discrete transistors, three numerical indicator tubes, a neon lamp and a handful of minor components.

Input signal gating for the counter is performed on the counter board itself, by microcircuit IC2. As the counter gate must be capable of operation at the highest input frequency handled by the instrument, a high speed ECLtype device is used. The device is actually a Motorola MECL, type MC1004.

As the devices used on the input board to generate the gating signal are saturated-logic RTL devices, the actual gating signal fed to the counter board has the corresponding logic convention. Because of this a "logic level translator" is used to convert this signal into one compatible with the ECL gate device. The translation function is performed by one half of IC1, a Motorola type MC1017.

The first decade of the counter itself must also be capable of operating at the maximum input frequency handled by the instrument, and for this reason high-speed ECL devices are again used in this section. The decade consists of four Motorola type MC1013 flipflops, which have a rated maximum toggle frequency of 70MHz minimum. These devices are shown on figure 1 as ICs 3, 4, 5 and 6.

The second and third decades of the instrument handle somewhat lower maximum frequencies than the input decade, and for this reason these decades use devices of lower frequency capability. The devices which are used in this case are type CuL 9958, from

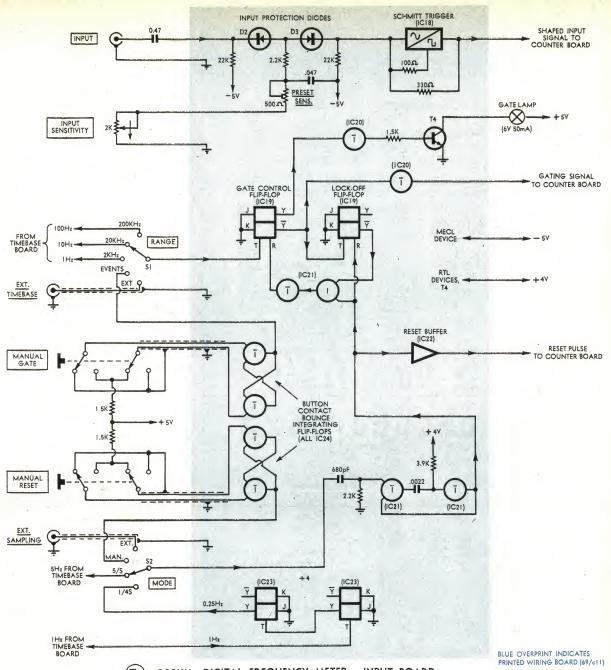


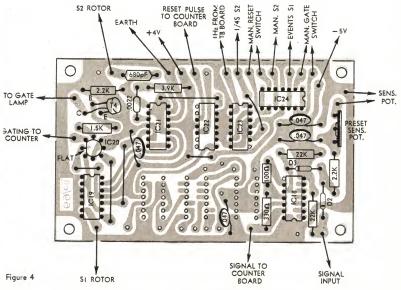
Figure 3

(EA) 200KHz DIGITAL FREQUENCY METER - INPUT BOARD

the Fairchild "Counting Micrologic" range. Each device is a complete decade counter (IC12, IC14), containing four flip-flops and associated feedback gating, and operating in 8421 BCD code.

The outputs of each of the three counting decades is decoded into decimal notation and prepared for application to the numerical readout tubes by devices IC11, IC13 and IC15. These are combined decoder/lamp driver devices type CuL9960, again from the Fairchild range.

As the decoder/lamp driver devices employ DTL circuitry, logic level translators must be used between IC11 and the ECL flip-flops of the first counting decade. The devices used in these positions (ICs 7, 8, 9, 10) are Motorola type MC1018, which are expressly designed for ECL/saturated logic translation. Device IC10 also acts as a level translator for the carry-over to the DTL device IC12.



The OS25 has set new standards for a low-cost, dual-trace oscilloscope. It is rugged, simple to operate and maintain and is attractively styled. Triggering facilities are unusually comprehensive for a low-cost instrument of this type and include internal triggering from either channel.

This oscilloscope has a vertical amplifier bandwidth from DC to 5 MHz with a maximum sensitivity of 100 mV/cm on each channel. The time base gives sweep speeds from 1 sec/cm to 0.5 μ S/cm using switched and fine controls. The operating mode best suited to the time base speed is automatically selected by the time base range switch; beam switching for the two slowest speeds and alternate sweep for the four highest speeds.

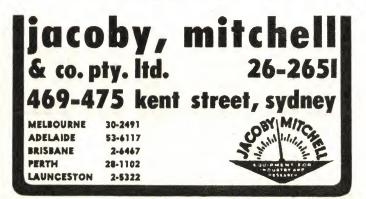
A bright clear display is obtained on a 5-inch helical PDA tube operating at a potential of 3 kV overall.

5 MHz Dual-Trace Oscilloscope OS25



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The numerical readout tubes used in the instrument are low-cost side-viewing types from the English "Hivac" range. Designated type XN3, they provide easily read numerals some 14mM high, and are intended for printed wiring board mounting. The tubes are available via trade suppliers from the Imported Components Division of Plessey Ducon Pty. Ltd.

Counter over-range is performed by one half of IC16, which is a Motorola type MC790P dual J-K flip-flop. Carryover from IC14 to the over-range flipflop is taken via an inverter transistor T1, which is necessary because although the DTL device IC14 and the RTL device IC16 both use similar logic levels, they employ opposite logic conventions.

Readout for the over-range is performed by a neon lamp, driven by transistor T3. The neon lamp used is a special type having long electrodes,

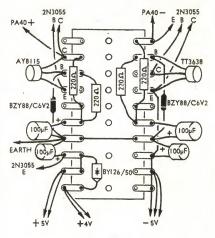


Figure 6

thus matching the numerals of the full decades. It is a Hivac type 23L, and is also available from Plessey Ducon Pty. Ltd.

Overflow detection is performed by the second flip-flop of IC16. The output of the flip-flop is fed via an inverter element to transistor T2, which drives the 6V/50mA panel indicator lamp. The inverter element is formed by half of IC17, which is a Fairchild type FuL914 dual gate.

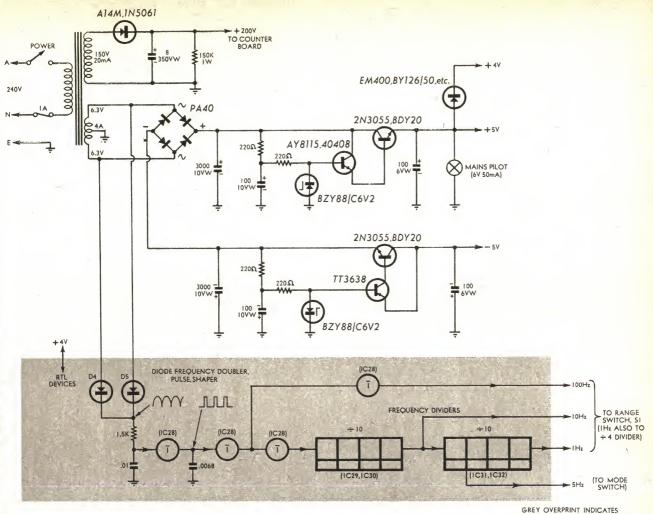
The second half of IC17 is used as a NAND or inhibitor gate which prevents the over-range neon from operating when the counter has overflowed. This has been done to avoid ambiguity and prevent reading errors.

As may be seen, reset signals are applied to all three counting decades and also to both the over-range and overflow flip-flops. As the reset signals fed to the counter board have saturated logic levels, a level translator is used to feed the ECL input decade devices. The translator uses the second half of IC1.

Figure 2 shows the component placement and additional wiring on the counter board. Assembly of this board should be a simple and straightforward operation if this diagram is used in conjunction with figure 1.

The logic/circuit diagram for the input board is shown in figure 3. In the present version of the counter design seven microcircuits are mounted on this board, together with

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Figure 5

one discrete transistor, two diodes and associated minor components.

Squaring of the input signal applied to the instrument is performed by IC18, a high speed ECL gate connected as a Schmitt trigger. The device used for IC18 is a Motorola MC1035, which is capable of operation in this configuration to well beyond 50MHz.

Adjustment of input sensitivity is performed by varying the DC bias applied to the input of IC18. This is done by means of the 2K input sensitivity pot, mounted in the front panel, with a small preset 500 ohm unit on the board used to set the maximum sensitivity position of the main control.

Input overload protection is performed by the two diodes connected in series with the signal path to IC18. Normally biased in forward conduction along with IC18, the diodes are arranged to disconnect the input for peak signal excursions greater than a few hundred millivolts in either direction. In effect, all signals greater than about 500mV P-P are clipped to this amplitude before passing to IC18.

Naturally if large enough signals are applied, the PIV rating of one or both of the diodes will be exceeded, and damage may occur. As the OA91 diodes used have a PIV rating of 115V, the risk of this occurring should be very slight in most applications; however, the operator would do well to bear the possibility in mind. Also on the input board is the counter gate control logic. This consists of two J-K flip-flop elements, an OR gate, three inverters and a discrete transistor. The two flip flops are provided by device IC19, which is a Motorola type MC790P. One half of the device is used as the gate control flipflop, whose toggle (T) input is fed with the selected timebase signal from the range switch (S1).

It is the Y-bar output of the gate control flip-flop which is actually used to control the counter gate, being taken to the gating input of the counter board via a buffer/inverter using half of IC20, a Fairchild FuL914 device. The Y output of the flip-flop is fed via the second half of IC20 to transistor T4, which is used to operate the gate indicator lamp on the front panel.

As the gate control flip-flop must only be allowed to open the counter gate for a single timebase signal period for each measurement, its operation is controlled by a lock-off signal applied to its DC reset terminal. The lock-off signal is provided by the second flipflop of IC19, which switches to the set state immediately the gate control flip-flop returns to the reset state after opening and closing the gate. The lockoff signal is applied to the reset input of the gate control flip-flop via an OR gate and inverter formed by two elements from IC21.

The purpose of the OR gate is to



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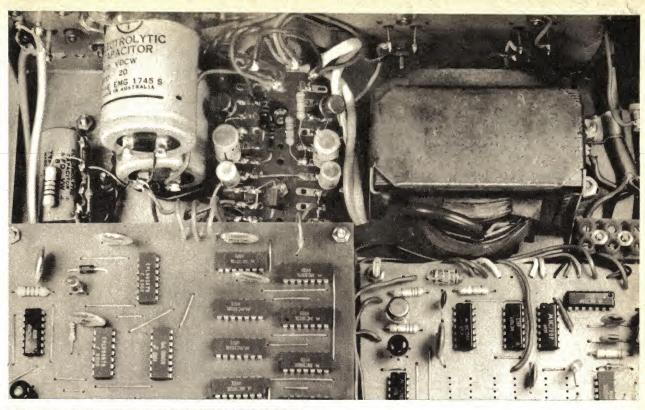
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Above is a view of the interior of the instrument, looking from overhead and towards the rear. Visible are the power supply components, and part of the counter and input boards. At left is a view of the rear of the case.

allow the gate control flip-flop to be reset, along with the lock-off flip-flop, by the normal instrument reset pulses. It is therefore the latter pulses which act as the "sampling command" pulses in the instrument; each reset pulse not only resets the elements of the counter, but also primes the gate control circuitry to allow a new measurement to be taken.

Shaping of the reset/sampling pulses is performed by the remaining two gates of IC21, which are connected in a monostable or "one-shot" configuration. The output from the monostable is fed directly to the gate control logic, and through a buffer amplifier (IC22) to the counter board. Device IC22 is a Motorola type MC788P dual noninverting buffer.

Selection of the reset/sampling signal source is performed by the mode switch S2. This selects one of four signals: (a) a 0.25Hz signal derived from the 1Hz timebase signal by the two flip-flops of IC23 (MC790P), giving a slow sampling rate; (b) a 5Hz signal taken from the timebase board, giving a faster sampling rate; (c) a "manual" signal generated by means of a front-panel "reset" button, with spurious bounce components removed by an integrating flip-flop using two elements of IC24 (MC724P); or (d) an external reset/sampling source.

The signal selected by S2 is differentiated before being fed to the monostable, to ensure correct operation regardless of the duration of the selected signal. Any signal having a pulse width greater than about 100nS is thus quite suitable for use as an external reset source.

The second front-panel pushbutton and the remaining elements of IC24 are used to generate manual gating signals for the "events" counting function.

The placement of components and interconnection wiring for the input board of the instrument is shown in figure 4, and again it should be a fairly simple matter to assemble and interconnect the board using this diagram in conjunction with the circuit/ logic diagram of figure 3. Note, however, that the board provides for integrated microcircuits and interconnections which are not used in this version of the instrument.

The remaining sections of the instrument to be described are the power supply and the mains-derived timebase. The circuit/logic diagram for these sections is shown in figure 5.

The power supply section of the instrument is fairly conventional. A simple half-wave rectifier circuit using a 150V/20mA transformer secondary winding is used to provide approximately 200V at low current for the readout display tubes, while a fullwave bridge rectifier circuit using a centre-tapped 12.6V/4A winding is used to provide supplies of +5V, +4V and -5V for the various microcircuits.

The low-voltage bridge rectifier is a single-package silicon unit, type PA40, by Electronic Devices Inc., of New York. It is available either directly or



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via trade suppliers from Watkin Wynne Pty. Ltd., who act on behalf of Australian General Electric Pty. Ltd., the importers. Watkin Wynne are also able to supply the transient-protected A14M diode used in the 200V supply.

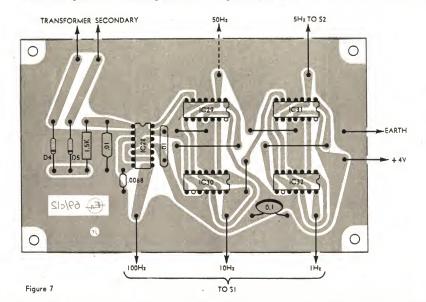
The reservoir capacitors for the lowvoltage supplies are bracket-mounted 3000uF units, this value being necessary because of the appreciable current drain. These and the other capacitors used in the prototype power supply were kindly supplied by Plessey Ducon Pty. Ltd. Readers may order similar units from this firm, through their usual trade supplier.

Both the positive and negative out-

The diodes are connected to the ends of the low-voltage transformer secondary in such a way that they perform full-wave rectification.

No reservoir capacitor is used at the output of the rectifier, the idea being that it is the 100Hz ripple component in the output which is shaped and used to produce the highest timebase signal. The small filtering components used are arranged only to attenuate higher order components, and to prevent malfunction due to mains transients.

Shaping of the 100Hz component from the rectifier is performed by the elements of IC28, which is an MC724 quadruple gate. Two of the elements



puts of the low voltage power supply are stabilised by means of simple series regulator circuits. The regulators are very similar, and use BZY88/C6V2 nominal 6.2V zener diodes in conjunction with BDY20/2N3055 series regulator transistors. The main difference between the two is that in the positive supply an AY8115 or 40408 device is used in conjunction with the main transistor in a Darlington or "superalpha" pair, for high current gain, whereas in the negative supply the reversed polarities require the use of a "complementary compound" configuration using a TT3638 PNP device.

whereas in the negative supply the reversed polarities require the use of a "complementary compound" configuration using a TT3638 PNP device. The -5V output from the supply is used for the ECL devices on the counting board, and for IC18 on the input board. The +5V supply is used for the DTL devices on the counting board, for the level translation ECL devices, and for the front panel pilot lamps. As the +5V supply would cause excessive dissipation if applied to the RTL devices, a simple series-diode system is used to derive approximately + 4V for these devices.

The power transformer used for the instrument is a rather special type, combining a low-current high voltage secondary with a high-current low voltage winding. The prototype transformer was kindly supplied by Ferguson Transformers Pty. Ltd., from whom similar units may be ordered via trade suppliers. The type number which has been assigned to the unit is PF 3144.

The mains-derived timebase system may be seen to be a simple one, using only five microcircuits, two diodes and three minor components. perform squaring, while the remaining two act as buffers. One of the latter provides the 100Hz timebase signal which passes to the range switch S1; the other provides the signal for the frequency divider elements used to derive the 10Hz, 5Hz and 1Hz timebase signals.

Each of the two divider decades used employs two MC790P dual J-K flip-flop devices, connected in the minimum-device configuration used in the author's Crystal Calibrator (September, 1969).

The main advantage of the mainsderived timebase system is economy, as noted earlier; only five microcircuits are involved, and no quartz crystal is required. The disadvantages are that the highest readily obtainable timebase frequency is 100Hz, limiting the selfcontained frequency range of the instrument, and that the short-term frequency stability of the power mains restricts measurement accuracy using the internal timebase signals to about 0.5—1 per cent.

0.3—1 per cent. For a low cost general-purpose LF instrument of the type involved here, these disadvantages are probably not great. However, for higher frequency measurements and for more critical applications, it is generally necessary to employ a more pretentious timebase system. For this reason the high frequency version of the design to be described in the third article uses a quartz crystal timebase divider system.

To assist constructors in wiring the power supply and timebase sections of the instrument, we have prepared wiring diagrams for the power supply resistor panel and the timebase board. These are shown in figures 6 and 7 respectively.

Physically the new instrument is housed in a simple low-cost metal case which is identical in style and external dimensions to that of our "10-Plus-10 Stereo Amplifier." The prototype case was kindly supplied by Heating Systems Pty. Ltd., who should be able to supply drilled and punched cases and front panels soon after this article appears. As may be seen from the photographs, the front of the

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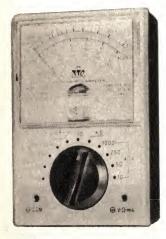
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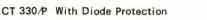


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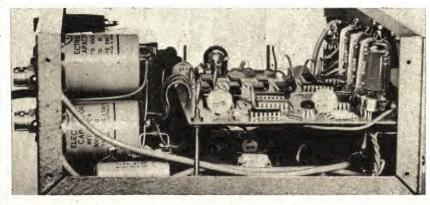
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instrument is fitted with an escutcheon plate having a rectangular window for the readout display. The window is provided with an optical filter made from orange-tinted "Perspex" sheet, the later being bolted to and behind the front panel proper by means of countersunk-head screws hidden behind the escutcheon.

Beneath the display window on the front panel are mounted the mains pilot, gate indicator and overflow lamps, and below these again the mains switch. manual gating button and

the power transformer, behind the range switch S1 and the sensitivity pot. The mains-derived timebase board is mounted alongside this board to the left, behind the mains switch, pushleft, benind the mains switch, push-buttons and mode switch S2. The counter board is mounted above the timebase board, supported by long screws in a position such that the numerals of the readout tubes are centrally placed behind the display window.

Construction of the instrument should present few problems even for of the instrument



A view taken from the left-hand side of the case, with the cover removed. The timebase board may be seen beneath the counter board.

manual reset button. Adjacent to these is the mode switch, S2.

The pilot lamps, mains switch and manual pushbuttons are all miniature types. The pilot lamps are Japanese "Sato" components, and may be ordered via trade suppliers from either I.R.H. Components Ltd. or the Imported Components Division of Plessey Ducon Pty, Ltd. The mains pilot has a green bezel, while the other two have red bezels.

The mains switch and pushbuttons are from the Japanese "NKK" range, and may also be ordered via trade suppliers from I.R.H. Components Limit-ed. The mains switch is coded type S-2012, while the buttons are coded type SB-2061.

To the right of the display window on the front panel are the range switch S1 and the sensitivity control, in that order. Mounted centrally between these controls is the input connector, completing the front panel fittings.

Mounted on the exterior of the case rear are the mains cord entry and the power fuse-holder, the two power supply regulator transistors (insulated by mica washers), and at the far right the two connectors for external timebase and external sampling input. The silicon rectifier bridge and 3000uF reservoir capacitors are mounted on the rear of the case also, but are inside.

The power transformer is mounted near the rear of the case, adjacent to the regulator transistors. Between the transformer and the reservoir capaci-tors is a 10-lug section of miniature resistor panel, and this is used to support the minor components of the low voltage power supply. The few components of the high voltage supply are mounted on a 4-lug tagstrip on the, other side of the reservoir capacitors, near the rear-panel connectors.

The input circuitry wiring board is mounted immediately to the front of

the relatively inexperienced construc-tor. The component placement on the printed wiring boards is shown in the diagrams, as are also the board inter-connections and most of the "hand" wiring. However, there are a few minor points regarding which it may be worthwhile to present the following brief comments.

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While preparing the present DFM article for publication, the author has been carrying out further de-velopment on the high frequency version of the design. As a result of this further development, the fre-quency range of the HF version has been almost doubled. When this version is described shortly, therefore, sion is described shorty, interior, it will be presented not as the 40MHz instrument predicted earlier, but as an instrument capable of making reliable measurements to beyond 70MHz.

A soldering iron having a small, well-tinned bit is recommended for making the soldered joints to the print-ed wiring boards, as this will allow the joints the med with well sold with the joints to be made without risk of bridging between conductors. The joints should be made rapildy, particularly those involving microcircuits and other semiconductor components, to prevent damage due to overheating.

The flying leads of the numerical indicator tubes and over-range neon should be bent very carefully to line up with the holes in the counter board, to prevent strain on the glass envelope.

Note that the correct orientation for the 14-pin and 16-pin microcircuits is shown in the wiring diagrams by a small hemispherical indentation on the device symbol. It will be found that each device has a similar indentation

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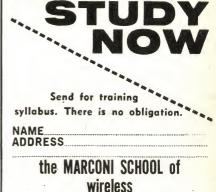
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MC01/FP

- FREQUENCY METER PARTS LIST -

COUNTER BOARD

SEMICONDUCTORS

- ICI: Motorola MC1017. IC2: Motorola MC1004.

- IC2: Motorola MC1004. IC3, 4, 5, 6: MC1013. IC7, 8, 9, 10: MC1018. IC11, 13, 15: Fairchild CuL9960. IC12, 14: Fairchild CuL9958. IC16: Motorola MC790P. IC17: Fairchild FuL914.

- 2N3565, BC108, TT3565. **T1**: or TT108.

- T2: 2N3569, or TT3569. T3: 2N3568, SE7001, or BSX21. Diode D1: EM401, BY126/50, etc. **REMAINING COMPONENTS**
- Printed board, code 69/d10.
- 3 XN3 numerical indicator tubes. 23L long-electrode neon tube.
- 1.5K 1 watt resistors. 4

- 3 47K ½ watt resistors. 1 220K ½ watt resistor. 9 0.1uF 25V ceramic capacitors.

INPUT BOARD

SEMICONDUCTORS

- IC18: Motorola MC1035.
- IC19, IC23: Motorola MC790P.
- 1C20: Fairchild FuL914.
- IC21, IC24: Motorola MC724P. IC22: Motorola MC788P.
- T4: 2N3569, or TT3569.
- Diodes D2, D3: OA91 or similar. REMAINING COMPONENTS
- Printed board, code 69/c11.
- 100 ohm $\frac{1}{2}$ watt resistor. 330 ohm $\frac{1}{2}$ watt resistor.
- 1.5K ½ watt resistor. 2.2K ½ watt resistors. 2
- 3.9K 1 watt resistor.
- 2 22K 1 watt resistors.
- 500 ohm tab pot (board mount-1 ing).
- 680pF polystyrene capacitor. .0022uF 30V mylar, polyester or
- polystyrene. 5 .047uF 25V ceramic capacitors.

TIMEBASE BOARD

SEMICONDUCTORS

1C28: Motorola MC724P. 1C29, 1C30, 1C31, 1C32: Motorola MC790P.

- Diodes D4, D5: OA91 or similar.
- REMAINING COMPONENTS
- Printed board, 69/c12.
- 1 1.5K ½ watt resistor.

at one end of the package. The round 8-pin devices have a flat or coloured line whose orientation is indicated in the diagrams.

Note also that there are two reset signal inputs to the counter board, the two being joined by a long link of insulated hookup wire.

The mains cord should be securely clamped to the case floor, after entry via a suitably grommetted hole, using a "C" clamp. This will prevent strain on the connections. The connections themselves are best made using a 3-segment length of "B-B" connector strip, which may be mounted to the right of the power transformer.

Signal interconnections between the various boards should be made in standard insulated hookup wire, and arranged to be as short and as direct

- 1 .0068uF polystyrene capacitor. 1 .01uF 30V mylar, polyester or polystyrene.
- 2 0.1uF 25V ceramic capacitor.

CASE & POWER SUPPLY

- 1 Case 101 in x 81 in x 4in, with front escutcheon plate.

- Power transformer, 240V to 12.6V CT at 4A, 150V at 20mA.
 Rotary switch, 1 pole 5 positions.
 Rotary switch, 1 pole 4 positions.
 Mains fuseholder with IA cart-video
 - ridge.
- 3 Co-axial panel connectors. 3 Miniature 6V/50mA lamp bezels (see text).
- 2 Miniature pushbuttons (see text). 1 Miniature SPDT toggle switch (see text).

SEMICONDUCTORS

- 1 A14M, 1N5061 or similar silicon diode.
- 1 EM400. BY126/50 or similar
- silicon diode. PA40 silicon bridge rectifier (8A). Nominal 6.2V zener BZY88/C6V2 or similar. diodes,
- 2 2N3055, BDY20 or similar NPN
- power transistors. 1 AY8115, 40408 or similar NPN
- power transistor. TT3638 or similar PNP power 1 transistor.

RESISTORS

- 4 220 ohm ½ watt.
- 2 1.5K 1 watt. 1 150K 1 watt.
- 1 2K linear carbon pot.
 - CAPACITORS

- 0.47uF 400V polyester.
 8uF 250VW electro.
 100uF 6VW electro.
 100uF 10VW electro.
 3000uF 10VW chassis mounting electro.

MISCELLANEOUS

2 large instrument knobs, 1 small knob; 10-lug section of miniature resistor panel; 4-lug tagstrip; 3-seg-ment length of "B-B" connector panel; 44in x 14in piece of orange tinted acrylic sheet (1/8in) for dis-play window filter; grommet for mains cord (3/8in); mains cord and plug; cord clamp; mounting screws. nuts, lock washers, power transistor hardware, mounting connecting wire, solder, etc.

as possible. Shielded leads need only be used for the connections to the two rear-panel connectors.

And finally, take care when mounting the two power supply regulator transistors to ensure that the device cases are properly insulated electrically from the instrument case. Use the standard mica insulating washers, with a smear of silicone grease on each side for thermal continuity, and fit the usual fibre or plastic sleeves to the mounting bolts. It is a wise precaution to check the insulation with an ohm-meter when the device is mounted, to prevent possible damage when power is applied.

There is only one adjustment to be made upon completion of the counter, after which it should be ready for immediate use. The adjustment

(Continued on page 174)



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PIONEER - FOR PURE SOUND

A shunt-regulated power supply

In January, 1969, we described a small variable power supply which was economical and burnout-proof. In this article, we describe a modified version featuring a high degree of regulation and low ripple output, yet economical to build.

By LEO SIMPSON

This power supply offers a degree of performance intermediate between that of the simple supply mentioned above and the high performance, 0-30V sup-ply described in September, 1968. It is easy to build and, as mentioned above, is proof against all normal abuse, making it suitable not only for "one-off" construction by the experimenter or servicemen but also for multiple construction for use in teaching institu-tions and development laboratories.

The performance of the unit is as follows: Output voltage is adjustable form 3V to over 20V; available load current at 3V is around 900mA, dropping to about 150mA at 20V. The output is highly regulated up to the point where current limiting occurs; in the middle of the voltage range it is better than 1 per cent for currents in excess of 500mA. Output ripple and noise is low, ranging from 20 to 40mV peak-to-peak, depending on load cur-rent and voltage setting. The accom-panying diagram shows the performance which can be expected at the different voltage settings.

While the circuit diagram of the sup-ply shows a total of five transistors, the operation of the unit is quite simple. The heart of the circuit is an active voltage divider circuit consisting of two 6.8 ohm resistors in series and a shunt element, a Darlington pair con-sisting of transistors T4 and T5.

The voltage divider is, in fact, a shunt regulator circuit. Reference to figure I will clarify the explanation. Notice that, whereas with conventional series regulator circuits the adjustable element is in series with the load, in the case of shunt regulator circuits and adjustable element is in parallel with the load.

The adjustable element can be likened to a zener diode with an adjustable breakdown voltage. The "zener diode" begins to conduct when the supply voltage rises above a certain point and in so doing, effectively limits any further voltage rise to a few per cent. The breakdown effect will not cause any damage provided the internal power dissipation is kept within limits. The series resistance limits the current drain so that over-dissipation in the shunt element and other power supply com-ponents is prevented.

For those readers not familiar with the operation of a Darlington pair ref-erence to figure 2 will help. The two transistors are interconnected as shown and can be treated as a three-terminal "black box" which operates as a single composite transistor. The current gain of this composite transistor is approxi-

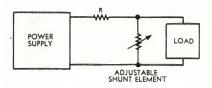


Figure 1: Illustrating the principle of an adjustable shunt-regulated power supply.

Figure 1

mately equal to the product of the cur-rent gains of the individual transistors. The effective "breakdown" voltage of the Darlington pair shunt element is determined by the bias voltage on the input, i.e., the base of the Darlington pair.

A major advantage of the shunt regulator configuration is that the regulating element, in this case the Darlington pair, is protected from damage due to short-circuit loads.

Because the output terminals are connected across the Darlington pair (disregard the diode for the moment) any load connected to the terminals is effectively in parallel with the Darlington pair (the adjustable shunt element) as is shown in figure 1. The current drawn by the load, therefore, is sub-tracted from that which is otherwise drawn by the Darlington pair, to main-tain a given output voltage. Thus, the greater the load current the less the dissipation in the shunt regulator element. If the output terminals are shortcircuited, the shunt regulating element is effectively removed from the circuit. The rectifier is then presented with the heavy but not unduly embarrassing load consisting of the series divider resistors.

It should be appreciated that the



in contrast with that of the more usual circuit, in which the transistor is con-nected as the series divider element. In such circuits the transistor dissipation rises with load current, and special precautions must be taken if the transistor is not to be ruined by excessive current on short-circuit.

One disadvantage of the shunt regu-lated supply is that, for a given voltage setting, the power consumption will be more or less constant, regardless of whether a load is connected to the external circuit or not. This means that these supplies tend to be wasteful of power when lightly loaded. For small supplies such as this one, however, this is of no consequence.

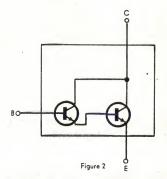


Figure 2: The Darlington pair configuration, in which two transistors operate as a single, composite transistor.

Although the shunt element is pro-tected by the basic circuit basic circuit configuration against over-dissipation due to excessive loading, it is also desirable to protect it against voltages generated externally. The situation can arise where two supplies are used in series, and, if a connection is made in error, damage can occur. For this reason we have connected a diode in series with the output to prevent any current flowing back into the supply. The diode will also protect the supply against positive voltage spikes generated by inductive loads.

As stated above, the "Darlington pair" is the shunt element. It will have foregoing state of affairs is somewhat an effective current gain, Beta, ap-



proximately equal to the product of the individual Betas of T4 and T5, i.e., a minimum of 800. Further current gain is provided by the PNP silicon transistor, T3. The very large overall current gain is necessary to keep loading of the "error" amplifier, T2, to a minimum and hence obtain the maximum voltage gain.

The error amplifier consists of a low leakage NPN silicon transistor with its base voltage provided by a voltage divider connected across the output terminals (the 5K potentiometer) and with a fixed reference voltage at the emitter. If the error amplifier's base voltage is slightly higher than the reference voltage it will conduct and cause T3, T4 and T5 to conduct, thus lowering the output voltage. As soon as the base voltage of the error amplifier drops slightly it will tend to turn off, causing T3, T4 and T5 to turn off, and allowing the output voltage to increase slightly. Thus the error amplifier maintains the output voltage very close to the desired setting.

Notice that the error amplifier operates in reverse fashion to what would normally be the case in a series-regulated supply. Moving the wiper of the potentiometer towards the negative end will turn the Darlington pair off and raise output voltage. Moving the wiper to the positive end will cause the Darlington pair to conduct heavily and lower the output voltage.

The degree of regulation available from any supply is in direct proportion to the regulation of the internal reference voltage source. Similarly, the ripple output from a supply is dependent on how smooth and ripple-free the reference voltage is. Hence, for good performance, the reference voltage must be very well regulated and almost completely ripple free. At this point, one of the inherent advantages of the shuntregulated supply comes to light.

In a high quality series-regulated supply, the reference voltage is often supplied from a separate winding on the power transformer because of the fluctuating load on the main winding With a shunt regulator, however, the loading on the transformer is constant for a given voltage setting and a separate winding to provide the reference voltage is unnecessary.

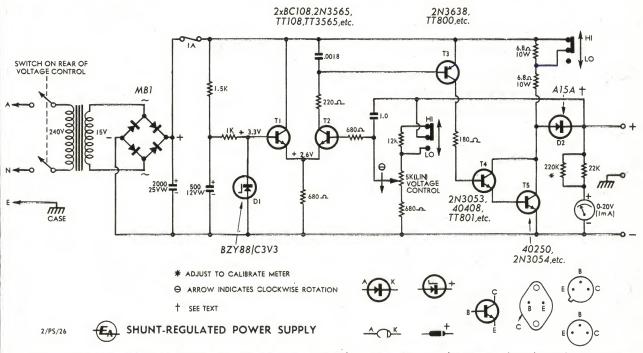
Because of the configuration of the circuit, the minimum supply voltage obtainable will be slightly more than the reference voltage. Thus, if we wish to turn the supply to nearly zero the reference voltage must be very low. The lowest available zener diode has a breakdown voltage of 3.3 volts (nominal). For this reason, we have arranged T1 in an "emitter-follower" configuration to provide a nominal reference voltage of 2.6 volts at the emitter of T2. This allows the supply to be set to 3 volts; a useful value for low voltage integrated circuits.

The purpose of the 1800pF capacitor connected from emitter to base of T3 is to prevent oscillation of the supply at high frequencies. The combination of the very high loop gain of the power supply and the phase rotation caused by the 1uF capacitor can result in oscillation at the slightest provocation. Readers might suppose that a capacitor from base to collector would achieve the same result, and this is true. However, the arrangement we have used also results in lower ripple output and is equally satisfactory in other respects.

The value of the voltage divider series element necessary to prevent excessive dissipation in the transformer, bridge rectifier and associated filter capacitor under conditions of maximum current drain (corresponds to the minimum voltage setting) is approximately 14 ohms, provided by two 6.8 ohm 10 watt resistors. However, because this value tends to unduly limit the current available from the supply at higher voltage settings, provision has been made to halve this element in value when required by means of a slide



A view of the layout inside the case. The tagboard adjacent to the transformer accommodates the recifier, 2000uF capacitor and two 6.8 ohm resistors.



The circuit diagram of the Shunt-regulated Power Supply. Note that, in the event of a short-circuit across the output, no damage apart from a blown fuse can result, since the regulating element consisting of the Darlington pair is effectively connected in parallel with the load.

switch which shorts out one resistor. The slide switch simultaneously inserts a 12K resistor in series with the potentiometer so that the output volt-age cannot be set lower than 10 volts, thus ensuring that the internal dissipation of the supply is limited.

Externally, the effect of the slide switch is to provide a second ("HI") range in which additional current is available, but only for the range of voltages between 10 and 20 volts.

As with the normal or "LO" range, an output short-circuit on the "HI" range effectively removes the Darlington pair from the circuit. However, the current load on the bridge rectifier and transformer is around 1.6 amps which will cause damage if the short is maintained for sufficient time. For this reason we have provided a 1 amp fuse to protect the transformer and bridge rectifier against overheating. The fuse will probably not "blow" if a short cir-cuit is applied on the "LO" range as the current is limited to 1 amp.

An output voltmeter is provided, to permit convenient adjustment and monitoring of supply output during operation. The meter used in the pro-totype is an economy 3-inch rectangular type of Japanese manufacture, des-ignated type VP-2A and having a stan-dard 0-1mA/100 ohms characteristic. We removed the original 0-1 scale markings with a typewriter eraser and replaced them with an appropriate 0.20V sumbering 0-20V numbering.

Neither side of the basic supply is internally connected to the case or mains earth, but rather, a third "earth" output terminal is provided to permit either

output polarity to be tied to earth if and when required. This approach offers complete flexibility, at no sac-rifice in performance and at an additional cost of only a few cents.

As may be seen from the photo-As may be seen from the photo-graphs, the supply is constructed in a sloping front case which is convenient for bench-top operation. The case was originally designed for the economy supply published in January, 1969. It measures 5in x 5in x 5in and has a

PARTS LIST

- 1 Sloping Front Case, 5 x 5 x 5in, to suit economy power supply described in January, 1969.
- Power transformer, 15V at 1 amp DC (A&R 2155 or equivalent).
- 3in rectangular meter, 0-1mA/ 100 ohms.
- DPDT slider switch. 5K (lin.) potentiometer with switch.
- 16-lug section of miniature resistor panel. 11-lug section of minature re-
- sistor panel.
- screw terminals red, green. black.
- 1 1-amp cartridge fuse and holder. **SEMICONDUCTORS**
- 1 40250, 2N3054, NPN silicon power transistor.
- 40408, 2N3053, TT801 silicon NPN transistor.
- 2N3638, **TT800** silicon PNP
- transistor. 2N3565 2108 2N3565 2 BC108. silicon NPN transistors.

wrap-over front panel. The case and printed front panel of the prototype was made by Heating Systems Pty. Ltd. and most kit suppliers would have similar cases already in stock.

The output voltmeter is mounted at the top of the sloping case panel, with the output potentiometer beneath it and the fuse and range switch mounted to the left and right of the latter, respectively. The three output terminals are mounted at the lower front of the case,

1 MB1 silicon bridge rectifier (or 4 1-amp diodes). BZY88/C3V3 zener diode.

- 1 A15A or equivalent high-current diode.

RESISTORS

(1-watt unless specified.) x 220K, 1 x 22K, 1 x 12K, 1 x 1.5K, 1 x 1K, 3 x 680 ohms, 1 x 220 ohms, 1 x 180 ohms, 2 x 6.8 ohms/10 watt.

CAPACITORS

(higher voltage ratings may be used) 1 2000uF/25VW electrolytic. 1 500uF/12VW electrolytic. 1 1uF/100VW polyester or metal-

- lised polyester.
- 1800pF polyester or polystyrene 1 (low voltage).

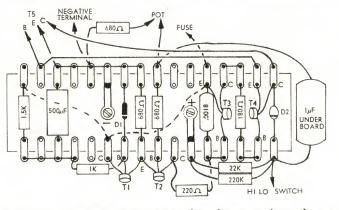
SUNDRIES

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with the earth terminal in the centre to allow convenient linking of either output terminal when required.

The power transistor is mounted on the outside of the upper rear of the case. Although the transistor body is connected internally to the collector and must therefore be isolated electrically from the earthed case, for efficient cooling of the device the two must be closely coupled thermally so that the case can act as a heatsink. To achieve this the lacquer finish of the case is removed from the area immediately beneath the transistor, and the mica insulating washer supplied with The power transformer used in the prototype was made by A. and R., type 2155. Any similar power transformer with a 15V secondary at 1 amp DC will be quite suitable. The transformer is mounted with the primary winding lugs nearest to the cord entry, so that the mains wiring is kept as far as possible from the low voltage circuitry. The mains cord enters via a grommetted hole in the rear of the case, then between the transformer stack and side of the case and finally terminated at the switch/pot. It is anchored by a clamp, which is held by the same screw which retains one of the transformer lugs and



The layout of components on the tagboard mounted on the rear of the meter movement. Note that the 1uF capacitor is actually underneath the tagboard. Compare with photo on page 79.

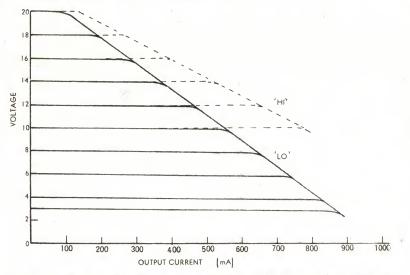


Diagram showing the degree of regulation to be expected at different voltage settings. Ripple and noise output will range from 20 to 40mV peak-to-peak, depending on the load and voltage setting.

the device is coated with the usual silicone grease.

If 40250 or 2N3054 transistors are not easily obtainable at the time you wish to build this unit the much higher rated (though only slightly more expensive) type 2N3055/BDY20 may be substituted, although it requires different mounting holes. At the time of writing, both 2N3054 and 2N3055 transistors are in good supply.

Although the interior of the case is quite small, it is not unduly crowded with the layout we have employed. We recommend that the layout shown in the wiring diagram and accompanying photograph be followed closely to make construction as straightforward as possible. a solder lug to terminate the mains cord earth. The earth wire is also connected to the front panel earth terminal.

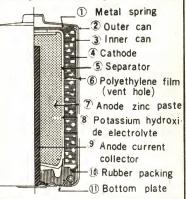
The bridge rectifier we used was silicon type, MB1, made by ITT. However, it may be more economical to use four individual 1 amp diodes and these can easily be accommodated. The voltage rating is not critical — any of the currently available 1 amp silicon diodes has sufficient voltage rating.

The bridge rectifier, 2000uF electrolytic capacitor and the two 6.8 ohm/10 watt resistors are accommodated on an 11-tag section of miniature resistor panel. It is important that the resistors are kept as far away

(Continued on page 171)



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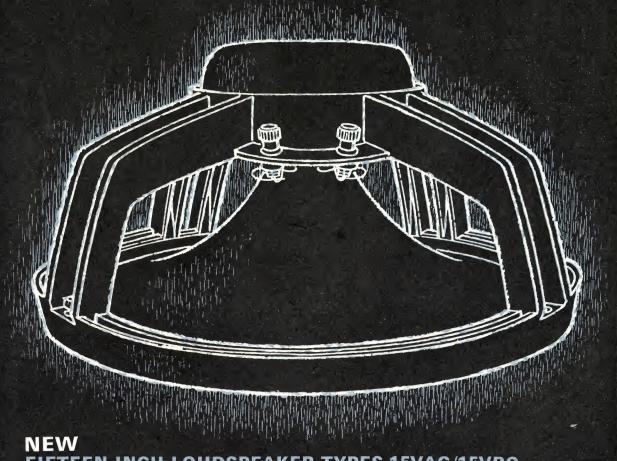
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In this article for our younger readers we present a series of amplifier circuits and answer some of the questions which arise out of the design of such circuits.

By Leo Simpson

Many of our novice readers have written to us over the past years asking for simple transistor amplifier circuits, for simple transistor ampliher circuits, preferably using particular transistors that they had in their possession. These requests have generally been hard to fulfil as the transistor types mentioned have often differed from those in our simple amplifier designs. As much as we would like to assist, we are not in the position to design circuits for indithe position to design circuits for individual readers.

Recently, however, we reviewed the situation and decided that one way in which we could help would be to present an article showing readers how to construct simple amplifiers using general-purpose transistors. The article could at the same time show readers the basic principles to be followed in order to achieve the best performance from typical oddment transistors. This is, in fact, that article.

Possibly, the first point to be considered when visualising a versatile am-plifier circuit is the DC supply voltage. This must be selected so that the various voltage, current and wattage rat-ings of all components will not be exthe same time are the value of the external load on the output transistor (loudspeaker or phones, etc.) and the required power output.

We decided upon 6 volts as the most useful "all-purpose" supply voltage for the following reasons:

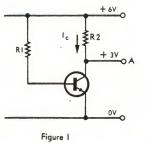
Firstly, it is low enough so that all transistors likely to be used will be operating within their voltage ratings. Secondly, it provides a reasonable

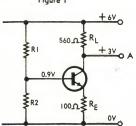
voltage swing across the load (reasonable power output) without an excessive IR drop (wattage) across the semiconductors; if we had decided upon 3 volts, for example, the usual 1-volt "saturation" voltage (minimum voltage drop) across most silicon transistors would leave only 2 volts peak-to-peak as the maximum obtainable signal across the load, resulting in very limit-

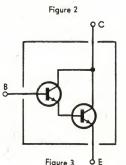
ed power output. Thirdly, and perhaps most im-portantly from the schoolboy experimenter's view, 6 volts can be ob-tained readily from two 3-volt cycle batteries, and these can be relied upon to last quite a long time.

In the case of the first four circuits to be discussed, the output load is intended to be headphones, of either the 2,000-ohm magnetic variety of the high impedance crystal types. We decided upon this because many of the requests for simple circuits have mentioned that headphones were to be used. Methods of connecting low impedance (typicallv 8-ohm) earphones will be discussed later in the article.

Having decided upon the supply volt-









age and external load for an amplifier stage, the next consideration is the zero signal current; this is dependent on the collector resistor, in the case of the circollector resistor, in the case of the cir-cuits discussed here, and on the bias-ing. Having selected a given value of collector load resistor, the bias must be set so as to obtain the maximum output voltage "swing" before clipping the signal waveform. Engineers like to call this composite voltage-current-bias setting the "DC working point."

Referring now to figure 1, let us consider one method of setting the bias and consequently the zero signal current, which is commonly encountered in beginners' circuits. In this case, the bias must be set so that the voltage at point A is equal to half the supply voltage, this condition giving the maximum output voltage excursion, or "swing."

Plainly enough, the voltage at point A will be dependent on the collector current flowing through the load resistor R2. In turn, the collector current will be equal to the product of the base current (flowing through R1) and the current gain, or Beta, of the transistor. (Beta is approximately equal to the ratio of collector current to base current). By varying R1 and thus the base cur-rent, the DC voltage at point A can be set. The transistor is then said to be "current biased."

While superficially a simple system, while superficially a simple system, current biasing has certain serious dis-advantages. The first is that no two transistors will have exactly the same Beta and so the DC working point has to be set up for each individual transistor. A second disadvantage is that the Beta efforts transition that the Beta of many transistors tends to vary with temperature. This means that a DC working point set on a cold day (by current biasing) would be off the mark on a hot day or after the transistor had generated its own internal heat.

The third and most serious dis-advantage of all is that with this bias-ing system transistors will amplify their own collector-base leakage current and this (leakage) is very dependent on temperature. Some improvement in the sta-bility of the DC working point can be obtained by using an emitter resistor but, in general, methods other than current biasing are to be preferred.

The most common method of biasing an amplifier stage is shown in figure 2. The two major features of the circuit are that there is a voltage divider which are that there is a voltage divider which holds the base to a fixed voltage (in-stead of letting it "float" as in figure 1) and an emitter resistor, incorporated to improve temperature stability. This emitter resistor ideally should be as high in value as possible to obtain the best stability, but in practice it should not be made so high that there is exnot be made so high that there is excessive voltage drop — and consequent power loss — across it. Generally, 0.5 volt is a suitable figure across the emitter resistor.

Now, for transistors which have a reasonably high Beta for all tempera-tures likely to be experienced, the col-lector current may be considered to be equal to the emitter current. Since we have selected 560 ohms as a suitable value of collector resistor and the desired voltage at point A is 3 volts, the collector current will be approximately 5 milliamps, therefore the emitter re-sistor can appropriately be 100 ohms. In fact, the desired collector current is obtained by setting the DC voltage drop across the emitter resistor and this is done, in turn, by setting the base voltage.

For collector current to flow the transistor must be forward biased. In general, a forward-biased semiconductor junction has a voltage drop across it which is fairly constant for current variations of two or three to one. For silicon transistors this voltage will be approximately 0.6V and for ger-manium types it will be approximately 0.25V. An average figure applicable to all transistors is 0.4V. Thus, to bias the transistor correctly, we would ar-range for the base voltage to be 0.4V above the emitter voltage. Hence, the voltage divider consisting of R1 and R2 is selected to give a base voltage of 0.9V.

The values of the voltage divider resistors are selected so that variations in



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(A unit of Jacoby Mitchell Holdings Ltd.) 376 EASTERN VALLEY WAY, ROSEVILLE, 2069 . Cables and Telegraphic Address: 'WESTELEC,' Sydney. Phone: 40 1212 the base current of the transistor will have little effect on the base voltage. Note that the effects of leakage current also have to be taken into account. In this respect germanium transistors are worse, as they have much higher leakage currents than silicon devices. In taking these facts into account, it is customary to arrange that the voltage divider resistors pass a current roughly 10 times that of the base bias current, in the case of germanium transistors. Somewhat lower current values can be used in conjunction with silicon transistors.

Thus, in figure 2, if the transistor had a Beta of 40 and the collector current was 5 milliamps, the base bias current would be 125 microamps. Thus, 1 milliamp would be a suitable current for the voltage divider resistors. Using Ohm's law, R2 would equal 1K and R1 would equal 5.6K to give a base voltage of 0.9V and a current slightly less than 1 milliamp through the resistors. Note that any error occurring due to our assumption of 0.4V as being the forward voltage drop for a semiconductor junction will generally be "swamped" by the error in selection of resistors from the 10 per cent preferred value range.

One can check the accuracy of the resistor selection by measuring the voltage at point A. If necessary, it can be adjusted by varying one or other of the resistors in the voltage divider.

resistors in the voltage divider. We have seen that the method of biasing shown in figure 2 provides a DC working point which is relatively free from the effects of temperature and which does not have to be varied to suit individual transistors. Thus, we have a circuit with predictable characteristics, but one which has the disadvantages of slightly higher current drain (through the voltage divider resistors) and lower input impedance than the circuit shown in figure 1 which is current biased.

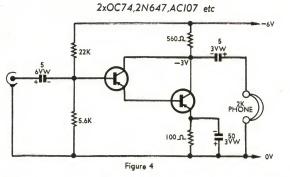
Note that, in the case of figure 2 we have shown an NPN transistor. All the above calculations can be applied to circuits using PNP transistors, but the polarities of all voltages in the circuits must be reversed.

Figure 3 illustrates a more complex configuration known as a Darlington pair configuration, in which two transistors (both either PNP or NPN) are interconnected as shown. They operate effectively as one composite transistor with a Beta equal to the product of the Betas of the two individual transistors. It is important to grasp this concept of the two transistors acting as one with a very high Beta.

An advantage of the Darlington pair configuration is that it offers, in a simple circuit, higher gain than could be obtained from two separate, capacitively coupled transistor stages of the type shown in figure 2. Another advantage is that it enables a higher input impedance to be obtained, especially when the output load is placed in the emitter circuit.

Figure 4 shows a practical amplifier using a Darlington pair configuration. Any general-purpose germanium PNP transistors, excepting high power types, can be pressed into service. Note that the Darlington pair is biased in the way shown in figure 2 (voltage divider) except that the voltage drop from the base to the emitter of the composite transistor is 0.8 volts instead of 0.4 volts since it has two forward biased

Typical "oddment" circuits



base-emitter junctions. Note that we have been deliberately conservative in specifying relatively low values for the voltage divider resistors, in spite of the fact that the bias current will be very small. This is to allow for the effects of high leakage current in possibly old, oddment germanium transistors. Much higher values could be specified if low leakage silicon transistors were to be used.

The 100-ohm emitter resistor is "bypassed" with a 50uF electrolytic capacitor to eliminate gain reduction due to emitter degeneration. If the emitter resistor is not shunted with a capacitor, the output signal voltage due to fluctuating collector current appearing at the collector of the Darlington pair, will appear with reduced amplitude across the emitter resistor. This, in turn, will counteract the signal input voltage appearing between base and emitter and thus cause a reduction in voltage gain. By connecting a capacitor across the resistor, as shown, the signal voltage appearing across the resistor is minimised and gain reduction avoided.

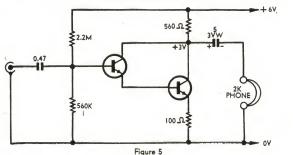
The value of the bypass capacitor

emitter degeneration to provide a high input impedance. Input impedance is approximately 500K and the typical voltage gain will be 5 times, regardless of the Betas of the particular transistors used. The emitter resistor may be bypassed to obtain a substantial increase in voltage gain but this will reduce the input impedance to approximately 50K.

Figure 6 is a direct-coupled "complementary" configuration using a PNP and an NPN transistor; the latter can be either germanium or silicon. Note that the biasing arrangement is essentially an extension of the method shown in figure 2. The voltage divider at the input determines the current flow through the first transistor and thus the voltage at its collector. This collector voltage then determines the current flow through the second transistor and hence the voltage at its collector.

The voltage gain can be varied by the negative feedback which is controlled by the size of the 100-ohm resistor. With the 100-ohm resistor in circuit the gain will be approximately 16 times. Reducing the resistor to zero will

2xBC108,2N3565,etc



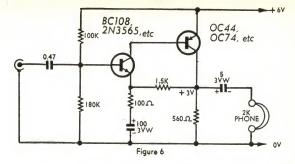
selected must be such that its impedance is low for the lowest signal frequency to be handled. The circuit in figure 4 has an input

The circuit in figure 4 has an input impedance of something less than 5K. Current drain is 5mA and the typical voltage gain to be expected is at least 40 with general-purpose germanium transistors. The gain can be reduced to a value of approximately 5 by omitting the bypass capacitor.

The circuit in figure 5 is basically similar to figure 4, except that we have specified silicon transistors, which, as we have already mentioned, can be expected to have a much lower leakage than germanium types. PNP transistors may be used merely by reversing the polarity of the supply voltage and the electrolytic output coupling capacitor. Note that we have not bypassed the emitter resistor. This is to make use of eliminate the negative feedback and maximum gain will result. This will typically be 125 times for the transistors we have specified. By manipulating negative feedback one can thus design for a desired order of gain.

Figure 7 is another direct coupled configuration. Here, the circuit uses DC feedback to the base of T1 to establish the DC working point. In this case the gain can be varied by the setting of the potentiometer, which isolates the 100uF capacitor to a greater or lesser extent from the 680-ohm emitter resistor. An equivalent effect can be be obtained by replacing the potentiometer with fixed resistors which add up to 10K but provide a suitable fixed tapping point.

All the above circuits are suitable for use with 2000-ohm dynamic headphones or the high impedance crystal



type. Low impedance types, such as the 8-ohm variety supplied with transistor radios cannot be used directly, because the output impedance of the amplifier stages we have described is too high.

The circuits can be used with low impedance phones if a suitable step-down transformer is coupled to the output, via the 5uF electrolytic capacitor. The transformer could be almost any type





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— a 6.3V heater transformer would be almost ideal. The 240V winding would be connected to the output of the amplifier while the phones are connected across the low voltage winding.

None of the amplifiers so far discussed has sufficient power output for use with loudspeakers. The circuit in figure 8 represents a novel and economical way of obtaining sound from a loudspeaker. It has one major drawback — DC flows through the loudspeaker voice coil. Normally, loudspeakers should not have DC flowing through them, as the current causes a fixed deflection in one direction and thus restricts the cone excursion in one direction more than the other; this could result in distortion on loud signals. If one is prepared to risk some deterioration in quality, the arrangement is a handy one to keep in mind.

The circuit is again a Darlington pair configuration. T2 should be a power transistor. The current flowing through the loudspeaker should be kept to a minimum consistent with power output, otherwise the cone excursion will be excessive and the power dissipation in the voice coil may cause an undesirable temperature rise. For these reasons and considering the battery drain, the impedance of the loudspeaker should not be less than 15 ohms and the drop across the loudspeaker should not be more than 3 volts. If higher impedance types are on hand they may be used provided the DC working point is ad-justed to 3 volts, as shown, to ensure adequate signal excursion. The voltage at the collector can be adjusted upwards by decreasing the 1K resistor, and vice versa.

Note that the power transistor does not need to be mounted on a heatsink, as, at most, it will only be required to dissipate 600 milliwatts of power.

Note also that the available power output with this amplifier is strictly limited because of the limitation on current flowing through the loudspeaker, and the current which can reasonably be drawn from dry cells. Finally, in figure 9 we have shown

Finally, in figure 9 we have shown an economical, complementary-symmetry amplifier with an output power of 300 milliwatts into an 8-ohm speaker. It represents the most economical method of providing this order of power, both in terms of component cost and battery consumption. Particular transistors have been specified and it is not intended as a circuit in which oddment transistors can be substituted.

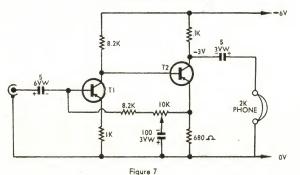
Note that loudspeakers with an impedance higher than 8 ohms may be used with a consequent reduction in power output and current drain. Current drain with an 8-ohm loudspeaker is 100mA at full power and a mere 1mA at no signal.

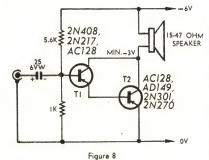
The operation of the amplifier is as follows: The input transistor is a highgain silicon NPN type functioning as a common-emitter amplifier stage. Following the input transistor is a silicon PNP transistor which performs further voltage amplification and also acts as the driver for the two output transistors. The output transistors are a complementary germanium pair, AC127/AC128.

Complementary-symmetry operation has the advantage of achieving the phase-splitting which is necessary for c'ass-B operation push-pull operation in the output pair itself. Class-B operation implies that the output transistors are biased so that they draw very little current under quiescent conditions, the current rising with signal level. For those not familiar with phase-splitting in complementary-symmetry amplifiers the principle is as follows:

Suppose, initially, that the signal from the collector of the driver transistor is positive-going, so that both output transistor bases are driven positive. ter of the input transistor. The degree of feedback is determined by the value of the 270-ohm resistor. Decreasing the resistor increases the gain and vice versa. The low frequency response of the amplifier is determined mainly by the value of the 16uF capacitor in series with the 270-ohm resistor and also by the size of the output coupling capacitor.

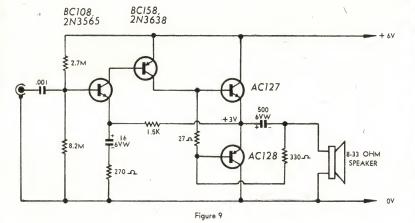
2x0C74,2N647,AC107, etc





Because all stages in the amplifier are direct coupled, the voltage at the junction of the output transistor emitters is determined by the ratio of the voltage divider resistors at the input. Normally, there should be no need to adjust this voltage, unless the supply voltage is changed.

The last feature of note in this amplifier is the low value of quiescent current necessary to reduce "crossover" distortion to acceptable limits. Cross-over distortion is visually apparent on an oscilloscope as a "nick" in



This will cause the upper (NPN) transistor to conduct and "charge up" the output coupling capacitor via the loudspeaker load, the lower (PNP) transistor meanwhile is turned off. During the following half-cycle, as the signal becomes negative with respect to the junction of the two emitters, the upper transistor turns off while the lower one conducts and discharges the output c o up ling capacitor through the loudspeaker load.

Class-B operation is thus achieved, with positive-going half-cycles being suppled to the loudspeaker from the positive supply rail and the negative-going half-cycles being supplied by the subsequent discharge of the output coupling capacitor,

coupling capacitor. Negative AC and negative DC feedback is applied from the junction of the output transistor emitters to the emitthe waveform that occurs when one transistor in the output stage turns off and the other begins conducting. This distortion is very irritating to the ear but can be reduced to negligible proportions by allowing a small current to flow at all times through the output pair; this is the "quiescent" or "no-signal" current referred to earlier. A suitable choice of quiescent current ensures a small overlap and a smooth transition between each transistor.

In this case, both output transistors are slightly forward biased by the voltage divider formed by the 330-ohm and 27-ohm resistors to give a quiescent current of approximately 1mA. This low current means that the usual temperature stabilisation components such as emitter resistors and thermistors can be omitted.





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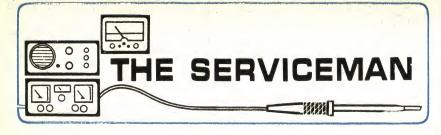


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Round circles and square eyes!

Servicemen, like everybody else, have those crazy days when the most unlikely things seem to happen in quick succession. I had just such a day a few weeks back.

It started out normally enough with a message to go to a particular address and have a look at a television set which was supposed to have "a peculiar pattern on the screen.

Perhaps I tempted fate by thinking to myself that most television sets suffered from peculiar patterns on the screen for most of the time. Patterns in the likeness of politicians, for example.

When I duly arrived at the address, I found to my discomfort that the real purpose of my visit was to provide an independent opinion in a dispute between customer and supplier. I certainly had no wish to become the "meat in a sandwich" but, since I was at the address, with a service fee at stake,' I had little choice but to go along with the situation.

The lady of the house explained that they had recently bought a new 25-inch television set from one of the major stores in Sydney. They had noticed, however, that there was a round ring on the screen about the size of a plate. When they rang the store and com-plained, the department manager had raid the he had never beard of such a said that he had never heard of such a thing and he felt that they must have seen a reflection in the tube face of something else in the room. After all, the set had been checked before it left the store and checked again after installation; nobody had seen anything amiss.

After a further complaint, the manager had sent out a serviceman who, as fate would have it, turned up late one afternoon when only a couple of the older children were home. The serviceman had had a good look at the set and pronounced it as perfect. As far as the store was concerned, the matter had ended there.

My job was to look at the set and, presumably, verify the owner's observation.

Since there seemed to be no obvious alternative, I walked over and switched the set on, to be greeted, shortly afterwards, by a seemingly perfect picture: plenty of brightness all over, good contrast, no smear, no ghosts and, as far as I could see with the naked eye, no peculiar patterns either!

I could only say as much.

At this, the lady of the house sug-

gested that I turn the selector to channel 14 which, on this set, is a blank channel. Naturally enough, I was greeted with a perfectly plain raster on the screen. I didn't need to be a sage to realise that switching to the blank channel was supposed to show up the peculiar pattern to best advantage.

However, as I kneeled in front of the screen, I peered in vain for any sign of pattern or mark or imperfection. The tube looked exactly what it was sup-posed to be — a new and healthy 25inch specimen.

Again I said as much.

"Now come back here," said the lady of the house, and I did so without any particular enthusiasm.

And blow me down There it was: As plain as you couldn't wish for — a darker, yellow brown line, about a half-



"You realise, of course, there's a slight additional charge for these fringe-area calls?" "PF these fringe-area calls?" Reporter."

inch wide and describing an almost perfect circle about nine inches in diameter in the centre of the screen.

As I moved towards the screen again, the line seemed to disappear till, from about a foot away, I could only just make it out because I knew what to look for and where.

But, even from close up if the screen was viewed obliquely, the circle was quite obvious.

Naturally, I had to accept the evidence of my own eyes and agree with the good lady that there was indeed a peculiar pattern on the screen and that they had every right to complain about it.

With the set tuned back to an active channel, the mark was virtually invis-ible most of the time — which was the reason I had missed it at first encounter. Only by looking carefully at midgrey areas which happened to coincide with segments of the circle could one see anything unusual.

That was until the picture faded through a blank grey screen into the next scene: then the circle was plain indeed.

Had it been a normal service situation, I would have advised the customer to forget it; the mark detracted so little from the value of the picture.

But this wasn't a normal service situation. The people concerned had-paid for a new receiver and they had every right to expect a picture tube free from obvious peculiarities.

In exchange for my service fee, I duly rang the store which had supplied the receiver and explained to the departmental head what I had observed. To give him his due, once convinced, he had no hesitation in promising to send out a serviceman forthwith, with a replacement tube. What had caused the circle on the

screen I could only guess.

During manufacture, the envelope of the picture tube is partly filled with water and the phosphor powder is poured into the water. It then slowly settles on to the inside of the screen face. The water is then carefully poured off ("Decanted," they call it) and the surface dried with warm air.

Possibly something had interrupted the process in the case of this particular tube and left a slight stain or discontinuity in the density of the phosphor around a small pool of water. Either that, or a pool of water on a previous occasion had left a ring of contamination on the inside of the glass, which had affected the phosphor.

Or was there a colouration in the glass itself?

That the tube had passed through all the inspections, right into the customer's home, is probably explained by the fact that such inspections are normally carried out from close up, in front of the tube. And from this position, the mark was simply not apparent.

Why, I haven't a clue. I only know that that's the way it was. Furthermore, the serviceman who effected the replacement rang me next day to compare notes and to seek mutual assurance that neither of us was mad!

I did suggest that he make sure to attach a note to the tube explaining why it was rejected; otherwise someone back at the picture tube store will want to know: "What the heck is supposed to be wrong with this perfectly good tube?"

The very next job, somewhat remote from my usual haunts, involved a new stereo system, which was reported to be anything but satisfactory.

From the message, I had mental visions of a large, and expensive system and a rather critical owner getting upset about something that fell short of perfection. It turned out to be a new system, to be sure, but it was a quite unpretentious one with two smallish loudspeakers that could be demounted

from the main cabinet and placed somewhat further apart.

And far from the trouble being subtle, it was a case of one channel being very obviously weak and distorted.

This could have been due to anything from the pickup cartridge onwards but my first step was to swap the two loudspeaker plugs over and try again. Since distortion still issued from the same loudspeaker, it seemed pretty clear that the loudspeaker itself was at fault.

While it was natural to suspect that the voice coil was fouling in the gap, I have also known somewhat similar behaviour to be caused by a dry joint between the lead from the voice coil and the tagstrip on the housing.

With this in mind, I switched the system off, unscrewed the rather frail rear cover from the loudspeaker cabinet and undid the four screws holding the loudspeaker in place.

My next — and quite automatic action was to raise the loudspeaker to my ear, with a thumb on opposite edges of the cone, to note whether I could hear a scraping noise as I moved the cone gently back and forth.

But I didn't get that far. Quietly, but very plainly, I was greeted by a voice

CASE HISTORIES

Yes our "Serviceman" will be happy to include in his columns items contributed by readers, such as the story featured overleaf. The material must be authentic — NOT fictional. It should be supported by mention of equipment, make and model (if possible and not for publication), voltage and current readings and a careful account of symptoms, diagnosis and corrective procedures. A contribution fee will be paid for items used.

that I recognised instantly as emanating from one of our local broadcast stations.

I must have forgotten to turn the set off! But no, it was off all right; and it was still turned to "Phono" where I had left it.

Then I suddenly realised where I was: off the beaten track, as I said, and only a mile or so from the particular transmitter.

Apparently, signal was penetrating the circuits of the amplifier through the power wiring or loudspeaker leads and was being rectified by one or other of the junctions in one or other of the output transistors.

Switched on, the equipment was a regular stereogram. Switched off, it was behaving like a crystal set!

Not that this schizophrenic behaviour had any bearing on the original complaint. As far as I could see, the loudspeaker connections were perfectly sound and the trouble was simply a warped or off-centre voice coil.

Since the unsought sound could be heard only when close to the loudspeaker. I saw no reason to 'get involved trying to eliminate it, but I imagine that, a bit closer to the transmitting aerial, it might have been too loud to ignore.

As an old-timer, I can chalk up one more thing to be said for valves. They never acted like this. When you switched them off, they went off and stayed off. They didn't keep on working in any roundabout fashion!

To round off this month's instalment, here is a story passed on to me by the Editor and submitted by P.E. of Como, N.S.W. He writes as follows:

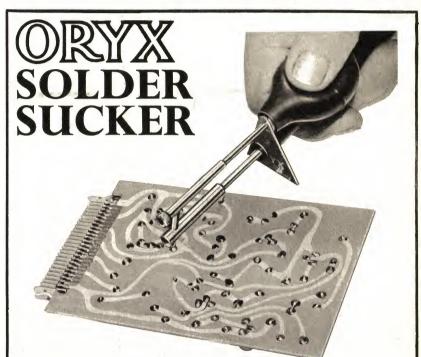
Repairing a radio receiver is like solving a mystery story, with the serviceman playing the role of detective. He collects facts, makes deductions and follows up clues, until the villain of the piece, a faulty resistor or other component is unmasked. This case was no exception.

Diffidently the owner produced an

early portable receiver of local manufacture.

"Some weeks ago I dropped it," he explained, "and since then the volume has been weak and there seems to be more background noise than usual." As an afterthought, he added, "And the volume control squeaks!"

My first thought was that the ferrite aerial rod had broken. Removing the back of the case showed that this had indeed happened, but on some previous occasion. It had been repaired fairly effectively with a piece of plastic tubing and some kind of adhesive. The battery voltage and current draw were



A new device introduced by Oryx, this de-soldering tool makes it easy to remove excess solder from circuit boards, from plated-through holes, and from terminals, etc. Consisting of a miniature Oryx iron to melt the solder, and an attached suction bulb and a reservoir for the removed solder, the unit is small and light enough to be used easily with one hand. It has its own built-in stand, so it can simply be put down on the bench between operations. Operating on very low voltage for greatest safety, it requires only 18 watts at 6, 12 or 24 volts AC or DC, or 25 watts at 12 or 24 volts AC or DC. Highly efficient and precisionmade throughout, the unit is extremely effective for use on the

production line, by servicemen, by test technicians, and in prototype and breadboarding activities. The solder reservoir is stainless steel, easily cleaned; the suction tip is heavily chrome plated so that solder will not adhere. The unit Model SS-18-6V is furnished complete with an Oryx 18 watt, 6 volt miniature soldering iron, ready for operation from a suitable 6 volt transformer or other 6 volt source. For higher temperature operation. the 6 volt iron may be removed, and any of the following Oryx models used in its place - Model 12-6, 12 or 24 volt AC or DC, or an Oryx 25 watt, 12 or 24 volt AC or DC, both used in conjunction with an Oryx de-soldering adaptor.

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A speed change will shortly be available as an optional extra. (The pickup arm depicted in the illustration is a masterpiece of British engineering - the "Transcriptor" fluid-damped hydraulic arm.)

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RADIO: Unofficial history

When a certain commercial radio station in Brisbane acquired a new manager, the staff were left in no doubt that things were in for a change. "Efficiency" was the keynote, and as anybody who did not look as though he was essential to the enterprise soon found himself out of a job, the place fairly hummed with activity. Even the musicians became unusually industrious! New program ideas were tried, and the upshot of all this was entirely satisfactory to the station owners —the costs were down and the ratings were up. One of the aims of the new-look station

One of the aims of the new-look station was to be first with the news. The "withit" image had to be sustained wherever possible, and one of the dodges used to be first off the mark was to get public figures to record suitable speeches in advance against the eventuality of the sudden death of prominent world figures. Within minutes of the news being received of the death of such a figure, the announcement could be made, the speeches played over, and suitable devotional music played as a mark of respect. The value of such preparation will be appreciated by those who have had to interrupt a comedy program for such an announcement, only to find that they have nothing suitable to put to air.

suitable to put to air. Reflecting the new efficiency policy, superbly edited recordings were made on disc, and a selection of sacred music set aside against the day when the emergency arose. One day, the planning paid off, A much loved and respected member of the Royal Family passed away, the news arriving in the middle of a soap opera. The program was cut, and the appropriate disc having been retrieved from the stock of prepared speeches, it was placed on the turntable and put to air as per the standing instructions.

But where was the set of sacred music discs? Nobody knew, and they certainly were not where they should have been. In this emergency, everybody from the cleaner and cook to the program and technical staff joined in the search, knowing that they had only a few minutes to find the missing discs before the recorded speeches ended. In the meantime, the recorded voices of the public figures were lamenting the untimely death of the British Prime Minister, Phones rang furiously, but in vain; nobody could spare the time to answer them in the general panic occasioned by the search for the missing discs.

But there were a few red faces later, when listeners began to inquire about the sudden and entirely unexpected death of the Prime Minister, who, as it happened, was remarkably fit. Like Mark Twain, the report of his death was "greatly exaggerated."

In the inevitable "inquest," the truth came out. The right disc had been handed to the panel operator, but he had played the wrong side! (C. D., Sherwood, Qld.)

(Readers are invited to submit contributions to "RADIO: Unofficial History" and a publication fee will be paid for those used. Stories must be humorous and they must be true. Letters must be signed and the locale of the story indicated as a mark of good faith. The Editor reserves the right to re-phrase contributions as necessary to preserve uniformity of style.

next measured as a routine procedure and found to be normal.

Checking the reception of the local stations proved to be inconclusive. The gain was noticeably below par and the background hiss above normal, but the set was still working. In fact, it looked like a case of "general debility" which can consume a lot of time and components to restore the original performance. Turning off the volume control switch reminded me of the third fault. At the moment the switch contacts opened the speaker emitted a small "squeak."

A quick look at the circuit diagram showed that it was a conventional 7-transistor line-up. A mixer-oscillator, two IF stages and a diode detector, followed by an audio amplifier, audio driver and push-pull output.

The audio amplifier and the front end were de-coupled from the driver and output stages by a 220-ohm resistor and an 80uF electrolytic capacitor. If this capacitor had dried out, it could possibly explain the loss of gain and the tendency towards audio instability. However, bridging it with a new 100uF microfarad capacitor only changed the pitch of the "squeak" when the switch was turned off.

Before consigning this receiver to the shelf marked "Curly Ones" for more mature consideration, I decided to run over it with a multivibrator signal injector. Starting from the output stage I worked my way back towards the converter. All was normal until the 2uF capacitor coupling the volume control to the audio amplifier was reached. Applying the signal injector to the output side of this capacitor gave a strong signal from the speaker, whilst applying to the input side gave very little. The villain of this story had been exposed—a partially open coupling capacitor.

Replacing this coupling capacitor cured all three faults. The volume increased, the background hiss became almost inaudible and the "squeak" disappeared. Presumably the additional loading of the volume control and diode detector circuits fixed the second two faults.

In retrospect, I had seriously to doubt the client's account of what had happened. Quite possibly, the performance of the receiver had been deteriorating over a long period, as the electrolytic coupling capacitor gradually dried out. It was only when he dropped the set and became apprehensive about the damage it might have suffered, that the owner realised that the set was performing poorly.

On the other hand, the capacitor could have suffered damage in the fall by one of the connections tearing loose internally.

As for the hiss, this would be more noticeable, anyway, in an old set, with the audio gain control turned abnormally high to make up for the lossy coupling to the front end. The squeak would indicate that the audio end was either unstable, or on the verge of instability with the coupling circuit almost open; this could have added to the noise.

But, typically, I had to forget about the "ifs" and the "might be's" and press on with the next job. The main thing was that the receiver had been fixed.

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FORUM

Program lines and microwave links

When we sit down each evening to listen to the radio or to watch our favourite television program, we may possibly associate it with the Australian Broadcasting Commission, or a particular commercial station. Very rarely does one stop to think that behind the distribution of radio and television programs is a vast network of lines and radio links provided by the Australian Post Office.

Conducted by the Editor

Responsible for this introduction is a letter to hand from Mr E. J. Wilkinson, Assistant Director-General (Radio), Australian Post Office Headquarters, Melbourne. He writes as follows:

Dear Sir,—"I refer to the lists of broadcasting and television stations operating throughout Australia and the Territory of Papua/New Guinea, which were published on pages 108-111 of the January, 1970, issue of Electronics Australia. In view of the popularity of the lists and the many uses to which they are put, I trust you will allow me to make an observation concerning the national broadcasting and television transmitting stations.

"From a study of the notes accompanying the tables of stations, all your readers may not appreciate the involvement of the Australian Post Office in providing and operating these stations. Under the direction of the Federal Minister concerned (the Postmaster-General) responsibility for the national services in Australia is vested in three Commonwealth Authorities:

• Australian Broadcasting Control Board: Planning, standards, overall control.

• Australian Broadcasting Commission: Programs and establishment and operation of studio technical facilities.

• Australian Post Office: Establishment and operation of transmitting plant and program relay facilities.

"These responsibilities cover medium and short-wave stations and also apply to the operation of the National Broadcasting Service in the Territory of Papua/New Guinea.

"I would stress that there is very close and friendly co-operation between the three bodies and my desire in setting out the separate responsibilities is merely to draw attention to the Post Office role, not to emphasise it. Especially have I in mind the large number of Post Office technical staff who help to bring national sound and television programs to the homes of your readers. Many of these are living and working in remote and lonely parts of the Commonwealth or Papua/New Guinea, and the majority are keen readers of Electronics Australia."

Yours faithfully, E. J. Wilkinson.

Changing the subject, a letter on this page draws attention to the mounting problem posed by SCR devices, as seen by a New Zealand reader.

In fact, we did make a specific point about bi-directional thyristors in last month's editorial but our correspondent could not have known this when he penned the letter. The important difference is that we referred to the interference in only general terms; our correspondent is much more specific. He works in a situation where there is a concentration of SCRs and where

SCR controllers

Dear Sir,

As a regular reader of your journal I wish to express my appreciation of it and to pose a problem which may be suitable for mention in "Forum." I would like to ask whether you have

I would like to ask whether you have heard any mention of trouble from SCR power controllers in the form of AF interference on the mains and into telephone circuits.

In the laboratory where I am working, we have several SCR-controlled ovens, adding up to about 10KW, all told. If one of these is on, the interference is noticeable through the intercom system. If they are all on, the intercom is all but unusable. To a lesser degree, the trouble is also apparent in the telephone circuits.

I gather that this kind of interference on the mains also causes the supply authorities some trouble, as it the interference is sufficient to make its presence felt in a very definite way.

To be sure, one must reasonably ask whether all practical steps have been taken to suppress interference from the oven controllers, even if only to minimise the trouble as distinct from eliminating it altogether. Have the controllers been fitted with optimised capacitors and/or inductors? Are they encased in adequate metal boxes, suitably earthed? Has the wiring been run in earthed metal conduit rather than the now usual plastic variety? These are the kinds of precautions we suggested in our recent "Musicolour" unit, knowing that they would limit interence to a level where it would at least be non-obvious.

In saying this, we are not seeking to set ourselves apart from anyone else. We would welcome legislation to control electrical interference. If that makes it necessary for our staff's vehicles to be checked for interference and our projects to conform to certain radiation standards, yet to be set, that's just part of the deal.

As for SCR interference upsetting control devices operated by the electricity supply authorities, that's the biggest laugh of all! Cynically, I see it as almost a recommendation for using SCRs by the thousand, for control tones themselves are a blight on our peace of mind.

Within a couple of days of writing the February editorial, I had occasion to attend the funeral of an esteemed friend. As something like 200 people sat in the church listening quietly to

can trigger hotwater systems, etc., in some instances.

It seems to me that the action of these controllers is to produce a whole string of harmonics of 50Hz right up into the RF region.

I know of no practical method of filtering or of stopping this interference. It is as pernicious as control tones superimposed on the lines by the supply authorities but it is potentially more troublesome. Certainly, due to the very low cost of SCR devices, the situation is rapidly worsening.

In our case, there are few, if any, ovens available having other type controllers. New Zealand's D.S.I.R. are investigating the problem but have not yet evolved any practical solution. Have you or any of your readers heard of any?

-R.S. (Wellington, N.Z.).

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UNIT 1: Armstrong 526 complete with 2 Empire 2000 loudspeakers. ERA Mark III turntable beloarivere which tracks the Empire beloarivere cartridge at 1/10th of a gram fiz-quency response is 1 dB from 20-20.000 Hz, overall frequency response 4 to 40,000 Hz. Output voltage 5 mv per channel. TOTAL PRICE ... \$930.00



The same with Armstrong 521, the same as the 526, but without the tuner:

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two directions, the inclusion guaranteed for 10,000 hours or three vears, whichever is sooner. Retail Price \$665. Our Price with two Jordan Watts loudspeakers, frequency range from 20-20,000 cycles. \$750.00 Total PRICE The same with Nord Mende 8001/T 3 motor professional tape TOTAL PRICE

UNIT 7: PE 34 belt-driven turntable. Empire 888E cartridge, frequency response from 10-30.000 Hz, output voltage 8 mv per channel, with Schaub-Lorenz Model 4000 tuner/amplifier, 25 watts per channel, from 20-33,000 cycles, 2 Harman Kardon HK 40 loudspeakers com-plete in cabinets. TOTAL PRICE -. \$780.00

UNIT 8: Harman Kardon SC 1510 music Centre, power output: 25 watts. 1 HF (50 watts E.I.A. peak). Frequency Response: Plus or minus 1.5 db 18-30,000 Hz at 1 watt. Harmonic Dis-tortion: Less than 1 per cent. Inter-modulation Distortion: 0.25 per cent at 1 watt. Harman Kardon SC 1510 fully transistorised compact unit, complete with 2 HK 10 loudspeakers: TOTAL' PRICE \$500.00



The cartridge designed for checking test records The new Empire 1000ZE—stereo calibration standard

Each 1000 ZE cartridge is individually calibrated to have a flat frequency response within plus or minus i DB from 20-20,000 Hz. There are no electrical or mechanical resonant peaks and total IM distortion at the standard 3.54 cm/sec groove velocity does not exceed .05 per cent at any frequency within the full spectrum. Stereo separation is better than 35 DB at 1 KC and remains at least 25 DB or better all the way out to 20,000 Hz. Overall frequency response 4 to 40,000 Hz. Output voltage 5 my per channel. The calibration standard 1000 ZE stereo cartridge was designed to provide professional users, such as recording studios, radio stations, scientific and engineering laboratories, as well as serious audio-philes with the ideal standard for record playback evaluation. The 1000 ZE tracks effectively at strus forces as low as .1 gram and never subjects the disc, whether it is vinyl pressing or master lacuuer, to any visible wear or groove deformation, in high performance pickup arms (for example the Empire Gartridge ever developed. Assembled under carefully controlled conditions, the for its superior performance. The stereo performance of the Empire cartridge sites a new standard in listening quality. The Empire cartridge is previously available. Monophonic records, it outperforms the finest monophonic cartridge steres and the monophonic records, it outperforms the finest monophonic cartridge steres and compare the work of the Empire cartridge steres and an exer subjects the direct at each phase of the Empire cartridge steres a new standard in listening quality. The Empire cartridge steres previously available.





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words of tribute, the atmosphere was shattered by a protracted series of 1000Hz tones reproduced through the amplifier system.

If ever I felt hostile about the practice it was then. I can only hope that last month's editorial and the workshop on interference to which it referred will start the ball rolling for some action on this whole vexed question.

Speaking about being hostile, a number of readers have expressed themselves as such, from time to time, since we adopted the term Hertz in place of cycles per second. They described the change in terms such as untimely, unnecessary, undesirable, deplorable, snobbish, etc. And choosing to ignore the real reason why Hertz emerged as an international term, they forecast that we would have to reverse our decision in due course. Some even tried to press us into leading a crusade to have the word rejected by the World's technical Press.

If we had ever been tempted to do anything like this—and we certainly weren't—any chance of us dropping the term Hertz would have disappeared with the recent announcement by the Federal Government of a changeover to the metric system of weights and measures.

Very plainly, as a nation, we are supporting the principle of uniform international scientific and engineering standards. Hertz happens to be a part of it.

As a piece of counter propaganda to those whose letters have been featured from time to time, I thought you might like to read one which arrived recently from a correspondent in South Australia.

Dear Sir.

As a migrant from the Continent. I have read with much amusement the various arguments regarding the "new" terminology. I simply cannot understand why people find fault with Hertz instead of cycles-per-second or, for that matter, Celsius degrees instead of Fahrenheit. The time is now in sight when these people will have another thing to get ulcers about: metric weights and measures.

In my opinion, the move comes none too soon, as Australia, in many ways is backward, if not archaic. Mind you, we are not alone in this respect but that is no excuse.

To get back to all that fuss about Hertz, etc., I had to "unlearn" what I had been taught and get used to your standards and it was not all that hard. I am not a genius, or anything anproaching one, and I cannot really see what the fuss is all about.

I am not 40 yet but, brother, have I seen some changes? It's impossible to stop the world. A lot of people need to pull their socks up and get on with the job. This country might then get somewhere.

V. S. (Whyalla, S.A.).

Having re-read the letter, I can only hope that V.S. is a big bloke. You need to be, when you express yourself in this uninhibited fashion!

From a reader in Melbourne comes a letter enclosing a clipping from a suburban newspaper. It tells of a new type of shoe which, in warm weather, will ensure that the wearer does not suffer from hot feet. On the contrary, he or she will have among "the coolest feet in Australia."

Knowing how cold one's feet can get, at times, in Australia, I'm not sure that I would be in the market for shoes which carried such a promise. But the chance of shedding at least a few degrees would certainly be welcome at times.

The interesting thing is that the article blames the problem of overheated feet on to static electricity. Get rid of this, and down comes the temperature. I quote:

"Basic principle of the Stat-E-Con sole, as its name implies, is to earth the static electricity which normally builds up in the body, resulting in the hot-foot condition, which has come as a by-product of today's widely used synthetic soles."

Commenting on this, our correspondent (H.P., East Malvern) says:

"This may not be a field in which I am particularly well informed but I fail to see how the presence or absence of a static charge on a person's feet could affect their temperature and comfort. In any case, it would appear that, the moment the person touched any earthed object with any part of their body, the charge would be dissipated anyway."

I'm afraid I must express agreement with these sentiments. To be sure, certain plastic soles can produce considerable discomfort on hot days and sandals with a minimum of "upper" are no exception. But I would have to be convinced that it is not simply a matter of thermal insulation and the lack of means by which heat from that very hard working area of skin can dissipate.

Increase the thermal conductivity of the soles by any convenient means and I imagine that the discomfort would diminish immediately.

I have no way of knowing whether the Stat-E-Con soles exhibit increased thermal conductivity as well as electrical conductivity, or whether only the latter. But, if static electricity is entirely to blame for hot feet then an alternative method of cooling them would be to use a metal walking stick or trail a chain, as some car drivers used to do.

On this basis, Dickens' famous caracter, the Ghost of Jacob Marley, must have had quite frigid feet.

In saying this, I am not discount ing the possible significance of antistatic soles in surgery and other situations where static charges could produce unexpected sparks, leading to involuntary movement and even ignition of volatile gases. But that is quite a different thing from hot feet.

Come to think of it, I could do with a pair of anti-static trousers. Time and again I slide across the front seat of my car and receive a "belt" as I touch the door-handle.

And wouldn't it be curious if conductive trousers turned out to be the answer to the proverbial "hot seat"?





ELECTROLUMINESCENCE .

principles of semiconductor and phosphor techniques

Electroluminescent devices under development in the U.K. are expected to eventually be widely used in both the technical and domestic spheres. One likely use is as a flat picture display for TV receivers.

By ARON VECHT

Everyday electronic equipment conveys information of ever-increasing complexity to us. In almost all cases this is done by some visual signal (usually an electrical message converted into a light signal). These signals range from a simple on/off, indicated by a single lamp, to a complete picture, that may contain about a quarter of a million dots of light. There is therefore, a continuous demand for better light sources that can effectively display the required information.

In the past, simple incandescent (or neon) lamps were used as single indicators, while the cathode ray tube could convey more complicated information. Both these devices have the disadvantages of bulk and a fairly limited life. The conversion to light of electricity is indirect; in one case, the process occurs via heat, while the other makes use of the action of an electron beam on a powder phosphor layer. However, the conversion of the energy is inefficient, ranging from 1-20 per cent.

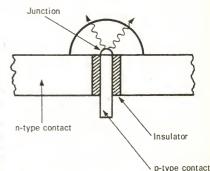
Ideally we require a robust, flat, efficient source of light which has a long life. Such a lamp should convert the electrical signal directly into light. This process is termed electroluminescence. The stage of research and development has now been reached where two types of lamps of considerable promise have been made. These lamps, that are now becoming available, have been developed from two very different areas of research.

The first is a direct outcome of semiconductor technology and an extension of the detailed investigation of the elements silicon and germanium to compounds such as silicon carbide and gallium arsenide. The lamps in this group are junction devices, the light being emitted at the junction of P and N type semiconductors.

The second is a development of research on the materials that convert the electron beam energy in the cathode ray tube into light. Such materials are usually applied to the cathode ray screens as powders and are termed phosphors. One of the most efficient phosphor systems used in the past is based on zinc and cadmium sulphides. When they are prepared to a high degree of purity, doped with copper or silver impurities and treated in a special way, the required phosphor properties are obtained. If some of these phosphors are placed inside a capacitor with at least one transparent electrode, light can also be obtained directly by the application of an AC field. The phosphors have now been considerably modified and the light sources produced using this technology may be called powder electroluminiscent cells.

In devices where only small areas of illumination are needed or where long life is essential, junctions made from silicon carbide or gallium arsenide and related compounds are being used on an ever increasing scale. Unfortunately, unless technology changes a great deal, these devices will remain expensive, as they are produced from perfect single crystals which can only be grown to a certain size.

Such devices, however, have the advantage of a long operating life. Thus, where the labour cost of dismantling apparatus is high they will replace conventional bulbs. Further applications are for very small light sources and in electronic equipment that requires light emitting devices to switch rapidly. Junction devices that can be switched on or off in nanoseconds (a nanose-



Simplified diagram of a junction electroluminescent device. The emission area is about 1 sq. mm.



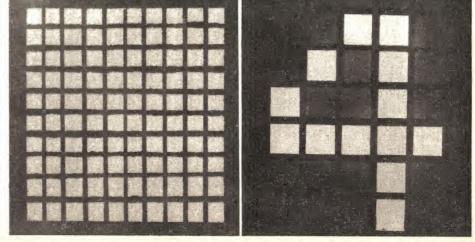
Simple DCEL letter display, photographed from its own illumination. The letters can be obtained either by evaporating the back electrode through a mask, or, as in the example illustrated, by photo-etching the transparent electrode.

cond is a thousand-millionth of a second) can now be produced.

The problem with gallium arsenide lamps and lamps made from related compounds, was primarily the colour of the light produced, Efficient light sources can be made that emit in the infra-red but efficiency falls off a lot as light emission in the visible region is obtained. Originally it was thought that

RIGHT: A hundred dot cross matrix photographed from its own illumination. Each dot is a discrete electroluminescent cell, separately powered.

FAR RIGHT: Showing how a cross matrix can be used for a number display, by selection of the appropriate contacts to illuminate the desired dots. (Photographed from its own illumination.)



At last a high fidelity Cassette Stereo

It took Teac years of research to develop a compact stereo cassette recorder with the same high quality record and playback as available in reel to reel stereo tape decks. Their success was the A-20 cassette stereo deck --- \$209.50 Aust. The A-20 features a 4-pole hysteresis synchronous motor, Dual VU meters, all silicon-transistorised pre-amplifiers, and uni-directional stereo microphone. This cassette stereo tape deck was made to match the Teac AS-200 integrated amplifier (120 watt RMS continuous power output and wide dynamic range. Frequency response 20-80,000 Hz-\$389 Aust.), and Teac LS-350 3-way 3-speaker system (full 12" woofer, easily handles 40 watts-\$154 Aust.), but can be easily connected to any quality equipment to give you the convenience of cassette, and the quality of reel to reel tape.

Specifications:

- 2 heads
- 4 track, 2 channel stereo
- Frequency response 60 to 10,000 Hz
- Wow and flutter less than 0.2%
- Tape speed 17/8 i.p.s.
- C-60, C-90, or C-120 tape

TEAC

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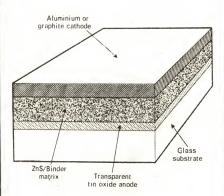
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-20

such light sources would not be used much, but two methods have been introduced which overcome this problem. Firstly, methods have been developed for growing single crystals of materials that emit in the green part of the spectrum. Best results are being obtained by the growth of solid solutions of two compounds producing a material still showing reasonable efficiency in emitting visible light. An example of this is graded growth gallium arsenide phosphide which gives a useful red-emitting device. Alternatively, new materials have been developed that can convert infra-red light to the visible part of the spectrum. Such materials, can simply be coated on the windows of infra-red emitting gallium arsenide lamps, producing green light.

But for large area displays covering thousands of square cm another approach is required and powder electroluminescent cells can be employed. These are cheap to make and can basically be considered as a painted layer between two electrodes. At one time it looked as if such devices could only be employed at fairly high voltages (over 100) using AC supplies. More recently,



The general arrangement of elements in a powder electroluminescent cell for DC. The surface area may vary from as small as one hundredth of a square millimetre to thousands of square centimetres.

it has been shown that this is not the case and that low voltage (30V) direct current panels can be produced.

A major problem that remains to be solved is the maintenance of these large area panels. Early experiments indicated that direct current electroluminescent (DCEL) lamps were merely scientific curiosities that emitted light for only a few minutes. Although light emissions lasting about a thousand hours can now be achieved, this is not quite good enough. A light output which lasts for five to ten thousand hours is needed and will probably be obtained.

The light emission from the DCEL lamps is yellow-orange, this colour being obtained by adding a manganese impurity to the phosphor. This is a most useful colour, as it corresponds to the part of the spectrum to which the eye is very sensitive. Further work is now being done to obtain useful green and blue emissions. This has recently been done by replacing the manganese impurities by traces of rare earth elements and green and blue lamps have been produced. Although the development of these phosphors is at a very early stage, rare earth activated materials will increase the range of colours that will eventually be obtained from DCEL lamps.

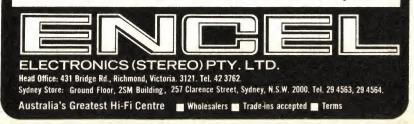
So far, only the powder phosphor systems, where the phosphor powder is incorporated in a binder, have been described. Zinc sulphide and related compounds can be evaporated and the deposited thin film, after suitable treatal properties to those observed in powders of these materials. This is different from gallium arsenide and its related compounds which can only be used in single crystal form.

Thin films of zinc sulphide activated with manganese and copper can be made to electroluminesce. Up to now, the properties of such films have not matched the performance of powder phosphors. When the light emitting processes are better understood, evaporated devices may well perform better and ultimately replace the powder devices. Thin films can be prepared very cheaply and research workers are after large area devices compatible with solid state technology.

The potential of these devices appears to be enormous. Such lamps will certainly find wide application for digital readout and illumination devices in a great many electronic equipments, and when other problems of storage and address have been solved, electroluminescent lamps may be used in flat picture displays to replace cathode ray tubes in television systems. In a much wider field, they could be used in situations where large areas of uniform illumination are required. Exit signs, notice boards and clock faces can be directly illuminated by them, and the low voltage DC application immediately indicates their use in car dash boards and similar situations.



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A READER BUILT IT

Parlour Game-Another Version*

Although this is yet another version of the electronic game described on previous occasions, it offers some novel features. One is the method of displaying the "machine's move" instructions, and another a means to vary the machine's "program" when the players learn how to beat it.

The submitted circuit was evolved after reading your articles on "Switchcraft." (Radio Television and Hobbies, November, 1959). The idea is not new but readers may welcome a switching circuit which can be used to entertain one's friends.

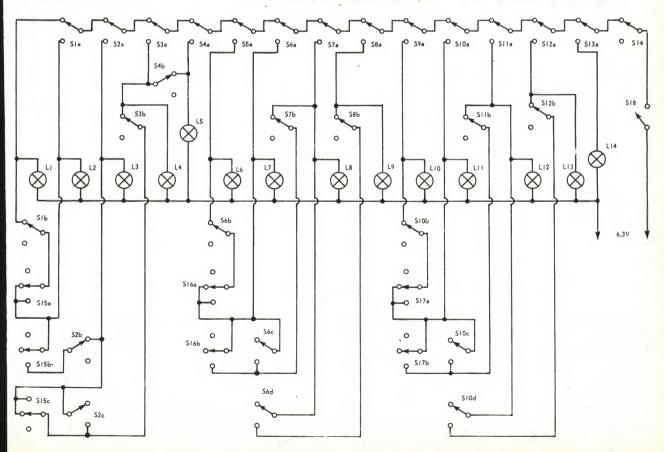
To play the game 14 switches are turned down in sequence from left to right. The player and the box take it in turn to move, turning down one, two, or three switches at each move, as they please. Each tries to leave the last move to the other. When it is the box's turn to move the player presses the switch S18 and then, on the box's behalf, turns down the switches over which a light appears. It is then the player's turn again. The switches S15, 16, and 17 are used to vary the circuit when someone beats the box, so that he cannot win again by making the same moves.

I purchased 18 obsolete lever keys from the post office for 5c each. Switches SI to S14 are two-position types. Most of them need to provide three change-over functions (the "a" "b," and "c" functions shown on the circuit) and two, S6 and S10, need four such functions ("d"). These switches are normally set in the horizontal position (the position represented on the circuit) and pushed down to represent the various "moves." Switches S15 to S17 are three-position types, and S18 is a spring return type.

I mounted the switches in a wooden

frame, arranged in two rows. From S1 to S14 makes up the top row and S15 to S18 are spaced out to make the bottom row. There is a 7/16in hole above each switch S1 to S14 to accommodate a 6.3V globe. These were purchased cheaply at a chain store. The unit's total cost was under \$2. (L. A. S.)

* This circuit was submitted by a reader some time ago, and since it may no longer be appropriate to publish the name and address as supplied, we have used initials only. If the reader concerned cares to contact us, we shall be pleased to arrange payment for the item.



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SPEAKER ENCLOSURES



SPEAKERS

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MODEL No.	IMPEDANCE [Ω]	FREQ. RANGE [c/s]	INPUT [W]	SPEAKERS [mm]	DIMENSIONS [mm]
FCS-104	8	95~20,000	8	100(W), 85(T)	250H×158W×173D
FCS-200	8	60~20,000	40	200(W), 50(T)	530H×294W×240D
FC5-207	8	45~20,000	30	200(W), 50(T)	540H×295W×220D
FC5-208	8	70~20,000	30	200(W), 50(T)	$480 \text{H} \times 280 \text{W} \times 200 \text{C}$
FCS-250	8	50~20,000	30	250(W), 80(T)	597H×321W×300
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COMPACT SPEAKER SYSTEMS

MODEL No.	IMPEDANCE [Ω]	FREQ. RANGE [c/s]	INPUT [W]	SPEAKER [mm]	DIMENSIONS [mm]
BF-1035	8	110~18,000	8	100(FULL-RANG)	320H×200W×174D
BF-1635	8	60~16,000	10	160(FULL-RANG)	$384H \times 240W \times 174D$
BF-2035	8	45~16,000	15	200(FULL-RANG)	477H×298W×254D

FULL-RANGE SPEAKERS

DIAM [mm]	ETER [in.]	MODEL No.	۷.C. IMP. [Ω]	RESONANT FREQ.(f.) [c/s]	FREQ. RANGE [c/s]	SENSITIVITY [db]	MAX. INPUT [W]
100	4	FE-103	8/16	65~ 95	fo~18,000	96	10
160	61/2	FE-163	8/16	40~ 60	fo~ 20,000	98	10
200	8	FE-203	8/16	35~ 5 <mark>5</mark>	fo~16,000	100	15 ,
200	8	FE-201	8/16	60~ 90	fo~16,000	100	8

WOOFERS

	ETER [in.]	MODEL No.	V.C. IMP. [Ω]	RESONANT FREQ.(fo) [c/s]	FREQ. RANGE [c/s]	SENSITIVITY [dB]	MAX. INPUT [W]
160	61/2	FW-162	8/16	40~60	fo-3,000	95*	30
200	8	FW-202	8/16	25~35	fo~ 2,000	97	45

W.A. D. K. Northover, 1 Dunvegan Road, Applecross, 6153, TAS: Nichols Radio, 91 Weilington Street, Launceston, 7250. N.S.W.: Jacoby Mitchell. 469-475 Kent Street. Sydney. 2000. VIC.: Macron Electronics. 70 Batesford Road. Chadstone. 3148.

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A READER BUILT IT . . . continued Improved Burglar Alarm

Those readers interested in burglar alarms may care to add this circuit suggestion to their files. It is aimed at getting the ultimate life from the system's batteries.

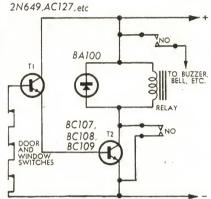
In the October, 1969, edition of "Electronics Australia" (page 99) there was featured a transistorised burglar alarm. In this the writer states that the current drain of the system is about 1.5mA and that the service life of the batteries should be almost as long as the shelf life. Having little else to do at the time I immediately proceeded to carry this idea to its logical conclusion, i.e., no current drain until operated.

Reference to the original circuit shows that the 1.5mA was flowing through the 5.6K biasing resistor and while increasing the value of this would give some improvement, it is a compromise at best. For this reason I re-placed the passive biasing network with an active one, as shown.

With this configuration the non-operate current is the Icbo (collector current when emitter current is zero) of T1, normally 10-20uA. Operation of the circuit depends on the Iceo (collecthe circuit depends on the iceo (collec-tor current when base current is zero) which flows when the base circuit is opened by any of the door or window contacts. This provides forward bias for T2, in place of the forward bias provided by the 5.6K resistor in the available disputi original circuit.

Note that only a germanium type transistor can be used for T1, as the bias current required to turn on T2 will normally be higher than that which can be provided by a silicon type.

Using this circuit, the batteries should now have a service life which



really is equal to the shelf life. Admit-tedly, the improvement may be some-what academic, and the circuit was originally designed more as an exercise than anything else. However, the basic idea may appeal to some readers. (Sub-mitted by: B. J. Robertson, 23 Stan-ley Terrace, Christies Beach, S.A. 5165) ley 7 5165.)

Faster Etching Hint

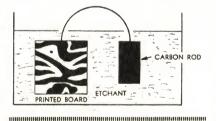
Readers who make their own printed wiring boards may like to try this simple idea to speed up the etching process.

I have found that when etching a printed circuit board it takes a long time and a lot of ferric chloride to etch away a small amount of copper.

By soldering a wire to the copper on the board and connecting the other end of the wire to a carbon rod, immersed in the bath, a cell is formed. The car-bon can be salvaged from an old battery. The wire connecting to the copper board will need to be painted with resist to prevent it from being etched along with the copper pattern.

This will speed up the etching process without the need to use more etchant. (Submitted by: G.H., Ben-digo, Vic. 3550)

(Editor's Footnote: "Reader Built It" projects are published for the general interest of experimenters and as a source of ideas. Based on readers' contributions, they have not been tested in our laboratory and we cannot accept responsibility for them.)



OLD COMPONENTS

Like most other hobbyists with more enthusiasm than money, I have col-lected a lot of old wiring parts - particularly resistors and capacitors. Re-cently I managed to borrow an LRC bridge and found to my dismay that many of the old paper capacitors and even a few of the mica capacitors were leaky and off value. A lot of the re-sistors had gone high.

The bad ones I threw out but I marked the poor ones with a spot of lacquer with the idea of using them where they would still do. Checking old parts is not only likely to save trouble but it is a good technical exercise. (C.D., Orange, N.S.W.)



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*CROSS-FIELD HEAD *3 motors *Sensing tape continuous reverse (Auto. reverse) *Manual reverse *3 speeds, 3 heads *3 speed capstan drive motor *Automatic stop/shut off *Automatic pinch wheel release *Automatic lever release *4 track stereo/monaural recording and playback *40W music power solid state amplifier with two integrated circuits *Fine vinyl leather or wooden cabinet *Matching speaker, SW-125 (3 way, 30 watt input). Prove it by the sound!



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SQUEECH - HOW TO GET MORE WORDS INTO LESS TIME

Squeech means "squeezed speech" — and the word is formd by dropping out a few letters of the original expression and then joining up the rest. In a way, this is something like the manner in which the effect is created, as the following explanation will show.

By Jorma Hyppia

The ability to speak fast, yet accurately and with clarity, is a skill which few people possess. Some people carefully cultivate this skill, such as news readers and radio commentators, but the average person who does not have such incentives as the forenamed seldom acquires the skill. Yet in many spheres of professional and commercial activity, such a skill would be a decided asset. Basically, this would mean the ability to impart more information within a given time.

Most people are never likely to acquire the ability to speak rapidly yet intelligibly, so a speech recording device which allows playback with adjustable speed, yet without affecting pitch of the original voice, looks very interesting. When this device also has the ability to slow down speech as well while retaining the original pitch, it looks doubly interesting. As any tape recorder user knows, it is a simple matter to speed up recorded sound— you simply play it back at a higher speed than that at which it was recorded. But this speedup is achieved only with the sacrifice of intelligibility; with every doubling of playback speed, the pitch of the sound is raised a full octave. Unfortunately, this can make the deep voice of a basso profundo sound like the chattering of a cartoon chipmunk.

The problem, then, is to increase the playback speed without changing the pitch. One way to do this is by programming a computer to scan prerecorded speech material and compress it. This method is now used only in compressed speech research because of the high cost; the tedious programming that is required costs about \$900 per minute.

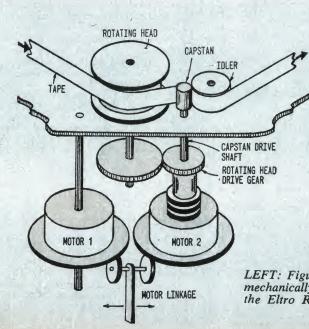
At present, the more practical means

of compressing speech is by utilising a mechanic-electronic device called a Rate Changer. Such equipment is already on the market. It costs several thousands of dollars, but it's a far cheaper solution because it can quickly compress pre-recorded tapes without the elaborate programming required for computers.

The first rate changer— called an acoustical pitch and tempo regulator was invented by a German scientist, the late Anton Springer, in the early 1950s. His original TeleNorm equipment was later improved and is now manufactured by Eltro Automation of Heidelberg, West Germany.

The secret of the Eltro Rate Changer lies in a unique application of a fairly common recording component, a rotating playback head. An ordinary tape recorder has a stationary head with a single sensing gap. If a prerecorded tape moves across this fixed head at varying speed, pitch changes will occur. But if a multi-gap rotating head is substituted for the fixed head, the tape can be speeded up (or slowed down). Constant tape-to-head-velocity is maintained by rotating the head in the proper direction at the proper speed. So long as the tape-to-head velocity remains constant, pitch stays unchanged. Figure 1 shows the ingenious mecha-

Figure 1 shows the ingenious mechanism used to maintain this constant



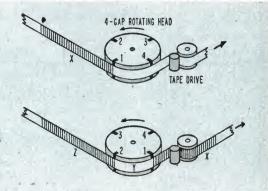


Figure 2. The rotating head of the Rate Changer. The way in which this arrangement leaves out segments of the tape when scanning, to produce compression, is explained in the text

LEFT: Figure 1. This diagram shows the arrangement of two mechanically linked motors and rotating tape head which allow the Eltro Rate Changer to increase or reduce tape playback speed while maintaining constant pitch.



4

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speed ratio between the tape and the head. The velocity of the capstan that drives the tape and that of the rotating head are held in exact synchronisation by means of an electric field lock achieved by using two mechanically linked AC motors.

Motor 1 has a fixed speed of 900rpm angular velocity, which is equivalent to 15 ips linear velocity, the normal tape speed. This motor is coupled to Motor 2 by means of a sliding clutch-like linkage consisting of two rubber-tyred wheels engaging discs attached to the **rotors** of the motors.

Motor 2 is of synchronous type having four-pole construction and a speed of 900rpm. An important design aspect is the freedom of the field or stator section of the motor to rotate around the rotor. This field section is coupled to the rotating head by means of two gears.

When the linkage is set at its 100 per cent position, Motor 1 drives the rotor of Motor 2 at a speed of 900rpm; the rotor shaft in turn drives the capstan at the same speed. Since 900rpm is the normal synchronous velocity of Motor 2, its field section remains stationary during the 100 per cent setting.

Now, if the control knob is moved to shift the linkage so as to increase the rotor speed of Motor 2, the field section of Motor 2 will move just enough to compensate for the speed-up and maintain a rotor-to-field synchronisation of 900rpm. In so doing, the field section moves the gears, thus transmitting the same compensating movement to the rotating playback head.

The speed of Motor 2 can be varied continuously from 450rpm to a maximum of nearly 1800rpm; this means that the tape transport speed is variable from about half to double the normal speed of 15ips. In other words, there's a range extending from 7½ips to 30ips tape speed.

No matter what the actual tape speed may be within this range, the electrical field lock maintains a constant 15 ps velocity between the tape and playback head. As a result, the pitch of the recorded sound remains unaffected by tape speed changes.

The foregoing discussion explains how constant pitch is maintained. But this does not yet explain why compression and expansion take place.

Let us take compression first. The principle used is a well known one, in which small segments of information are left out during a re-recording process. This is how it is done.

The tape to be treated is loaded on to the normal recorder, but instead of being fed to the head and feed mechanism of the recorder, it is fed to the Rate Changer, where it is sensed by the rotating head. Figure 2 shows how the segments of information are omitted.

The top diagram shows the starting position as the tape begins to move from left to right, with the head rotating in the same direction (counterclockwise). Gap 1 is just coming into position to sense the shaded section of tape marked X. By the time the head has rotated a quarter turn, section X has been sensed and has moved to the position shown in the lower drawing.

Just as gap 1 moves away from the tape and becomes temporarily ineffective, gap 2 begins to sense the next shaded section marked Z. Note

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that an intermediate section, Y, cannot be sensed by either gap. Gap 1 is movnot catch up with section Y. Two important consequences result: (1) the ing away from the tape, and gap 2 cansound information on section Y is eliminated, and (2) the **playing time** represented by section Y is also eliminated (this occurs because the instant that the last sound on section X has been sensed, re-recording of section Z begins).

What has happened is that a small amount of time compression has been achieved by sacrificing a small amount of recorded information. This process is repeated again and again throughout the length of the tape; the accumulated small time compressions, interspersed throughout the tape, add up to a large overall reduction in the total playback time.

Does this chopping out of bits of sound information create distortions in

Speech compression now appears to be of primary interest in terms of potential applications. However, speech expansion also has uses. In this case the playing time is lengthened without introducing pitch changes.

The Eltro does this with equal ease when the control knob is properly adjusted. Basically, expansion is created in much the same way as is com-pression except that the tape velocity is made slower than the relative playback velocity, hence the head gaps tend to catch up with tape segments already scanned once. Instead of eliminating information bits, the head now replays bits periodically.

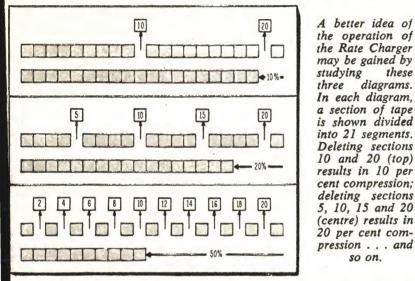
Frequency of thse replays depends on the way the instrument is adjusted. The highest, limiting expansion of 200% is achieved when each bit (13.35mm segment) is reproduced twice before the head goes on to the next bit. This condition yields a tape that re-

> these diagrams.

deleting sections 5, 10, 15 and 20

(centre) results in

so on.



the compressed sound? None that you can perceive with the ear. Reason is that each deleted segment is kept shorter than 35 milliseconds, and this is threshold sound duration that the human ear is just able to perceive. This perception phenomenon is known as the Haas Effect.

The diagrams in figure 3 show 10%, 20%, and 50% degrees of compression. The middle row in each section of the liagram represents a length of tape divided into 21 blocks; each block repreents a tape segment that is 13.35 milimetres in length. At a 15 ips tape peed, this length of tape represents 84.68 milliseconds of playing time, a period slightly shorter than threshold percentual time of 25 milliseconds This erceptual time of 35 milliseconds. This ength is automatically measured out by he playback equipment because it is equal to the gap-to-gap distance of the otating head.

If the Eltro Changer's control knob s adjusted so that there is a 10% inrease of the tape velocity (about 6.5 ips), every tenth bit of sound inforation on the tape is eliminated. This results in a time compression of 10%. If the tape speed is increased by 20% to about 18ips), every fifth bit is emoved to achieve a 20% time com-ression. Finally if the tape speed is loubled to 30 ips, every second bit is emoved, and the total playing time is hopped in half.

quires twice as much playback time as due original recording. To obtain lesser degrees of expansion, the system is ad-justed so that fewer information bits are reproduced twice.

Business and industry may find uses for squeech-for management training purposes, for indoctrination of salesmen, for review of board meetings or sales meetings, for scanning client con-ferences. And consider the harassed secretary or typist who must cope with the dictation of a fast-talking boss. If the employer's dictation is slowed down, the typist is likely to make fewer mistakes when transcribing the material. On the other hand, speeded up recordings might be just the thing for testing the proficiencies of secretarial applicants.

There are many other potential appli-cations for squeech. One more might be mentioned, if only because it is so unusual. Squeech may solve a particularly vexing problem in deep sea exploration. (See "Electronics Australia," December, 1969, page 29.) The addition of helium to the breathing atmosphere of divers hampers telephone communications because the gas causes a pitch increase in the voices of the divers. This pitch increase greatly reduces intelligibility. However, a Rate Changer could be used to restore such off-pitch speech to normalcy without in any way deterior-ating the sound quality. (By arrange-ment with "Radio-TV Experimenter.")



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CLASSICAL RECORDINGS

Reviewed by Julian Russell

AVANT GARDE—Compositions by Koueg, Pongracz, Riehn, Zimmermann, Cage, Schnebel, Gruppo Nuova Consonanza, Kagel and Stockhausen. Set of six discs. Deutsche Grammophon Stereo 643/541-6.

All but dedicated admirers of often way-out contemporary music will find little to interest them in the first three reviews this month. But I feel that this is no reason why they should not be included, though I do not intend to act as a missionary for the school just for the sake of being thought "in the groove." I find some of it impressive, an occasional piece moving, and others totally incomprehensible. But the six discs might also provide the merely curious with some idea of what some contemporary composers are doing, if not a very clear picture of where they are going.

Because Stockhausen is the best known of the composers contributing to this DG set, I shall start with his disc which offers on one side "Mixture" for orchestra, sine-wave generators and ring modulators (version for small orchestra), and on the reverse "Telemusic." The "tele" in "Telemusic" means far distant, not music for television. In it you will hear clicks, bangs, flutters, whistling glissandi, timpani and other notes, notably some clear bell tones, all produced in the Studio for Electronics Music, NHK, Tokyo, Japan. Some of it sounds genuinely Asian and calls up memories at times of the old Parlophone 78 set of Eastern Music. There is one curious sequence that sounds like a gutter overflowing in the rain. And there are frequent repetitions of a sustained note.

There are also some enchanting effects like fairy tambourines, and some notes so high that they are barely on the threshold of audibility. There is even a noise that sounds like a steam locomotive and, in another section, curious disembodied voices. Again you occasionally hear what sounds like the static and distortion in a badly received radio program, but the superb quality of the recording makes it obvious that this is the effect Stockhausen intended and not the result of bad engineering Many of the electronically produced sounds are now pretty familiar to students of this school, but they are indubitably put together by a master craftsman. I feel that I might even grow to like it.

"Mixture" starts like Honegger's "Pacific 231," a famous echoic piece of the 1920s. There are also sounds produced by standard musical instruments, their timbres in many cases changed by the use of electronic filters. It all sounds to me — though I must stress that mine is an untutored opinion — very like the "musique concrete" of the past decade. I cannot say that I was moved by either work, but I was certainly disturbed enough to encourage their repetition.

"Improvisations" by the Gruppo Nuova Consonanza can perhaps best be described by a quotation from the sleeve annotations. "To unite composition and interpretation, which have hitherto always been separate functions in traditional European musical practice, in a simultaneous creative act, is the declared aim . . . of the group. The musicians alternate between various instruments in diverse formations . . A lively mind and personal modesty in all those taking part are absolutely vital if a group of composers are to work together successfully."

The "improvisations" are controlled by rehearsals of spontaneously produced sounds which are taped and afterward altered either directly or by the addition of new sounds. The notes go on to state that "all the pieces . . . are authentic 'life' improvisations which have not been edited." They originated in the Experimental Electronic Studio, Rome. The first piece is titled "E poi?" which translated means "And then?" or "After that?" and is, I think, used as a quotation from the concluding bars of Iago's "Credo" in Verdi's "Otello." The music consists for the most part of single notes delivered by different instruments, or alternatively, very brief phrases. The result often resembles the fragmentation of the Post-Webern school.

Another piece is called "Quasiraga" and is reminiscent of sitars played at impossible speed with stenographic clicking taking the place of the accompanying tabla. Indeed, it has a genuine raga effect in long, slowly increasing climaxes.

A third piece, "Light Music," according to the sleeve notes, receives its stimulus from jazz, though I found this difficult to detect.

"Ancora un Trio" consists of a very strange series of short notes produced by a trumpet, some of them sounding for all the world like hiccups. There is an occasional longer phrase not unlike something from Stravinsky's "sacre du Printemps."

A "Credo" begins with a sound like a large jet plane passing overhead and goes on to low growls. There are interjections by male speaking voices with here and there a phrase that sounds like Italian double talk. There is even a fragment of a march as it might be played by a village band. I can only say that there was nothing I either liked or admired in the whole recital, if it can be called that.

I found nothing to attract me in Kagel's "Hallelujah," either. And I found no enlightenment in the annotations which state that "Kagel's compositorial (sic) techiques are often secretly based on Jewish theology: musical analysis can occasionally trace analogies to, for instance, the 49 stages of meaning in the explanation of every place in the Torah as taught by talmudic tradition." It is a choral piece which opens with some rhythmic figures reminiscent of Stravinsky's "Les Noces" but soon introduces some cat-like miaowing and descending glissandi like expiring old men. A solo voice now and again uses the "speech-song" technique exploited by Schonberg in his "Pierrot Lunaire" but I found the whole exercise extremely depressing.

American John Cage is represented on one disc by his "Atlas Eclipticalis" for one to 98 orchestral players (86 possible parts) and his "Winter Music" for one to 20 pianists, To refer to the sleeve notes again "the parts of Atlas Eclipticalis are transcriptions of stellar constellations made legible in the form of notes. There is no score and thus no regulated combination of instruments: what is apparently intended is the cosmos as a model of anarchy. . . . The conductor accordingly has no commanding function but merely indicates the passing time. The musicians are to read the circular movements of his arms as rotating second-hands."

"Winter Music" consists of 20 pages which can be played by one pianist or distributed between two and 20. In the recording, five pianists play different pages simultaneously. I find it quite impossible to take such a travesty of music seriously. On the same disc, Schnebels "Glossolalia" (the medical term for the scriptural "speaking in tongues") has several voices speaking and muttering in German, their inflections rising and falling in pitch, sometimes in solo, sometimes together. There are a few shrieks, and groans, too, and it might be interesting if delivered in an English translation. I did catch one English phrase which goes: "After this cue beginning 20 seconds madly." This piece, too, offers nothing which, to me, can be described as music.

Bernd Zimmermann is given a disc to himself on which one work is a "ballet blanc" called "Presence" and the other "Intercommunication." The first is a trio for the classical combination of violin, cello and piano. The second a duo for cello and piano. The ballet has a plot which brings together the unlikely combination of Cervantes' "Don Quixote," Joyce's "Molly Bloom," and someone called "Roi Ubu," conceived by Alfred Jarry. Each character is represented by one of the three instruments and quotations from Strauss' "Don Quixote," Prokofieff's 7th Piano Sonata and Stockhausen's "Zeitmesse" are easily recognised by those who know the works, Between these stable points the music is, in comparison to most of the other pieces in the set.

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played by instruments whose tone can be immediately recognised. And much of it is what might be described as valid music, though of course, atonal and polyrhythmic. The quotations supply what might be called wayside stations in a journey into the unknown.

I found "Intercommunication" one of the most fascinating pieces in the whole set. Although the solo cello produces some unusual sounds in the way of timbres, I found myself not only interested but to some degree in sympathy with the strangely static mood of the whole piece. This, I am quite certain, I could grow to like.

The sixth and last disc — at present they cannot be bought separately but will be available in that form later this year — features more electronic music by Gottfried Konig which slides up and down, flutters and often sounds like an unoiled chaff-cutter. The first item is called "Terminus"; the second, "Green Function," is much the same, with the addition of a sound like a toneless alarm clock going off.

"Phonothese" is a little more musical and often has an attractive fragility. "Chants de Malador" has long periods of silence and almost inaudible sounds interrupted by great explosions of noise. One extraordinary effect sounds as though it was produced by a hail storm of steel ballbearings.

Well, there they are. And the listening to and writing about them has been one of the most onerous chores I have undertaken for a long time. But one compensation was the magnificent quality and engineering of the whole set.

*

*

MESSIAEN—Cinq Rechants, XENAKIS—Nuits.

PENDERECKI-Stabat Mater. Soloists of the French Radio and Television Choirs conducted by Marcel Couraud. Record Society Stereo S/6323.

Admirers of Messiaen -- and I add here that I am one, to indicate that I am not opposed to the whole of the avant garde movement—should have no difficulty with his contribution to this disc. It is written for 12 solo vocalists who sing some vague French phrases about Tristan and Isolda and other famous lovers interspersed with a strange language invented by Messiaen himself. Since the melodic line often has a strong Asian flavour, these weird words might be taken as imitating Hindu without the use of its actual vocabulary. But however odd this may read the result is indubitably musical and the third song in the cycle, a soprano vocalise over a hummed accompaniment, is as lovely as anything I have heard for many years. Messiaen wrote the sleeve notes, too, and these should go a long way to explaining to newcomers what the music is about and how it was conceived and constructed.

Xenakis, too, should need no introduction to anyone even interested in contemporary music. He has been much played in Australia during recent years and is fast growing in popularity among coterie audiences. His piece is dedicated to political prisoners in presentday Greece and evokes a nightmare picture of the terrors of a concentration camp, even to having yelping jackals prowling about outside. No praise



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Price (including sales tax) \$39.50



could be too high for the manner in which the singers present this inordinately difficult music which takes emotional tension to what must be close to the point of ultimate tolerance. The whole is a wonderful technical accomplishment by composer and performers.

Since Penderecki later incorporated his "Stabat Mater" into his great "St. Luke's Passion," it will be well known already to the many admirers of that exciting oratorio. The "Stabat Mater" consists of six strophes expressing alternately pain and faith in a manner that cannot fail to make an immediate impact on any sympathetic listener. Some of the music is in Gregorian form, some modelled on the later polyphonic school, and some half-spoken. All of it is eloquent and the recording and performance faultless.

* *

LULLY — Pieces de Symphonie. English Chamber Orchestra conducted by Raymond Leppard. Record Society S/6322.

Those who think of Lully only in terms of tinkling spinets will be surprised at what is on offer here. There are triumphal marches complete with trumpet trills on high notes, as brilliant as one could wish, though redolent at the same time of Louis XIV formality. There is an impressive Chaconne and some entrancing slumber pieces. Among the 18 pieces, most of them brief, you will recognise Lully as a greatly gifted melodist. He was also one of the founders of what has since developed into a modern symphony orchestra. His orchestration, though tending at times to be formal, sometimes sur-, prises with a remarkably subtle effect. Rhythmic sprightliness is not neglected (Air for Dancing from Bellerophon) nor humor either (Entrance of Polyphemus from Acis and Galatea).

The English Chamber Orchestra is admirably conducted from a mostly inaudible harpsichord by Raymond Leppard, but except for this I have nothing but praise for the whole production. Eminently pleasing.

WERDER — String Quartet No. 4; Music for Clarinet and String Quartet. Austral String Quartet. Donald Westlake (clarinet). EMI Stereo OASD7553.

Felix Werder was one of our first Australian contemporary composers to win recognition not only in Australia but also overseas. Indeed the string quartet on this disc was dedicated to the Pascal and taken with them back to Europe where it received performances over the French radio. By the way, the Pascal cut the work for their performances. The version offered here is one abridged by the composer in 1963. The work in its original form was finished in May, 1955.

Werder is not as way out as some of his slightly younger Australian contemporaries and I have long thought him to be a romantic at heart. However, he has managed to rid himself almost completely of romantic tendencies—not at all a fault in my mind. His music, even as early as the quartet, is characterised by the unbending logic of a Max Reger and it would not be difficult to imagine Reger writing similar music had he lived during the present period. And since Reger is today held in such little esteem, I hasten to add that I mean no disrespect to Werder by my com-parison. It must not be forgotten that Reger, like Werder, had his deeply lyrical moments.

The Music for Clarinet and Strings dates from as recently as 1965. Its chief interest to me centred on the eloquent playing of the clarinet part by Donald Westlake. Another feature I found quite entrancing is a scherzo of unusual delicacy from this fundamentally serious composer. The disc was produced by EMI (Australia) in association with the APRA Music Foundation and is a credit to all concerned in its making. It is well worth a place in the record library of anyone interested in contemporary music of the more accessible kind. Without having corre-sponded with Werder, I imagine he must be very happy about the way he has been served here.

* *

HAYDN - Cello Concerto in D Major.

MONN - Cello Concerto in G Minor. Jacqueline du Pre (cello) and the London Symphony Orchestra con-ducted by Sir John Barbirolli. E.M.I. Stereo OASD 2466.

I have enjoyed Miss du Pre's previous recordings so much —as well as her splendid TV biography — that I was really cast down with dis-appointment at this new release of hers. The Haydn has an absolutely lacklustre first movement in which the composer's line is pulled about inexcusably to suit the soloist. Admittedly the remaining movements are a little better but by no means what one would have expected from this artist. It would be a great pity if this un-usually gifted young cellist were to develop an idiosyncratic style to the detriment of the compositions she plays.

I met Monn's G Minor Concerto here for the first time and have little desire to renew its acquaintance. I thought I might have found some interest in the harpsichord continuo played by Australian Valda Aveling, especially as her part is based on one written by Schonberg. Alas, she was, as I wrote about Leppard in the Lully, hardly ever audible. I am afraid that I can find almost nothing to recommend about this disc.

*

ENGLISH MUSIC FOR STRINGS — Chacony in G Minor (Purcell); Introduction and Allegro (Elgar); Simple Symphony (Britten); Two Aquarelles (Delius); Sir Roger de Coverley (Bridge). English Chamber Orchestra conducted by Ben-jamin Britten. Decca Stereo Britten. Decca jamin SXLA6405.

This is a delightful recital. The English Chamber Orchestra is right at the head of all similar combinations and under Britten's impeccable direction is well-nigh incomparable. Britten has a well-nigh incomparable. Britten has a sure sense of style no matter what he conducts. He is stately in the Purcell "Chacony," warmly appreciative of the Edwardian comfort of Elgar's "Intro-duction and Allegro." Since the playing space on both sides is well filled, I suppose it was economically percessary to include these two pieces in necessary to include these two pieces in the same key on the one side. However, since all the bands are separated by

generous divisions there is nothing to prevent you playing the pieces in whatever order you like. At any rate my comment about the keys of these two works does not alter the fact that Britten's is, I think, the best perform-ance of the Elgar I have ever heard. The fact that he lingers rather more than is usual over the slow section serves only, in my opinion, to contrast the mood of the Allegro when he about the Elgar I must offer special thanks to the members of quarter who join the orchestra in this item.

On the reverse side is Britten's deli-cious Simple Symphony, based, by the way, on pieces he wrote as a child. Here, at a slightly later date, they are put together with every evidence of master craftsmanship. If you want to sample an example of the orchestra's superb playing, try the pizzicato Scherzo movement and pay attention to the constantly varying dynamics. The two Delius fragments were arranged by the composer's faithful amanuensis Eric Fenby. They are tender frag-ments and caressed with a lover's touch by Britten and his orchestra. The recital ends with a novelty — to me, at any rate — Frank Bridge's ingenious and exhilirating free fantasia on the old dance tune Sir Roger de Coverly. Don't miss this beautiful record.

In Brief . . .

MOZART — Symphonies Nos. 1, 2, 3, 4 and 5. London Philharmonic conducted by Erich Leinsdorf. World Record Club Stereo S/4637.

This disc has little to recommend it other than the interest it might provoke in works seldom or never heard in the concert hall. The symphonies themselves are of varying merit from move-ment to movement. The engineering is far from good and the playing coarse and sometimes downright impatient. Its club price is the only strong point in its favour.

* * MOZART — Symphony No. 31 (Paris). No. 35 (Haffner). No. 32 in G (K. 318). Stuttgart Classical Philharmonie conducted by Karl Munchinger. Decca Stereo SXL6402.

This, too, is not out of the top drawer. The orchestra, which is new to me, produces only a commonplace reading under Munchinger, notably in the ab-sence of any really pianissimo playing. This means a deadening lack of dynamic variation and a general atmosphere of monotony. These are not very early works, as are those reviewed on the previous disc, and are worthy of a much better performance. Sound is only average.

*

RAMIREZ — Misa Criolla; Seven South American Folk Songs. Los Huanca Hua. World Record Club Stereo S/4605.

*

I can recommend this disc warmly to all those in search of sane novelty. Although none of the voices is trained in the European sense of the word there is no doubting the fervour and expressiveness of the chorus. It is, in fact, a breathtaking choir. Occasional falsetto notes from male singers and the general rhythmic treatment give it all a strong South American flavour. The singers have an infallibly sense of pitch and phrasing. Without disrespect, I think it would be true to describe this exciting form of the Mass as a Mass for dancing. And this applies especially to the Gloria. The seven folk songs on the reverse side are all admirable examples of this art. Some of them sound unusually modern with the big beat and "Yeh, yeh, yeh" sound of pop music of the last decade. But I enjoyed every bar.

LOWE — Ballads. Fish-Dietrich c h e r-Dieskau (baritone); Jorg Demus (piano), Deutsche Grammaphon Stereo 139416.

*

The songs of this 19th century German romantic are seldom heard nowadays except for an occasional performance at vocal recitals. But they are all eminently pleasing, if sometimes a little sentimental. But Fischer-Dieskau's fine sense of style goes far to counteract this tendency. They range from the heroic to the humorous and except for a rare high note that seems to suggest tiredness are admirably sung and beautifully accompanied. Well worth the at-tention of lovers of the middle European romantic school.



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Interest: Australian choir, songs. Performance: Well done, lads! Quality: Clean, well balanced. Stereo: Normal.

Saint Augustine's College at Brookvale, N.S.W., is run by the Augustinian Fathers. The College Choir, which I would judge to number about 50 boys, provides an excellent example of what can be accomplished by careful trainging of a group of schoolchildren and this is undoubtedly one of the points of interest about the album.

Their performance is of such an order to have warranted instrumental support by George Golla on guitar, Reg Robinson on bass and Errol Scarlett on piano — a professional contribution that has added much to the final sound.

Of added interest is the fact that all the songs are the work of a 31-year-old Franciscan priest, Newcastle-born Father Leo Watt. Slanted somewhat towards folk-style, they describe episodes from the lives of well-known Bible characters: Moses, Jonah, Ruth, Elias, Job, Daniel, Joshua, David— actually twelve tracks in all, playing for about 30 minutes.

The music itself is bright and pleasant, in its class, but the words from fifty young throats don't fare quite as well. You can make out the themes provided you know them beforehand. But I imagine that most people, who would be interested in a record such as this, would have heard the stories many times.

In short, if the contents appeal, you can buy with confidence. (W.N.W.)

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* *

SUNDAY WITH THE KING FAMI-LY. With the Alvino Rey Orchestra conducted by Ralph Carmichael. Compatible stereo, Light Records LS-5514-LP. (Available from Sacred Productions Australia, 181 Clarence Street, Sydney, and other capitals). Interest: Gifted family group. Performance: First class

Performance: First class. Quality: Excellent. Stereo: Nicely spread.

For those who may need an introduction to "America's most beloved Chorus," the jacket carries a coded picture of the eight King brothers and sisters, grouped with their husbands, wives and children. Blessed with much more than the usual collective talent, the 39-strong group can perform as a full choir, or break up into smaller male, female, and mixed groups— with an odd solo or narration for extra measure.

On this album the various groupings are used to provide a variation in sound, complementing that provided, anyhow, by Ralph Carmichael's arrangements. The result is that, in a program which involves 22 familiar hymns, playing for 45 minutes or more, the sound does not become wearisome; perhaps we should add the phrase "to those who would normally buy this type of album."

As one might guess from the title, the hymns are those which one would expect to hear any Sunday in any one of the thousands of non-conformist churches throughout the world. Space does not permit their listing but, be assured, you'll know them.

A well-produced, generous program,

which will bring endless pleasure to those who enjoy the old hymns. (W.N.W.)

* *

THAT OLD TIME RELIGION. The 130-voice Amen Choir. Directed by John Gustafson. Arrangements by Ralph Carmichael. Compatible stereo, Light Records LS-5519-LP (From Sacred Recordings Australia, 181 Clarence Street, Sydney, and other capitals).

> Interest: Bright choral singing. Performance: Exhilarating. Quality: Clean, well balanced. Stereo: Beautifully spread.

In the field of sacred music, choirs are so numerous that they need to be better than merely good to make a reviewer sit up and take notice. This album did just that.

The choir is first rate, with such a well-blended, forward sound that it is hard to realise that it is 130 strong. The direction is good, the instrumental touches are well integrated and, back of it-all, the arrangements by Ralph Carmichael are outstanding.

Mind you, a program composed largely of Negro spirituals lends itself to musical development. The 12 track titles are: Old Time Religion — Stand By Me—What A Friend We Have In Jesus — Swing Down Chariot— Lead Me Gently Home— Down By The Riverside — Battle Hymn Of The Republic — One Of These Days— Just A Closer Walk— Near The Cross — Deep River — Bound For The Promised Land.

Clean, well-balanced sound and a playing time of 36 minutes round off an album which I would heartily recommend. (W.N.W.)

Instrumental, Vocal and Humour . . .

RIMSKY-KORSAKOV'S GREATEST HITS, Various orchestras and conductors, C.B.S. stereo SBR 235347,

> Interest: Tuneful classics. Performance: Mostly satisfactory.

Quality: Good sound, some tape hiss.

Stereo: Normal.

For those who follow these reviews regularly, I need only say that this latest release in the C.B.S. "Greatest Hits" series of famous composers is very much "the mixture as before." The orchestras are the same, the treatment is the same — the tunes are different. In this case, the producers had the advantage of being able to choose from the works of a composer whose gift for melody and orchestration are second to none. The results are a feast of glorious melody: The Flight of the Bumblebee — The Young Prince and the Young Princess from "Scheherzade"—Procession of the Nobles from "Mlada" — Hymn to the Sun from "Le Coq D'or — Dance of the Tumblers from "The Snow Maiden" — Song of India from "Sadko" — The Sea and Sinbad's Ship for "Scheherzade" — Canto Gitano and Fandango Asturiano from "Capriccio Espagnol."

The orchestra/conductor combinations are the Philadelphia/ Ormandy, The New York Philharmonic/Bernstein, and the Columbia Symphony/Kostelanetz — all excellent bodies of players. While I am not entirely happy about some aspects of the performances (I like the two pieces conducted by Kostelanetz to be rather more "dolce" for example) I feel there is little point in going too deeply into such matters. These discs will give considerable pleasure to those who are becoming interested in the classics, and I feel this is their main purpose. On the technical side, the sound quality is of good standard, but there is noticeable tape hiss in some tracks. (H.A.T.)

* *

PASTORAL SYMPHONY, No. 6 in F. (Beethoven). The Pittsburgh Symphony Orchestra, conducted by William Steinberg. Music For Pleasure, compatible stereo MFP-A9027.

> Interest: Economy classic. Performance: Satisfactory. Quality: Very good. Stereo: Normal.

For those seeking a cheap recording of Beethoven's popular "Pastoral" symphony, here is a perfectly respectable performance for \$1.99. Although presumably a few years old, the sound quality is of excellent standard. As for the performance, this may not please those who have certain views about how this work should go. Steinberg starts off rather fast, giving the impression that he has not entirely shaken off the habit of city bustle on his arrival in the country, but settles down to leisurely enjoyment in the slow movement, which is as calm and pastoral as one could wish. The bucolic festivities of the third movement are lively enough, the storm movement is appropriately noisy, and the shepherd's tune appropriately devotional. Good value. (H.A.T.)

SYMPHONIC POEMS. The Pines of Rome — The Fountains of Rome — The Birds. (Respighl.) The London Symphony Orchestra conducted by Istvan Kertesz. Decca (E.M.I.) stereo SXL 6401. Interest: Program music. Performance: Fine. Quality: Excellent. Stereo; Excellent.

*

The provision of Respighi's three most popular works on one disc represents excellent value for money, and as far as I know, it is the first time it has been done. It does entail a turnover in the middle of "The Birds" and although this is inconvenient, it is inevitable. This is a fine performance, in which the climaxes are brilliantly realised — in this respect, it is superior to the New Philharmonia/de Burgos recording reviewed recently. However, those who have already bought that recording need not feel too badly about it. In the slower section, the languishing beauty projected by the Philharmonia players is not realised to the same extent by the London Symphony. Whether you buy one or the other will depend, I imagine, in your preference for the fill items. Personally, I feel the "Birds" suite is a better fill than the Stravinsky pieces offered in the Philharmonia recording. (H.A.T.)

* * * MUSIC OF THE DANCE. Ballet Classics. Stereo, Calendar SR66-9663.

> Interest: As per title. Performance: Good, average. Quality: Clean but lacking somewhat in bass.

Stereo: Not outstanding.

From the Swiss Elite catalogue, this album comes in a decorative but singularly uninformative jacket listing the track titles only, but with no mention of the composer, the orchestra (or orchestras) featured, the conductor(s) or the venue. One can only guess that the orchestra is one or more of those featured frequently by Elite — the Viennese Promenade, or the Vienna National Opera Orchestra.

The bass is "wooden" rather than ponderous and the spread is not expansive but the sound is nevertheless quite clean and, at the Calendar price, will represent good value to those to whom the music appeals.

The excerpts featured are: Hungarian Dance No. 5 (Brahms) — Slavonic Dances No. 5 and 6 (Dvorak) — Ballet Music from "Coppelia" (Delibes) — Hungarian Dance No. 6 (Brahms) — Slavonic Dances No. 7 and 8 (Dvorak) — Ballet Music from "Carmen" (Bizet) — Polovtsian Dances from "Prince Igor" (Borodin-Korsakov-Glazounov).

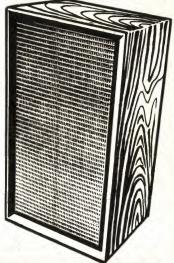
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Interest: Mainly non-classical. Performance: Pleasing style. Quality: Very good. Stereo: Normal.

The aim of Carmen Dragon for many years has apparently been to present fine melodies, whatever their origin, in full orchestral dress, presumably for the benefit of those who are not normally listeners to the classics. This second selection from earlier recordings illustrates this fact well, since no less than eight of the 12 tracks are arrangements of traditional and popular songs: All Through the Night — Jeannie with the Light Brown Hair — Home on the Range — Black is the Colour of My True Love's Hair — Lady of Spain — Rule Britannia — The Wide Missouri — America the Beautiful. The other four tracks are the ever popular Prelude to "Carmen"; the lively, and in America universally known, reel "Turkey in the Straw"; the dreamy Debussy number "En Bateau" which I cannot imagine anybody disliking, whatever their musical taste; and one of the finest of Italian traditional melodies, "Carnival of Venice."

It should not be too difficult for any prospective purchaser to make up their minds about the merits of this selection. If it suits your taste, the arrangements and performance are both highly competent, and the technical side is up to standard — clean sound, good stereo spread and silent surfaces on the review copy. (H.A.T.)

* *

ON THE BEAUTIFUL BLUE DAN-UBE. The New York Philharmonic Orchestra, conducted by Leonard Bernstein. C.B.S. stereo SBR 235339.

Interest: Strauss waltzes. Performance: Unconvincing. Quality: Excellent. Stereo: Normal.

Performances of Strauss waltzes, by large orchestras, and without cuts, are very much to my liking, and I am always glad to have for review a disc such as this, in which five of the most popular waltzes are presented in full orchestral dress—in fact, as Viennese tone poems. Side one has "Blue Danube" and "Emperor" waltzes; side 2 has "Vienna Blood," "Artist's Life" and "Voices of Spring." So far, so good but what of the performance.

Nobody will dispute the status of the New York Philharmonic and its present conductor, Leonard Bernstein, or deny that they are able to present very impressive performances of great orchestral works — but Johann Strauss! Hardly their cup of tea, I thought, when this disc arrived. The tautness which has been a notable feature of the orchestra's performances, and the driving energy of Bernstein's conducting, hardly seem suited to the relaxed atmosphere and gaiety of Strauss' music — and so it turned out. I was determined to approach this disc with an open mind, but with the best will in the world, I cannot approve this performance wholeheartedly. True, the standard of individual performers, the quality of tone, and the lush recorded sound leave nothing to be desired, but

the atmosphere achieved by the Vienna Philharmonic, for example, and the special lilt which they impart to the accompaniment, is missing. With so many competitive versions available, it is difficult to recommend this one. (H.A.T.)

- POMP AND CIRCUMSTANCE. New York Philharmonic conducted by Leonard Bernstein. C.B.S. stereo
 - SBR 235331. Interest: Orchestral marches. Performance: Appropriately rous-

ing.

Quality: Excellent. Stereo: Well spread.

I find the New York Philharmonic and Bernstein much better suited to the and bernstein much better suited to the type of rousing fare presented here. In addition to Elgar's "Pomp and Circum-stance March No. 1," from which the disc takes its title, there are: March of the Toreadors from "Carmen" (Bizet) — War March of the Priests from "Athalie" (Mendelssohn) — Fest March from "Carmen" (Menders) "Athalie" (Mendelssohn) — Fest March from "Tannhauser" (Wagner) — Coronation March from "The Prophets" (Meyerbeer) — Procession of the Sardars (Ippolitov-Ivanov) — Rakoczy March (Berlioz). This is extrovert music of the kind which Bernstein revels in and the orchestra obviously finds it

more to its taste than Strauss. The ormore to its taste than Strauss. The or-chestral tone is superb, and I must par-ticularly mention the cellos in the glorious second subject in the Elgar piece (the "Land of Hope and Glory" tune). The sound quality is of the high-est standard. (H.A.T.)

*

BATTLE OF BRITAIN. Original soundtrack recording. Music composed and conducted by Ron Goodwin. "Battle of the Air" composed by Sir William Walton and. conducted by Malcolm Arnold. United Artists (Festival) stereo SUAL-993.586. Available in mono. Interest: For filmgoers. Performance: Robust. Quality: Excellent. Stereo: Normal.

The producers of this film epic must have been disappointed that Sir William Walton could not be prevailed upon to write the whole score, with the result that the prolific Ron Goodwin got the task. Mr Goodwin churns out film scores the way Mozart churned out German Dances — to order, and delivery guaranteed before the date requir-ed. If the results are not memorable, the scores do what they are required to do. If they do not survive as works of art, well, they were not intended to be

Moog synthesizer — classics and rock

THE WELL TEMPERED SYNTHESI-ZER. More electronic perform-ances by Walter Carlos on the Moog Synthesizer. C.B.S. stereo SBR 235351.

> Interest: "Switched On" sequel. Performance: Fascinating. Quality: The best. Stereo: Excellent.

In view of the great success of "Switched on Bach" it was inevitable that there should be a sequel. Other companies have attempted to cash in on the interest generated by Walter Car-los' first Moog Synthesizer disc, and I have dutifully listened to some of them, but have had to report in lukewarm terms. Here I have no hesitation in resorting again to superlatives. Once again, Carlos has restricted his work to the baroque period, the music of which somehow sounds entirely appropriate when recreated in this medium. The music consists of four Scarlatti sonatas; the Fourth Brandenburg Concerto of Bach; the Bouree, Air and Allegro De-ciso form Handel's "Water Music", and two works by Monteverdi - "Orfeo" suite and "Domine Ad Adjuvandum."

Of these, the Scarlatti pieces came over the best. I thought the treatment brilliant, and touched with a real beauty. The Handel pieces, particularly the Air, seemed to me the weakest part of the disc. The Bach work is perhaps not quite so successful as in the first disc, but extremely interesting just the same. Of the Monteverdi pieces, the "Domine Ad Adjuvandum" is 'the more interesting, since Carlos has tried to create choral effects, which are slightly start-ling on first hearing, but entirely fascinating. A worthy sequel to the first success, which I feel sure will find al-most equal favour with those who found "Switched on Bach" an enjoyable experience. The sound quality is of the highest order, and the spread of sounds across the stereo spectrum add greatly to one's enjoyment. (H.A.T.)

SWITCHED-ON ROCK. The Moog Machine. Stereo, CBS SBP-233730.

Interest: Moog in another mood. Performance: Lots of know-how, skill

Quality: No "accidental" noise, or distortion.

As one of the older generation, I would not presume to pass judgment on this as rock in its own right, but I imagine that, beat notwithstanding, much of the sound will be too gimmicked to gain automatic acceptance by the top-40 crowd.

On the other hand, this very gim-mickry, both in the main theme and the sonic goings-on in the background will commend itself to those who are

partial to the psychedelic. "Switched-on Bach" went over well because it was framed on a familiar structure. So is this album, in the sense that the sound rests on a foundation of rhythm expertly laid down by Leon Rix on drums.

But drums or no drums, I must concede the industry, the patience, the skill and the inspiration under aseptic conditions - which allowed the rest of the team to build up the sound one finger at a time, adding it phrase by phrase to the 16-track tape.

I almost forgot the track titles: Spin-ning Wheel — Jumpin' Jack Flash — The 59th Street Bridge Song — Get Back — Yummy, Yummy, Yummy — The Weight — Time of the Season — Aquarius — Let The Sunshine In — You Keep Me Hangin' On — Hey Jude.

If you want an opposite number for your "Switched-on Bach," this could be it. Or maybe you just like the idea of helectronic hep! (W.N.W.)



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such. As for Walton's "Battle of the Air," this is perhaps not as outstanding as the same composer's "Spitfire Prelude and Fugue," but I suspect the two pieces will tend to become companion pieces in concert programs.

As with most film scores, the interest will lie mainly with those who want a souvenir of the film. (H.A.T.)

* * *

PEER GYNT Incidental Music. The Halle Orchestra conducted by Sir John Barbirolli, with Sheila Armstrong, soprano and the Ambrosian Singers. Studio 2 Stereo (E.M.I.) TWO269.

Interest: The complete music. Performance: Routine. Quality: Excellent. Stereo: Well spread.

This is not the usual "Peer Gynt" suites, but the (almost) complete score as written for Ibsen's play by Grieg, with only a few minor pieces left out. This requires a chorus (The Ambrosian Singers, in this case) and two sopranos. Here, Sheila Armstrong gives a pleasing performance of Solveig's music, and Patricia Clark sings Anitra's song during the Arabian Dance. Apart from Solveig's song, which to me always sounds so much better when sung, there does not appear to me to be much advantage in this version over the suites. There are some extra pieces (Overture, Norwegian Bridal Procession, and Solveig's Cradle Song) which are not found in the suites, but recent recordings of the suites have had some generous fills. There are no particular points of the performance which call for comment. The orchestra plays as competently as one would expect, the Ambrosian singers have only a minor role which allow them very little scope, and of the two singers, Sheila Armstrong sounds the m or e experienced and confident. (H.A.T.)

* * *

DON TWEEDY. Love Theme from "Romeo and Juliet" and other arrangements. United Artists (Festival) Stereo SUAL-933,518. Available in mono.

Interest: Film themes. Performance: Pleasing style. Quality: Excellent. Stereo: Good.

I gather that the only part played by the man with top billing on the sleeve is the arrangement of the tunes, but the uninformative waffle of the sleeve note doesn't give any enlightenment. What this disc actually offers is a selection of the theme tunes and songs from recent films. These are certainly competently arranged, and show some imaginative touches in some tracks. There is also an impressive line-up of names in the credits, where no less than nine musicians are credited as soloists. The main thing is that the music is very pleasant listening. The tunes are: Love Theme from "Romeo and Juliet" — Goodbye Columbus —100 Rifles — We, from "Me, Natalie" — Oliver — Southern Star — Ole Turkey Buzzard, from "Mackenna's Gold"—Jean, from "The Prime of Miss Jean Brodie" —The Windmills of Your Mind, from 'The Thomas Crown Affair" — The Night They Raided Minsky's — Hushabve Mountain — Love Theme from "Hannibal Brooks." (H.A.T.) ON WINGS OF OPERA. Regina Resnik, with the orchestra of the Royal Opera House, Covent Garden, conducted by Edward Downes. A Decca recording, released exclusively in Australia by World Record Club. Stereo S/4660. Interest: Opera arias. Performance: Magnificent. Quality: Excellent. Stereo: Normal.

Opera lovers who are members of World Record Club will be sure to give this disc a warm welcome. Discs featuring arias from operas have appeared only seldom in the W.R.C. programs in recent years. This disc has the outstanding artist Regina Resnik, now at the pinnacle of her career, with a pleasing selection of the most popular arias from Bizet's "Carmen" (Habanera — Seguidillas — Chanson Boheme — Carreau! Pique!), plus the following: Air des Adieux from "Jeanne D'Arc" (Tchaikowsky) — Softly Awakes My Heart, from "Samson et Dalila" (Saint Saens) — So Ist Es Den Aus from "Die Walkure" (Wagner) — Condotta Ell'era in Ceppi from "Il Trovatore" (Verdi) — O Don Fatale from "Don Carlos" (Verdi).

Madame Resnik is usually classified as a soprano, and I was surprised to find her apparently singing mezzo in this selection. Her rich-toned voice sounds particularly good in the "Carmen" arias, also in the "Dalila" aria, but there is not one track in which she does not sound entirely magnificent. The orchestra provides support of a high standard. (H.A.T.)

SONGS YOU LOVE. David Hughes, tenor, with orchestra or piano accompaniment, Music for Pleasure compatible stereo. MFP-A8072. Interest: Welsh tenor. Performance: See review. Quality: Excellent. Stereo: Normal.

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This program of very popular songs is sung by David Hughes with all the expression and sweetness of tone one expects from a Welsh tenor. However, he has a tendency to drift off pitch which the critical listener may find irritating. Apart from this (and let's face it, many listeners are unable to detect this type of fault), this is a very pleasing recital, comprising: Where'er You Walk (Handel) — Panis Angelicus (Franck) — Ave Maria — Angels Guard Thee — Silent Worship — The Lost Chord — I'll Walk Beside You — Absent — Faery Song — Drink To Me Only — Roses of Picardy. This is a modern recording, with excellent quality sound. (H.A.T.)

HELLO, PARIS. Petula Clark. Disque Vogue (Festival) Stereo.

*

Interest: P.C. sings French. Performance: Lively style. Quality: Some reservations. Stereo: Three channels.

Be a bit careful about this one if you are a Petula Clark fan, and you do not particularly care for foreign language songs. Although the song titles are clearly given in French, some people may not realise that Petula Clark is bi-lingual, and is equally at home in French as she is in English. On the other hand, if you enjoy French songs, as I do, you will find little to



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Play Bach Stereo Reissues

PLAY BACH Numbers 1, 2, 3, 4. Jacques Loussier, piano and organ; Pierre Michelot, double bass; Christian Garros, drums. London (E.M.I.) stereo. Numbers given below.

> Interest: Bach, modern style. Performance: Unique to this group.

Quality: Clean sound.

Stereo: Reprocessed.

The Jacques Loussier Trio are now so well known in consequence of their numerous recordings and personal ap-pearances (they were in Australia only last year) that it is presumably not necessary to explain what they are trying to achieve with their "modern inter-pretations" of the music of J. S. Bach. Sufficient to say that they have so successfully blended the baroque and jazz idioms that their performances have found favour with both classical music and jazz enthusiasts.

Their first discs (Play Bach One to Play Bach Four) were only available in They back roury were only available in mono, for some inexplicable reason. These present re-issues have been re-processed for stereo. The necessary filtering and rearrangement has been skilfully done and has menutation in the skilfully done, and has resulted in the piano being in the right channel with the bass and drums on the left--vir-tually two channel, with the middle left open. I do not imagine that those who already have these discs in the original mono are likely to be tempted to purchase these reissues for the dubious advantages of simulated stereo, but for the benefit of those who *****

complain about. Petula Clark's French accent is impeccable and she sounds as confident, lively and entirely enchanting as she does when singing in English. She has been very well recorded, so that every word she sings comes over as clear as a bell, but on the other hand, the background chorus which accompanies her sounds muffled and distorted. Personally, I do not think this matters one bit, since their con-tribution is not particularly important. The orchestral accompaniment has a strong beat in most tracks which should please younger listeners. (H.A.T.)

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THE BEST OF NINA AND FRED-ERICK. Columbia (E.M.I.) Stereo SCXO 6364.

Interest: Folk song duo. Performance: Fine entertainment.

*

Quality: Good throughout. Stereo: Varies.

Unlike many folk singers, Nina and Frederick have never set out to represent the social conscience by purveying the sentiments of "Protest songs." Instead, they have tried to be entertainers pure and simple, and in this they have Succeeded superbly. True, they do sing Pete Seeger's "Where Have All the Flowers Gone?" and Bob Dylan's "Blowin' in the Wind" in this selection, but one feels they are doing so more in sorrow than in anger. The rest of the songs here are mainly lighthearted numbers, reflecting the happy philoso-phy of this charming pair. Listen to the Ocean — Inch Worm — Little Donkey I Would Amor Her - Long Time

missed the first release, here is a brief rundown on the contents of each disc.

Number 1. SAHA 7751. Prelude 1 - Fugue 1 - Prelude 2 - Fugue 2 -Toccata - Prelude 8 - Prelude 5 -Fugue 5. The preludes and fugues are from the "Well-Tempered Clavier" set. The Toccata is from the well-known "Toccata and Fugue in D minor." Number 2. SAHA 7752. Partita No. 1 — Choral — Prelude 6—Aria—Pre-

lude 16 — Fugue 16 — Prelude 21. All six movements of the Partita are played, so that this work takes up the whole of Side 1. The Chorale is "Jesu, Joy of Man's Desiring," and the Aria is from Suite No. 3 in D, known popu-larly as "Air on the G String."

Number 3. SAHA 7753. Italian Concerto - Two Part Inventions Nos. 1, 2, 5, 18 and 15. Chromatic Fantasy in C minor. The Italian Concerto is possibly the most ambitious essay tackled by the group in these four discs, and has elaborate passages for all three.

Number 4. SAHA 7754. Overture Number 4. SAHA 7754. Overture from Cantata No. 28 — Choral No. 16 "Have Pity on Me, Oh Lord God" — Chorale No. 16 "Christ our Saviour is Come to Jordan" — Fantasy and Fugue in G minor — Choral No. 1, "Sleepers Awake." I found this the least interesting of the four discs. In the overture, Loussier plays organ as well as piano, and overdubbing is used to combine two instruments. This to combine two instruments. This seemed to me to spoil the unique character of the group's work.

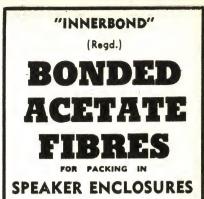
The sound in all four discs is clean, but lacks the immediacy of the best modern recordings, (H.A.T.)

Boy — Maladie D'Amour — Sippin' Cider — Little Boxes — Scarlet Rib-bons — Mary's Boy Child — Puff the Magic Dragon — Hole in the Bucket — Sucu Sucu — Baby It's Cold Out-side. The last-named is from the very successful Royal Albert Hall live performance reviewed on disc in these columns last year, and includes a hilarious send-up of the Oxford-accented Englishman as a lover. A thoroughly enjoy-able disc all through. (H.A.T.)

DONEGAL. DEAR OLD Bing Crosby (with chorus in some tracks) and orchestra. Calendar (Festival) mono only R66-621. Interest: Irish ballads. Performance: Suave and sentimental.

Quality: Good mono sound.

I remember Bing Crosby recording Irish songs long before the beginning of the L.P. era, but I imagine that this present selection, in good quality mono sound, comprises songs of early L.P. vintage, to judge by the very acceptable sound quality. Bing's suave voice is ideally suited to the type of sentimental ballad included here, The sentimental ballad included here, The Rose of Tralee—Dear Old Donegal— When Irish Eyes are Smiling—The Donovans—Danny Boy—The Isle of Innisfree—Galway Bay—How Can You Buy Killarney—I'll Take You Home Again Kathleen—Tobermory Bay—Where the River Shannon Flows—Did your Mother Come from Flows-Did your Mother Come from Ireland? Here is enough sentiment and nostalgia to suit even the most home-



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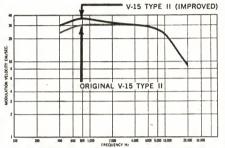
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* *

CHORALES AND CHORALE PRE-LUDES FOR ADVENT AND CHRISTMAS. King's College Choir, Cambridge; Andrew Davis, organ; David Willcocks, organ and conductor. A H.M.V. recording, released exclusively in Australia by World Record Club. Stereo S/4604.

but

Interest: See title. Performance: Lightweight, pleasing. Quality: Good standard.

Stereo: Normal.

+

An interesting approach has been made to the selection of Bach chorales included here. First, a choir sings a verse of the chorale to "familiarise the listener with the melody" and then the organ plays the Bach work built upon it. To a modern listener, these are masterpieces, but it is perhaps not surprising to find in the sleeve note that Bach was censured by some churchmen, who said that he had "made many strange tones with them, so that the congregation was confused thereby." Pearls before swine? Perhaps, but we should also remember that it is only recently that the music of Mahler has received any degree of acceptance.

Twelve chorales are presented: Wachet Auf—Nun Komm' der Heiden Heiland—Allein Gott in der Hoh' —Christum Wir Sollen Loben Schon— Her Christ, der Ein'ge Gottes-Sohn — Vom Himmel Hoch — Lobt Gott, Ihr Christen — Jesu Mein Freud — Der Tag, der Ist so Freudenreich — Wir. Christenleut' — Puer Natus in Bethlehem — In Dulci Jubilo. The famous King's College Choir, with its highly trained members, do not have much to do, but as always, they sing delightfully. The organ is a smallish sweet-toned affair, but no details are given of its stops and couplers. To judge by this rather lightweight performance, it has only limited resources. The interest in this case lies more with the music than with the organ, I feel. (H.A.T.)

*

THE BEST OF LAURINDO AL-MEIDO, Volume 2. Laurindo Almeido, guitar. Capitol Stereo SP 8696.

> Interest: Master guitarist. Performance: Splendid. Quality: Excellent. Stereo: Not significant.

Having extracted great enjoyment from Album 1, issued a few months back, I was delighted to receive this second album of Laurindo Almeido. Although quite different in content, this disc is, in its own way, possibly even better than the first — although 1 should point out to intending purchasers that the interest is rather more specialised. In Album 1, Almeido was presented in a selection of popular light classics, mostly non-Spanish. Here the selection is either of Spanish origin, or of recent works composed especially for guitar (including one item by Almeido himself). Another difference is

ELECTRONICS Australia, March, 1970

Apollo Mission

MAN ON THE MOON. Narrated by Walter Cronkite. Produced by CBS News. CBS, Mono. BP233712.

> Interest: The project documented. Performance: Well planned. Quality: Communications.

When I prepared to play this record, I had more or less assumed that it would be a straightforward recording of the Apollo 11 mission. And with all its momentous import, one had seen the original TV coverage and replays so often that the urge to listen to the sound wasn't all that great.

In fact, this latest Moon album, ex-pertly narrated by Walter Cronkite, embraces the whole of the U.S. space program which led up to Apollo 11. It recounts the early Soviet successes and the realisation that the U.S. was lagging in space rocket technology.

It records the personal plea of Dr

that here all pieces are played straight, with no over-dubbing such as one found in the first album.

Side one begins with some of the better known Spanish works: Malaguena and Tango in D (Albeniz); and Spanish Dances Nos. 5 and 10 (Granados). If you do not recognise them by the titles, you will certainly know the tunes when you hear them. From here on, the you near them. From here on, the pieces become more specialised and perhaps lesser known; Sacro Monte and Sevillana (Turin) — Tarantella (Cas-telnuovo-Tedesco) — Vals (Ponce) — Choro de Saudade (Barrios) — In-vention in Two Parts (Almeido) — En Los Tricles (Podrizo) — Brauda for Los Trigales (Rodrigo) — Prelude for Laurindo (Mancini) — La Coquette (George M. Smith).

Space does not permit individual notes on these pieces here, but each is described in the sleeve note, so that intending purchasers should make a point of reading the comments before pur-chasing, if in doubt about any of these numbers. In summary, I should say that this disc will be appreciated more by those who are able to appreciate the finer points of guitar playing, rather than those who appreciate the popular classics. (H.A.T.)

JOHN OGDEN PLAYS POPULAR LISZT. John Ogden, piano. His Master's Voice (E.M.I.) stereo OASD 2416.

Interest: See title.

Performance: Brilliantly executed. Quality: Excellent sound. Stereo: Not significant.

There is surely no need to explain the aims of this disc — however, I the aims of this disc — however, I question the inclusion of some of the pieces under the title "popular Liszt." Included here are: Etude d'execution transcendante apres Paganini — Huntranscendante apres Paganini — Hun-garian Rhapsody No. 15 in A minor (Rakoczy March) — Polonaise in E major—Two Concert Studies (a) Wald-rauschen (b) Gnomenreigen — Liebes-traume, (a) No. 1 in A flat, (b) No. 3 in A flat—Concert Study No. 3 in D flat (Un Sospiro)—Valse Oubliee No. 1 —Harmonies poetique at religieuse -Harmonies poetique et religieuse, No. 7, Funerailles. Even the sleeve note admits that the Polonaises were never popular, and personally I have

Werner Von Braun for a more ambitious approach to the space program, the recommendations of then Vice-President Johnson and the momentous announcement by President Kennedy of the target: Man on the moon in this decade.

The narration traces the evolution of unmanned and manned flights leading up to the Apollo program, itself punc-tuated by the tragic loss of three astronauts by fire.

And then the Apollo 11 mission it-self, with narration and explanation linking the actual highlights. Despite earlier reservations, to listen was to recall the tension of those historic moments, heard and seen around the world in real time.

This is a record with which I have not the slightest intention of parting. I think you'll feel the same way when you've heard it. (W.N.W.).

my doubts about some of the others. However, these comments should not be allowed to detract from the quali-ties of this recital. John Ogden is rapidly acquiring a reputation as one today. Not only does he have an assured technique, but also the ability to produce the kind of singing tone which makes his playing a joy to listen

He seems to be able to handle the most difficult passages in these very difficult pieces without strain. Yet despite this prodigious technique, he is not a flashy pianist — although here I would like to say that I did not enjoy his performance of the D flat study, which begins at white heat, and grad-ually subsides to the gentle reflective mood from which the piece has obtain-ed its name of "The Sigh." Others may find this approach perfectly valid, but I prefer the slightly melancholy, nostalgic approach favoured by most plantists. In general, however, this is a splendid re-cital, featuring virtually faultless play-ing, and with recorded sound of the highest quality. (H.A.T.)

THE SENTIMENTAL BLOKE, by C. J. Dennis. Read by Pe-O'Shaughnessy. ter Encore (E.M.I.). Mono only. OEX 9576. Interest: Australian verse epic. Performance: Sounds authentic. Quality: Adequate.

*

believe this reissue on E.M.I.'s \$2.50 Encore label to be the first low-price full recording of "The Sentimen-tal Bloke." This being so, there should tal Bloke." This being so, there should be many takers. I suppose most in-digenous Australians will know the C. J. Dennis epic, telling of the Bloke's courtship of the fair Doreen, his wed-ding, subsequent fall from grace and bitter repentance, and the birth of "the Kid." The tale is simple enough, but his earthy philosophising and ripe language earthy philosophising and ripe language have delighted several generations of Australians. It is to migrants, especially those from Britain, that I recommend this disc. There is a fair chance that they will never have heard of the Bloke, and I can promise them an enjoyable experience. Peter O'Shaugnessy's reading sounds

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authentic enough for the most part, and only occasionally his pronunciation al-lows the accents of the educated Australian to show through. If you have not yet acquired a recording of "The Sentimental Bloke" for your collection, it is an opportunity not to be missed. (H.A.T.)

Popular Jazz

"KING OF THE SAVOY" - CHICK WEBB (Volume II). Festival Jazz Series (Calendar) stereo Heritage SR66-9653 (also available in mono).

> Interest: Great band of the thirties. Performance: Very valuable and eniovable.

Quality: Well transferred.

Stereo: Electronically rechannelled.

This re-issue, on the \$2.95 Calendar label, represents the second volume by Chick Webb in Festival's Jazz Heritage Series. Like all the albums in this series the material is derived from the catalogues of American Decca. Volume One of the Chick Webb Band was reviewed in the December, 1969, issue. Although Volume One was the better

album musically, containing tracks from the period 1929 to 1936, this album is still most enjoyable. The earliest tracks date from the period when Ella Fitz-gerald's singing was becoming rather more important (commercially) than the band itself. Nevertheless, the Chick Webb Band was still resident in the Savoy Ballroom in Harlem during this period and its tremendous swing and appeal for dancers can be heard on the 14 tracks. Four Ella Fitzgerald vocals are included, "The Dipsy Doodle" and "Hallelujah" (1937), the famous "A-Tisket A-Tasket" (1938) and "Unde-cided" (1939). We also get some flag-waving drum work by Webb on arrangements like "Clap Hands," Liza" and "Harlem Congo." Although the ar-rangements are a shade less interesting than on the first volume, there are some wonderful moments from Sandy Williams, Bobby Stark, Taft Jordan and Ted McRae.

Stanley Dance's sleeve notes are of considerable interest and assistance, particularly to younger collectors who are unfamiliar with the music of the Chick Webb Band. Of the two Chick Webb L.P.s, I would recommend Vol-ume One before this L.P. but, given the lack of Webb material which is available at the present time, most big band collectors will certainly wish to purchase both volumes. (T.F.C.).

"KANSAS CITY PIANO" — Count Basie, Pete Johnson, Jay McShann, Mary Lou Williams. Festival Jazz Heritage Series (Ca-lendar) stereo SR66-9654. Also - Count available in mono.

Interest: Four great pianists, 1936-41.

Performance: Magnificent throughout. Quality: Well recorded and re-

mastered. Stereo: Electronically rechannelled.

As I said in my review of this album when it was originally released, "it has given me as much pleasure and musical satisfaction as any in the past year or so." In the 12 months since then, repeated playings of this album have merely served to enforce that first opinion.

The Basie tracks are, without doubt, minor jazz classics; and the tracks by Pete Johnson, Jay McShann and Mary Lou Williams are first-rate examples of the style of piano-playing which emerged from Kansas City in the late 1930s.

The Living Shakespeare

THE TAMING OF THE SHREW by William Shakespeare. With Peter O'Toole as Petruccio, and Sian Phillips as Kate. The Living Shakespeare series, issued by World Record Club. Mono.

Interest: Shakespeare "digest."

Performance: Excellent.

Quality: Good sound, quiet surfaces.

One's judgment of what is "good Shakespeare" can be coloured so much by what one has heard and seen before that it is hardly safe to offer criticism of individual performances. Actors strive for their own individual inter-Actors pretation of the roles they play, and if one has heard a particular performance of a play which gave special pleasure, the temptation exists to judge all other performances against this standard. For this reason, I will not attempt to comment on the individual performances here, beyond saying that the acting throughout is of a high order. Instead, I will deal with the aims of the Living Shakespeare series, and try to indicate the degree of success obtained.

The main aim is to present shortened versions of the major works of Shakespeare, using top-ranking actors. In editing, the intention has been to preserve

the story line, to maintain the interest, and to eliminate soliloquies and humorous sidelights which, while in-teresting in themselves, and even representing some of the glorious Shakes-peare verse, can be omitted without detriment to the plot. This has a similarity to the technique used in Reader's Digest Books, and the results are some-thing similar. The idea will appeal mainly to those who, for various reasons, do not want the complete versions of the plays (even assuming they were available. In the case of the present disc, the story line has certainly been maintained, but the editing leaves one with a slight feeling of breathlessness, as the plot rushes on from one situation to the other, without pause.

Where the series will be particularly valuable is in educational establishments, where students are being introduced to the great works of English literature. Adult readers interested in gaining an insight into the Shakespea-rean works, without wanting to get too deeply involved, will also find this series worth investigating. On the other hand, those who already know their Shakespeare, and want to listen to the plays occasionally, may not be entirely satisfied by these shortened perform-ances. (H.A.T.)

The Basie tracks, four of the ten which he recorded for Decca in 1938-39 with Freddie Green, Walter Page and Jo Jones, show him at the peak of his form. Aside from being the complete band pianist, Basie has one of the most satisfying solo piano styles in iazz.

Two of the three tracks by Mary Lou Williams were recorded in 1936 while her fascinating version of Mor-ton's "The Pearls" comes from a 1938 session. Her direct, down-to-earth ap-proach on "Overhand" and "Clean

(Continued on page 130)



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AUSTRALIA'S LOWEST PRICES



(Continued from page 127)

Pickin''' shows the influence of Earl Hines and the Kansas City boogie pianists.

Pete Johnson was, I think, the greatest boogie pianist of all. His four tracks come from one session in 1941 and they include the famous "Basement Boogie" and "Death Ray Boogie" in addition to "Just for You" and "Pete's Mixture."

Jay McShann was (and still is) a superb pianist, very much in the Basie mould. The three tracks (all written by himself) are "Vine St. Boogie," "Hold 'Em Hootie" and "So You Won't Jump" which were recorded in 1941. They are excellent examples of his solo piano and, in addition, they feature the splendid rhythm section of Gene Ramey and Gus Johnston.

I hope I have made it clear that this album is highly recommended—indeed indispensable. Nat Pierce's sleeve notes are suitably constructive and the album plays for 40 minutes. (T.F.C.)

* . . .

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"RARE ITEMS" — LOUIS ARM-STRONG. Festival Jazz Heritage Series. (Calendar) stereo SR66-965 (also available in mono).

Interest: Armstrong trumpet and vocals, late thirties.

Performance: Generally excellent. Quality: Bright recordings, well transferred.

Stereo: Electronically re-channelled.

This album is another of the Festival Jazz Heritage Series reissued on Calendar at the much more realistic price, \$2.95.

As I suggested in my original review of this album, I would be more than happy to argue that the majority of Armstrong's finest trumpet solos were recorded in the mid-thirties. Apart from some superb trumpet playing on every track, 11 of the 14 tracks contain splendidly typical Armstrong vocals.

This particular set, which was recorded between 1935 and 1944, is not quite the pick of his work in this period, but it is a most rewarding and enjoyable album. It should, I suggest, be played in conjunction with the Armstrong thirties' material which has been made available in Australia on the excellent Swaggie albums.

The backings, by what was substantially Luis Russell's Orchestra, are excellent and both Charlie Holmes and J. C. Higginbotham make occasional appearances for brief but very telling solos.

The pick of the tracks for me are "Thanks a Million" (1935), "Ev'ntide" and "Thankful" (1936) and "Jubilee," "Struttin' With Some Barbecue" and "It's Wonderful" (1938).

I care rather less for the three tracks made in the early forties, "Everything's Been Done Before," "Hey Lawdy Mama" and "Groovin" but the last named is a previously unissued 1944 recording.

Dan Morgenstern's sleeve-notes are sympathetic and helpful, but, unfortunately, full recording details are not given. The playing time is 41 minutes and, particularly at the bargain price of \$2.95, it should find a ready space in the shelves of any collector who is interested in Louis Armstrong. (T.F.C.)

TRADE REVIEWS AND RELEASES

ambient light conditions. The decoding and indicator tube driving circuitry is comprised of integrated circuits which give increased reliability and reduce the number of components considerably.

The display time is continuously variable from less than 0.1 sec. to at least 4 seconds or may be held indefinitely by switching to the hold position. The display may be reset by push button or external reset.

Data output is available from pins on the Display printed board in 8421 BCD code. Outputs are high impedance, unbuffered.

The TC11 may be operated from 45-60Hz AC mains supplies, having voltages from 100-125V or 200-250V. Power con-

ADVANCE I5MHz TIMER-COUNTER

The Advance Timer Counter TC11 is a recent addition to the range of digital instruments manufactured by Advance Electronics Ltd. It is intended for the measurement of frequencies up to at least 15MHz. Making extensive use of integrated circuits, the number of components has been reduced considerably from that of previous models while increasing the standard of performance.

Although the frequency range of the TC11 is quoted as 15MHz minimum, typical samples will function reliably well above this figure. The sample instrument we had for review operated reliably up to 20MHz. The exact figure would depend on the input amplitude. A three-position slide switch provides input sensitivities of 10mV. 100mV or 1V. The input impedance is 1 megohm shunted by 18pF, making it suitable for use with typical oscilloscope probes. The input is protected from damage against any likely overload. Two other inputs are provided for start and stop signals which are operative on time and count functions only.

The number of digits in a frequency measurement can be extended beyond the readout capability of four by taking two measurements, one to obtain the most significant digits and another to obtain further digits while overspilling the first significant digits. In this way, resolution down to 1Hz may be obtained but, for accuracy greater than one part in 100K, an external frequency standard must be used.

used. The major part of the circuitry, apart from the input amplifier, is accommodated on two printed boards measuring approximately 7 x $7\frac{1}{2}$ inches. The input amplifier contains nine discrete transistors and is accommodated on a small, shielded printed board adjacent to the input sockets and attenuator.

The upper board, which hinges out for convenient servicing. accommodates the timebase circuitry. The internal standard is 100KHz crystal oscillator in the Pierce configuration. It is set to within one part of 100K and typical stability is 3 parts in 100K for the range from 10 to 40 degrees Centigrade. The drive from the oscillator is fed via squaring circuitry to integrated circuit decades which divide the frequency down in stages of 10 to 1Hz, giving gating times from 0.1 millisecond to 1 second.

There is a check position in which the instrument counts its own clock signal over 1 second, giving a reading of 9999, 0000 or 0001 if everything is as it should be.

A jack is provided on the rear panel to enable an alternative time standard to be used. This may be a sinusoidal source at any frequency between 10KHz and 2MHz with an amplitude between 0.5V and 10V RMS or a suitable pulse source from 10Hz to 2MHz at 1V to 20V peak to peak.

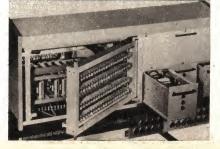
Frequency ranges are Hz, Hz x 10,



The Studio 2 audio mixer at GTV-9, Melbourne, supplied by Optronics Pty. Ltd. has 22 input channels, 12 being microphone inputs and 10 being high level inputs. Four of the high level inputs are fed via a 20-input 4-output electrically interlocked relax matrix. Two of the high level matrix channels enter the main mixing bus via equalisers which provide a 12dB/octave slope and a maximum boost or cut of 20dB. Four low frequency and three high frequency turn-over points can be selected by panel switches. The relay matrix is constructed on a double-sided printed circuit board of epoxy

The relay matrix is constructed on a double-sided printed circuit board of epoxy glass supported on a hinged aluminium U-channel frame. Operation of the matrix is via four rows of 20 illuminated push buttons. A fifth row of push buttons provides pre-fade facility, while a sixth row of lamps serves as cue indicators.

Four line level outputs are provided as





follows: Main, as primary program output; Auxiliary, as secondary isolated output; P.A., to feed public address facilities; Foldback, to feed foldback facilities to live performers. Dual main amplifiers are provided, with a manual front panel selector and illuminated indicator. Monitoring facilities are derived from 20 electrically interlocked push buttons. One input to this row is from a 24-position rotary selector. A 30W high-quality internal monitor amplifier feeds an external loudspeaker.

Dual, automatic changeover, power supplies are incorporated for no-break changeover if a power supply fault should occur. A front panel override key is provided. (Optronics Pty. Ltd., 62 Berkeley Street, Huntingdale, Vic. 3166.)



Hz x 100, KHz and KHz x 10. Multiple period measurements may be made from 10 to 100K selected in decade steps over a frequency range from 2Hz to at least 100KHz. Time period measurements may be made with ranges identical to that for multiple periods with single or two line operation between any of the three inputs. Similar provisions are made for event counting, the counting period being controlled by push-buttons on the front panel or external signals. The display consists of four neon

The display consists of four neon numerical indicator tubes behind a red tinted filter which results in bright clear display which is easily viewed under high sumption is 25 watts. External dimensions of the instruments are $11\frac{1}{2} \times 5\frac{1}{4} \times 9-7/8$ inches, weight is $10\frac{1}{2}$ lb and the case is finished in blue-grey vinyl-coated steel with a white front panel.

with a white front panel. Examined and tested in our laboratory the sample TC11 gave every indication of being a well-designed and reliable instrument. Its performance comfortably met the manufacturer's specification and it appears to be very good value for money at the price of \$360 plus tax. Australian distributors of Advance equipment are Jacoby, Mitchell and Co. Pty. Ltd., 469-475 Kent Street, Sydney, to whom all inquiries should be directed. (L.D.S.)



INSTRUCTIONS

Remove paper backing and place adhesive side downwards in the selected position. Press down firmly. When used with plain board drill from the 'Cir-Kit' side. Pass through component lead, bend over and cut to length. Solder in usual way.

to length. Solder in usual way. When used with 'punched' board lay strip between rows of holes, pass component leads through holes adjacent to strip, bend the leads over the strip, cut to length and solder in the usual way. Alternatively lay strip over the holes and using a drawing pin or scriber prick a hole in the 'Cir-Kit' in the required position.

position. "Cir-Kit' strip can be bent or curved to whatever form you require and used on either or both sides of the board. When joining two pieces of "Cir-Kit" bend over the end of the overlapping strip so that a metal to metal contact is made and solder in the unit way. the usual way.

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PRINTED BOARD ETCHING KIT

The Bishop Graphics printed board etching kit contains all the chemicals and most of the hardware needed to etch a printed wiring board. It is designed specifically for the small manufacturer specialising in "one off" products, or the laboratory which needs to make a "one off" board preparatory to quantity production.

There is a real need for such a system. There is a real need for such a system. A major problem confronting workshops and laboratories engaged mainly in developmental work—including our own at "Electronics Australia"—is that of pro-viding a "one off" printed wiring board on which a prototype of a proposed pro-ject may be built. There is obviously no point in organising for quantity produc-tion until the prototype has been tested, modified if necessary, and finally proved. While there are organisations who can provide a "one off" service—and who do it very well—ther are obvious advantages

practical experience in producing printed boards, has a good background in photo-graphy. Armed with the kit, the book of instructions, and a small negative from one of our previous projects, he set about

making a printed wiring board. Initially we set up a temporary dark-room in a windowless storeroom attached room in a windowless storeroom attached to our own laboratory which seemed to meet the requirements given in the in-structions. However, we soon realised the limitations of this arrangement and took advantage of a well equipped, air-condi-tioned darkroom attached to the quality



The complete board etching kit. Although only two packets of etchant are shown, six are supplied. The aluminium tray is used for the developer, which is a strong plastic solvent.

in being able to do this job on the spot, assuming the availability of a system which does not unduly tax existing facili-ties or call for more than ordinary care and skill. One of the main advantages is the saving of time, particularly that which is otherwise involved in transport of derivers the head moniforturer of drawings to the board manufacturer, the need to wait one's turn for a place on his production line, and the transport to return the finished board.

Because of this background we were Because of this background we were more than ordinarily interested in this kit. It is produced by Bishop Graphics Inc., U.S.A., and imported into Australia by Circuit Components (A/asia) Pty. Ltd. (formerly Craftsman Glass). The kit consists of an aerosol can of photo resist, a can of developer, six packets of etchant powder, a bottle of stripper (to remove resist from the finish-ed board), two trays, a contact printing

ed board), two trays, a contact printing frame, a quantity of copper clad epoxy laminated board, and an instruction book-let. The kit is designed with the intention that the user can spray a selected sheet of copper clad laminate, allow it to dry, ex-pose it to a suitable light source through a negative of the required pattern, develop a negative of the required pattern, develop the image by washing away the resist which has not been exposed to light, then remove the copper so exposed by means of the etching bath. The result should be a finished board, ready for drilling, in only a few hours. In order to test the system under what we felt would be reasonably typical condi-tions, we passed the kit over to one of our staff members who, while having no

control laboratory belonging to our parent company.

But even with these rather special facili-ties, we quickly discovered that the job called for a good deal more experience than was implied by the relatively simple and quite limited instructions given in the instruction manual.

instruction manual. In fact, our major criticism of the sys-tem is directed at the instruction manual. What is needed is a set of instructions which are sufficiently comprehensive and precise as to prevent the beginner from falling into the many traps which await him in this field. Such a manual should not only advise what not to do; it should advise what will happen if the wrong thing is done, thus allowing the user to recognise his mistake. The inadequacy of these instructions is

The inadequacy of these instructions is such as to make us seriously question the usefulness of the system as it stands. Any-one contemplating using the kit should be prepared for the inevitable failures in-

volved in "learning the hard way." For the benefit of such readers, here are For the benefit of such readers, here are some of the problems we encountered, together with what appears to be the solution as far as we can determine. In this regard we would point out that we used a whole can of photo-resist, a can of developer, and all the copper clad laminate (in approximately 2 in square sections) in the original kit, without mak-ing what we would call a perfect board. The best we achieved were a couple of rough efforts which could have been electrically usable. It was only after several more attempts that we produced a board which approached commercial qual-

board which approached commercial qual-ity. Cleaning the board: The instructions say: "Scrub with Ajax Cleanser and a stiff brush." Unfortunately, there is no way of knowing what this means in terms of the Australian market. There appears to be at least three Ajax cleaning preparations available here and no way of knowing which, if any, approximate the American product referred to. More importantly, it appears that the

More importantly, it appears that the term cleaning is an oversimplification of what is required. While it is true that all foreign matter must be removed, our own foreign matter must be removed, our own photo engraving department advise that the type of surface presented to the resist is important. A bright, shiny surface is not only not required, but is actually wrong. What is required is a planned degree of roughness, typically a "matt" finish, which will provide a "tooth" for the resist to grip. Otherwise there is a risk that the resist will lift under the action of the schemt of the etchant.

As nearly as we can determine Bon Ami powder or fine pumice powder would be near equivalents, and there may be some advantage in applying these with a Scotchbrite pad. However, working on a tip passed on to us by someone with many years' experience in the printed board industry, we tried a completely dif-ferent approach. The board is first cleaned in the true sense, using a solvent such as methylated spirit, and allowed to dry. Without touching the copper surface, it is then dropped in the etchant bath for about 3 minutes, which produces a fine matt surface. If there is a tendency to discolouration in patches, the board may be removed, rinsed with water, and return-ed to the bath to complete the prescribed period. period.

Drying the resist: The instructions say, "... place the board flat for air drying or in an oven at 110° to 120°F. ... For further processing the board must be completely dry, no tackiness, no solvent smell."

There are two problems which can arise at this point. The first is insufficient dry-ing. The "no tackiness no smell" instruc-tion is quite inadequate. A board can appear to satisfy these requirements, yet be still solvent under the dry skin which forms on the outside. When this happens, patches of resist whether acted upon by light or not, will lift under the action of the developer, leaving this portion of the board without any pattern. This situation is further complicated by what appears to be a change in sensitivity between the partially dry resist and a completely dry one. Thus, any exposure experience gained on incorrectly dried resist will be false, and this requirement will have to be re-learned. The second problem is the reverse of There are two problems which can arise

The second problem is the reverse of the first. If, in an effort to ensure com-

The second problem is the reverse of the first. If, in an effort to ensure com-plete drying, oven drying is too prolonged, or at too high a temperature, the resist appears to fog, exactly as if it had been exposed to light. The result is inability to develop any significant image. From our own experience we would recommend either air drying overnight or oven dry-ing at 120°F for three hours. The latter assumes the availability of a light-tight, thermostatically controlled oven. **Baking after development:** No mention is made of this in the instruction manual, yet it appears to be standard practice in both the printed board and photo-engrav-ing industry. The problem at which it is aimed is that of failure of the resist in the etching bath. Our chief chemist, in charge of the laboratory, suggested that we could toughen the resist by baking the board after development but before etching. The exact time and temperature are not critical provided that the tem. the board after development but before etching. The exact time and temperature are not critical, provided that the tem-perature is not high enough to damage the base material. To date we have worked on the basis of several hours at 200°F. However, it may well be that this time could be shortened.

Etching: The instructions suggest that the etching bath should be of such a

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strength, temperature, etc., that the etch-ing is complete in 45 minutes to one hour. And on this basis they claim that one packet of etchant should be sufficient for up to 25 square inches of board. This may well be true, but the point is that our own experience, and all the advice we could gather from the industry, sug-gests that the faster the etch the finer the detail that can be reproduced. This requirement appears to involve the prob-lem of undercutting. Most commercial organisations appear to aim for an etchlem of undercutting. Most commercial organisations appear to aim for an etch-ing time of 10 to 15 minutes, with a few special systems as short as 5 minutes and

special systems as short as 5 minutes and capable of resolving extremely fine detail. The best board we produced, and which approached commercial quality, was etched in 12 minutes in a freshly pre-pared etchant solution. Even though the board amounted to no more than 4 square inches an attempt to process a second board amounted to no more than 4 square inches, an attempt to process a second board of the same size in the same solu-tion was a failure. On this basis the cost of the etchant would appear to be un-realistically high. We are hoping to try one of the cheaper etchants, based on ferric chloride, but time has not permitted this so far.

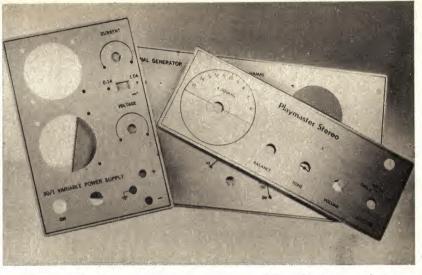
this so far. At the risk of labouring the point, we would emphasise again the need for a fast etch. A prolonged etch can produce an effect very similar to that resulting from breakdown of the resist by the etchant; at best it results in a rough looketchant; at best it results in a rough look-ing pattern, in which less relevant infor-mation, such as a type number, may have been lost. At worst, it results in a board in which vital parts of the pattern have been lost, rendering it virtually worthless. Apart from low activity of the etchant, we have no doubt that the system we tried is chemically sound. But, if you feel inclined to experiment along these lines be aware that the production of successful boards involves a lot more skill and ex-perience than the instruction booklet would have you believe. If you have suf-

perience than the instruction booklet would have you believe. If you have suf-ficient need for such a system, and can justify the time needed to gain this skill and experience, then go ahead. If not, think carefully before you invest. The materials are available either as a complete kit, or separately as individual items. Thus, a customer may replenish his kit as individual items run out or, where he already has most of the hardware available, purchase only the chemicals. Further details, price structure, etc., may be obtained from Circuit Components (A/Asia) Pty. Ltd., 460 Bexley Road, Bexley, N.S.W. 2207. (P.G.W.)

TRADE RELEASES -- in brief

WARBURTON FRANKI LTD., 372 Eastern Valley Way, Chatswood, N.S.W. 2067. Agents for Go-Power Systems, U.S.A. Low-cost small engine dyna-mometer. Developed for engines from HP to 60HP, and weighing only 35lb. Engine rpm and torque are measured to an accuracy of 1.5 per cent, from which the horsepower can be determined. The dynamometer uses a water brake to which the horsepower can be determined. The dynamometer uses a water brake to absorb the engine power and change the rotating torque of the engine to a station-ary torque that is measured by a pre-cision hydraulic load cell. The engine rpm is measured by a mechanical tachometer. A knob on the control con-sole regulates the engine load, while an-other knob adjusts the engine throttle between 0 and 100 per cent. between 0 and 100 per cent.

EXPERSION & CUMING INC., Canton, Mass. 02021, U.S.A. Eccosorb CV. A series of versatile broadband absorbers which can be used from 400MHz to over 100GHz. Six types in the series have thicknesses ranging from 3 to 18 inches. All members have reflectivities over 25-GHz of better than 50dB down on total reflection. Features include: effective at in-cidence angles to 70 degrees; rugged flexible foam construction; light weight — 0.71b/sq. ft. for thinnest type, 41b/sq. ft. for thickest; available in a weatherproof version. resion.



Illustrated is a selection from the wide range of "Oxford" front panels for Playmaster projects available from Heating Systems Pty. Ltd., 19 The Boulevarde, Caringbah, N.S.W., 2229. The panels are brushed aluminium with etched lettering, lacquered finish. Heating Systems has been a sup-plier of metalwork for "Electronics Australia" projects for many years, and has produced metalwork for virtually all of these.

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33/DEL70

University

T.V.T. VALVE TESTER



Due to the demand for the model T.V.T. Valve Tester, "University" have re-introduced the unit and it is now available from University Graham Instruments Pty. Ltd., or representatives in all States. This fine instrument can be used as a portable or counter type Valve Tester. It is designed to operate from 240 volts A.C. and has provision for testing radio valves as well as T.V. valves. An important feature of the model T.V.T. is that all the elements in a valve are brought out to in-dividual lever switches. This allows for great flexibility and also provides for valves which may have unusual connections or unusual sockets. It makes it possible to apply filament voltage to any base pin. The model T.V.T. incorporates the University model W4 all polystyrene meter with multi-coloured scale. The scale is marked "Good"—"Bad" so that quick and rapid indication of the condition of the valve under test is given.

test is given. The case is fitted with a carrying handle which lies flat when not in use, and a comprehensive instruction

booklet listing valve test settings is provided.

The outside dimensions of the unit are 14" x 11" x 6".

Valve Tester Price \$88.00 each, plus 15 per cent Sales Tax Also available is a Picture Tube Adaptor model T.V.2. This allows for testing television picture tubes without the necessity of removing the tube from the television receiver.

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Modei N.F., 1012 STENTORIAN SPEAKER 10in Unit 12,000 galas magnet. Universal impedance speech coli at 3, 7.5 and 15 ohms, Capacity 10 watts. Frequency response 30 c.p.s. to 14,000 c.p.s. Bass resonance 35 c.p.s. \$14 (including Sales Tax).

15in BASS GUITAR ELECTRONIC ORGAN SPEAKER This superb 15in unit is available with 8 ohm or 15 ohm Volce Coll, Power handling 30 watts R.M.S. 60. watts (peak). Frequency response to 500 cycles. Resonant frequency 60 plus or minus 12 cycles. Sensitivity 103 plus or minus 2 db/watt. Total flux 11.600 Maxwell. Flux density 9.360 gauss. \$30 Including Sales Tax POSTAGE FREE Anywhere in

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Model T.10 STENTORIAN TWEETER Speech Coli is aluminium wire wound on an aluminium former rigidly fixed to an aluminium diaphragm. giving high standard of reproduction when used with Stennorian H.F. 1016 speakers. Speech coli impedance 15 ohms. Response 200/15,000 c.p.s. flux density. 14,000 gauss. Capacity: 5 watts. \$16.00 (including Sales Tax).

CX 3000 CROSSOVER NETWORK W./B. Crossover is of the filter type and is fitted to all the Duplex Loudspeakers. It is available for use separately, the 3,000 c./s. type is haif section series connected having an attenuation of 12dB per octave. CX 3000. \$6.50 (including Sales Tax). T359 TWEETER

3,000-15,000 c.p.s, Size overall 312in diam. x 2in deep. Voice coli Impedance 15 ohms. \$6.50 (including Sales Tax). (All Post Free In Australia.)



ELECTRONICS Australia, March, 1970

UNIVERSITY LABORATORIES, 733 Allston Way, Berkeley, Calif. 94710, U.S.A. Continuous He-Ne gas lasers, models 351 and 361. Features include: CW outputs of 3mW and 4mW (respec-tively) of coherent visible red light (6328 Anostroms), that control hearn ediustment Angstroms); theta-control beam adjustment allows beam angle to be changed by plus or minus two degrees in any direction without changing the beam centre; Laser-tron tube with permanently aligned hemi-spherical internal mirrors in a coaxial pyrex envelope; separate solid-state power supply.

HEWLETT-PACKARD AUSTRALIA PTY. LTD., 22-26 Weir Street, Glen Iris, Vic. 3147. Hybrid hot-carrier diodes. Prices have been cut by up to 25 per cent on quantity orders. These diodes have the HF performance of point-con-tact diodes but with much higher reverse breakdown voltages. They have the high temperature chacteristics of silicon but the turn-on voltage is low (410mV at 1mA) as for germanium. They have fast recovery as for Schottky-barrier diodes, but are also rugged like PN junction diodes.

IRH COMPONENTS PTY. LTD., The Crescent, Kingsgrove, N.S.W. 2208 Rotary volume control switch, type 320. Features include: Rated at 250V 3A 0.75 power factor (inductive); moulded mela-mine cover with internal flash barrier between switch poles; life expectancy exceeds



25,000 actuations; low voltage DC rating of 12V 10A; contact resistance less than 5 milliohms after 50,000 actuations; avail-able in four configurations — SPST nor-mally open, SPST normally closed, SPDT and DPST; combined with IRH-patented converter unit it become a convert converter unit, it becomes a compact in-line push-push switch in same configurations.

DISTRIBUTORS CORPORATION PTY. LTD., 24 Johnston Street, Fitzroy, Vic. 3065. Agents for Master Instruments. Decade resistance boxes. Feature switches with sterling silver contacts and decades each with five resistors to reduce capacitance and residual resistance. Each decade is a self-contained integral unit, inter-connected with copper strips to adjoining decades. The switch layout used eliminates wiring completely and reduces capacitance and residual resistance to a minimum. A



2oz copper clad epoxy board contains the circuit on one side and a series of 20 con-tacts on the other, with moving contacts of fine silver riveted and soldered to a copper ring. Contact resistance is of the order of 400 uohms with a repeatability of plus or minus 100 uohms. Overall accura-cy is .05 per cent plus or minus .002 ohm. Resistors from 0.1 to 10 ohms are wound with Manganin wire, and 100 ohms and above are wound with Karma wire. They are of the flat card type to minimise in-ductance. ductance.

Lamp-signalling Telephones

AMALGAMATED WIRELESS (A'SIA) LTD., 47 York Street, Sydney, 2000, has re-ceived an order from the Postmaster-Genceived an order from the Postmaster-Gen-eral's Department worth nearly \$1 million for lamp-signalling tele-phones of the type illus-trated. This phone was designed in Germany, but A.W.A. is to manu-facture them in Aus-tralia under licence. It facture them in Aus-tralia under licence. It is intended to operate mainly in small office systems, with incoming calls normally taken at calls normally taken at one point and then routed to its destina-tion. Direct connection to up to 10 internal phones is obtained by pushing one of the 10 buttons in the two front rows.



Each phone has access to four exchange lines, which can be selected by pushing one of the four dark (red) buttons in the rear row. The user can dial directly into the public network, and all sets are equipped for "hold" or "call-back" during

RCA LTD., 11 Khartoum Road, North Ryde, N.S.W. 2113. Electronic teaching devices. All solid-state training aids to prodevices. All solid-state training aids to pro-vide a means of converting text-book theory to practical reality. Complete with a comprehensive instruction manual, the trainers present a progressive sequence of experiments and tests to take a student logically through his program. The first three units are: Digital computer logic systems trainer, model 1600-DCS. A labo-ratory trainer designed to enable students

external calls. Lamps under the push-buttons light up to indicate an engaged exchange line. Signalling is by means of a soft-toned buzzer for internal calls, but by flashing light behind the appropriate push button for exchange line calls. A call is accepted by pushing the button illuminated by the flashing light.

to construct and operate logic configura-tions basic to digital computers. Digital computer logic systems demonstrator, model 1700-DCS. Electrically identical to the 1600-DCS but oversized and mounted vertically for demonstration purposes. Basic electronic components trainer, model 702-FD. A compact durable, completely self-contained device that provides all components and power inputs required to enable students to perform a wide range of basic experiments.

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ELECTRONICS Australia, March, 1970



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(2)

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OBE BAR GENERATOR

2.)

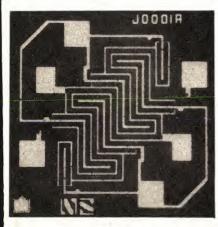


Mr Tan (left), sales engineer in Malay-sia for Philips Telecommunications of Australia, discusses a new project with export manager, Mr K. J. Horan, during a recent visit to the company's South Australian factory. Mr Tan spent about a month in Australia to familiarise him-self with the comwith the company's products and policies.

CONTROLS SSOCIATED PTY. LTD., 14 Enterprise Avenue, Padstow, N.S.W. 2211. Elmaset precision made card frames and cabinets. For printed circuit cards and inodular units of many differ-ent sizes and kinds. All structural parts of the system are provided with slots or ent sizes and kinds. All structural parts of the system are provided with slots or tapped holes to allow rapid and simple subdivision of units into almost any required size. The principle material is a light alloy with high corrosion resistance. The range includes all other necessary small components such as screws, nuts, washers, spacers, etc.

NATIONAL SEMICONDUCTOR CORPORATION (represented in Australia by Rutherford Electronics) has moved its world headquarters facility to 2900 Semi-conductor Drive, Santa Clara, Calif. conductor D 95051, U.S.A.

RUTHERFORD ELECTRONICS PTY. LTD., P.O. Box 30, North Balwyn, Vic., 3104. Agents for National Semiconductor Corporation, U.S.A. Monolithic, N-channel, dual FETs, series FM3954. Eliminates the difficulties in matching and testing individual die by integrating both transistors on one chip. The geometries of both FETs are intertwined to obtain a per-fect match (as illustrated). Features in-



clude: very close tracking regardless of bias point from 50uA to 500uA; low leakbias point from SouA to S00UA; low leak-age of 100pA; and high gain of 1000umhos. Applications include: bal-anced modulators and mixers; analog switching; multiplexers; AGC; RF appli-cations to 30MHz; high slew rate operational amplifiers.

THE AUSTRALIAN TELE-COMMUNICATIONS DEVELOPMENT ASSOCIATION has re-elected Sir Samuel Jones as chairman for a third term. Sir Jones as chairman for a unity term, on Samuel is chairman and managing director of Standard Telephones and Cables Pty. Ltd. The Association has added 11 com-panies to its membership and now com-prises 49 firms engaged in teleprises 49 firms engaged in tele-communications, electronics and related manufactures. The new member companies are: Electronic Industries Ltd., Elmaco Industries Ltd., Hewlett-Packard Australia Pty. Ltd., Hills Industries Ltd., Jacoby Mitchell Holdings Ltd., Nylex Corporation Ltd. (cables division), Radio Corporation Pty. Ltd., RCA Ltd., Servex Electrical Co. Pty. Ltd., Union Carbide Australia Ltd., and Weston Electronics Pty. Ltd.

MOTOROLA INC., Phoenix, Arizona, U.S.A., has formed an Australian semicon-ductor company, Motorola Semiconductor Products Group. The

new firm, located at Regent House, 37-43 Alexander Street, 43 Alexander Street, Crows Nest, N.S.W. 2065, is a branch of Motorola Australia Pty. Ltd., a sub-sidiary of the parent: corporation. Named to head the new organisation as marketing manager is John Dunleavy, formerly Motorola's regional manager for semi-conductor sales in Scandinavia, The local company will com plement the afforts of Cannon Electric



plement the efforts of Cannon Electric (Australia) Pty. Ltd., Motorola's franchised semiconductor distributor with offices in Melbourne, Sydney and Adelaide.

PLESSEY TELECOMMUNICATIONS PTY. LTD. has appointed Mr V. St. G. Magnusson — the former deputy assistant director-general, postal engineering, of the Postmaster-General's Department — as a consultant. Mr Magnusson, who has re-tired from the P.M.G.'s Department, took part in the initiation and launching of the Sydney Mail Exchange, and developed the present philosophy of mail flow and the modern concept of the machine system for the handling of large volumes of mail. He is a senior member of the Institution of Radio and Electronic Engineers (Australia).

AD. AURIEMA INC., the U.S. princi-pal of Auriema A'sia Pty. Ltd., has moved to 120 Liberty Street, New York, N.Y. 10006, U.S.A.

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International Correspon Dpt. 527, Division of Electro 400 Pacific Highway, Crows Branches in all States and N	nics, Nest, N.S.W. 2065.

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TECHNICAL BOOKS AND PUBLICATIONS

Transistor data

TRANSISTOREN - Transistor interchangeability tables. Published by De Muiderkring N.V., Bussum, Netherlands, 1969. Plastic covers, 3[‡]in x 5[‡]in, 192 pages. Price in Australia \$2 plus 20c postage.

An earlier edition was reviewed in our December, 1967, issue. This edition is basically the same as the earlier one, and the comments made are still applicable. For the benefit of new readers and those who may have missed the earlier review, we present again our original comments substantially as they appeared then:

"A useful publication for those who are cutting their teeth on transistors, and particularly for those of the amateur radio fraternity. As one might ex-pect, it is particularly good in its cov-erage of European transistor types. It also gives a reasonable number of American and Japanese types, although not nearly as many as one would like in a 1969 publication of this type. Even so, it would make a valuable addition to the amateur's reference shelf or to the service library, more so in view of its modest cost."

Our review copy was supplied by Technical Book and Magazine Co. Pty. Ltd., 289-299 Swanson Street, Mel-bourne, Vic. 3000, from whom copies are available ex-stock. (J.H.)

Transistor practice

SEMICONDUCTORS FROM A TO Z, by Phillip Dahlen. Published by Tab Books, Blue Ridge Summit, Pennsylvania, 1969. Soft covers and hardbound, 5½in x 8½in, 272 pp., many photographs and diagrams. Price in Australia \$6.15 and \$9.95.

As the author explains in his preface, this book has been adapted from a series of articles written for and pub-lished in the U.S. magazine "Electronic Technician/Dealer." The name of the journal concerned gives a strong indi-cation of the type of reader for whom the book was written: the service technician.

One might expect such a book to be rather practical in its approach, and this certainly is the case. In fact this reviewer considers that "pragmatic" would probably be a more appropriate description. The book plunges straight into the practical operation of bipolar transistor circuits, and then proceeds in almost cavalier fashion through FETs, tunnel diodes, integrated microthrough circuits (ICs), varicaps and miscellaneous devices and applications.

Author Dahlen makes no apology for this approach, supporting it by the statement that the average service technician need not concern himself with the actual theory of operation of semi-

conductor devices. However, while this is undoubtedly true to a certain extent, surely most service technicians need at least a basic insight into device operation in order to troubleshoot solid-state circuitry efficiently and effectively. One does not have to have a Ph.D. in solid state physics, to be sure, but without the basic concepts progress is rather painful and one's fumbling, as many service technicians have found and are still finding.

As it is, the present book merely seems to add yet another volume to the already appreciable number of "practical" books on semiconductors which either assume a pre-existing background of basic theory, or else decide as author Dahlen has, that such a background is not really necessary. It is up-to-date, to be sure, dealing with recent devices and their applications, and thus it may be of interest to those already possessing a basic background. But for those without such a background it will really not be of all that much value.

The review copy came from the Australian representatives for Tab Books, who are Grenville Publishing Company. By the time this review appears, copies should be available from all comprehensive book stores. (J.R.)

DX information WORLD RADIO AND TELEVISION HANDBOOK, 24th edition, 1970. Published in Denmark by J. Frost Paper covers, size 9in x 6in, 400 pages. Price on application to

booksellers.

This annual comprehensive guide to the world's medium-wave, short-wave and television stations again reaches a new pinnacle of usefulness to DX listeners, as it is virtually impossible to criticise the contents and layout, and it is safe to assume that the high standard of accuracy of past issues has been maintained in this 24th edition.

Critics of past editions have complained of small type and too many ar-ticles of a general nature on radio re-ception. This year, larger type has been used, and most of the hobby-type arti-cles have been omitted, as they have been accommodated in a new publica-tion devoted to the DX hobby, entitled "How to Listen to the World." The leading articles for this edition are entitled: How to use the Handbook — Satellites in the 70s—Radio Australia's Darwin Relay - Broadcasting reception expected during 1970. Then fol-lows the usual listings of world time in all countries, Time and Frequency Stations, DX Clubs of the World and A11 DX programs.

However, the real heart of the book However, the real near of the continents is the complete listing by continents and countries of station details, ad-dresses. schedules, frequencies, lan-

guages broadcast, verification policy. and other useful information. This is followed by another list, in order of frequency, of medium and short wave stations, for cross reference purposes. In my DX activities, I find the Handbook invaluable to identify stations not previously heard and not noted in any of the DX magazines. When the station is located in the Handbook, all the necessary details are there to enable the user to send a report to the station. Listings cover over 11,300 mediumwave stations, including over 4,000 operating in North America; and some 4,050 short-wave stations.

The editor takes a deep personal interest in ensuring the accuracy of the handbook. He has visited most of Europe's broadcasting stations to make personal contact with the engineering staff, with the result that he obtains up-to-date and detailed information on programs, frequencies and schedules.

"World Radio Handbook" should be in the hands of every radio listener who wishes to tune stations beyond his own. shores. As a professional monitor my-self, I found that the Handbook is used on numerous occasions every day. It is available from technical booksellers throughout Australia, and in New Zea-land from Arthur Cushen, 212 Earn Street, Invercargill. (A. Cushen.)

Network analysis

NETWORK COMPUTER ANALYSIS, Edited by George W. Zobrist. Published by Macdonald and Co. Ltd., London, and Boston Technical Publishers, Inc., Cambridge, Massachusetts, 1969. Hard Massachusetts, 1969. Hard covers, 10in x 7in, 303 pp., many diagrams. Price in U.K. £10.

As the title of this book is a little ambiguous, I should perhaps begin this notice by explaining that it deals not with the analysis of computer networks, but with the application of digital computers to the analysis, design and modelling of electronic cir-cuits. In other words, it is concerned with those activities often grouped under the heading "computer-aided design" or "CAD."

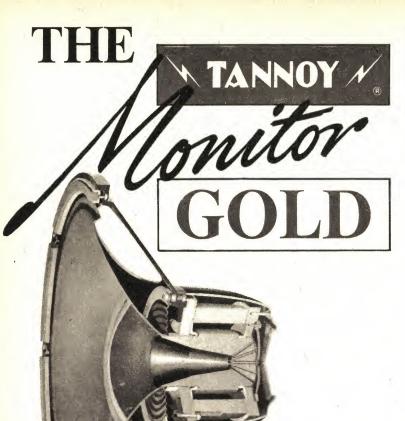
The material presented is apparently based on seminar lectures presented at the University of Missouri in 1967 by some of the leading authorities in this field. Most of it deals with four of the major network analysis programs which have been evolved, known respectively by the acronyms ECAP, NASAP, NET-1 and SCEPTRE.

As those familiar with CAD tech-

SENIOR TECHNICAL OFFICER UNIVERSITY OF MELBOURNE, DEPARTMENT OF OPHTHAMOLOGY. POSTION No. 576400.

The Appointee will be responsible for research projects and the development of instrumentation in the Bio-Engineering field. Applicants should preferably be in the age group 25 to 40 years, should hold a degree in engineering (electronics) or equivalent and should have a minimum of 2 year's experience in this field. Salary will depend on qualifications and experience. Terms of appointment are available on 662-1644.

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167 Queen Street, Melbourne. 67 9161 • 70 Merivale Street, Brisbane. 4 1631 • Cnr. Darby and King Streets, Newcastle. 2 5166 • 231-233 Bulwer Street, Perth. 28 6400 • 48 King William Road, Goodwood, Adelaide. 72 2366 • 42 Frederick Street, Launceston. 2 1804 • 123 Murray Street, Hobart. 3 3836-7 niques will no doubt be aware, ECAP is a network analysis program employing a "piecewise-linear" approach, and consists of three packages which deal with DC, AC and transient conditions. NASAP is a program based on signalflow graphs, while NET-1 and SCEPTRE are non-linear programs used for stored-model analysis and transient radiation effects problem solving respectively.

As one might perhaps expect from the origin of the material, it consists basically of broad descriptions of the various analysis programs and their application. It is not intended to be a collection of software manuals, preparing for or assisting in the use of such programs. There are no program listings. The idea is mainly to give the reader a picture of the way in which these new techniques may be used to solve many complex and cumbersone design and analysis problems.

The four analysis programs considered in the book are introduced and discussed separately in the first four chapters. Following these are three chapters dealing with more general aspects of analysis programs and their use. Chapter 5 examines bipolar transistor and FET models for computer analysis, chapter 6 discusses computer design of active RC filters, with particular reference to NASAP, while chapter 7 discusses a reliability program utilising circuit analysis programs.

The various chapters have been written by different contributors, and there are inevitable minor variations in style. However, in general the text may be described as clear and concise, and well illustrated by diagrams and numerical examples.

In view of the material presented and the background assumed both in electronics and computing techniques, the book will really only be of interest to senior engineering students and professional circuit designers and analysts. For these people it should provide an interesting and worthwhile introduction to CAD techniques.

The review copy came direct from the U.K. publisher, and no information was supplied regarding Australian price and availability. (J.R.)

AUDIO AMPLIFIERS. Edited by J. R. Davies. Data Book Series No 18. Published by Data Publications L t d., London. First printing January, 1969. Stiff paper covers, 5½ x 8½in, 124 pages, illustrated by photographs and diagrams. Australian price \$1.50 plus 20c postage.

This book was reviewed in our August, 1969, issue on page 157. We have been informed that copies are available from Technical Book and Magazine Co. Pty. Ltd., 289-299 Swanson Street, Melbourne, 3000.

LITERATURE—in brief

BISHOP TECHNICAL MANUAL AND CATALOG 104A, 1970 edition. Published by Bishop Graphics Inc., U.S.A. Inquiries to Circuit Components (A'sia) Pty. Ltd., P.O. Box 70, Bexley, N.S.W. 2207. The 68-page manual describes more than 15,000 pressure-sensitive electronic component drafting aids, techniques and systems. Pressure-sensitive patterns, symbols, tapes and multi-pad configurations are completely described with illustrated instructions for their use. New products include: Bishop "B" Neg Negative Draft-ing System for the preparation of nega-tives for prototype boards without photo-graphy; Bishop Red and Blue Tape Method for preparing artwork' for two-sided boards in perfect registration.

MI CONTACT, Issue 14. Published by Marconi Instruments Ltd., U.K. Inquiries to Amalgamated Wireless (A'sia) Ltd., P.O. Box 96, North Ryde, N.S.W. 2113. Contents include: M.I. announces a new 120MHz frequency meter; MI-Sanders microwave signal source; The Queen awards M.B.E. to Marconi Instruments executive; Q measurement with confi-dence; Still top value in RF voltage measurement; Accurate measurement of colour television system characteristics; colour television system characteristics; "Autotest" deliveries to Europe in four weeks flat; Consolidation of serveiing facilities; A new coaxial attenuator joins the MI-Sanders range; RF attenuator TF2163S handles fast pulses.

TELECOMMUNICATION JOURNAL Vol. 37, No. 1, January, 1970. Published by the International Telecommunication Union (I.T.U.), Place des Nations, 1211 Geneve 20, Switzerland. Contents include: Geneve 20, Switzerland. Contents include: Economic study of satellite systems for telecommunications, air traffic control and navigation, by B. Manuali and C. Ganier; British Post Office transistors for deep-water submarine telephony, by M. F. Hol-mes and D. Baker; and a report on the activities of the International Radio Con-sultative. Committee (CCLB) Study

activities of the International Radio Con-sultative Committee (C.C.I.R.) Study Groups during the period 1966-1969. The section "Ideas and Achievements" includes reports on the Federal Republic of Germany's Azur satellite, Hungary's telecommunication industry, and a propos-ed new field strength standard. The sec-tion on "Union Activities" includes re-ports on the visit of the Secretary-General to Latin America, the meeting of the joint C.C.I.T.T./C.C.I.R. Regional Plan Committee for Latin America, the 4th session of the Inter-American Telecom-munication Commission, and a meeting of the integrated global ocean station systhe integrated global ocean station sys-tem.

TECHNICAL INTERFACE, Vol. 1, No. 3, 1969. Published by AIM Asso-ciates Cambridge Ltd., U.K. Inquiries to Rutherford Electronics Pty. Ltd., 62 Jack-son Court, Doncaster, Vic. 3108. Con-tents: AIM Phase-Lock Techniques; Pulse Methods, a Theoretical Background, part 1; Pre-amplifiers and Equalisers, part 1: A New Low Drift Phase Security Methods, a Theoretical Background, part 1; Pre-amplifiers and Equalisers, part 1; A New Low Drift Phase Sensitive Detec-tor, PSD 122A; Principles of Phase Sensi-tive Detection; A Theoretical Look at Lock-in Amplifiers; Minilock — a New Miniature Lock-In Amplifier System; New Instruments from AIM; Company News.

STANDARDS ASSOCIATION OF AUSTRALIA is seeking comment on two iraft Australian standard specifications. Doc. 1488 prescribes requirements for Iraft Australian standard specifications. Doc. 1488 prescribes requirements for lesign, construction, physical properties and type testing of containers and cell povers for lead-acid batteries of the auto-mobile type. Doc. 1492 applies to the performance, calibration and charac-eristics of pure tone audiometers for liagnostic and screening purposes. It will stablish requirements intended to ensure hat the testing of the threshold of hear-ng of individuals will give uniformity of results. esults.

Copies of the documents may be btained, without charge, from the various offices of the Standards Association of Australia in all capital cities and New-astle. Comment on the provisions of the Iraft standards is invited from persons or reanisations experienced in the relevant ields and should reach the head office of the Association, 80 Arthur Street North Sydney, N.S.W. 2060, or any pranch office, not later than 31 March, 1970.

HEWLETT-PACKARD JOURNAL, Vol. 21, No. 4, December, 1969. Published by the Hewlett-Packard Co., U.S.A. Inby the Hewlett-Packard Co., U.S.A. In-quiries to Hewlett-Packard Australia Pty. Ltd., 22-26 Weir Street, Glen Iris, Vic. 3146. Contents: Network Analysis in the Range 100KHz to 110MHz, by William A. Ryland and David R. Gildea; High Impedance Probing to 500MHz, by Joel Zellmer. The former article describes a new Hewlett-Packard instrument which presents swent display of amplitude new Hewiett-Packard instrument which presents swept display of amplitude response up to 80dB with .05dB resolution. It discusses: Measuring method; Theory of operation; Frequency response; Amplitude measurement; Phase measurement; Trans-ducers; Operation; N-Port power flow measurements: Network analyses applicameasurements; Network analyser applica-tions. The latter article describes a new DC-500MHz voltage probe which can be used with analysers, counters, and oscilloscopes.

NEW TECHNOLOGY, No. 34, November, 1969. Published by the British Ministry of Technology and the Central Office of Information. Obtainable free on application to the Central Office of Inforapplication to the Central Office of Infor-mation, Hercules Road, Westminster Bridge Road, London S.E.1, England. Contents: The Feeding of Successful Decision Makers; Management Decision through Information; RAE plus PERA plus Airmec-AEI equals NCADS; Work for Industry in Mintech Research Estab-lishments; ERDE Advises on Adhesives and Sealants; News; Statistical Indicators.

LONDON CALLING, Vol. 4, No. 9, January, 1970. Published by the B.B.C., Bush House, Strand, London, W.C.2, England. Program bulletin of the B.B.C. world service. Contents: Broadcasts in English to the world; program highlights; daily schedules; frequency charts and tables.

RACAL AUST. REVIEW, Vol. 1, No. 2. October, 1969. Published by Racal Elec-tronics Pty. Ltd., 47 Talavera Road, North Ryde, N.S.W. 2113. Contents: I.D.T./Link Simulator — Moulding To-morrow's Drivers; New Products from Racal; Showcase — The New Zealand Trade Fair; Australian Post Office Appro-val for Racal-Milgo 4400/24PB Modems.

AURI-NEWS, Vol. VIII, No. 10, October, 1969. Published by Ad. Auriema Inc., U.S.A. Inquiries to Auriema (A'sia) Pty. Ltd., 443 Kent Street, Sydney, 2000. Contents: Apelco solid-state depth sounder and marine radiotelephone; Blonder-Tongue field strength meter; International Data Sciences pseudo-noise transmission test set; Rotron solid-state inverters; General Instrument thermoelectric genera-tors; International Instruments cathodic tors; International Instruments cathodic protection indicator; National solid-state communications receiver and solid-state amateur 5-band transceiver; Tarzian selenium rectifiers; Stackpole rocker and slide switches; Magitran hi-fi speaker system; Kepco power supplies.

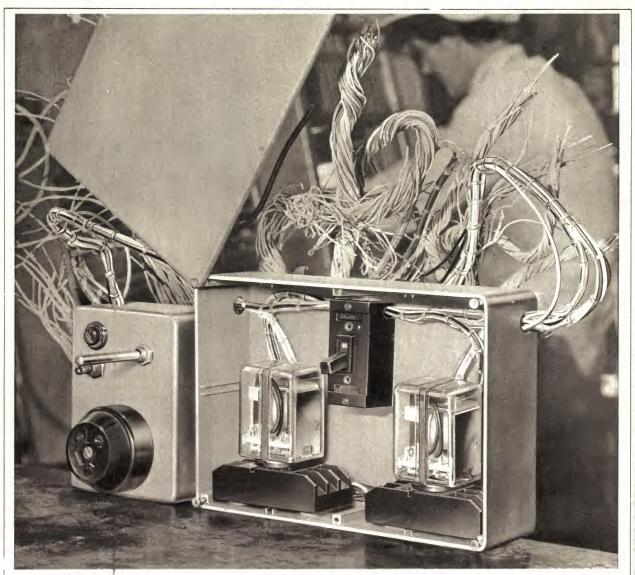
CUMULATIVE INDEX TO THE CLASSIFICATION OF PATENTS, third microfilm edition. Published by the U.S. microfilm edition. Published by the U.S. Patent Office. Obtainable from the Clear-inghouse for Federal Scientific and Technical Information, U.S. Department of Commerce, Springfield, Va. 22151, U.S.A. Price \$70 (U.S.) Contains the official listing of all patent numbers issued up to December 31, 1968—more than 3,400,000 in all. The index consists of 16 reels of 16mm film; seven reels of original (primary) classification, and pine reels of reels of 16mm film; seven reels of original (primary) classification, and nine reels of cross-reference (secondary) classifications. Listings are arranged numerically by class and subclass for use in conjunction with the Manual of Classification. Reels may be purchased individually for \$6 each. Available separately on one microfilm reel is "The Complete Record of the Classification of Design Patents." This reel, also priced at \$6, contains both original and cross-reference classifications of design materia.

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ASSOCIATE worldwide telecommunications and electronics



AMATEUR BAND NEWS AND NOTES

Australis Oscar V in orbit

The Australian built amateur radio satellite was successfully launched in January and has been tracked by enthusiastic amateur operators throughout the world.

by Pierce Healy, VK2APQ

On Friday evening, January 23 listeners to Wireless Institute stations in Victoria and New South Wales, heard an on-the-spot description of the launching of the NASA space vehicle which placed the Australis Oscar V in orbit around the earth. Description of the launch was given by members of the AMSAT group from the space tracking and control centre at Goddard in the United States. The main communication link was be

The main communication link was between the Goddard centre and the Project Australis co-ordinator, Richard Tonkin, at the Australis Project Headquarters in Melbourne University. The conversations and technical details exchanged between the two centres was relayed interstate by landline and official transmissions were made on amateur band VHF and HF channels.

Shortly after 11.30 p.m. E.S.T., acquisition of the signals from the satellite was reported both in Melbourne and Sydney. The telemetry data was recorded on both 144.050MHz and 29.450MHz. These initial reports indicated that all systems were operating satisfactorily.

Since the launching many amateurs in all States, as well as other parts of the world, have been able to record the data transmitted. It is expected that the satellite will continue operation for about two months from the time of launching. Details of the orbital predictions will be given from all W.I.A. stations during

Details of the orbital predictions will be given from all W.I.A. stations during the Sunday morning news broadcast sessions on 7146KHz. Reports from stations tracking the satellite are necessary for the success of the project. These should be sent to Project Australis Coordinator, Richard Tonkin, 5/39 Tooronga Road, East Malvern. Victoria, 3145.

THE ASIAN SCENE

An initial report on the First All India Amateur Radio Convention in Bombay was contained in last month's notes. Further details of the event will be given when a copy of the official report comes to hand.

After the convention my trip was continued on December 31 to Delhi, where I stayed until 3 January. During that time I visited Doyle Edmondson, VU2-BEO, who is stationed at the U.S. Embassy in Delhi. On the evening of December 31, which I spent with Doyle,

News and notes of Divisional and Club activities submitted for inclusion in these columns should be forwarded direct to Pierce Healy, 69 Taylor St., Bankstown, N.S.W. 2200. contact was made with Keith Johnston, VK7RX and Tom Moore, VK7FM.

VK7RX and Tom Moore, VK7FM. This contact developed into what must be the first DX contact with a station using the AX prefix. Daylight saving time in Tasmania put stations in that State ahead of mainland stations in the right to use the Cook Bi-centenary prefix. The contact with Keith started before midnight Tasmanian time and at the witching hour Keith signed as VK7RX and called as AX7RX, under which call the contact was continued. VK7FM, realising what had transpired, again joined in the contact to give Doyle his second AX contact within minutes.

withm minutes. This was surely a unique contact — a visitor to VU land, VK2APQ, participating unexpectedly in the first ever QSO made between a DX station and an AX prefix station. Doyle's confirmation QSL card was given to me to bring back for VK7RX and VK7FM.

New Year's Day was spent on a trip to Agra and a visit to the Taj Mahal. The beauty of the Taj must be seen to be fully appreciated, and the experience could form the subject of a separate story.

On the evening of January 2, I was the guest of Amar Bannerjee, VU2CZ, Secretary of the Amateur Radio Society of India, M. G. Karnik, VU2CK and Anil Sen, VU2SA, at the Delhi Flying Club. This meeting was most interesting, as it allowed me to meet executive members of the only amateur radio society in India which did not support the convention in Bombay.

in India which did not support the convention in Bombay. The next stop was Bangkok, Thailand. After leaving Delhi during the morning of January 3, we were flying parallel to the mighty Himalayas — and what a sight to behold! What VHF locations? But what a lot of snow and ice; During this flight, the cities of Calcutta and Rangoon were seen.

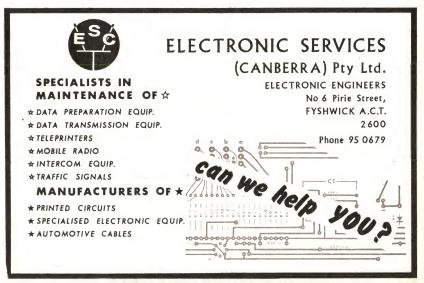
Rangoon were seen. On arrival at Bangkok I was met by an old friend, Howard Rider, VK3ZJY, now HS1ABA and Forrest McClure, HS-1EI, and was escorted by them to my hotel. The evenings of January 3 and 4 were spent at the home of John Doherty, HS1AF, from where contact was made with John Lark, VK2ALK. Both evanings were spent discussing

Both evenings were spent discussing aspects of amateur radio, both the local scene in Thailand and the international scene. Also present at these evenings were Chuck Farr, W6AJW on leave from Laos, and Fred Laun, HS5ABD, vice-president of the Society of Thai Amateur Radio. Due to other commitments the president of the Society was unable to be present.

On January 5 it was announced that Thailand would in future be divided into nine districts but only five would be allotted; also, all call-signs would be revised. Three letter calls would be allotted to non-Thai nationals. It is interesting to note that the call-signs are issued by the Society of Thai Amateur Radio — STAR. The next stage of the trip was to

The next stage of the trip was to Hong Kong, where I arrived January 6. That evening was spent in the China Fleet Club at an unofficial gathering of members of the Hong Kong Amateur Radio Transmitting Society. Lyell Louttit, VS6BE/VK2BE, was present at this function.

More about Hong Kong and Singapore next month.



ELECTRONICS Australia, March, 1970



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QUARTER CENTURY WIRELESS ASSOCIATION

The Sydney Chapter of the Q.C.W.A. meets on the second Wednesday evening of each month at the Combined Services Club, Barrack Street, Sydney, for dinner and get-together.

Membership is open to amateur opera-tors who have held a licence for at least 25 years. For details write to: The Secre-tary, who is George Wilson, VK2AGO, 31 Glenview Street, Greenwhich, 2065; or Brian Anderson, VK2AND, 14 Stuart Street, Longueville, 2066.

NEW PUBLICATION

NEW PUBLICATION A new publication, "OHM" (Oriental Ham Magazine) is being published by Pacifica Publications in Hong Kong. The publisher is Phil Wight, VS6DR and the editor is Roy Chalu. Editorial board: Herb Asmussen, VS6AD; Maurice Caplin, VS6AA and Ken Young, VS6AL. The first issue was in October 1969. Subscrib-tion rates are: Surface mail, world-wide, \$2 U.S. per year. Airmail, Australasia, \$10 U.S. per year.

"OHM" contains several technical articles of topical interest as well as a summary of up-to-date information on happenings in South-East Asia. The quality of the publication is very good. The size is $8in \times 5\frac{1}{2}in$ and the copy seen had 24 pages, liberally illustrated with Thete and determe with photos and sketches.

NETHERLANDS PREFIX

Radio amateurs in the Netherlands may. in the future, be permitted to use the call sign prefix "PD" on special occasions in-stead of the current "PA" call. Also possible is the use of a digit other than the zero now employed by the Dutch nationals. At the present time foreigners under reciprocal agreements use a PA9 prefix.

RTTY CHAMPIONSHIP

The committees of several RTTY groups and societies have decided to made an award to the "World Champion of RTTY."

The objects of this award are as follows: 1. To promote greater interest for the

- RTTY operator taking part in the various RTTY contests. To increase the competitive spirit during the course of the contests dur-
- 2.
- auring the course of the contests dur-ing the year. 3. To make available an award to the radio amateur who has demonstrat-ed his ability to operate RTTY dur-ing a period of one year. At the present time the contests which will count towards this new award are as

follows

1969 BARTG Spring RTTY contest.
1969 DARC RTTY WAE Contest.
1969 Volta RTTY DX Sweepstakes.
1969 Alex Volta RTTY Contest.
1970 Giant RTTY Flash Contest.
Other societies who organize inter-

Other societies who organise inter-national contests are invited to join in this new idea, to increase interest in the RTTY mode for radio amateurs.

RTTY mode for radio amateurs. To arrive at the final score, and to de-cide the winner, the following points sys-tem will be used for each contest: 30 points to the winner; 25 points for 2nd place, 22 points for 3rd place; 20 points for 4th place; 18 points for 5th place; 17 points for 6th place; 16 points for 7th place, etc., to 1 point for 22nd place, and all other entrants. For the final score for each year only

For the final score for each year, only the best four scores (out of a possible of five) of each operator will be used.

In order to take part in this award contest, it is not necessary for entrants to send in a claim, as the entries of all com-petitors in the contests listed will be automatically included.

DUNEDIN CONVENTION CONTEST

An 80-metre "All Modes" contest will be held in conjunction with the 44th Annual Convention to be held in Dunedin at the Overn's Birthday works and 1000 at the Queen's Birthday weekend, 1970.

It is to be held in April, 1970, and the rules are simple. You are invited to contact as many ZL4 stations as possible on 80 metres and to work them on as many different modes as possible, viz: you may work each station on CW, SSB, AM, etc., and score points each time

If you desire, you may work the same station several times running SO LONG AS YOU USE A DIFFERENT MODE EACH TIME. The ZL4 may continue to work you on the same mode as he started or he may change if he desires. It is YOU who have to change the trans-

YOU who have to change the trans-mission mode. Example: You may work ZL4FD on AM. You will receive points. You may then call and work him on SSB. You receive more points. To count, the con-tacts MUST be made during April, 1970, and you may contact any ZL4 station at any time during this period. Rules: Rules:

Band: 80 metres only.

Time: During April, 1970, only. Modes: As many as you like. -

JAMBOREE-ON-THE-AIR

Two national reports on the 1969 Boy Scout Jamboree-on-the-Air, held on October 18 and 19, have been received. The first is from D. D. Devan, 9M2DD, of Malaysia, whom I had the pleasure of in January when I visited Singapore early in January when taken on a visit to his home in Johore Bahru by Peter Pang, 9V1AZ. The report gives details of the activities

Points: Dunedin stations, 10 points each time worked, other ZL4 stations, 5 points each time worked. Note: DUNEDIN STATIONS ARE

BONUS STATIONS. Logs: Send a list of stations contacted,

operational condition, brand new and ready to plug into your linear amplifier. Value-over \$60.

Value—over \$60. To win this prize it is mandatory that you be at Dunedin convention in person to accept it. If the first placegetter is not at the convention to receive it in per-son, the second, third or fourth placeget-ter, as the case may be, will receive the

ter, as the case may be, will receive the prize in person. A "Mystery" station will be on the air each Sunday evening during April. He will be a Dunedin station and will call "CQ, CQ, CQ. This is the convention mystery station, ZL4 . . . (as the case may be) calling CQ" for 20 seconds at 1930, 2030 and 2130 hours NZST. He could be on any mode and in any part of the 80 metre band. If you work him, you get 50 points every time.

> of 11 stations that participated in the event, and mention is made of several other amateur operators who also gave assistance. The Malaysian Boy Scouts Headquarters station 9M2BP, was operat-ed from the Selangor Boy Scouts' Associa-tion's Castle Camp, just out of Kuala Lumpur city. Contacts with 10 Australian stations were made during the weekend. stations were made during the weekend.

In summing up his report, the Malay-

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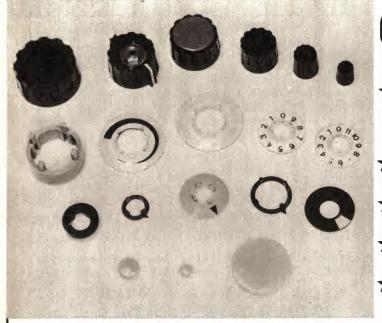
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VICTORIA

sian National Organiser, Ahmad Bin H. A. Rashid, paid tribute to Television Malaysia for their coverage of the activity at the headquarters station; also to several willing assistants, including Avatar Singh, 9M2AV, whom I had met at the First All India Amateur Radio Conven-tion in Bombay. According to the report, a rough estimate indicates that no less than 600 scouts took part in the 1969 Jamboree-on-the-Air.

The second report was from Noel Lynch, National Organiser for the Australian Boy Scouts' Association. Noel's report contained news from Branch Organisers in all States of Australia and Papua-New Guinea. From the participation figures given in the reports it seems that many of the previous totals have been exceeded. In Victoria, 3,000 Scouts and Scouters par-ticipated together with 1,000 Guides and Guiders.

Nearly all reports mentioned the fact that they had a contact with the Inter-national Amateur Radio Club Station, 4U1ITU, which operated in conjunction with the Headquarters of the World Scout Bureau in Geneva, Switzerland. One interesting point in the report is

One interesting point in the report is the fact that there are now 15 official Scout Group stations operating in Aus-tralia. The report, which has been sent to the World Bureau, acknowledged the press, radio and television coverage and paid tribute to all who assisted in making the event an outstanding success.

WIRELESS INSTITUTE ACTIVITIES

The twenty-fourth Federal Convention of the Wireless Institute of Australia will be held in Adelaide over the Easter holi-day weekend, March 27-30, 1970. The South Australian Division is the host to Federal Councillors from the other Divi-sions. This convention coincides with the 60th Anniversary of the formation of the WIA. W.I.A.

NEW SOUTH WALES

The annual meeting of the New South Wales Division will be held on Friday, Wales Division will be held on Friday, March 20, when the annual reports will be presented and the council for 1970 will be elected. On Saturday evening, March 21, the annual dinner will be held at the Argyle Tavern, Sydney. Bookings for the dinner should be made in writing to the Secretary Wireless Institute Centre, 14 Atchison Street, Crows Nest. Tickets are \$5 each which must accompany the request for booking. On Sunday, March 22, the annual field day will be held at the divisional trans-mitting station VK2WI. Quarry Road, Dural. Field events are being arranged as well as a display of equipment by trade houses.

houses

At the January meeting of the Division, the Federal Councillor, Pierce Healy, VK2APQ, presented his report for the past year, in which the attention of members was drawn to matters that required con-sideration by those who had the well-being of the Division and amateur radio at heart Following some discussion on the points raised, the meeting re-elected Pierce, un-opposed, for a tenth term as Federal Councillor.

URUNGA CONVENTION

The organising committee extend to

The organising committee extend to you a warm invitation to attend this very popular convention held on the North Coast of New South Wales, and trust that you and your family will be among the visitors to enjoy the hospitality of Urunga over the Easter holiday weekend. There will be plenty of prizes, including a special jackpot for a Sunday morning event, and another very worthwhile award—a week's free accommodation for two at the Ocean View Hotel, Urunga. There will also be trophies and 1970 Urunga pennants for presentation to suc-cessful competitors. cessful competitors.

In appreciation of the services given to amateur radio over a period of 21 years by the late Crieff Retallick, VK2XO, and the tremendous amount of work he had done in organising the Urunga Con-vention each year, the convention com-mittee have decided that this year the con-vention will be known as The Wireless Institute of Australia Urunga Convention —Crieff Retallick Memorial Year. The program, which is definitely for all the family, will start on Good Friday, March 27, with a general meeting and get-together at the Ocean View Hotel, commencing at 8 p.m.

Saturday, March 28 9 a.m.-12 noon. Registration at the booth (to be set up in the park opposite

Ocean View Hotel). Fees: Men. \$2.50; Ladies \$1.50; Children free. Registration Officer: Clive Jackson, VK2TD. 10 a.m.-11 a.m.: 144MHz novelty trans-mitter hunt, which will be within a radius of three miles from the registration point. 11.30 a.m.-12.30 p.m.: 7MHz hidden transmitter hunt.

transmitter hunt. transmitter hunt. 2.30 p.m.-3.30 p.m.: 144MHz hidden transmitter hunt. There will be four transmitters, two each on 144.1MHz and 146MHz, located at two sites. The winner will be decided on the time taken to locate all four transmitters.

2.45: Events will be held for the ladies and those not participating in the field event

event. 8 p.m.: Social evening in the School of Arts, Urunga. All members and their families are invited to be the guests of the organising committee. 9 p.m.: Auction of members' surplus equipment. (No junk, please.)

Sunday, March 29 10.30 a.m.-12.30 p.m.: 144MHz hidden transmitter hunt. There will be four trans-mitters, two each on 144.1MHz and 146MHz, located at two sites. This is a jackpot competition, and in addition to the normal prize for the event there will be the jackpot prize which was not won last year. last year.

2.30 p.m.-4 p.m.: All-band scramble, any

8 p.m.: Prize giving and social evening at the Urunga Golf Club.

at the Urunga Golf Club. The competition requirements are: All events will be controlled by an official starter strictly on time from the park opposite to the Ocean View Hotel. Please note: The 144.1MHz transmission will be carrier only and the 146MHz transmitter pulse modulated. The ruling of the committee on any matter will be final. Accommodation booking should be made direct with the hotel or motels at Urunga. Further information may be obtained from: Brian Slarke, VK2ZCQ, North Bank Road, Bellingen, N.S.W. 2454; or Ray Chaplin, VK2SB, either on the air or by phone—Nambucca Heads 154. 154.

QUEENSLAND

Classes conducted by the Queensland Division for the Amateur Operator's Certi-ficate of Proficiency examination were scheduled to commence on February 11. These classes are designed to assist those wishing to obtain their amateur licence. This year it is intended to use visual aids as an adjunct to the lectures. However, assistance is required in the construction as an adjunct to the rectures. However, assistance is required in the construction of such aids. The Class Organiser, Syd Carter, Masaman Terrace, Taringa, 4066, would like to hear from anyone willing to undertake the construction of such aids.

Instructors for the classes are Stan Armstrong, VK4SA, Reg Hildred, VK4RE, and Jack Morris, VK4JQ. The fee for the class is \$6. The class organiser would be pleased to hear from other amateurs who would assist as instructors. The inaugural meeting of the Sunshine

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Coast Amateur Radio Club was held on Tuesday, January 27, in Nambour on the Sunshine Coast. Election of Office Bearers resulted as follows: — President, John Purdon VK4PU; Vice President, Ken Chiverton VK4VC; Secretary, Wayne Shaw VK4WE: Treasurer, Bill Ryan VK4WR; Public Relations Officer, Norm McRae. A spokesman for the club said that the meeting was very successful with 20 per-sons attending, 12 of whom were licensed amateurs. The next meeting was to be held on the third Tuesday in February.

WESTERN AUSTRALIA

Ted Gabriel, VK6TG, continues his work in the organisation of the WICEN net-work in Western Australia. Ted reports that every Sunday morning, after the call-backs following the VK6WI news broad-oast on 40 metres, a WICEN call-back and discussion session is held on 7100KHz. During these sessions information is passed on, questions answered, band con-ditions reported and other emergency frequencies checked. frequencies checked.

The call-backs are conducted by each net controller calling in his group mem-bers in turn, and arrangements are made for exercises to be conducted and WICEN activities discussed.

The new Albany District Radio Club includes many of the local bush fire brigade members. This is an example of how WICEN can be integrated with local emergency activities. An invitation is ex-tended to all persons interested in participating in this very worthwhile organisation.

VHF NOTES

The 144MHz beacon transmitter located at Mount Barker near Albany, which has an output power of 40 watts, is proving to be an asset to VHF operators interested

WORKED NORTH QUEENSLAND AWARD

605000000

To commemorate the Diamond Jubilee To commemorate the Diamond Jubilee of the Wireless Institute of Australia and the bi-centenary of the voyage of Captain James Cook along the east coast of Aus-tralia, The Townsville Amateur Radio Club will issue an award to be known as "Worked North Queensland Award." The award will be made under the following rules: 1. The award is available to any licensed

- 1. The award is available to any licensed amateur radio operator who is able to confirm contact with five amateur radio stations in North Queensland.
- 2. North Queensland is defined as that part of the State of Queensland north of the latitude of Sarina and includes
- of the latitude of Sarina and includes such cities as Mackay, Ayr, Townsville, Charters Towers, Mount Isa and Cairns. 3. Confirmation is required in the form of QSL cards or a check list, the accuracy of which is confirmed by an executive officer of a radio club or society.
- society. The Townsville Amateur Radio Club is the sponsor of the award. Any queries relating to the award will be resolved solely by the club committee. A handsome multicolour certificate will be sent to those who apply and qualify 4. The

 A nandsome multicolour certificate will be sent to those who apply and qualify for the award.
 Applications should be addressed to: The Secretary, Townsville Amateur Radio Club, P.O. Box 964, Townsville 4810, Ouesreland. Queensland.

in VHF propagation. The beacon has been heard in Perth on a number of occasions, and at the end of January was heard at good signal strength in Adelaide.

W.I.A. Youth Radio Club Scheme

With the commencement of the 1970 school year, the Y.R.C.S. clubs are just getting under way again. This month there is little news to hand, as most schools had just re-opened when these notes were being compiled.

However, there is an item that may be of interest. While attending the First All India Amateur Radio Convention in Bombay last December, I (Pierce Healy, VK2APQ) had the privilege of addressing about 200 delegates to the convention on various aspects of amateur radio in Australia.

tralia. Among the subjects covered was the Youth Radio Club Scheme, and I was able to illustrate this aspect with some colour slides of the Westlakes Radio Club. I was very pleased with the interest shown in this aspect of amateur radio, and I was asked a number of questions about the operation of the scheme and the results and benefits gained. From the interest shown it is possible that similar clubs will be organised in India. Y.R.C.S. members who are interested

Y.R.C.S. members who are interested in SWL may like to correspond with the Madras Radio Listeners Club, C/o Rao's Radio Research Lab., 28k. Pandalai Road, Tondiarpet, Madras 21, India.

NEW SOUTH WALES

After the holiday recess the Maitland Radio Club resumed activities on January

Radio Club resumed activities on January 23 and the enrolment of new members took place on Saturday 24th. The club was able to look back on the past year with great satisfaction. The membership now stands at 116 and the attendance figures from February to December totalled 2,842. The committee looks forward to further progress during the coming year, and is calling for more instructors for the increasing number of classes being held. classes being held.

A-special course of theory instruction for advanced members who wish to sit for the Amateur Operator's Certificate of

Proficiency has been arranged to prepare members for the P.M.G. examination to be held in August. Classes are held Friday nights. Six members attended the first class.

The club is preparing for its exhibition to be staged at the forthcoming Maitland Show, where last year a great deal of public interest was shown.

Dublic interest was shown. The executive officers of the club have arranged for a sale of surplus radio and electronic items to members. Last year, the club received donations from business firms, the electronics industry and individuals. The equipment includes radio transmitters, receivers, high-quality ampli-fiers and Morse code training equipment. It is essential that the equipment be cleared, as all available space is needed for classes and other activities. Club members A. Counsell, VK2ZFH and A. Dever, VK2AWD, are working on the construction of six-metre FM equipment to operate on the net frequency 52.525MHz.

52.525MHz.

Congratulations have been extended to the club's patron, Sir Allen Fairhall, VK2KB, who was awarded a K.B.E. in the New Year's Honours List.

SOUTH AUSTRALIA

Allen Dunn reports that the South Australian Youth Radio Clubs that got away to an early start in 1970 were: Port Augusta Youth Radio Club where activities were recommenced on January 17; and the Barossa Valley Youth Radio Club, which held an outing for senior members on the same date. The Barossa Club outing included a visit to a well-known radio surplus store, and to amateur stations VK5ZDX, VK5GG/T and VK5EK, where each of

and to amateur stations VK5ZDX, VK5GG/T and VK5EK, where each of the operators described his station and gave a short talk on a particular aspect of amateur radio. A visit was also made to the A.B.C. broadcast transmitters at Pimpala. After

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190-220-235V input. Isolated output 110V 10A, 220 V 5A and 24-26V at 5A, \$25. Free on rail. TORRINGTON BLOWERS Twin blower 200 cfm each side Motor 240V 0.4A. \$10.00. Edge Connectors, single units 50c 16 pin 0.1", block of 8 50c
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Batteries. Two 1.3V ary cens. Size AA, "Eveready" 915 Overload-protected by dual silicon diodes. \oplus Mirror scale. Double-jewelled $\pm 2\%$ meter. $\oplus \pm 1\%$ temperature-stabilized film resistors.

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Model RH-20 \$15.00 Postage 50c



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C Volts: 0.25, 2.5, 10, 50, 250, 1000 (20,000/V) DC

C Volts: 10, 50, 250, 500, 1000 (10,000/V) AC

DC Current. 50 uA, 25mA, 250mA Resistance. $7k\Omega$, $700k\Omega$, $7M\Omega$

Decibels. -10 +22 (at AC/ 10V) +20 +36 (at AC/ 50V). Upper frequency limit 7kc.

Batteries: Two 1.5V dry cells. Size AA, "Eveready" 915

Model RH-55 \$20.00 Postage 50c



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- *AC Volts: 12V, 60V, 300V, 1200V (14,000 ohms/V). *DC Current: 60 A, 12mA,
- 300mA. *Resistance: 10K ohm, 1Meg
- ohm, 10Meg ohm. *Decibels: -10 db +23 db.

Model RH-60 \$25.00 Postage 50c



50,000 Ohms per Volt DC 10,000 Ohms per Volt AC Specifications:

DC Volts: 0.25, 2.5, 10, 50, 250, 500, 1000 V Volts. 10, 50, 250, 500, AC

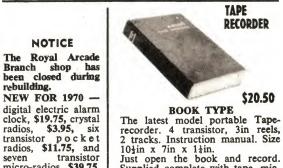
- 1000 V
- DC Current. 25 uA, 5 mA, 50 mA, 500 mA

Resistance: 10 kΩ, 1 1 MegΩ, 10 MegΩ 100 kΩ,

Decibels. -10 + 62 db Accuracy: DC $\pm 3\%$, 4% (of full scale) AC±

- Batteries. Two 1.5 V dry cells.
- Size AA, "Eveready" 915

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1970 B.E.R.U. CONTEST

Radio amateurs throughout the British Com-monwealth are invited to take part in the 33rd B E.R.U. contest to be held on March 7-8, 1970. The attention of entrants is drawn to Rule 1, and in particular to the requirement for sepa-rate log sheets for each band. This new rule has been hitroduced to simplify the adjudica-tion of this very popular contest. Reprints of these rules, the general rules for HF contests, and supplies of log sheets and cover sheets, may be obtained from B.E.R.U. HF Contest Committee, Radio Society of Great Britain, 35 Doughty Street, London WC1, Eng-The low-power service of the contest to the service

and. The low-power section of the contest has been dropped because of minimal support in recent years.

Rules 1. The General Rules for R.S.G.B. HF Contests. as published in the January, 1969, edition of Radio Communication will apply. 2. When: from 0001GMT on Saturday, March 7. 1970, to 2359GMT on Sunday, March 8, 1970.

3. Eligible entrants: Members of the R.S.G.B resident in the British Isles, and radio ama-teurs licensed to operate within the British Commonwealth and British Mandated Terri-tories.

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Bowl.

Commonwealth Call Areas:

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Contraction in the second se	reas are recognised for	the purpose of the 1970 I	B.E.R.U. Contest.
A2/80/ZS9* AC3 AP2 AP5 C2/VK9 (Nauru) . G/GB/GC/GD/Gi/ GM/GW MP4B MP40 MP40 MP41 VE1 VE2 VE3 VE4 VE4 VE5 VE5 VE6 VE6 VE6 VE6 VE6 VE6 VE6 VE6 VE6 VE6	VK9 (Norfolk Island) VK9 (New Guinea and Bismarck Island) VK9 (Papua). V0 VP1 VP2A (Antigua and Barbuda) VP2 (Dominica) VP2G (Granada) VP2K (Monserrat) VP2K (Monserrat) VP2K (Monserrat) VP2K (Monserrat) VP2K (Monserrat) VP3 / BR* VP5 (Turks and Calcos) VP5 (Turks and Calcos) VP5 (Turks and Calcos) VP5 (PP* VP6 (PP* VP7 VP6 (Falklands)	hte purpose of the 1970 VQ9 (Aldabra) VQ9 F VQ9 F VR1 (British Phoenix Islands) VR1 (Gilbert and Ellice and Ocean Islands) VR2 VR4 VR3 VR4 VR5 VS5 VS5 VS5 VS5 VS5 VS5 VS5 VS	ZL (Auckland and Campbell Islands) ZL (Chatham Island) ZL (Chatham Island) ZLS (N.Z. Antarctica) ZM7 ZS3 /7P8* (Lesotho) ZS9* (See ZA2) 4S7* (See ZA2) 4S7* (See ZA3) SN2* (See ZA6) SV* (See ZM6) SZ4 SY5 7P8* (See ZM6) SZ5 7P8* (See ZS8) 7Q 80* (See ZS8) 7Q 80* (See YP6) 8C* (See YS9) 8R* (See YS9) 8R* (See YS9)
VK3 VK4 VK4 (Willie island)	VP8 (Falklands) VP8 (Grahamland) VP8 (South Georgia) VP8 (South Orkneys) VP8 (South Sandwich) VP9	ZD3 ZD5 ZD7 ZD8 ZD9 ZE	8R* (See VP3) 9G1 9H1 9J2 9K2 9L1
VK5 VK6 VK7 VK8 VK9 (Admiraity Island) VK9 (Christmas Island) VK9 (Cocos Island)	VQ1 VO8 (Agalega and St. Brandon) VQ8 (Chagos) VQ8 (Cargados)	ZF9* (See VP5) ZK1 (Cook Island) ZK1 (Manihiki Island) ZK2 ZL	911 9M2 (W. Malaysia) 9M6/9M8 (E. Malay- sia) 9VL 9YL 9Y4 (See VP4)
* British Isles count	as one call area, as do o	others that are cross refer	

a very interesting day which lasted from 8 a.m. until after midnight, the boys are now well informed on such aspects as VHF; ATV; HF-DX; and OSCAR satellites.

The prize for the most successful student at the Youth Radio Club Scheme exami-nations held in 1969 was Robert John-son, of the Elizabeth Amateur Radio Club. For his achievement Robert received a book on transistors donated by Philips Electrical Pty. Ltd.

The most progressive club for 1969 was the Barossa Valley Youth Radio Club. The final number of certificates issued to successful Youth Radio Club members during 1969 was: Elementary, 24; Junior, 8; Intermediate, 4.

TASMANIA

During 1969, 10 clubs were registered in Tasmania. Of these, the following were most active:

Queechy High School Taroona High School

Friends School Deloraine High School Scotch College Hobart Teachers' College Devenport Boys' Brigade Glenora Area School Six of the clubs have licensed amateurs as club leaders. Unfortunately, some of these groups may be inactive in 1970 due to transfer of their leaders. Certificates awarded during 1969 were

to transfer of their leaders. Certificates awarded during 1969 were 25 Elementary and 6 Junior. In addition, David Bradley, a member of Queechy High Y.R.C. gained his A.O.L.C.P. and was issued with the call sign VK7ZCY. The WIA

Friends School

sign VK7ZCY. The W.I.A. is to conduct a radio class on alternate Saturday mornings at 10.30 a.m. during 1970. This is to follow the Y.R.C.S. certificate courses, and will be held at the W.I.A. Club Rooms, 147 Liverpool Street, Hobart (second floor). Further information about Y.R.C.S. activities in Tasmania may be obtained from the Supervisor, R. Emmett, VK7KK, 6 Haig Street, Lenah Valley, 7008. **ELECTRONICS** Australia, March, 1970

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WF

I.A.R.C. PROPAGATION RESEARCH COMPETITION

Known as "A DX Contest with a Pur-pose," the 1970 International Amateur Radio Club Propagation Research Com-petition will take place between February 28 and April 19, 1970. As a "Contribution to Propagation Re-search" (C.P.R.) the International Amateur Radio Club initiated a program in 1963 aimed as supplementing propaga-

in 1963 aimed as supplementing propaga-tion predictions by gathering data on actual amateur radio contacts and feeding this data into a computer for purposes of verification and extending the usefulness of the predictions.

magazine. The official world map showing the 90 zones (75 I.T.U. Zones plus 15 zones created by the I.A.R.C.) was pub-lished in the February, 1967, issue of this magazine.

	RULES:
	Dates
CW/RTTY	Section - 0001GMT
February 28 to	2400GMT March 15.
	-0001GMT March 28 to
2400GMT April	19.

Categories:

Entries will be accepted from fixed

I.A.R.C. PROPAGATION RESEARCH COMPETITION

LOG SHEET Page of Pages CPR Zone Contest log of amateur radio station Aeronautical CW Phone Fixed Mobile BandMHz Land RTTY Maritime Fill in only when Date/ Serial Number OSO is Multiplier Time Station Points GMT Sent Received Zone No. Country Total Zones, Countries, Points this sheet SUMMARY SHEET Page of Pages CPR Zone Call Single band Single operator Phone Teletype Multi-operator All band CW Mobile Band Score 0508 Zone Multiplier Country Multiplier Points Band Band 1.8MHz 1.8MHz 3.5MHz 3.5MHz x 7MHz 7MHz x 14MHz 14MHz x 21 MHz 21 MHz x 28MHz 28MHz х Total All bands Instructions To determine All-Band score, total each column with double lines. Single-I Stations are permitted to operate on more than one band. However, indicate and total Single-Band only the band you wish to be judged. Transmitter description and power Receiver Antennae Other operators (suggestions, criticisms, and comments) Remarks Club participation This is to certify that in this contest I have operated my transmitter within the limitations of my licence and observed fully the rules and regulations of the contest. Signature Call Name USE BLOCK LETTERS Street and number City Country Logs must be postmarked not later than 1 June, 1970. Submit logs to: L.M. Rundlett, Chairman, Contest Committee, 2001 Eye Street, N.W. Washington. D.C. 20006, U.S.A.

The final aim is the preparation and publication by the I.A.R.C. of a manual giving prevailing propagation conditions, and probable communication time be-tween each of the 75 I.T.U. zones, as a function of the amateur band used, month and the action control used. runcuon of the amateur band used, month and the solar activity. In order to generate interest in this activity, the I.A.R.C. instituted the "C.P.R. Award." The con-test is described as "a further effort to generate greater interest in this project," hence it is known as a "Contest with a Purpose."

In the January issue of these notes the C.P.R. List of Countries used in conjunc-tion with this competition was published. Please note that C.P.R. Zones are not the same as the WAZ Zones used by CQ

and mobile stations, single-band, all-band and all events. Single-band entries must be single operator only. SWL Participation:

SWL participation is encouraged. SWL rules are available from and all logs

should be submitted to: Mr Stewart Foster, G-10173, Manager SWL Contest Activities, 68 Goldsmith Walk, Lincoln, Lincs, Golasm. Lincoln, Luc. England.

Objective:

To work as many stations in as many different C.P.R. Zones and countries as possible. The I.A.R.C. Country and Zone list will be binding.

Contact Points:

Fixed to fixed stations -1 point; Fixed station to mobile station -2 points; mobile station to fixed station -2 points; mobile station to mobile station -2 points, points. (Note: No contact points for QSOs within your own zone).

Multipliers:

A multiplier of one (1) for each new zone and one (1) for each new country worked on each band and mode. For the purpose of this contest only, the following shall count for the countries multiplier; (i) All separate countries as shown on the official I.A.R.C. Country List. (ii) Each state in continental U.S.A. (iii) Each province of Canada and (iv) Each re-public of the Soviet Union.

Scoring:

(a) The same station may be worked as many times and as frequently as desired.

(b) Contacts lasting more than six minutes with the same station may be scored as separate contacts for each six minutes or fraction. To count as extra contacts, these extended contacts MUST be entered in the log as a new contact at the end of each six minutes. A single entry showing total points will be counted one contact.

(c) Multiplier credit may be claimed only once for each zone and each country worked on each band and mode.

(d) Contact points are not allowed for QSOs with your own zone, but zone and country credit may be claimed once only for each band and mode.

(e) Total score may be obtained by multiplying total points by total countries by total zones. If you are computing All Band or All Events scores, then country and zone totals are the sum of all bands, for All Events, the sum of all modes.

(f) Contacts with stations not in the contest or contacts made while engaged in other contests may be scored by supply-ing the correct zone number from the ligt

list. Logging: Use official I.A.R.C. log sheets or a fascimile with 40 QSOs per page. Fill in every line. If you void an entry, draw a line across the entire page. Enter the claimed contact point credit in the proper column. Enter the zone and coun-try in the designated column once only for each band and mode. Make all entries COMPLETE. You may enter your zone number only once on each sheet but be sure to enter the worked station's zone for each contact. Use separate log sheets for each mode and band. Use GMT only.

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LISTENING AROUND THE WORLD

Nederlands plan Madagascar relay

Details of the progress of the Radio Nederlands relay station in Madagascar have been announced. Three 300KW transmitters are being installed at a site north of Tananarive.

by Arthur Cushen

Radio Nederlands' new relay base in Madagascar is now under construction and is expected to come into operation next year. It will consist of three 300KW transmitters with the necessary directional aerial systems to cover Africa, Asia and the Pacific.

Jim Vastenhoud, who has rejoined the staff of Radio Nederlands after seven years with Dutch television has been appointed as a technical project co-ordinator station as a major project to ordination station as a major project. He reports that the sites are selected, the three 300KW transmitters and the aerials ordered, and a number of lots for the houses of employees bought. The new Madagascar

The new Madagascar relay, together with the services from Holland and Bon-aire relay, should enable Radio Nederlands to cover most of the world.

to cover most of the world. The transmitters will be located some 30 miles north of Tananarive, the capital of Malagasy. They will use 13 curtain-type areials suspended from 300-foot towers. The major service area of the transmitters will be Africa, Australia, New Zealand, In-donesia and South East Asia.

TESTS FROM MANILA

The South East Asia Radio Voice, which we reported last issue as testing on 15420KHz, has advised us of further tests on two 17860KHz. new channels, 11910 and

A letter from the Technical Director, S.E.A.R.V., P.O. Box 4148, Manila, states: "Our main lobe is directed to 280° with a width of about 60°. Our target areas are India, West Malaysia, Burma, Thai-land, East Pakistan and the China Main-land (South Portion). Your location is practically on the side lobe, but somehow a very ideal location for receiving DX signals."

The present schedule is:

GMT	KHz	
0030-0130	15420	
1130-1245	15420	
1300-1400	11910 or	17860

RECENT VERIFICATIONS

BRUNEI: John Eig, of Toowoomba, Qld., has verified Radio Brunei, which sent him a green and yellow card showsent him a green and yellow card show-ing a map of the country. The reception was for the short-wave outlet. The card came airmail in 12 days from the date of logging the station. COLOMBIA: Transmissora Caldas has verified Andrew Gardner, of Yeronga, Qld., with a friendly letter in Spanish

Notes from readers should be sent to Arthur Cushen, 212 Earn Street, Inver-cargill, N.Z. All times are GMT. Add hours for Perth, 10 hours for Sydney 12 hours for Wellington.

and a small pennant. The station is heard on 5020KHz, and is best around 0700 with its all-night transmission. Return post is not necessary for this one. The reply came in three months, and was signed by Ignacio Escobar Uribe.

CONGO: Kinshasa on 4880KHz, veri-fied Siegried Stoeger of Aldgate, S.A., with a friendly letter in French (according to "Australian DX News"). The reply was received in two months, and no return postage was enclosed. The letter was sign-ed by V. Nikuna, Chief Engineer.

PERU: Radio Loreto has confirmed our PERO: Radio Loreto has confirmed our reception with a letter and postcard, which verifies the reception on 5050KHz, of all-night broadcasts. According to the letter, the station operates OAX8D on 1150KHz medium-wave, OAX8E on 5050KHz and 0AX8F on 9504KHz. The power on the there was frequencies has recently been short-wave frequencies has recently been increased from 1KW to 10KW. The veri-fication letter is signed by Erico Ruiz Salas, the station manager. The address is Casilla 174, Jiron Arica No. 228, (write Bert) Iquitos, Peru.

ENGLISH FROM MOSCOW

English broadcasts for Australia and ew Zealand are carried over Radio New Moscow's Siberian relay station on both medium and short-wave.

GMT	KHz
1100-1130	629, 9780, 9730, 11870
1130-1200	629, 1475, 7290, 9730,
	9780
1230-1300	629, 1475, 5960, 7290,
	9710, 9730, 9780
1330-1400	629, 1475, 6160, 7290,
	9780, 9730, 11870

LATIN AMERICAN NEWS

Some information which will enable listeners in the South Pacific to hear new Latin American stations in the coming winter, is taken from the latest issue of the Danish Short-Wave Club's "International

Bulletin." Listeners in the northern hemis-phere are listening to many Latin Ameri-can signals at the moment. These stations will be audible in our area shortly.

will be audible in our area shortly. PANAMA: Radio Mirimar, Apartado 4402, Panama 7, on 6030KHz is a new station on short-wave. The call is HP5B and the schedule is 1030-0300GMT. CHILE: Radio CE953, using 9530KHz with 1KW, is on the air 1100 to 0500GMT. The station has the mailing address of Casilla 49-D, Arica. COLOMBIA: Radio Atlantico Barran-quilla, is active on 4905KHz, and has been heard to 0500GMT. The station verifies with a letter and pennant. Radio Atlan

with a letter and pennant. Radio Atlan-tico has been inactive on short-wave for some months.

VENEZUELA: Radio Merida is VENEZUELA: Radio Merida is a new station operating on both medium and short-wave. The station operates 95YVTL on 1490KHz medium-wave, and as YVTR on short-wave 9720KHz. Both stations have the power of 1KW. The address of the station is Radio Merida, Avenida Prin-circl Marida Varazuela cipal, Merida, Venezuela. ARGENTINA: Radio Argentina Exterior,

Buenos Aires, has been observed in Ger-man from Monday to Friday at 2100GMT on 11710KHz. The station has also been heard in English at 0600 to 0700GMT on 9690KHz by Chris Davis of Featherston, N.Z.

BOLIVIA: Radio Cruz del Sur has moved from 4985 to 5025KHz. This is the second time this station has made this frequency change to avoid interference. The station is keen to receive reports, and verifies change to avoid interference. The states is keen to receive reports, and verifies with a colourful card. The address is Cajon 1408, La Paz, Bolivia. ECUADOR: Several signals from Ecuador

are being observed in the 49M band. Radio Mundial is using 5965KHz with 1KW and is on the air 1200 to 0400GMT. The address is Casilla 12-44, Riobamba. Radio Colon, using 5970KHz, has the address Apartado 2912, Quito. Radio Me-tropolitana, on 6150KHz, has been heard at 0400 and again at 1100GMT. The attain address is Manhi 566 w Farster station address is Manabi 556 y Fargas, Ouito.

HIGHER POWER FOR GUYANA

The Guyana Broadcasting Corporation, at Georgetown, is to add a further ser-vice on medium and short-wave wth a new "action radio" type program. The station was officially opened on January 1, and is the most powerful voice in the eastern Caribbean.

HONOUR FOR ART CUSHEN

Our short-wave correspondent Art Cushen has been honoured by the Queen in the New Year Honours List by the award of an M.B.E. This honour is in recognition of his community services in radio, broadcasting and journalism, and for work in the field of blind welfare. We warmly congratulate him on his award, and for the success he has achieved in his chosen field despite the handicap of total blindness from which he has suffered for many years. He is now recognised as one of the world's most prominent listeners, and besides his work for "Electronics Australia," to which he has been a regular contributor since 1952, he is a regular broadcaster for Radio New Zealand, the N.Z.B.C., and Radio Nether-lands, in his own programs; the short-wave editor of the Our short-wave correspondent Art Cushen has been lands, in his own programs; the short-wave editor of the N.Z. Radio DX League's publication; and his contribu-tions to SW listening are known throughout the world.



Two medium-wave transmitters are on 560KHz with 20KW and on 705KHz with 2KW. Two short-wave transmitters will operate on 3290 and 5950KHz, both with the power of 10KW. The station slogan "Action Radio" is to be used. The station is an off-shoot of the Guyana Broadcast-ing Corporation, which has been heard on 5980KHz at 0910GMT, using 2KW.

CYPRUS VERIFIES

CYPRUS VERIFIES A fine verification card has been received by Bob Padula, of Melbourne, Vic., con-firming the reception of broadcasts from the Cyprus Broadcasting Corporation. The station is now using 11910KHZ and has been heard after ETLF leaves the air at 1915GMT. A program of Mediterranean-style music was observed, with identifica-tion in Greek and English, when the sta-tion closed at 2100GMT. The station an-nounced that they would return to the fre-quency at 1900GMT next day. The verification card is most attractive,

The verification card is most attractive, being printed in full colour. It has full verification details, and states the transverification details, ar mitter power is 30KW.

KGEI SOON 250KW

KGEI SOON 250KW In a matter of weeks station KGEI at San Francisco, operated by the Far East Broadcasting Company, will be using 250-KW. A verification letter from the station Assistant Engineer Mr Tom Tweedell in-forms us of these plans. Mr Tweedell said "It is very interesting to hear from people who have been acquainted with KGEI since its beginning in 1939 at the World's Fair. Our transmit-ter and studios are located near Belmont in a new subdivision of Redwood City, California, about 25 miles south and slightly east of San Francisco. We are still using the original basic transmitter which was at the fair. The power was raised to was at the fair. The power was raised to 50KW shortly after it was relocated here on the then mud flats, and it has been further modified since FEBC acquired the

further modified since FEBC acquired the station in 1960. "Our new 250KW transmitter is still to be constructed in Iowa. We had originally expected to have it some time ago, but as a prototype for the manufacturer it has taken longer than planned. We hope to have it later this year, but installation and testing may take some months thereafter." The negent schedule of KGEU is:

The present schedule of KGEI is:

The present schedule of KGEI is: GMT KHz 2220-0200 15240 0203-0503 9715 During October the station was heard for the period 0203-0503GMT on 11955KHz, but from November this was changed to 9715KHz, to provide a better signal in the coverage area stretching from Mexico to Argentina. The station's address is P.O. Box 15, San Francisco, California 94101. Verification, which is in the form of a card, pennant and letter, notes that English programs are from 0400GMT. The 9715KHz frequency is mixed with other stations, and at 0455GMT is block-ed by Radio Nederland at Bonaire. SLOW DOWN AT RADIO

SLOW DOWN AT RADIO CANADA INSTALLATIONS The plans of the International Service of the Canadian Broadcasting Corpora-tion, Montreal, were discussed in the September issue, with the news of the installation of five 250KW transmitters at Sackville for early operation. Due to Canada's present economic re-cession, the Government has rephased the

cession, the Government has rephased the new transmitter and antenna plan over a longer period of capital spending. The first two of the 250KW transmitters will be testing by the end of this year. The additional three 250KW transmitters required to complete the project will be tested late 1971. The new antenna systems and other work at Sackville is now expected to be completed by 1974, when the new transmitting facilities will be fully operational. cession, the Government has rephased the operational.

The slowing down of the project has delayed the final date for completion by two years, but the increase in power for the Montreal signals should be noted later this year. In Montreal, work proceeds on the huge new radio and television centre LAFAYETTE Solid State

5-Watt 27 MHZ Two-Way Radio



\$169.50 (Crystals Extra) Model P.M.G. Type Approved (Licence Required) HE-20T

Cool Instantaneous Operation

- Crystal Controlled Transmit and 455 KHz Mechanical Filter. Provide Transmit and TVI Trap.
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 - May also be used as P.A. Ampli-fier with External Speaker.

This solid state transceiver is ideal for 27MHz communications. Solid state circuitry features low battery drain and provides instant operation; 5-watt transmitter input with efficient push-pull audio modulator; a Pi-network for matching the output to 30-100 ohm antennas; an extra-sensitive superhetrodyne matching the output to 30-100 ohm antennas; an extra-sensitive superhetrodyne receiver. Fine selectivity and adjacent channel rejection is obtained through a 455 KHz mechanical filter. Sensitivity: .7 uV for 10 db signal to noise ratio. Receiver also incorporates automatic floating series-gate noise limiter and variable squelch control resulting in virtually no background noise between calls. A rear mounted low-loss antenna jack accepts SO-239 type connector used with ground plane and direct mounting antennas. Complete with fused DC line cord for negative ground battery and push-to-talk mike. Size: $8\frac{1}{2}$ in D. x $4\frac{1}{2}$ in H. x $11\frac{1}{2}$ in W.

.5-Watt 3 Channel Walkie Talkie



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- Sturdy Metal Case.
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- Range Boost for Extended Talk Power,
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Lightweight 2-way transceiver includes three switchable channels. Call alert system sends or receives a pleasant alerting tone for convenient calling. 14 transistors, 1 diode, 1 varistor superhet circuit with noise limiter and variable squelch, .5 watt transmitter with range boost. Supplied with telescopic antenna, batteries, carrying strap, and crystals for 27.240 MHz.

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with speaker and amplifier. from \$90.00			buried pipes, etc. Freight pay- able at nearest attended railway
CIRCULAR SLIDE RULE	P.M.G. Phone Jack and plugs, 25c	BRAND NEW	station. \$39.00
3% in diameter. Will do the same work as the conventional	each, 45c the pair. Post 7c.	IN CARTONS Special discount for quantity	4 DIGIT RELAY COUNTERS
slide rule. Instruction book in- cluded.	NIFE CELLS	807 75c X6iM \$2.20	50-volt D.C., suit siot car. Lap counters, etc.
\$1.25 each Post 10 cents.	1.2 Volt fully charged, 4in x 3in x 1in 4 AH. \$1.00 each	65N7GT 95c CV850 \$1.50 8989 \$1.00 1H6G 30c	\$1.25 each. Post 13c.
REFLECTOR GUNSIGHT Contains these lenses:	Post, N.S.W., 25c; interstate 35c.	5U4G 95c 832 \$5.00 77 \$1.00 6AK5 \$1.50	ALTEC STUDIO MICROPHONES
1 Lens 1 In Focus, 11/2 diam. 1 Lens 1 11/16 Focus, 11/2 in	WALKIE TALKIE TWO-	EF50 35c 6X4 \$1.00 6U7 75c 12SK7 50c	639B Western Electric, top grade, original cost \$250, ideal Broad-
diameter. 1 Air-spaced Lens, 11/4in diam.	P.M.G Approved Citizen Band.	5Y3. \$1.75 VR65 25c	cast Studio, music recording, Church and play recording, etc.
1 Filter Lens, 1 Graticule. 1 Lampholder. \$1.85	9 Transistor, \$79.00 per set of 2. Post, N.S.W. 50c; interstate, 60c.	6C4 50c VT4C 75c 2 x 2 75c AU5 \$1.00	Fraction of original cost. Price on Application.
Post.: N.S.W. 30c; Interstate: 40c. P.M.G. TYPE	in the	6AG5 80c 80 \$1.25 12AU7 \$1.00 6AK5W \$1.50	240 VOLT 522 POWER SUPPLY
TELEPHONES		5	Supplies all necessary voltages to operate 522 transceiver from 240
Standard desk type with magneto bell calling device, Range 30 miles.	A Constant of the second secon	CATHODE RAY TUBES 3FP7 \$2.95 5BP1 \$3.50	V A.C. Complete and ready to plug in \$30.00.
Uses standard batteries at each phone. Any number can be con-	P.M.G. TYPE KEY SWITCHES.	3JP1 \$2.95 V1669 4/1 \$2.95 CY2184 \$2.95	SOLENOIDS
nected together on single line. \$23.00	45c each. Post, 15c.	PLEASE ADD POSTAGE	Plunger Type 12V 300M.A. Suit electric camera control, miniature trains, radio, etc.
(2 TELEPHONE SETS) 30c cartage to rail. Freight pay-	BC 221 Frequency Metres	ON ALL ARTICLES	\$1.25. Post, 10c. 200 Mill. amp., 24 volt. 1/8in push
able at nearest attended railway station.	\$55.00		movement. \$1.25. Post 10c.
Please note we are now able to include 1/2 mile of telephone cable FREE with each set of			LENSES
Phones,	0		TOP GRADE ACHROMATIC 2in DIAMETER, 20in FL ideai as
BATTERY CHARGERS 240 volt A.C. Input.		TELESCOPES	telephoto lens, telescope objectives. \$13. Postage 46c.
240 volt A.C. Input. Each battery Charger will charge either 6 or 12 volt batteries.	45 x 40 coated Lens with tripod \$10,95	30 x 40 with Tripod	CONDENSER LENS
2 amp. without meter, \$13.75 2 amp. with meter, \$15.75 Post N S.W. 70c; Interstate 95c.	30 x 30 Power Coated Lens Brand new,	\$7.95 Post N.S.W., 70c; interstate \$1.20	21/2in DIAM. 2in FL. \$1.50 each or \$2.50 per pair. Post 2ic.
	\$3.75	PETROL MOTOR	CONDENSER LENS
ELECTRIC MOTORS	60 magnification with a 60mm coated objective lens.	GENERATOR SET BRAND NEW EX-ARMY 300 watt, 15 volts, 20 amps.	1½in diam. 1½FL. 50c each. Postage, 17c.
11/2 to 3 voits D.C Ideal for model boats, cars, pianes, etc.	With tripod.	Made in Canada, Complete with	FOUR CHANNEL
Strong torque. Only 65 cents each or 10 for \$4.00.	\$23.00	tools, instruction book, spares, etc. Only \$75.00 \$1 cartage to rail, freight pay-	BRANCHING AMPLIFIER With 4in Vu, meter GLORAD. Complete with Portable Power
(Post 7c).	As illustrated. Postage, 95c; Interstate \$1.20.	able at nearest attended railway station.	Converter. 600 ohm balanced input and output. Ideal for outside
(2-way radio) R.C.A. America RT 68, 24 volt, operated 10 watt out-	HIGH STABILITY	C.M.A. CABLE	broadcasting, etc. \$39.50
os, 24 volt, operated 10 watt out- put 38-54 megacycles F.M. crystal locked. Transmitter and receiver	RESISTORS	240 volt 3/.036 black, new and perfect. 100yd rolis \$3.00; 6 or	MONITOR SPEAKER
using frequency synthesiser in 100 K/cs: step 10 channel per	I.R.C. brand new, usually 80c ea. 50 assorted values for only	more. 30c cartage to rail. \$2,50	UNIT Ex-A.B.C., consisting of low re-
Leads, mike and headphones	\$3.75 Post 15c.	Frequency Counter Cintel type 388, \$250.00	sistance 8in speaker in Acoustic Labyrinth Baffle Box, complete
\$45, 60c cartage to rail. Freight payable at nearest attended rail-	RECEIVER 8C A.W.A. With ABC and D Colls.	VIBRATORS, 6 volts, 7-pin 75c cach.	with 10-watt ampilfier, 600 ohma pius 8dbm input, 240 volt A.C.
way station.	Complete with all spares. \$90.00	UNISELECTORS, 4 BANK, \$4.00 Post, N.S.W., 25c; interstate, 30c.	operated. \$37.50
C2-way radio) 62 set ideal small	ZOOM FOCUSING	iNSTRUMENT TRIPODS, sturdy, wooden frame, Telescope, Ex- tend to 4ft 6in \$13.00	TEN CHANNELS
ships, Hams, etc. 1.6 to 10 megs. Crystal locked or V.F.O. controlled	MICROSCOPE Battery and mirror illuminated	SELSYN MOTORS MAGSLIP Mk. 11 \$5.25 ea,	VHF TRANSCEIVER Types TR1934 100-125 meg/cys.
5 watt output. Complete with an- tenna, headphones and mike \$60. 60c cartage to rail. Freight payable	900 x magnification, complete with disecting kits, slides.	No. 19 TWO-WAY RADIOS Soid a sis without power supply.	and TR1935 i25-150 meg/cycles. 28 volt DC operated AM single crystal iocks both TX and RX on
at nearest attended Railway Station.	\$14.50. Postage N.S.W. 65c. Interstate 85c	leads, accessories, etc. Only \$15. Or complete with above gear, \$35.	same channel complete with generator.
HEAD PHONES	TYPE S POWER SUPPLY	BINOCULARS PRISMATIC. Coated Lenses	\$33.00
Low impedance moving coil fitted with rubber muffler to reduce ex-	(240 Vac supply for AT 5-ARB) suit most types of Disposal trans- mitters and receivers outputs 250	Brand new. Complete with case. 8 x 30	RECORDING TAPE Ex broadcast studio E.M.I. 3600
ternal noise, fitted with press to	mitters and receivers outputs 250 volt, 10ma 550 voit 200ma, 300 volt 100ma, \$30.00	7 x 50 \$22.15 10 x 50 \$23.07	feet on 101/2in spooi, \$4.50. Post-
talk, dynamic hand microphones. Ideal for use with all types of transceivers, \$3,50 pair. Same with	TELEPHONE WIRE	12 x 5 \$23.95 20 x 50 \$26.50 Post. N.S.W., 70c: Interstate, \$1.20	age 85c, 600 feet on 5in spool \$1.45, postage 13c, 150 feet on 3in spool, 65c, postage 9c.
black felt muffler, \$4.50 pair. Post N.S.W 25c; Interstate 30c.	21 gauge copper, plastic covered. Ideal telephone or beli wire. 1.320ft coil of twin (equal Va	3000 TYPE RELAYS	CASSETTE TAPES C60 \$1.60. C90 \$2.20. C120 \$2.99.
COLLINS TRANSCEIVERS	mile) \$7 per coil. Post, N.S.W. 70c; interstate \$1.20.	P.M.G. 200 Ohm — 1.500 Ohm Coils, \$1.25 each.	Post 13c.
Auto-tuned 100-150 megacycles, 10 channels	SCOOP PURCHASE	A.W.A. AMPLIFIERS	TELEPRINTER PAPER TAPE
\$65.00	Gramo Motors. New. Made in U.S.A. 4-speed 240 volt A.C. 50 cvc Oniv \$2,75 each	240 VAC with pick up Terminal. Used in good order Ex Studio.	8¼in x 6 5/8in Full Page
16'6" WHIP AERIALS	50 cyc. Only \$2.75 each. Post, N.S.W. 30c; interstate, 40c.	5-watt model. \$15.00 SPECIAL lucky dip valve offer,	\$1.50 per roll. WHEATSTONE BRIDGE
6-Piece, brand new, \$5.75. 60c cartage to raii, Freight payable at nearest attended railway station.	CO-AXIAL SWITCH 70 ohms 4 positions,	15 new valves in cartons for only \$2.00. We haven't got time to	Top grade
nearest attended railway station.	can be motor driven completely waterproof 70 ohms type con-	sort them, so you reap the benefit. Post 60c.	\$65.00
AVO MULTI METER Type CT 38	nectors. Housed in metal case $9in = x - 8in = x - 8in = 5.00$ each. Post		
\$75.00	ASTRONOMICAL	Deitch	Bros.
A.W.A. AUSTRALPHONE	TELESCOPE	PCITCI	PIUS.
Transceivers 12 V New Complete Station. 1.6 to 10 megs on transmit.	31/2in reflector 126 X magnifica- tion. Complete with 4 X finder and equatorial mount.	70 OXFORD STREE	T. SYDNEY. 2010
0.54 to 16 megs on receive. \$150.00	\$59.00 Post \$1.50		NO C.O.D.
1		, ventry t	
158 ELECTRONIC	S Australia, March, 1970		and the second second

for the Canadian Broadcasting Corpora-tion, which will also house the Radio Canada studios.

Canada studios. The transmissions from Montreal are well received in the service to the South Pacific, from 0830 to 0930GMT, using 9630 and 5970KHz. The special program for the short-wave listener, "Radio Canada

9630 and 5970KHz. The special program for the short-wave listener, "Radio Canada Short-wave Club," is broadcast at 0845GMT on Saturday. Radio Canada recently celebrated its 25th anniversary of short-wave broadcast-ing. The service commenced on December 25, 1944. It was originated from Sackville, New Brunswick, the site of the present transmitting facilities. Just before the transmissions began, 25 years ago, we heard the tests of CHTA using 15220KHz, then the initial service with a limited schedule of 1115 to 1700GMT. From then on, further trans-mitters were added until three 50KW units were in use. Callsigns, which numbered were in use. Callsigns, which numbered over 30, were verified. A 7500 watt trans-mitter was installed to provide a service to, Northern Canada.

WORLD RADIO MARKET

WORLD RADIO MARKET Some idea of the types of radio receivers used by listeners throughout the world has been gleamed from a recent survey conducted by Radio Japan. It was found that some 30 per cent of the short-wave receivers used by listeners who took part in the survey were of Japanese manu-facture. Then followed sets made in the Nederlands, United States Germany and Great Britain. The survey, which was made of listeners throughout the world, found that more Philips sets, were in use than any other brand of receiver, then followed the Japanese National and Sony brands. Radio Japan services appear to be re-ceived well throughout most of the world. Their monthly program magazine is now

Their monthly program magazine is now mailed to over 100,000 listeners.

UN RADIO FOR CONGO

The United Nations has announced that they plan to operate a short-wave station from the Congo to serve European lan-guage speaking listeners in southern Africa. This move is seen as a measure to combat the broadcasts of Radio South Africa and attempt to tell southern Africa of the United Nations feelings on apartheid.

apartheid. The stations will be in the Congo Kinshasa. This was the former Belgium Congo, which during the early 1940s was one of the best received countries in Africa. The Belgian Government moved there after the occupation of their country in 1940 and operated the "Goodwill Station," which was transferred back to Brusssells at the end of the war. The Belgian station ORU formerly carried many English programs, but in recent years these have been reduced to two ten-minute sessions each day. Some of our verifications from the old Belgium Congo include such stations as OTC at Leopoldville. The station had the power of 50KW. During the struggles in the Congo some

During the struggles in the Congo some years ago, another powerful station was set up by Kitanga, at Elizabethville. This station is now known as the "Voice of African Brotherhood," and broadcasts from the renamed city, now known as Lumumbashi.

RADIO PORTUGAL EXPANSION

The broadcasts of Radio Nacional, Lis-bon, Portugal is familiar to short-wave listeners, and even more so in recent years, with their "Voice of the West" transmissions.

missions. The station was planned in 1949 and was completed in April 1953. At the outset it was equipped with two 100KW and one 50KW transmitters. Four transmitters of 100KW were added and since then an additional 100KW and a 10KW trans-mitter have been installed.

The transmitting site also houses a 100KW medium-wave transmitter, used for the medium-wave service to Europe on 755KHz. Some 22 high-gain directional aerials are used, and at the present time

NEW SCHEDULES OPERATING

DARWIN BECOMES OPERATIONAL

On December 20, 1969, Radio Australia celebrated its 30th year of broadcasting. At the same time the relay station at Darwin was phased into the schedule. We covered the Darwin relay station in the January 1969 issue, with details of the receiving site and the transmitters. This month the complete Darwin installation is expected to be put into full operation after a period of testing over several months. Three 250KW transmitters will boost Padio Australia circular to Asia Radio Australia signals to Asia.

Radio Australia signals to Asia. Radio Australia commenced on December 20, 1939, using two low-powered transmitters at Sydney, and a 2KW transmitter at Lyndhurst in Victoria, while another transmitter at Perth began broadcasting to South Africa. Today Radio Australia has broadcasts in eight languages, English, French, Indonesian, Mandarin, Thai, Japanese, Cantonese and Vietnamese. Radio Australia has some 58 hours of transmissions every day. It carries 44 news bulletins in its day's schedule. The service teaches hundreds of thousands of Indonesian, Thai and Viet-namese to speak English, and its transcription service supplies programs to 59 stations in 29 countries. In conjunction with the Australian Post Office, Radio Australia now operates 12 high-powered transmitters at three sites, Shep-parton, Lyndhurst and Darwin. The Darwin transmitters and facilities cost some \$8-million and took ten years to plan and establish. Recular daily transmissions from Darwin are as follows:

Regular daily transmissions from Darwin are as follows:

GMT	KHz	Language	
2300-0030	15130	English	
2300-0030	15355	Indonesian	
0030-1000	17715	English	
0030-1230	15355	English	
1000-1130	6055	Indonesian	
1136-1330	6055	Mandarin	
1230-1330	9650	Vietnamese	
1330-1430	9650	Thai	
1330-1430	6055	Cantonese	

On Sundays only, transmissions begin at 2300GMT and run through to 1400GMT. In March, when the full facilities at Darwin and the aerial system will have been completed, it is planned to extend the schedule to cover both South Asia and East Asia.

A WEEK'S FAVOURITE PROGRAMS Readers often ask for information on some of the most interesting programs which are on short-wave each week. I find my listening always confined to some of the major DX sessions, as well as programs about short-wave listening and listeners. A typical week on my listening calendar is listed below, I should explain that this is only a small number of the 30 DX programs available, but these are the ones best received.

GMT	KHz	SUNDAY Country	Program
0515	11750, 9410	Britain	Program Letter Box
0530	15240	Australia	Mail Bag
0545	7150, 9640	Britain	Listening Post
0630	11730	Holland	Happy Station
0730	11710	Britain	DXers Calling
0815	7150, 9640	Australia	DXers Calling B.B.C. World Radio Club
0835	7150, 9640 9630, 5970	Canada	Listeners Corner
1005	11875, 15235	Japan	Listeners Corner and DX News.
		MONDAY	
0915	11775, 9590	Switzerland	DX Merry-go-round
0730	11890	Philippines	FEBC Mailbag
		TUESDAY	
0645	11730	Holland	His and Hers
1245	9625	Sweden	Sweden Calling DXers
0.000		WEDNESDAY	
0645	9540, 11780	New Zealand	Arthur Cushen's DX World (First Wednesday)
0835	17815, 21545	South Africa	DX Corner
0936	9745, 11915	Ecuador	HCJB DX Party Line
1030	9520, 11830	New Zealand	DX World
0415	11000	THURSDAY	
0645	11730	Holland	DX Jukebox DX Jukebox
0815	9715	Holland	DX JUKEBOX
0730	9540, 11780	FRIDAY New Zealand	Mailbag
0750	9540, 11760		
0840	9630, 5970	SATURDAY Canada	Radio Canada Short-wave Club
0840			
		GLISH FROM	
	st schedule receiv transmissions as:	rea from the Ol	RTF in Paris for English broad-
GM		KHz	
	-0530		9700, 11920, 11930, 15120, 17730

GMT	KH
0515-0530	715
1100-1115	152
1930-1945	151

7155, 7255, 9700, 11920,	11930,	15120, 17730	
15295, 17720, 21580			
15185 15295 21580			

The address for reports is now P.O. Box 9516, Paris 16, France. This address was announced in January, when the station was heard asking for reception reports.

ANNOUNCEMENT Deitron KITSETS

Are you interested in Kit Sets or parts for all future Electronics Australia projects. If you are, watch for future advertisements in this magazine.

As from March 1st, 1970 all parts or complete kits of parts for all future E.A. projects will be available from DEITRON ELECTRONICS (SALES) PTY. LTD. or their distributors which will be listed in their advertisements. Interstate outlets will also be appointed (enquiries welcome)

N.B. All Kit Sets will be of the highest quality components, e.g. Elna, Piher, Fairchild, A.&R: Deitron and many other well known brands. [All sheet metalwork & circuit board available]

Cable Address: "DEITRONICS", SYDNEY.

"Phone: 31-5430

RLINGHURST, N.S.W., 2010

31-6786



some special logarithmic aerials are being designed for the European service.

Of the original sets of aerials, six are directed to Asia and the Far East, seven to Africa, two to South America, six to North America, and two to areas off Newfoundland for the Portuguese fishing fleet. A special curtain antenna is used for European broadcasts for European broadcasts.

FLASHES FROM **EVERYWHERE**

EUROPE

- U.S.S.R.: Radio Kiev, Ukraine has English broadcasts to Europe and North America which are scheduled from March 1 as follows: 2230-2300GMT on 9640, 7120KHz; 0030-0100GMT on 11730, 11700, 9760, 9660, 9610KHz; 430-0500GMT on 11960, 11730, 11700, 9760, 9660, 9610KHz.
- **YUGOSLAVIA:** Radio Belgrade has started using 7240KHz for its Home Service says the Swiss DX Session. Programs have been heard from 1400 to 2400GMT. The same service is carried on 6150KHz. Radio Belgrade's foreign service has transmissions in foreign service has transmissions in English from 1530 to 1600GMT on 9620, 11735 and 15240KHz: 1830-1900-GMT and from 2000 to 2030GMT on 6100, 7200, 9620.
- GREECE: The National Helenic Broad-**REFUS:** The National Helenic Broad-casting Service, at Athens, now operates: 0700-0815 0900-1000, 1030-1300, 1930-2100, 2200-2230, 230-2330 GMT on 9605, 11720KHz; 1330-1515, 1630-1700, 1830-1900GMT on 7295, 9605KHz; and 1730-1800GMT on 11720, 15425KHz.

AFRICA

- SENEGAL: According to "DX News of Norway," Radio Senegal, Dakar, now has an International Service. The schedule from the station shows that it has a 100KW SW transmitter on the air with the International Service from 1800 KT or 11805 KT 1800 to 1830GMT on 11895KHz.
- CONGO: Radio Brazzaville has ONGO: Radio Brazzaville has been heard on the new frequency of 15145-KHz according to "Australian Radio DX News." This channel carries the relay of news in English from Paris at 1930GMT. The time of this news bulletin was recently changed from 1915GMT. Following the news, the station has its own announcements at 1944GMT in French and English and then follows the interval signal. On another frequency, 15190KHz, Brazza-ville is observed at 2000GMT with a been

program in French; this transmission closes at 2030GMT.

MAURITANIA: According to Swiss DX Session, Radio Mauritania now broad-casts on the folowing schedule: Monday to Saturday 0700-0800, 1800-2230GMT on 4850KHz; 1200-1430GMT on 7245, 9610KHz; Sunday 0800-1400GMT on 7245, 9610KHz; 1700-2300GMT on on 4850KHz.

The address of the station is P.O. Box 200, Nouakchott, Mauritania.

ASIA

- IRAQ: Baghdad Radio has programs for Europe which include English 1930-2020, German 2020-2100 and French 2100-2200GMT. These programs are carried on 6030 and 6905KHz A ser-vice in Arabic is on the air 1800-2230-GMT on 7180KHz and 1100-2300GMT on 11782KHz; and sometimes from about 1800GMT on 6155KHz.
- CEYLON: The Commercial Service of Radio Ceylon at Colombo, is now on the following schedule for the morning broadcasts.

GMT	KHz
0130-0430	7190, 11800, 15230
	(service in Hindi).
0130-0330	9720, 15230
	(service in English).

CAMBODIA: Radiodiffusion National Cambodia is reported by the Japanese Short-Wave Club to be operating on 690 and 740KHz. The present weekday schedule is 2315-0100, 0400-0700, 0900-1700GMT; and Sunday 0015-1600GMT.

DZH4 ON 2425KHz

We were surprised to hear a new signal from the Philippines in the 120-metre band, when we tuned DZH4 relaying medium-wave station DZHP in late January. This station was received on 2425KHz. Later, we heard DZHP confirm, after the news bulletin at 1130GMT, that DZH4 was carrying the program also carrying the program also.

The Philippines has two signals in the 90-metre band, but this the first use of the lower band. Programs were in English throughout, with frequent commercials, mainly of American style, after each musical item, and the station had the standard encourses style, after each musical item, and the station had the standard announce-ment that "You are tuned to DZHP broadcasting from Manila on United Nations Avenue, 1130KHz on your radio dial." At 1200GMT or 8 p.m. Manila time, the complete network of the stations operated by the Radio Mindanao Network were called in for a network program.



Jim Vastenhoud, who has been appointed technical project co-ordinator for Radio Nederlands (see page 156). He is well known for his work with DX Jukebox, being technical advisor to the program.

News in French is at 2330 (Sunday 0030), 0530 and 1230GMT; English 2345 (Sunday 0045), 0545 and 1245GMT. Each bulletin of 15 minutes duration.

CEYLON: The Ceylon Broadcasting Cor-poration now issues a new verification card, which shows a selection of wild life of Ceylon. This card has been re-ceived by some of our Australian read-ers, in confirmation of recent reception reports.

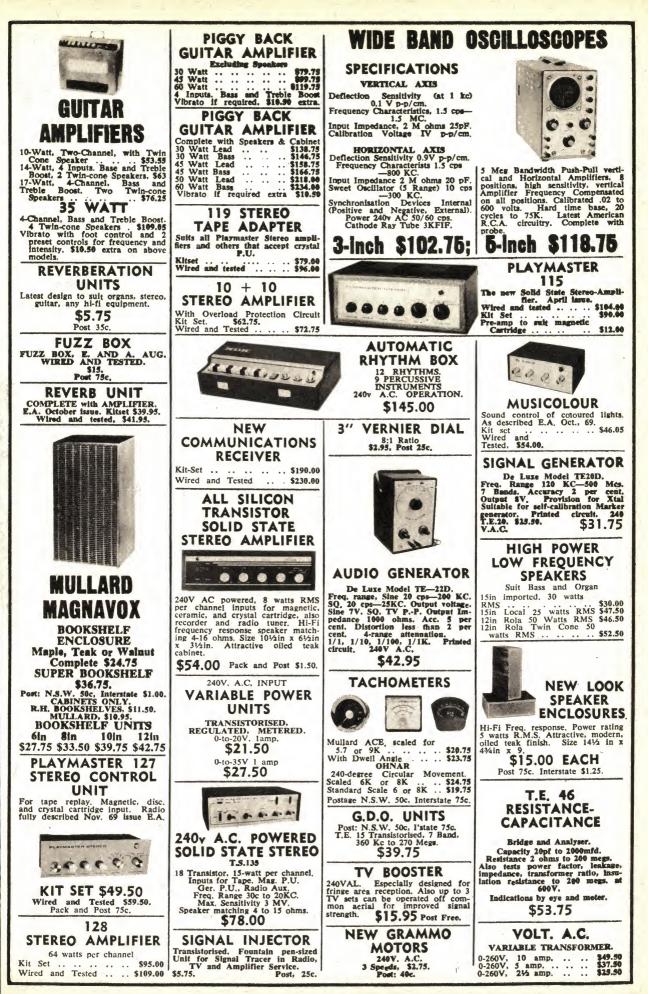
BROADCAST BAND NEWS

- TURKEY: A new 300KW transmitter on medium-wave, opened last November, is located at Diyarbakir. The transmitter
- located at Divarbakir. The transmitter broadcasts the radio programs of Turkish Radio and Television, and operates on 1061KHz, from 0355 to 2200GMT.
 COLOMBIA: A new station reported in "Sweden Calling DXers" is "La Voz Portena" Aereo Baranquilla. The station is using 1500KHz, and the station is already confirming reception reports by a verification card.
 LIBYA: Bengazhi Radio how has programs in English with news at 1600-1615. Five minute programs of news in English, Italian and Frency are broadcast from 1800 and 2000GMT on 1546KHz.
 - 1546KHz.





ELECTRONICS Australia, March, 1970



ELECTRONICS Australia, March, 1970

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AMPLIFICATION	*****	****	★ ★ PHONE 51-3845 51-7008
		RAD	A CONTRACTOR OF A CONTRACTOR A
		MAL	
STO E	ELECTRONICS		A AVENUE, MIDDLE COVE AFTER HOURS 40-5391
126 VICTOR		ARRICKVILLE	51 2945
	TA KUAD M	AKKICKVILLE	- JI-304J
NEW VALVES All valves 75c unless otherwise stated. 1G4 75c 125K7 50c 1H5 75c 723A \$6.00 1S5 75c \$90 \$1.75 1T4 913 \$1.75	LAB STANDARD (METERS) 7in in Cedar Cabinets. Leather Cases. 0 to 10 amps. 0-20 amps. 0 to 50 amps. 0-250 amps. \$10.50	DUMONT 5" WIDE BAND OSCILLOSCOPE LABORATORY MODEL. Tested, New condition, \$99.00	100 YDS HOOK-UP WIRE 10 Assorted Colours. \$1.00 Post 25c.
6AK6 75c 289B and 6AR6 Socket \$5.75 6B6 75c 866A \$1.50 6B8 75c 954 \$50cket 6B76 956 \$50cket \$5cket 6C8 75c 956 \$50cket 6C8 75c 9006 \$9cket 6C6 75c 9006 \$9cket 6C6 75c EF36 75c 6J6 75c EF39 75c 6J76 75c EM35 75c	CAVITY TUNING	COSSOR 1 1049 DOUBLE BEAM \$170.00	TYPE 1935 V.H.F. TRANSCEIVER 100 to 155 megs. New condition. \$29.75
6K6 . 75c 6U7 . 75c 6K7 . 50c VR105/30 \$1.50 6K7 . 75c VR150/30 \$1.51 6SA7 Metal 75c T240 . \$1.00 6SC7 6C6 . \$1.25 \$5H7 . \$6C7 . \$1.26 6SS17 . 95c 6L6 . \$1.50 \$5C8 \$5C8 \$5C8 6SS17 . 95c 6L6 \$1.50 \$5C8 \$75c \$6X5 . \$15c8	PYE EX-TAXI TRANSCEIVER. Complete All Valves, speaker, mic. Clean condition. \$32.00	NEW MOBILE R.F. LINEAR AMPLIFIERS 2 to 10 Megs. 200 Watt P.E.P., 12v Power supply. Easily converts to other brands. Suitable for S.S.B.	BENDIX FREQUENCY METERS New, factory fresh. Modulated units. With A.C. supply. \$75.00
6X5 . 75c 6G8G . \$1.50 7C5 . 50c 618G . \$1.50 12AT7 12AU7 12AU7 \$1.00 12BE5 6AW8A \$1.00 12SU7 6EM5 \$1.00 2A3 6EM7 \$1.00 2C26 6CW7 \$1.00 2X2-879 50c 12BH7 \$1.00 3A4 6DX8 \$1.10 5X4 . 50c 6AU4 \$1.00	TYPE 62 TRANSCEIVER 2 to 10 megs. NEW. \$49.50	Silver. Variable Inductance. Sufficient reserve power for exciter, \$15.00 No. 19 TRANSCEIVERS	WANTED Communications Receivers. Test equipment. P.A. Gear. Large or small surplus stock. Best prices. Call, write or phone any time.
SY4 S0c GBW7 75c SZ4 1R5 75c 75c GAC7 75c 6X9 51.00 GAG5 95c 6Y9 \$1.00 GAG7 50c 6H37 \$1.00 GAG7 50c 6H38 \$1.00 GAJ3 50c 6H38 \$1.00 GAL5 75c 649 \$1.00 GAM5 75c 649 \$1.00 GAN5 \$1.25 6F6 75c	RELAYS Weston Microamp Meter Relays 75UA-218UA \$5.00 12 volts, DPDT, 5 amp \$2.00 12 volts, DPDT \$1.25 100pf TX var. condensers \$1.00 Plil-speed Polarised relay \$5.00 2000 ohms \$1.25	2 to 8 megs. 15 valves. New condition. \$19.75 ALSO BRAND NEW. \$27.00	NEW DYNAMIC OR SOUND POWERED MICROPHONES Pushbutton Operation. Low Impedance,
NEW POWER TRANSFORMERS	NEW C.R.O. TUBES	TRANSISTORS	\$1.25 Post 50c.
240VAC. 50cps. Primary standard fil. windings. 385VCT 80MA	3AP1-906 3in \$2.75 CV112 3in \$3.00 VCR97 6in \$3.75 ACR10/VCR139A 3in \$3.00 CV152 134in \$3.225 SE5A7 \$9.75 \$9.75 09D \$9.75 \$9.75	2N422	EX PMG HAND SETS TELEPHONE HANDSETS \$3.00 Pack & Post 50c.
240/240 60MA \$2.50 125MA filter choke \$2.00 100MA filter choke \$1.25 Add Pack & Post. NEW POWER TRANSFORMERS	T55—P2 \$9,75 T31—P2 \$9,75 KEP1 \$9,00 4/1 \$9,00 SFP7 \$4,75 SCP7 \$4,75 SFP7 \$4,75 SFP7 \$4,75 SFP7 \$4,75 SFP7 \$4,75 SFP7 \$64,75 SFP7 \$61,61 magnetic deflection colls	TRANSCEIVER Inbuilt 24VDC power supply. Variable tuning. Freq. 38-56 MHZ. F.MV.F.O. Controlled. Output 2 watts.	PORTABLE BLOWER MOTORS 230VAC. 220 waita. Complete with fiexible hose. \$15.00 Pack & post. \$1,50.
124V Doubler 300MA \$6.75 130V Doubler 400MA \$7.75 145V Doubler 450MA \$9.75 150 x 150, 30MA \$3.75 225 x 225, 50MA \$4.25 193.3in C.R.O. Transformer \$12.95 150V Doubler 6003MA \$12.75	\$10.00 TWIN SHIELDED MICROPHONE CABLE P.Y.C. covered.	\$95.00 BLOWER MOTORS 24-28VDC, 10,000 RPM 400MA. Cap. 24GFM. Free air. \$5.75	VACUUM PUMPS Huppert type B3X, MK111, ^{1/2} " shaft, \$25.00
WHIP AERIALS	15c per yard. \$13,50 per 100yds. Add pack & post.	Pack & Post 50c.	EX FORESTRY
Base to suit \$1.00 Roof Mounting, Flexible Base, suit Autos 3ft 1in diam. Screw to- gether sections	LIGHTING PLANT Johnson 1 h.p. Engine, 12V, 30 amp. Generator. New. Tested. \$72.00	COAX CABLE P.V.C. covered. 72 ohms. 20c per yard. \$18.00 per 100yds. NEW DIEHL	COMMISSION Portable Transceivers, Battery operated, Freq. 3-7 MHZ. Suitable conversion marine band. Completevalves, meter, speaker, mic. \$15.75
CHASSIS PUNCHES SIZES, 4/sin, 4/sin, 1/in, 11/sin with tapered Reamer and Carry Box. \$5.75 Post 50c. Interstate \$1.00.	2 H.P. ENGLISH J.A.P. PETROL ENGINES Tested. Perfect order. \$39.00	12" industrial exhaust fans, 115VAC, 1.75A, \$30.00	NEW 34ft Vertical Collapsible Antennas. Complete with Guys and Base Insulator. \$7.75

ELECTRONICS Australia, March, 1970



MAKESHIFT EQUIPMENT: I have en-closed a not-so-recent article from the "Sydney Morning Herald." It tells how a few high school students picked up signals rew high school students picked up signals from weather satellites using a tape recorder, which was played into a tele-vision set and viewed — in their lunch hours at that! Could your magazine write an article on how improvised equip-ment like this could be set up for a track-ing station or how TV programs could be recorded with a conventional tape recorded with a conventional tape recorder? I like your magazine and am looking forward to interesting articles in the 70s. (D.K., Peakhurst, N.S.W.)

the 70s. (D.K., Peakhurst, N.S.W.) • There is a lot more complication be-hind the student ventures than you have interpreted the article to mean. In fact, university students in Australia have built and operated similar equipment and we carried a picture and brief story about their efforts some time back. Even without synchronous motor drive, the antenna poses a fair order of challenge to design, construct and mount. While some success may be had with discarded radar receivers, there is the problem of securing a suitable unit and adapting it for the purpose. The incoming signals might well be recorded on an ordinary tape recorder, because the relatively slow rate at which the picture is built up involves only a modest bandwidth. There is nothing in the story to suggest that the students did — or could — record regu-lar television pictures on an ordinary recorder. Most likely, the picture would have been reconstructed, line by line, on the picture-tube face, with the camera lens open for the duration of the scan. It would be more akin to facsimile than to television. The activities of the second group, involving observation of orbits, etc. would have been a joint effort involving a lot of time by dedicated students, and probably dedicated lecturers as well, in a science laboratory situation. It's a fine way to learn but it involves a lot more than you appear to imagine. Behind it would be a lot of text book material, practical experience, and constructional know-how that would not easily be covered even in a series of articles. We have little hope of tackling anything like this in the forseeable future. • There is a lot more complication beeven in a series of articles. We have little hope of tackling anything like this in the forseeable future.

CON-FREQUENCY-WAVELENGTH **VERSION:** Have just purchased a dual-wave portable receiver and am becoming very interested in short-wave listening. However, I am not sure of the relation-ship between Kilohertz and Metres, and this causes problems in seeking stations which have been mentioned in your "Listening Around the World" columns. Could you please tell me of the way to convert frequency into wave-length and vice-versa? (D.R., Broadwater, N.S.W.)

There are numerous ways of remem-• There are numerous ways of remem-bering the relationship between frequency and wavelength, D.R., but to our mind the easiest way is to remember that wave-length of radio waves is inversely pro-portional to frequency, and that the wave-length is 1 metre at a frequency of 300MHz (Megahertz). If these two facts are remembered, it becomes a fairly easy matter to find the wavelength of a

particular frequency and vice-versa. What-ever the number by which one must divide 300MHz to give the frequency, this same number should be used to multithis same number should be used to multiply by 1 metre to give the wavelength. Hence a 30MHz signal will have a wavelength of $(300/30) \times 1$, or 10 metres, while a 10MHz or 10,000KHz signal will have a wavelength of $(300/10) \times 1$, or 30 metres. Another form in which this relationship may be expressed is F x L equals 300,000. Here F represents the frequency in Kilohertz, L the wavelength in metres. in metres.

MINIATURE TV RECEIVER: Would it be possible for you to design a miniature transistorised television receiver using one of the common 3in or 5in cathode ray tubes and a wide-band oscilloscope? (N.S., Whyalla Norrie, S.A.)

• You appear to have combined two separate ideas in the one request, N.S., but we assume that you are thinking of a transistorised wide-band oscilloscope. (We have described a number of valve type wide-band oscilloscopes.) We have no wide-band oscilloscopes.) We have no immediate plans for an oscilloscope along these lines, but we will take a look at the situation to see whether it might be a proposition for the home constructor. The possibility of a TV set along the lines you suggest is much more remote. First, we doubt whether anyone would want to spend a lot of time and money to produce a set using an oscilloscope type CRT. Secondly, it is very unlikely that the home builder could build a set for the same or lesser price than he could buy one, which makes the idea even less attractive attractive.

SOLID STATE SERIES: I find your magazine interesting, instructive and help-ful. May I in particular, offer congratu-lations to Jamieson Rowe for his exceplations to Jamieson Rowe for his excep-tionally good series on the subject of solid state. Having in mind the number of readers who appear to lose track of what has been described in the past, and who want to know about prices, etc., would it not be possible to bring out an annual catalogue containing projects that annual catalogue containing projects that have been featured during the year, along with relevant prices, advertisements, etc.? (G.H., Red Hill, A.C.T.)

• Thanks for the encouraging remarks, which have been brought to the attention of Mr Rowe. Without going into likely costs and revenue, we could not be sure about the commercial viability of an annual, such as you suggest. Many years annual, such as you suggest. Many years ago, we did bring out one or two special books of the "annual" variety. Our main porblem at the moment is that we just could not cope with the extra work that would be entailed.

P.A. AMPLIFIER: I am interested in a 30-60W transistorised high-quality P.A. amplifier with output of 70-100V. Is it posampinier with output of 70-100V. Is it pos-sible that the latest transistor guitar am-plifier could be modified for P.A. use, and if so, do you intend to publish de-tails shortly? If it is not suitable, have you such a project in mind for later publi-cation? (D.D., Swan Hill, Victoria.)

• We can only say "No" to both ques-tions. We do not regard the guitar ampli-fier as suitable for modification for your requirements, and we have no plans for presenting as a construction project an

"ELECTRONICS Australia" Information Service

As a service to readers "ELECTRONICS Australia" is able to offer: (1) Photographs, dye-line prints As a service to readers "ELECTRONICS Australia" is able to offer: (1) Photographs, dye-line prints and other filed material to do with constructional projects and (2) A strictly limited degree of personal-ised assistance by mail or by reply through the columns of the magazine. Details are set out below: PROJECT REPRINTS: For a 20c fee, we will supply data, as available from our files. The amount of data available varies but in no case does it include material additional to that already published in the magazine. For complicated projects involving material extracted from more than one issue, an extra fee may be requested. As a rule, requests for project data will be answered more speedily if the projects are positively identified and the request is not complicated by questions requiring the atten-tiol. of technical personnel. Where articles are not on file, we can usually provide a photostat copy at 20c PER PAGE. 20c PER PAGE.

PHOTOGRAPHS, DYE-LINE PRINTS: Original photographs are available for most of our projects. from 50c plus 8c postage for a 6in x 8in glossy print. In addition, metalwork dye-line prints are available for most projects for 50c each; these show dimensions and the positions of holes and cut-outs but give no details of wiring.

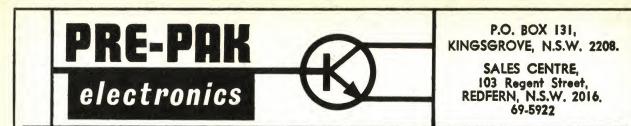
BACK NUMBERS: A fairly good selection is available. On issues up to six months old the cost is the face value, plus 5c surcharge. From seven to 12 months, 10c surcharge; over 12 months, 20c surcharge. Package and postage is 10c extra per issue. Please indicate whether a PROJECT REPRINT may be substituted if the complete issue is not available.

Substituted if the complete issue is not available. REPLIES BY POST: This provision is made primarily to assist readers in matters relating directly to articles and projects published in "ELECTRONICS Australia" within the last 12 months. Note, however, that we cannot provide lengthy answers, undertake special research or modifications to basic designs. A 20c query fee must be enclosed with letters to which a postal reply is required; the in-clusion of an extra fee does not entitle correspondents to special consideration.

Clusion of an extra tee does not entitle correspondents to special consideration. OTHER OUERIES: Technical queries which fall outside the scope of "Replies by Post" may be sub-mitted without fee and may be answered through the columns of the magazine at the discretion of the Editor. Technical queries will not be answered by interview or telephone. COMMERCIAL EQUIPMENT: "ELECTRONICS Australia" does not maintain a directory of com-mercial equipment, or circuit files of commercial or ex-disposals receivers, amplifiers, etc. We are there-fore not in a position to comment on proposed adaptation of such equipment, or on its general design. "ELECTRONICS Australia" does not deal in electronic components. Prices, specifications or other assistance must be sought from the appropriate advertiser or agent. DEMITTAVES:

Where the charge may be in

REMITTANCES: These must be in a form negotiable in Australia. Where the charge may be in doubt, an open cheque, endorsed with a limitation, is recommended. ADDRESS: All requests for data and information, as set out above, should be directed to The Assistant Editor, "ELECTRONICS Australia," Box 2728 G.P.O., Sydney, N.S.W. 2001: 5/69



Until you have seen the prices in our ALL NEW ILLUSTRATED 1970 CATALOGUE TO OBTAIN THE LATEST PRE-PAK CATALOGUE

Send the coupon below which entitles you to membership of the Pre-Pak Electronics Club. Only members of the Pre-Pak Electronics Club will be privileged to buy components at the special prices advertised in our catalogue and supplements, and to receive the benefits of our club services. Include \$1.00 with the coupon to cover membership printing, cost and postage.

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COMPUTER BOARDS Containing a variety of NPN and	INTEGRATED CIRCUITS	SELENIUM BRIDGE RECTIFIERS
PNP germanium transistors and a		20v 1A KA1 \$1.00
host of other components, these		20v 1A A1
4in x 2 ¹ / ₂ in boards are supplied		20v 2A LT91 \$1.50
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100 Boards 20c ea. 50c	min min	Suit guitar amps., etc.
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disappointment order now.	the second se	15in Aust. 30w \$50.00
		Freight \$1.00 ea.
BARGAINS	G.T.S. CAPACITOR	
2N3054 \$1.90	Discharge Ignition	STEREO HEADPHONES
2N3055 \$1.90	by Summit.	SDH-7 25Hz-15KHz \$7.50
BC108 50c	A MODEL TO SUIT	SDH-8 20Hz-17KHz \$9.50
BC109 60c		MAGNETIC CARTRIDGES
BF115 65c	EVERY MOTOR.	
AC125 80c	6 months' guarantee.	At 66.
AC126 80c	Deluxe \$39.95	$20 \text{Hz} - 20 \text{KHz} \pm 2 \text{db}.$
AC127/128 \$1.75	Competition	Tracking weight .5-2.5 grams.
AC187/188 \$1.85	(higher output) \$48.00	\$8.50.
AD161/162 \$3.20	Marine	At 215, \$11.50 .
RD101/102		At 33, \$13.95.
EM404 30c	Commentaria and a second se	Post 25c.
BA100 35c	MODEL MF-15	NEON MADE TESTING
OA91 20c		NEON MAINS TESTING
		SCREWDRIVERS \$1.00
Magnetic Pre-Amp Kitset	meter, 2,000 Ω/V	HI-FI TWIN-CONE
As in E.A., Oct., 1965.	designed for	SPEAKERS
All parts supplied.	radio service.	8 ohm or 15 ohm.
Use for pick-up or tape heads.	the state of the s	
Mono \$4.90. Stereo \$9.00.		
	MULLARD	R.M.S \$12.00
TWEETERS	Semi-Conductor	8" 30Hz-15KHZ 8W.
3 ¹ / ₂ in 5KHz-16KHz	Interchangeability list, latest	R.M.S \$12.00
12w R.M.S., \$3.30.	edition. \$1.00.	10" 30Hz-15KHZ 10W.
3tin 5KHz-18KHz		R.M.S \$12.40
15w R.M.S., \$4.10.	Miniwatt valve and transistor	12" 30Hz-15KHZ 10W.
Post 50c.	data book, latest (7th) edition.	R.M.S \$12.84
	\$3.05.	
SUN-LITE DELUXE	11 34	TO PREPAK ELECTRONICS:-
2 STATION INTERCOM	CLEVELAND ST.	I enclose cheque/m.o. for \$1.00 for
Supplied with 100ft wire and		your new catalogue with 10 x 10 coupon
9 volt battery.	JHR AS	I enclose cheque/m.o., for \$1.00 for your new catalogue with 10 x 10 coupon and membership of the Pre-Pak Electronics Club.
\$11.25	the state	Name
Pack, and Post. 50c.	f T	
		Address
PACK AND POST	LAWSON SQUARE	
10c ANY ORDER	Redforn REDFERN ST.	I Destanda
	REDFERN ST.	Postcode
UNLESS INDICATED.	Station T	

ANSWERS – continued

amplifier such as you describe. In general, we can only publish circuits which will interest a sizable portion of our readers, and the more specialised equipments such as the type you require do not fall within this category. Sorry.

ENJOYS READING E.A.: I was agreeably surprised to see details of my "Simple Variable Power Supply" in the December issue "Reader Built It." I am very happy with your magazine which, in my opinion, goes from strength to strength. The December article on the noise silencer was interesting and I intend to incorporate something like it in my Sony CRF 230. Radio reception is very good on Norfolk Island but static is an ever-present nuisance on the broadcast band during summer. (P.B., Duncome Bay.)

• Thanks for your letter. Payment has been authorised for the item, now that we are sure of your present address. Static may be a problem but our guess is that quite a few of our readers would be prepared to put up with it in exchange for a few months on Norfolk!

WATT POWER: Manufacturers seem to label their guitar amplifiers with fictitious power ratings. I would like to know if there is any test instrument with which I can measure the power output of amplifiers while they are still in the shop. (A.H., Clarence Park, S.A.)

• Unfortunately there is no single test device or simple method to measure the power capability of a guitar amplifier in a shop. About the best you can do is seek a reputable dealer.

PHOTO-METER: Currently on the photographic accessories market is an instrument known as a "Photo-meter." I feel that this would make a good constructional project for your magazine. Essentially, the instrument indicates correct diaphragm opening for flash photography. A photocell is placed in the area of exposure measurement and the flash synchro-cable is connected to the photometer. Operating a "press-hold" button will cause the flash set-up to fire and the light value at the cell is indicated on the meter, calibrated directly in "F" values. Such an instrument is useful in measuring the light at the edge of the angle of flash and also where multiple flashes are to be used. (N.H., Darwin, N.T.)

• Many thanks for the suggestion N.H., and we will certainly keep this idea in mind. We assume that the device would be intended for use mainly with electronic flash sources, rather than expendable bulbs since use with the latter could be quite expensive. This would be particularly so where multiple flash was involved and it was necessary to make several test firings in order to achieve the required lighting balance and coverage.

PEN-FRIEND SOUGHT: Would you please publish my name and address? I am aged 14, and would like to hear from anyone living near me who is also interested in amateur radio. Also would you explain briefly what is the meaning of the word "VOX." (Allan Downie, 2 Inge Street, Mt Gravatt, Brisbane, Qid. 4122.)

• As you can see above, A.D., we have published your name and address to comply with your request. We hope that you receive the desired replies. The word "VOX" is actually a contraction of "voicecalled a "Vox unit" is strictly one which is capable of operating a radio transmitter automatically whenever the operator is speaking. Such units typically consist of a microphone preamp, a signal detector with fast-attack/slow/decay time constant characteristics and a power amplifier to operate a relay for transmission switching; also a circuit to prevent operation from sounds emanating from the receiver speaker (this is sometimes called "anti-Vox"). In recent years the term "Vox" has often been extended in meaning to cover any device used to permit automatic voice control of equipment. Hence another variety of "Vox" unit is used to operate tape recorders and automatic message devices.

STEREO CASSETTE EQUIPMENT: I am looking for a stereo cassette or cartridge recorder system which must be self-contained, able to operate from 12V in a car or 240V in the home. I want to be able to re-record my own material from my present hi-fi system. I am not worried about the number of tracks, etc., but naturally want reasonably good results and a reasonable price. (C.R., Tarragindi, Qld.)

• There have been references in our own and other publications to units of this general type but we have no up-to-date file of information on hand from which we could draw conclusions about availability, price, quality, service back-up etc. for the various systems which might meet your need. We can only suggest that you do what we would have to do ourselves — follow up advertisements, hi-fi dealers, etc., and draw conclusions therefrom.

TRANSISTOR DELTAHET: Several years ago, you published a series of articles on the Deltahet receiver. Later you supplied me with a set of those articles. On the basis of those articles, I built two Deltahet receivers and both are still going strong. Thanks for your magnificent description. Still, the temptation to build something new again is here, and so I would like to ask you whether you propose to publish a transistor version of the Deltahet receiver. Any information would be appreciated. (B. H., Munich, West Germany.)

• Thank you for your letter and we are indeed pleased to learn that you have built not one, but two, Deltahet receivers and that they are so successful. We have been asked many times about the possibility of a transistor version of this popular receiver. In point of fact, the designer of the original Deltahet has been working on a transistor version for quite a while, in his spare time. Development is well under way and some construction work has already been done. While this is all good progress and we have little doubt regarding a successful outcome, it will be some time before it is ready for publication.

TRANSISTOR SUBSTITUTE: I refer to your article "A 'Different' Metal Locator" in the January, 1970 issue. An excellent replacement for the 2N2712 is a BC107 or BC108. The specified type is listed by G.E. as "economy planar NPN small signal amplifier audio to 30MHz," possessing the following characteristics (with BC107/8 characteristics given for comparison):

 parison):
 hFE Vceo
 Pt
 Ft

 2N2712
 75-225
 18V
 200mW
 120MHz

 BC107
 125-500
 45V
 300mW
 175MHz

 BC108
 125-500
 20V
 300mW
 175MHz

 The suggested replacement, BFX13, will be more expensive than either the BC107, BC108.
 (R.H., Mt. Lawley, W.A.)

• Many thanks for this information, which we gladly pass on to our readers. Thanks also to others who have written in on similar lines. Some readers have also indicated that the BSX77 is a suitable replacement. BUY RIGHT... FROM ENCEL

MICRO CARTRIDGES provide excellent performance at modest cost

In each price range Micro cartridges offer outstanding performance . . . at Encels extremely modest prices. The two most popular magnetic cartriges continue to be the 2100-5 and the VF 3100. The ceramic type SC-303 will always be a best seller. SC-303: The economical ceramic stereo cartridge for the budget conscious buyer. Frequency response 20-15,000 Hz. 15 deg. tracking angle. Comes with diamond stylus. Price (including sales tax) \$6.90.

2100-5: Economical moving magnet model. Input sensitivity: 5mV. Frequency response: 20-20,000 Hz plus or minus 3dB. Tracking angle 15 deg. Channel separation: 3dB at 1kHz. Recommended tracking pressure: 1-3 gms. Stylus: Conical diamond. Comment: Performance equal to a cartridge three times as expensive.

Price (including sales tax) \$14.50.

VF-3100 stereo cartridge continues to attract great attention. Frequency response: 20-28,000 Hz. Channel separation: 2dB. Two models — VF — 3100E with elliptical diamond stylus; VF-3100/5 with conical diamond stylus. (Both track efficiency at 1½ gms). Styli are replaceable.

Comment: FV-3100 has established a new performance standard for lowerpriced magnetic cartridges.

rice	VF-3100/5	\$19.50.
F-31	OOE	\$24.50.

"Extract" Comment from "Electronics Australia" (Page 119, February, 1969) "frequency response checked out at plus or minus 2dB. from 30Hz. to 20 kHz . . . a very good performance indeed."

MDP—3 Dust Bug. Picks up dust automatically as the record plays. Price (including sales tax) \$3.50.

MA77-Mk II Static Balance Tone Arm High sensitivity arm with split and revolving counterweight for easy balancing adjustment. Anti-skating device eliminates inside-force distortion. Accepts all <u>1</u>" mounting cartridges. Direct reading scale for stylus

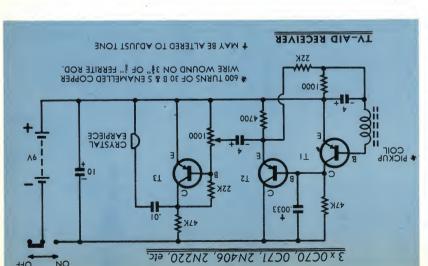
adjustment. Oil dampened arm lift incorporated. Price (including sales tax) \$44.50





pennitnoo – ANSWERS

complete success even by mose with no previous wiring even by mose However, the wiring encourage diagram published in the original article did have one error the 22K and 47K resistors in the collec-tor unit of T3 (at the right-hand corner posed. Copies of the article are avail-posed. Copies of the article are avail-able through the Information Service for 20c (please quote file number on this scott vd neve sees with no other listeners discomfort. The con-struction has been specially simplified to allow the unit to be assembled with a favourite program without causing other con-A small audio induction receiver appeared in the October, 1963, issue of "Radio, Television and Hobbies," as our magazine was then known. The unit picks up the sound from a tele-vision set or radio by induction from a loop of wire placed around the room. It permits the hard-of-hearing to follow a favourile program without causing a favourile program without causing



·100Z 3/MS/9.) Letters should be addressed to the Assistant Editor, "Electronics Australia," Box 2728, G.P.O., Sydney,

lished details of such an addition? (A.R.B., Nth. Carlton, Vic.)

• Sorry, A.R.B., but we haven't done so. For the time being at least, we're straid you will have to einer try out the scheme you suggest in the remainder of your letter, or inquire from other publi-it may be worthwhile to consider a num-ber of transistors biased back to conduct only when the meter voltage reaches suppropriste levels. Small hamps could pos-sibly be connected directly in series with the transistor collectors. the transistor collectors.

saved my money (it was not a cheap book) as the coils were not given so that they could be readily made up. **OVERSEAS BOOKS:** I was pleased to read your answer to a "Young Reader" in the Answers to Correspondents for mation for which I have been searching for quite a while. Recently, I purchased an English radio book with articles on how to build various items. However, I saved my money (it was not a cheap saved my money (it was not a cheap

TECHNICAL DATA SHEETS SENT FREE ON REQUEST VWDFILLERS 28'95 Stylus at no extra cost. GP94-5 STERED CERAMIC FOR TRANSISTOR *UNOMAID* GP94-1 STEREO CERAMIC 56°L\$ 11116Q MILL 6P93 STEREO CRYSTAL 55'L\$ 6992 MONO CERAMIC Stereo Compatible ... \$6.55 entry and a second seco 56.22 6991-2 HIGH OUTPUT MONO CRYSTAL Stereo 29.22 ... alditegmo) ostate JATZYAD ONOM 1-1940 fifted with Diamond Stylus at no extra cost. covering all the main types needed today, each Acos 90 Series — a family of pick-up cartridges SODA REPLACEMENT LOKG LIFE CARTRIDGES

brazse.

Association of the source advertusements' Also, is there an average life for a picture tube? The picture tube in our television set is easily ten years old and the original one. Is this a usual case or not? (L.R., Hurstville, N.S.W., M.L., Dulwich Hill, R.S.W., and others.) TV TUBES AND COLOUR: Can you tell me how the effect of colour is pro-particularly on some advertisements? Also is there an average life for a nicitude

...............................

picture. • The colour effect which you mention has been used on some TV advertisements (Ampol is one, we understand) and it is referred to as "subjective colour," which just about explains it! This is a phenome-non which has been known for a very long mon which has been known for a very long with a flicket rate which is imposed on the with a flicket rate which is imposed on the picture.

picture. The result is highly variable. Some people see bright colour, some weak co-lour, some no colour at all. More im-portantly, there does not appear to be any consistency in the hue of the colour seen. It might range from blue to pink and reproducing system. This is limited of rubes to last for ten years or so. In fact, in mission rate. It is not unusual for picture inbes to last for ten years or so. In fact, in each be normally expected. We would not expect the make of set to have any bearing expect the make of set to have any bearing on this.

Kingswood, N.S.W.) WEGATIVES: Could you please tell me where I could purchase the negatives employed in the manufacture of the fol-lowing printed wiring boards—Type 69p9, used in the Playmaster 127 Control Unit, and Type 70p1 used in the Playmaster 128

negatives for printed wring boards. We can supply positive reproductions of the patterns (full size) through our informa-tion service at 50c each. ● We are not normally able to supply wring boards. We

The completed one of the auto factor processing against the average ago, and which you described a few years ago, and which you described a few years ago, and would be increased considerably by the would be increased to be would be increased considerably be would be increased to be would be increased considerably by the would be increased considerably be would be increased to be would be increased considerably by the would be increased considerably be would be would be increased considerably be would be increased considerably be would be would be increased considerably be would be increased considerably be would b TACHOMETER ALARM: I have recent-

ELECTRONICS Australia, March, 1970

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sinaph neilerteuh alos

Sydney, N.S.W. Phone 731227

29 Majors Bay Rd., Concord,

• A four channel audio mixer was described in February, 1966 (File No. 1/MX(6) and a high impedance 4 channel mixer using FETs appeared in February, 1967. We have not published any kind of serial booster. Thank you for the words of pusite.

MIXERS, Etc.: Have you ever published a mono four channel transistor micro-phone mixer and also have you published a transistor serial booster for fringe ateas? I would like to compliment you on an interesting and informative magazine. (M.G. Cardiff, N.S.W.)

the problems you describe. The problems you describe a former who may be in a position to get around rigidly to the more experienced reader, who may be in a position to get around the problems you describe.

or other obstacles resulting from the over-seas origin of a design. Alternately, it is better to make use of Australian publica-

• Thank you, G.M., for your letter. We are pleased to learn that you were able to get the information which you needed. Yes, we are aware of the problem of overseas books as you have outlined overseas books, it would be buying an overseas book, it would be out the risk of this problem, wise to check on the risk of this problem, or other obstacles resulting from the over-

Would you please warn your "beginner". readers against this type of occurrence. (G.M., Balwyn, Vic.)

HO

323 ELIZABETH STREET. (2 Doors from Little Lonsdale Street) **MELBOURNE, VIC, 3000**

 MODEL
 C-1000
 POCKET
 MULTIMETER,
 1000
 ohms/per
 Volt,
 AC

 Volts:
 0-10/50/250/1000
 (1000
 opv),
 DC
 Volts:
 0-10/50/250/1000

 (1000
 opv),
 DC
 Current:
 0-100mA
 Resistance:
 0-150K
 ohms
 (3K

 centrel.
 2 colour
 scale,
 Range
 Selector
 Switch.
 Dimens.:
 3½ x
 2¼ x

PRICE: \$6.50 post free

MODEL 200H MULTIMETER, 20,000 opv, DC Volts: 0-5/25/50/250/ 500/2500V (20,000 opv) AC Volts: 0-15/50/100/500/1000V (10,000 opv) DC/Amps: 50uA/2.5mA/250mA, Resistance: 0-60K/6M ohm (scale centre 300 ohm—30K ohm, Capacitance: 10uuf to. 001uF/.001uF — .luF, D3 scale 20 db to plus 22 db, Size 4½ x 3¼ x 1 1-8.

PRICE: \$11.25 post 30c.

MODEL CT330 MULTIMETER, 20,000/OPV, DC Volts, 0-6/6/30/ 120/600/1.2K/3K/6K Volts, AC Volts: 0/6/30/120/600/1.2K Volts (10K/OPV), DC/Amps: (0-0.06mA/60mA/600mA, RESISTANCE: 0-6K/600K/6M/600Megohm. (30/3K/30K/300K ohms) centre scale: Capacitance: 50 uf to .01 uf .001 to 0.2 uf. Decibels: -20 to plus 63db size approx. 5¹/₄ x 3 5/8 x 1³/₄.

PRICE: \$16.75 post 30c.

PRICE: \$19.50 post 30c.

TELEPHONES: 677329, 674286

WATT SOLID STATE STEREO AMPLIFIER 10 Transistor, 3.5 Watts per channel, Crystal/ Ceramic input (250mV), Frequency Response 50-20,000 c/s, 8 and 16 ohms output, polished wood case, metal front panel. Dimensions: 8V2in x 3in x 5 3/8in.

RADIO

SUPPLIERS

Special Price \$34.50. Post 75c



RE EALISTIC DX-150 SOLID STATE COMMUNICATION RECEIVER

Features: 240V A.C. or 12V D.C. operation. 30 Transistors and Diodes. 535 Kc. to 30 Mc. in 4 Bands. Bandspread tuning, "S" Meter, AM/CW/SSB. Product Detector for SSB. Compact size 14 1/8in x 91/sin x 61/sin. Polished metal panel, small internal speaker.

F.O.R. PRICE: \$229.50 Matching external speaker \$13.30 extra.



No. 62 TRANSCEIVERS. Wireless set No. 62 Mk.2 (PYE) Frequency Range 1.6 to 10 McS. in 2 bands, inbuilt 12-volt Genemotor Power Supply. Clean condition, Fully air tested on Transmit and Receive.

F.O.R. PRICE: \$49.50



WESTON LM-330 MOBILE TAXI RADIO. Weston LM-330 Mobile TAXI RADIO. Low Band A.M., 60 Kc. Bandwidth, 70-80 Mc. Crystal Channel Locked, Single Channel, In-built Transistor Power Supply, 12-volt operation, suit country taxi service or conversion to Ham Bands, inc. microphone and cradie. AS NEW AND AIR TESTED. F.O.R. PRICE: \$45. Packing 50c

F.O.K. PRICE: \$45. Packing SUC LAFAYETTE *5 WATT C.B. TWO-WAY RADIO MODEL HE-20, FULLY TRANSISTORISED. SOLID STATE, 13 Transistors, 10 Diodes, 27.240 Mc. Provision for 23 channels, CRYSTAL channel locked, Push-pull Audio Modulator, 455 Kc. mechanical filter, spotting switch for accurate reception, TVI Trap, 230V A.C. and 12 Volt (positive or negative ground). Inbuilt P.A. Amplifier. IDEAL FOR FIXED BASE STATION OR EMERGENCY MOBILE, includ-ing microphone and mobile cradie. * Subject to P.M.G. approved licence. F.O.R. Price: \$169.50. Tax Paid Fibreglass Helical Aerial 4tt high, cowl mount, for mobile use \$16.50 extra.



BENDIX BC-221 FREQUENCY METER. 125Kc. to 20 Mc. including A.C. power supply. CRYSTALS, Calibration Book etc. V. clean condition. F.O.R. Price: \$49.50. P'ckg. 75c



Mail Order Specialists







MODEL OL-64D MULTIMETER. 20,000/OPV, DC Volts: 0-0.25/ 1/10/50/250/500/1000V at 20K/OPV, 5000 volts at 10K/OPV, AC Volts: 0-10/50/250/1000V at 8K/OPV, DC/A: 50uA/1mA/50mA/ 500mA/10 amps. RESISTANCE: 0-4K/400K/4M/40Megohm. DB Scale: --20 to plus 36db. Capacitance: 250pF to .02uF. Induct. 0-5000H. size 534 x 4 1/8 x 134in.





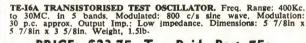
MODEL AS100/DP HIGH SENSITIVITY 100,000/ohms/volt DC, Mirror Scale, PROTECTED MOVEMENT, SPECIFICATIONS: 6/20/120/300/600/1200 Volts A.C. (10K/OPV), Volts D.C.: 3/12/60/120/300/600/1200 (100K/OPV) D.C. Amps; 12uA/6mA/60mA/300mA/12 Amps, RESISTANCE; 2K/200K/20Mg/ 200Meg, Decibels: --20 to plus 63db, AUDIO OUTPUT: 6 Volts/30/ 120/300/600/1200V A.C., Size: 7/2/in x 5/2/in x 23/4/in.

PRICE: \$34.50. Post 75c



MODEL A10/P. GIANT (6¹/₂-inch), METER, CIRCUIT TESTER 30,000/OPV D.C. with inbuilt signal injector, overload protected, Specifications: A.C. Volts: 2.5/10/50/250/500/1000 at 30,000/OPV, 5000V at 10,000/OPV, D.C. Current: S0uA/1mA/50mA./500mA./1 Amp/10 Amp/A.C. Current: 1 Amp/10 Amp. Resistance: 10K/100K/1 Megohm/100 Megohm, SIGNAL INJECTOR: Blocking Oscillator cir-cult with a 25A102 Trans, DECIBELS: -20 to plus 63db, SIZE: 6¹/₂in x 7¹/₄in x 3³/₄in.

PRICE: \$55 Tax Paid. Post 75c



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